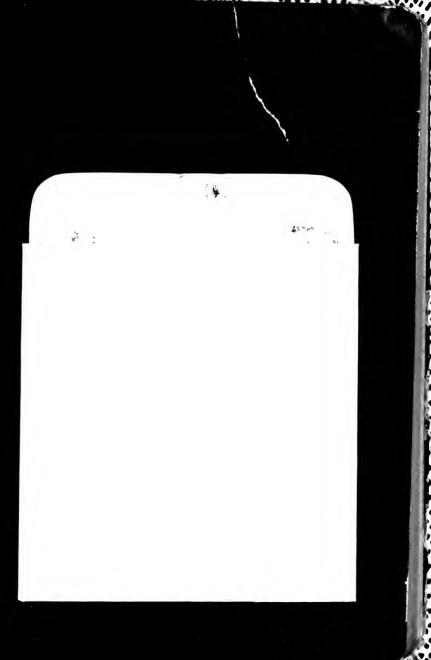


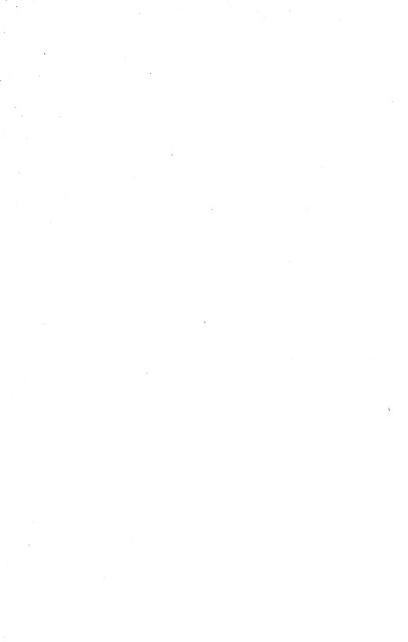
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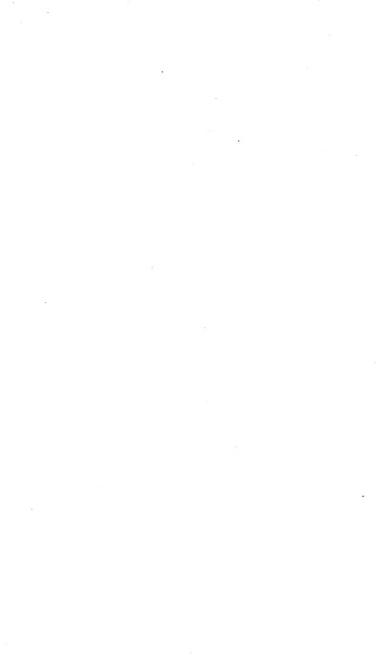












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Railroad Field Manual

for

Civil Engineers

BY

WILLIAM G. RAYMOND, C.E., L.L.D.

Professor of Civil Engineering and Dean of the College of Applied Science in the State University of Iowa. Member of the American Society of Civil Engineers and of the American Railway Engineering Association

FIRST EDITION
FIRST THOUSAND

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PREFACE

This book is for field use rather than for office use, though it is adapted to a large percentage of office work. It is made on a new plan which is not expected to gain immediate favor but which it is hoped will eventually appeal to railroad engineers as sensible and worthy of adoption, because its use will save time and lessen the liability of error. The degree is divided decimally instead of sexagesimally.

When the author was a young man engaged on railroad location he knew one or two engineers who had one vernier of their transits graduated to read hundredths of degrees for greater convenience in setting out curves. They would have done all their work in decimals if tables

had been available.

When the author was planning this book he gave much thought to the question of the division of the degree and the forms of the tables that would be most convenient and time saving for the field men who might use the book. He remembered that in practically every curve problem it is necessary at some stage of the solution to transpose from minutes and seconds to decimals of a degree or vice versa. membered that to lay out subchords would require much less mental effort if the transit were divided to read decimals of degrees rather than minutes. He wrote to a half dozen of the leading instrument makers to learn what would be the cost of changing the verniers on an old transit to read decimals of a degree and to know whether there would be any difference in price between two instruments ordered new, one to be divided in the usual way and the other divided to read decimals of a degree. All but one of the makers gave a price in the neighborhood of \$20 for changing the verniers on an old instrument, and no difference in cost for new instruments. The author then wrote to about fifty engineers, chief engineers of railroads, independent practicing engineers, and professors of railroad engineering in colleges and asked their opinions as to the desirability of a change in practice from sexagesimal to decimal division of the degree, and whether or not a table book based on the decimal division would help to bring about the change, if desirable. All but one of these engineers replied that the change is desirable. The one was a professor of railroad engineering. Of the others all but two thought it doubtful if the change could be iv PREFACE

brought about, owing to the conservatism of the craft. Two chief engineers of prominent eastern roads discussed the matter with their assistants and were so favorably impressed with the plan as to say that they would adopt it if they had the tables to make it possible. Those who thought it unlikely that the change could be brought about cited the difficulty with the introduction of the metric system as an argument. To this the author replies that the adoption of the metric system involves a change of unit. The adoption of the decimal division of the degree involves no change of unit and merely does for angle work what American engineers long since did for their linear work. The book still retains the 90° quadrant. To be sure, minutes and even seconds have become a sort of unit, but so were inches, chains, and links. These are practically done away with for surveyor's use and there would seem to be as good reason for doing away with minutes and seconds. Practically every computation involving trigonometric logarithms requires less work by the decimal system than it does by the sexagesimal system. Instruments will be graduated to read to hundredths of degrees directly or 0.6 of a minute.

Although the author believes that the "degree" of a curve should be the angle subtended by an arc of one hundred feet instead of a chord he has not adopted that definition, but has adhered to the definition approved by the American Railway Engineering Association.

Five-place tables have been adopted as representing as high a degree of precision as is warranted by the field work. Computations of tables and some few other calculations require more extended tables but these practically always arise in connection with office work where it is assumed that there are, or may be if necessary, six-place, seven-place, and even ten-place tables. The author has used seven-place tables, and occasionally ten-place tables, for the computation of the tables of this book. Persons do not always realize it, but considerable additional time is required to use six-place tables over that required for five-place tables. In his "Plane Surveying for Classroom and Field," the author discusses this question at some length and works examples to show the relative precision of four-place and five-place tables. The conclusions of the discussion are as follows:

- "I. It is useless to make linear measurements with a precision of more than I in 3500 if angles are to be read to the nearest minute only.
- "2. It is useless to use tables of more than four places for angles read to the nearest minute only.

"It is difficult for many persons to bring themselves to use the smaller tables because they seem to see a greater precision in the use of tables giving results that are true to five and six significant figures, and fail to realize that the field work on which the computations depend does not warrant any such degree of precision, which is therefore only a seeming precision that is misleading and does not exist in fact. It is true that linear measurements can in general be made with greater precision than the angle work gives and, hence, it is the angle work that fixes the precision and the tables to be used. The following rules may be formulated:

" For angles read to the nearest minute use four-place tables.

"For angles read to less than 0° 00' 30" use five-place tables.

"For work in general requiring certainty in the third significant figure use four-place tables, in the fourth significant figure five-place tables, and in the fifth significant figure six-place tables.

"But it must be remembered that no ordinary surveying work is precisely enough done to warrant results certain to more than four significant figures, and that five-place tables are as extensive as are warranted by any land, topographic, railroad, or other surveys except the most refined city, bridge, and geodetic surveys.

"Computation labor is increased about 50 per cent by using five-place tables instead of four-place tables, and about one-third by using sixplace tables instead of five-place tables."

Before using the logarithmic tables even persons somewhat familiar with the use of logarithms should read the explanatory text preceding the tables.

The text concerning spirals and the spiral tables are based on the American Railway Engineering Association's ten-chord spiral. The author is indebted to Mr. Jenks B. Jenkins, Valuation Engineer for the Baltimore and Ohio Railroad and Chairman of the Track Committee of the A.R.E.A., and who devised the ten-chord spiral, for assistance with this part of the work.

The author has endeavored to include beside bare tables — many of which have been computed for this book and are not found in other books — just so much of explanation of common field problems as would seem necessary to refresh the memory of young engineers who have not had these drilled into them by long experience.

A few tables have been taken from other books. Acknowledgment is due Mr. Shelby S. Roberts for courteous permission to use tables from his "Track Formulæ and Tables" and to the American Book Company for permission to use plates from the author's "Plane Surveying for Classroom and Field" for Tables I, XXIV, and LXXXIII, and to use the matter of Tables LXX, LXXI, and LXXVII.

Great care has been taken with the computations and the proofreading but it is incredible that so many new computations should have been made and the results printed without error. The author will esteem it a favor if persons will report any errors that may be discovered to him or to the publishers.

This book may be used about as conveniently as other books based on the sexagesimal division of the degree by those who do not care to have their instruments changed or to adopt the decimal division for their final records, and it has some features not found in existing field books that may commend it to field men. Therefore, it is put forth under the hope that it may find immediate approval in a few places; that it may be tried in some other places; and that familiarity and experience with it will convince users that the author is not a mere faddist but has contributed something of real use to the fraternity.

WILLIAM G. RAYMOND

STATE UNIVERSITY OF IOWA, IOWA CITY, IOWA, 1915.

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RAILROAD FIELD MANUAL

CHAPTER I

SIMPLE, COMPOUND, AND VERTICAL CURVES

SIMPLE CURVES

Fundamental notations and equations. — The curve running from A to B in Fig. 1,

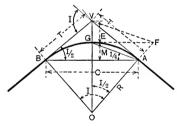


Fig. 1.

A = T. C. (tangent-curve).

B = C. T. (curve-tangent).

V = P.I. (point of intersection of tangents).

I =central angle or deflection angle of tangents.

 $T = \text{tangent distance} = R \tan \frac{1}{2} I$.

C = long chord = $2 R \sin \frac{1}{2} I$.

 $M = \text{middle ordinate} = R \text{ vers } \frac{1}{2}I.$

 $E = \text{external distance} = R \operatorname{exsec} \frac{1}{2} I$.

 $E = T \tan \frac{1}{4} I.$

 $C = 2 M \cot \frac{1}{4} I.$

 $C = 2 T \cos \frac{1}{2} I.$

 $GA = \frac{C}{2} \sec \frac{1}{4} I.$

Definition. — The "degree" of a curve in American practice is the angle subtended at the center of a circular arc by a chord of 100 feet. In Latin American states where the metric system is used the "degree"

is the angle subtended by a chord of 20 meters. If R be the radius and D the degree of a curve, then, in American practice,



$$R = \frac{50}{\sin\frac{1}{2}D} \cdot$$

Fig. 2. Table I gives R and its logarithm for various degree curves.

Tangent offset t = R vers $I = \frac{C^2}{2R}$. The tangent offset for one station is tabulated in Table I. For a subchord c the tangent offset is

$$t_c = t_{100} \frac{c^2}{10,000}$$

Approximate Fundamental Relations. — Approximately, radii are inversely as the degrees or

 $\frac{R}{R'} = \frac{D'}{D}$ (approx.).

Radius of a 1° curve is 5729.65 = 5730 (approx.).

$$R_D = \frac{5730}{D}$$
 (approx.).

Tangent distance for a D° curve of central angle I is

$$T_D = \frac{T_1 \circ}{D}$$
 (approx.).

Table II gives tangent distances for a 1° curve and various values of I, and Table III gives corrections to $T_D = \frac{T_{10}}{D}$ for more precise re-

sults. Values of C, M, and E, for D° curves are also found approximately by dividing the values for a 1° curve for a given I by D. Table IV gives values of E for a 1° curve.

A curve departs from a tangent approximately thus: $O = \frac{7}{8} n^2 D$, n being the number of stations from the tangent point and D the degree of curve. Two curves of degrees D

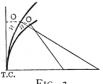


Fig. 3.

and D_1 depart from each other by the same approximate law, substituting the difference of degrees $D - D_1$ or $D_1 - D$ of the D of the foregoing formula.

The deflection angle Δ , for a chord of 100 feet is $\frac{1}{2}D$; for a subchord, c, it is given by

$$\sin\delta = \frac{c}{2R},$$

or; with sufficient exactness for all curves under about 8°,

$$\delta = \frac{c}{100} \times \frac{D}{2} = 0.5 \, cD$$
, in hundredths of degrees,
 $\delta = 0.3 \, cD$, in minutes.

FIG. 4.



The ordinate from a chord at any point given by its distance from the center is

$$K = \sqrt{(R+a)(R-a)} - \sqrt{\left(R + \frac{c}{2}\right)\left(R - \frac{c}{2}\right)}$$

or, approximately,

or

$$K = M\left(1 - 4\frac{a^2}{c^2}\right).$$

Whence, for

$$a = \frac{1}{8}c, K = \frac{15}{16}M;$$

 $a = \frac{1}{4}c, K = \frac{3}{4}M;$ (approx.).
 $a = \frac{3}{8}c, K = \frac{7}{16}M.$

If the point is given by the distance from one extremity,

$$K = \frac{Q \times S}{2 R} \text{ (approx.)}$$
$$= \frac{872 Q \times S \times D}{10,000,000} \text{ (approx.)}.$$

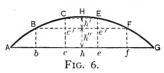
Approximately

$$M=\frac{C^2}{8R}, \qquad m=\frac{M}{4}.$$

Location by Offsets from Long Chord. -

$$AG = 2R\sin\frac{n}{2}D$$
, $n = \text{number stations } A \text{ to } G$,
 $BF = 2R\sin\frac{n-2}{2}D$,
 $Ab = fG = \frac{AG - BF}{2}$; $CE = 100 \text{ or } 2R\sin\frac{n-4}{2}D$,
 $bc = ef = Bc' = e'F = \frac{BF - CE}{2}$, etc.

 $Bb = Ff = Hh - Hh'' = R (\text{vers} \frac{1}{2} nD - \text{vers} \frac{1}{2} (n - 2) D), \text{ etc.},$



or

$$Ab = fG = 100 \cos \frac{n-1}{2}D.$$

$$Bc' = e'F = 100 \cos \frac{n-3}{2}D, \text{ etc.}$$

$$Bb = Ff = 100 \sin \frac{n-1}{2}D.$$

$$Cc' = Ee' = 100 \sin \frac{n-3}{2}D.$$
Use natural functions and move decimal.

In the particular figure $Hh' = 50 \tan \frac{1}{4}D$ because n is odd.

If the number of chords is not more than 8 or the degree more than 20 and of an even number of tenths, the long chords and middle ordinates may be taken from Tables V and VI, thus:

 $\overrightarrow{AG} = \text{long chord of } n \text{ stations.}$

$$Ab = fG = \frac{\text{long chord of } n \text{ stations} - \text{long chord of } (n-2) \text{ stations}}{2}$$
, etc.

b B T.C. A

Fig. 7.

Bb = Ff = middle ordinate for n stations - middle ordinate for (n-2) stations, etc.

Location from Chord Produced. -

Bb = R vers D, or 100 sin $\frac{1}{2}$ D for natural functions.

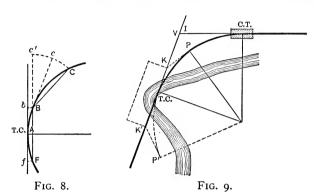
Bb = tangent offset of Table I.

AV or XA gives line of tangent.

Stretch the tape from A to B so that Bb shall measure as above. Produce AB to c',

one tape length, and swing about B until e'C = 2Bb. Produce BC to e' and swing about C until e'E = 2Bb, etc. If the curve begins with

a subchord, l, swing l feet above A to B (Fig. 8) until $Bb = l \sin \frac{l}{100} \frac{D}{2}$. Swing 100 -l about A to F until $Ff = (100 - l) \sin \frac{100 - l}{100} \frac{D}{2}$. Produce FB to c', 100 feet, and swing about B until $c'C = 2 \times 100$ sin $\frac{1}{2}$ D, or twice the tangent offset of Table I. Produce BC, etc., as



before. For ending use the same method reversed. Supposing the curve to be running from C to B to A, locate F by producing CB, measure over Ff and Bb, and establish A between f and b at l feet from B.

Problems. — Suggestions for passing obstacles. If TC only is in-accessible:

- (a) Run to V to CT and run curve backwards.
- (b) Assume a point on the curve beyond the obstacle; compute the tangent distance for the point as TC K.

tangent distance for the point, as TC - K; run to K; deflect angle at K and run to P and run the curve backward and forward. If CT is inaccessible the same methods with obvious modifications may be used.

To pass an obstacle on a curve one of the methods suggested by the figure may be used. The line AbC is run as ABC would be run only with the center on the opposite side.

To change TC or CT. First method: Assume or know the necessary change in

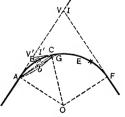
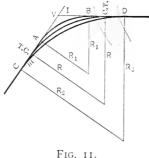


Fig. 10.

tangent distance and compute a new degree of curve. Second method: Assume a new D a round number, probably such as to accomplish the

desired result; change in CT or TC = change in tangent distances, or $m = T_2 - T_1 = (R_2 - R_1) \tan \frac{1}{2} I$.



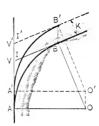
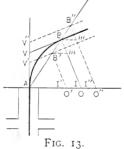


FIG. 12.

A curve ends in VB or V'B'; required to end in V'B' or VB. Degree does not change. It is necessary to find change in A.

$$AA' = VV' = BB' = OO' = \frac{K}{\sin I}.$$



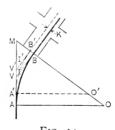


Fig. 14.

A curve ends in VB; required to end in V'B' or V"B" without changing A. Degree changes.

$$R' = R \mp \frac{K}{\text{vers } I}$$
, that is, change in $R = \frac{K}{\text{vers } I}$.

A curve ends in VB; required to end in V'B'. A and D change. $R' = R \pm \frac{K}{\text{exec} I}$, according as B' is inward or outward from B. AA' = (R - R') tan I, or K cot $\frac{1}{2}I$, A being moved ahead or back according as R' is less or greater than R.

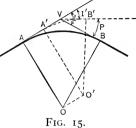
A curve ends in VB; required to end in VB'. Without changing degree AA' = R (tan $\frac{1}{2}I - \tan \frac{1}{2}I'$), and A is moved forward or back accord-

ing as I' is less or greater than I. Changing degree and keeping A fixed,

$$T$$
 is unchanged. $\therefore R' = \frac{T}{\tan \frac{1}{2} I'}$ or $T \cot \frac{1}{2} I'$.

A curve ends in VB; required to end in V'B. Fig. 16. D and A change.

$$R' = R \frac{\text{vers } I}{\text{vers } I'}$$



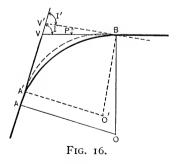
 $AA = (R \sin I - R' \sin I')$ and A is moved forward or back according as I' is greater or less than I.

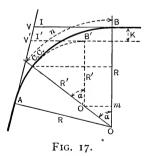
A curve ends in VB; required to end in V'B'. Fig. 17.

1. Assume new $R' \leq R$ according as B' is inside or outside VB. Then

$$\cos \alpha = \mathbf{I} - \frac{K}{R - R'}$$
 or $\mathbf{I} - \frac{K}{R' - R'}$,
 $n \text{ stations} = \frac{\alpha}{D}$.

Begin at *n* stations from *B* and run in curve of *D'* for *n'* stations = $\frac{\alpha}{D'}$.





2. Or, retaining A and letting n be total number of stations A to B,

$$D' = D \pm \frac{K}{\frac{7}{6}n^2}$$
, approx.

D' will be greater or less than D according as V'B' lies inside or outside of VB. Take D' nearest round number that will be sufficiently exact and run the curve D' for n' stations $=\frac{I}{D'}$.

3. Or, assuming a new degree less or greater than the original according as the tangent is to be thrown out or in, find n of Method 1 by

$$n = \sqrt{\frac{8K}{7(D-D')}}, \text{ approx.}$$

(D-D') is to be taken as the difference of degrees, subtracting the smaller from the larger. $\alpha=nD,\ n'=\frac{\alpha}{D'}$ to make the tangents parallel. Run curve of degree D' from C.C.

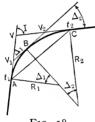


Fig. 18.

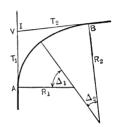


Fig. 19.

COMPOUND CURVES

Given R_1 , R_2 , Δ_1 , and Δ_2 ; required T_1 and T_2 . Fig. 18. $V_1 V_2 = t_1 + t_2.$

Solve triangle VV_1V_2 for V_1V and V_2V .

$$T_1 = VV_1 + t_1$$
: $T_2 = VV_2 + t_2$.

Given I, T_1 , T_2 , and R_1 ; required R_2 , Δ_1 , and Δ_2 . Fig. 19.

$$\cot \frac{1}{2} \Delta_2 = \frac{T_2 + T_1 \cos I - R_1 \sin I}{T_1 \sin I - R_1 \text{ vers } I},$$

$$\Delta_1 = I - \Delta_2,$$

$$R_2 = R_1 + \frac{T_1 \sin I - R_2 \text{ vers } I}{\text{vers } \Delta_2}.$$
(a)

Given I, T_1 , T_2 , and R_2 ; required R_1 , Δ_1 , and Δ_2 .

$$\cot \frac{1}{2} \Delta_{1} = \frac{R_{2} \sin I - T_{1} - T_{2} \cos I}{R_{2} \text{ vers } I - T_{2} \sin I},$$

$$\Delta_{2} = I - \Delta_{1},$$

$$R_{1} = R_{2} - \frac{R_{2} \text{ vers } I - T_{2} \sin I}{\text{ vers } \Delta_{1}}.$$
(b)

Given I, T_1 , R_1 , and Δ_1 ; required Δ_2 , R_2 , and T_2 .

$$\Delta_2 = I - \Delta_1$$

 R_2 is given by equation (a) above.

$$T_2 = (R_2 - R_1) \sin \Delta_2 + R_1 \sin I - T_1 \cos I$$
.

Given I_1 , I_2 , I_3 , and I_4 ; required I_4 , I_5 , and I_6 .

$$\Delta_1 = I - \Delta_2.$$

R is given by equation (b) above.

$$T_1 = R_2 \sin I - T_2 \cos I - (R_2 - R_1) \sin \Delta_1.$$

To end a compound curve in a new tangent, parallel to that first located.

(a) Move the curve parallel to itself along

the first tangent, a distance $AA' = \frac{K}{\sin I}$.

(b) Retaining the first branch, changing only the degree of the second,

$$R_{2}' = R_{2} \pm \frac{K}{\text{vers } \Delta_{2}},$$

$$R_{1}' = R_{1} \pm \frac{K}{\text{vers } \Delta_{1}},$$

according as the curve ends with the larger or shorter radius.

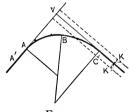


FIG. 20.

(c) Retaining both degrees, changing the Δ 's and the station of CC. If the new tangent is *inside* and the longer radius ends the curve the CC is advanced; if the new tangent is outside the CC is moved back; if the shorter radius ends the curve the movement of the CC is reversed. The new values for the *final* Δs are had from

vers
$$\Delta_2' = \operatorname{vers} \Delta_2 \pm \frac{K}{R_2 - R_1}$$
,
vers $\Delta_1' = \operatorname{vers} \Delta_1 \pm \frac{K}{R_2 - R_1}$.

To change the direction of the final tangent by a given amount. Solve the triangle VV'C for the new final tangent and the change in the initial tangent. The new I being known, retain the first radius and

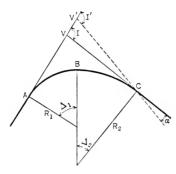


FIG. 21.

solve for the new final radius and the two central angles, by preceding equations.

VERTICAL CURVES

The rate of change of grade in passing sags and summits in the grade line, as recommended by the American Railway Engineering Association, is: For first-class railways change not more than 0.1 foot per station on summits and not more than 0.05 foot per station in sags; for second-class roads not more than double these rates.

How to determine the elevation of the several stations on the vertical curve will be shown by two examples. The first step is to determine the length of the curve; it will be convenient to adopt a rate of change that will give an even number of stations for the length.

Example 1. Two grades, -0.8 and +0.6, meet at station 462 where the elevation is 723. Required a vertical curve to connect with a change of 0.1 per station. The total change in rate is 0.8 + 0.6 = 1.4, giving 14 stations = 1.4 \div 0.1, of curve, or 7 stations each side of the vertex. The beginning of the curve is therefore at sta. 462 - 7 = 455 and the end is at 455 + 14 = 469. The elevation of 455 is $723.0 + 7 \times 0.8 = 728.6$; the elevation of sta. 469 is $723.0 + 7 \times 0.6 = 727.2$.

The rate of change for the first station is taken at half the station rate of change or 0.05. Therefore the elevation of

sta.
$$456 = 728.6 - (0.8 - 0.05) = 728.6 - 0.75 = 727.85$$

 $457 = \text{elev}. 456 - (0.8 - 0.15) = 727.85 - 0.65 = 727.20$
 $458 = \text{elev}. 457 - (0.8 - 0.25) = 727.20 - 0.55 = 726.65$
 $459 = \text{elev}. 458 - (0.8 - 0.35) = 726.65 - 0.45 = 726.20$
 $460 = \text{elev}. 459 - (0.8 - 0.45) = 726.20 - 0.35 = 725.85$
 $461 = \text{elev}. 460 - (0.8 - 0.55) = 725.85 - 0.25 = 725.60$
 $462 = \text{elev}. 461 - (0.8 - 0.65) = 725.60 - 0.15 = 725.45$
 $463 = \text{elev}. 462 - (0.8 - 0.75) = 725.45 - 0.05 = 725.40$
 $464 = \text{elev}. 463 - (0.8 - 0.85) = 725.40 + 0.05 = 725.45$

$$465 = \text{elev.} \ 464 - (0.8 - 0.95) = 725.45 + 0.15 = 725.60$$
 $466 = \text{elev.} \ 465 - (0.8 - 1.05) = 725.60 + 0.25 = 725.85$
 $467 = \text{elev.} \ 466 - (0.8 - 1.15) = 725.85 + 0.35 = 726.20$
 $468 = \text{elev.} \ 467 - (0.8 - 1.25) = 726.20 + 0.45 = 726.65$
 $469 = \text{elev.} \ 468 - (0.8 - 1.35) = 726.65 + 0.55 = 727.20$

It will be noticed that the final elevation agrees with that computed above; this proves the work. It will also be noticed that after the bottom of the sag is passed the elevations repeat themselves in reverse order. The bottom of the sag is not always the same station as the apex. This depends on the relative rates of the grades.

Example 2. — Two grades, -0.2 and -1.0, meet at station 867.0, where the elevation is 466.0. To connect the grades with a vertical curve changing at the rate of 0.1 per station. Total change in rate 0.8. Length of curve 8 stations. Beginning of curve sta. 867 - 4 = 863; end = sta. 871.

```
Elev. sta. 863 = 466 + 4 \times 0.2 = 466.8

Elev. sta. 871 = 466 - 4 \times 1.0 = 462.0

Elev. sta. 864 = elev. 863 - (0.2 + 0.05) = 466.8 - 0.25 = 466.55

Elev. sta. 865 = elev. 864 - (0.2 + 0.15) = 466.55 - 0.35 = 466.20

Elev. sta. 866 = elev. 865 - (0.2 + 0.25) = 466.20 - 0.45 = 465.75

Elev. sta. 867 = elev. 866 - (0.2 + 0.35) = 465.75 - 0.55 = 465.20

Elev. sta. 868 = elev. 867 - (0.2 + 0.45) = 465.20 - 0.65 = 464.55

Elev. sta. 869 = elev. 868 - (0.2 + 0.55) = 464.55 - 0.75 = 463.80

Elev. sta. 870 = elev. 869 - (0.2 + 0.65) = 463.80 - 0.85 = 462.95

Elev. sta. 871 = elev. 870 - (0.2 + 0.75) = 462.95 - 0.95 = 462.00
```

The work is proved since 462.0 is the elevation first found for station 871. There is no summit or bottom in this case as both grades are of the same sign.

TABLE I

Radii and their logarithms, and tangent offsets, and middle ordinates, for 100 feet chords of curves of degrees given. The degrees are given in degrees and decimals of a degree.

Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
0.00	_ ∞	∞	.000	.000	1.00	5729.65	3.75813	.873	.218
.02	286478 .90	5.45700	.017	.004	.02	5617.31	.74953	.890	.223
.04	143239.45	.15606	.035	.009	.04	5509.29	.74110	.908	.227
.06	95492.97	4.97997	.052	.013	.06	5405.34	.73283	.925	.231
.08	71619.73	.85503	.070	.017	.08	5305.24	.72471	-942	.236
.10	57295.79	4.75812	.087	.022	.10	5208.79	3.71674	.96o	.240
.12	47746.49	.67894	.105	.026	.12	5115.78	.70891	-977	.244
.14 .16	40925.57	.61199	.122	.031	.14	5026.03	.70122	-995	.248
.18	35809.87 31831.00	.55400	.140	.035	.16 .18	4939.38 4855.66	.69367	1.012	.253
.20	28647.90	.50285	.157	.039	.10		3.67895	.030 I.047	.262
.20	26047.90	4.45709	.175	.044	.20	4774·74 4696.46	.67177	.065	.266
.24	23873.26		.200		.24	4620.72	.66471	.082	.271
.24	22036.86	.37791	.227	.052	.24	4547.38	.65776	.100	.275
.28	20462.80	.31007	.244	.061	.28	4547.30	.65002	.117	.279
.30	19098.61	4.28100	.262	.065	.30	4407.46	3.64410	1.134	.284
.32	17904.95	.25297	.279	.070	.32	4340.60	.63756	.152	.288
-34	16851.73	.22664	.207	.074	.34	4275.90	.63103	.160	.202
.36	15915.52	.20182	.314	.079	.36	4213.02	.62459	.187	.297
.38	15077.86	.17834	.332	.083	.38	4151.07	.61825	.204	.301
.40	14323.97	4.15606	.349	.087	.40	4002.66	3.61201	1.222	.305
.42	13641.88	.13487	.367	.002	.42	4035.02	.60585	-239	.310
-44	13021.80	.11467	.384	.006	.44	3978.98	-59977	.257	.314
.46	12455.64	.09537	.401	.100	.46	3924.47	-59378	.274	.319
.48	11936.66	.07688	.419	.105	.48	3871.44	.58787	.292	.323
.50	11459.19	4.05915	.436	.100	.50	3819.83	3.58204	1.300	.327
.52	11018.46	.04212	.454	.113	.52	3769.57	.57629	.326	.332
-54	10610.37	.02573	.47I	.118	-54	3720.62	.57061	-344	.336
.56	10231.43	.00994	.489	.122	.56	3672.92	.56501	.361	-340
.58	9878.62	3.99470	.506	.127	.58	3626.43	-55948	-379	-345
.60	9549.34	3.97997	.524	.131	.60	3581.10	3.55402	1.396	-349
.62	9241.30	.96573	.541	.135	.62	3536.89	.54862	.414	-353
.64	8952.51	.95194	.559	.140	.64	3493.76	-54329	.431	.358
.66	8681.26	.93858	.576	.144	.66	3451.67	.53803	-449	.362
.68	8425.90	.92562	.593	.148	.68	3410.59	.53283	.466	.367
.70	8185.16	3.91303	.611	.153	.70	3370.46	3.52769	1.483	.371
.72	7957.80	.90079	.628	.157	.72	3331.28	.52261	.501	·375
.74	7742.73	.88889	.646	.161	.74	3292.99	.51759	.518	.384
.76 .78	7539.97	.87731	.663 .681	.166	.76	3255.57 3218.99	.50772	.536	.388
.70 .80	7345.67 7162.03	3.85504	.608	.170 .175	.78 .80	3183.23	3.50287	1.571	.393
.82	6987.35	.84431	.716	.170	.82	3148.25	.49807	.588	.393
.82	6820.99	.83385	.710	.183	.84	3114.03	.49332	.606	.401
.86	6662.36	.82363	.750	.188	.86	3080.55	.48863	.623	.406
.88	6510.05	.81364	.768	.102	.88	3047.78	.48308	.641	.410
.00	6366.26	3.80388	.785	.196	.00	3015.71	3.47939	1.658	.415
.92	6227.87	·79434	.803	.201	.92	2984.29	.47484	.675	.419
.94	6095.36	.78500	.820	.205	.94	2953.53	.47034	.693	.423
.96	5968.38	.77586	.838	.209	. 6	2923.40	.46589	.710	.428
.98	5846.58	.76690	.855	.214	.98	2893.87	.46148	.728	-432
1.00	5729.65	3.75813	.873	.218	2.00	2864.93	3.45711	1.745	.436
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46 2329.28 .36722 .147 .537 .46 1656.16 .21011 .010 .755 48 2310.49 .36370 .164 .541 .48 1646.68 .21661 .367 .755 50 2292.01 3.36022 2.181 .545 .50 1637.28 3.21412 3.054 .706 52 2273.83 .35676 .199 .550 .52 1627.98 .21165 .071 .766 54 2255.92 .35332 .216 .554 .54 1608.78 .20919 .089 .772 .56 2238.30 .34054 .251 .563 .58 1600.70 .20431 .124 .781 .60 2203.87 3.34310 .2260 .567 .60 1581.81 3.20189 3.141 .783 .62 2187.05 .33086 .304 .576 .64 1574.32 .19709 .176 .792 .62 154.17 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></td<>										
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.50 2292.01 3.36022 2.181 .545 .50 1637.28 3.21412 3.054 .764 .52 2273.83 .35676 .199 .550 .52 1627.98 .21165 .071.67 .768 .54 2255.92 .35332 .216 .554 .54 1618.78 .20910 .080 .772 .56 2238.30 .34992 .234 .559 .56 1609.69 .20674 .106 .777 .58 2220.95 .34654 .251 .563 .58 1600.70 .20431 .124 .781 .60 2203.87 .334319 .2269 .567 .60 1591.81 .320189 .3141 .788 .62 2187.05 .33986 .286 .572 .62 1583.02 .19049 .159 .796 .64 2170.49 .33656 .304 .576 .64 1597.43 .19792 .176 .68 138.10 .33083 .321 <th>48</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	48									
52 2273.83 .35076 .199 .550 .52 1627.98 .21165 .071 .766 .54 2255.92 .35332 .216 .554 .54 1618.78 .20919 .089 .772 .56 2238.30 .34092 .234 .559 .56 1609.69 .20674 .106 .777 .58 2220.95 .34654 .251 .563 .58 1600.70 .20431 .124 .783 .60 2203.87 .334319 .2260 .567 .60 1591.81 3.20189 3.141 .783 .62 2187.05 .33086 .304 .576 .60 1591.81 3.20189 3.141 .783 .64 2170.49 .33528 .321 .580 .66 1574.32 .19709 .176 .790 .64 2170.49 .33328 .321 .580 .66 1574.32 .19709 .176 .790 .68 2138.10										.764
.54 2255.92 .35332 .216 .554 .54 1618.78 .20919 .089 .772 .56 2238.30 .34992 .234 .559 .56 1609.69 .20674 .106 .777 .58 2220.95 .34554 .251 .563 .58 1600.70 .20431 .124 .781 .60 2203.87 .334319 2.269 .567 .60 1591.81 3.20189 3.141 .785 .62 2187.05 .33986 .286 .572 .62 1583.02 .19949 .159 .790 .64 2170.49 .33056 .304 .576 .64 1574.32 .19949 .159 .790 .68 2138.10 .33003 .339 .585 .66 1505.72 .19472 .193 .796 .72 2106.66 .32359 .373 .593 .72 1540.48 .18766 .228 .807 .74 2091.29 <										.768
.56 2238.30 .34992 .234 .559 .56 1609.69 .20674 .106 .777 .58 2220.95 .34654 .251 .563 .58 1600.70 .20431 .124 .781 .60 2203.87 .334319 2.269 .567 .60 1591.81 .320189 .3141 .785 .62 2187.05 .33986 .286 .572 .62 1583.02 .19949 .159 .796 .64 2170.49 .33656 .304 .576 .64 1574.32 .19700 .176 .799 .68 2138.10 .33003 .339 .585 .68 1557.22 .19472 .103 .790 .68 2138.10 .332681 2.356 .589 .70 1548.80 3.19000 3.228 .801 .70 2122.26 3.3241 .391 .598 .74 1532.24 .18533 .263 .81 .74 2091.29								.20010		.772
58 2220.05 34654 .251 .563 .58 1600.70 .20431 .124 .781 .60 2203.87 3.34310 2.260 .567 .60 1591.81 3.20189 3.141 .785 .62 2187.05 33986 .286 .572 .62 1583.02 .19949 .159 .796 .64 2170.49 .33656 .304 .576 .64 1574.32 .19709 .176 .796 .66 2154.17 .33328 .321 .580 .66 1565.72 .19472 .193 .791 .792 .68 2138.10 .33303 .339 .585 .68 1557.22 .19235 .211 .802 .70 2122.26 .32359 .373 .593 .70 1548.80 .18766 .246 .81 .74 2091.29 .32041 .391 .598 .74 1532.24 .18533 .233 .281 .76 2076				.234			1609.69	.20674	.106	-777
.62 2187.05 .33086 .286 .572 .62 1583.02 .19949 .159 .706 .64 2170.49 .33656 .304 .576 .64 1574.32 .19949 .159 .706 .66 2154.17 .33328 .321 .580 .66 1505.72 .19472 .103 .709 .68 2138.10 .33003 .339 .585 .68 1557.22 .19235 .211 .801 .70 2122.26 3.32681 2.356 .580 .70 1548.80 3.19000 3.228 .801 .72 2106.66 .32359 .373 .593 .72 1540.48 .18766 .246 .817 .74 2091.29 .32041 .391 .598 .74 1532.24 .18533 .263 .816 .76 2076.13 .31412 .426 .607 .78 1516.14 .18071 .208 .82 .80 204.68 <th< th=""><th>.58</th><th>2220.95</th><th></th><th>.251</th><th></th><th>.58</th><th>1600.70</th><th>.20431</th><th>.124</th><th>.781</th></th<>	.58	2220.95		.251		.58	1600.70	.20431	.124	.781
.64 2170.49 .33656 .304 .576 .64 1574.32 .19799 .176 .704 .66 2154.17 .33328 .321 .580 .66 1505.72 .19472 .103 .79 .70 2122.26 3.32681 2.356 .589 .70 1548.80 .319000 3.228 .80 .72 2106.66 .32359 .373 .593 .72 1540.48 .18766 .246 .81 .74 2091.29 .32041 .391 .598 .74 1532.24 .18533 .261 .81 .76 2076.13 .31726 .408 .602 .76 1524.10 .18301 .281 .82 .80 2046.48 3.31101 2.443 .611 .80 1508.06 3.17842 3.316 .82 .82 2031.97 .30702 .460 .615 .82 1500.17 .17614 .333 .84 201.66 .30485 <t< th=""><th>.60</th><th></th><th></th><th>2.269</th><th>.567</th><th>.60</th><th></th><th>3.20189</th><th>3.141</th><th>.785</th></t<>	.60			2.269	.567	.60		3.20189	3.141	.785
.66 2154.17 .33328 .321 .580 .66 1565.72 .19472 .103 .709 .68 2138.10 .33003 .339 .585 .68 1557.22 .19235 .211 .800 .700 2122.26 3.32681 2.356 .589 .70 1548.80 3.19000 .3228 .809 .72 2106.66 .32359 .373 .593 .72 1540.48 .18766 .246 .812 .74 2091.29 .32041 .301 .598 .74 1532.24 .18533 .263 .816 .76 2076.13 .31726 .408 .602 .76 1524.10 .18301 .281 .826 .82 2046.48 3.31101 2.443 .601 .80 1508.06 3.17842 3.316 .82 .82 2031.97 .30792 .460 .615 .82 1500.17 .17614 .333 .83 .84 2017.66 .30485 .478 .620 .84 1492.36 .17387 .351 .83 .88 1989.65 .29878 .513 .628 .88 1470.98 .11762 .368 .84 .88 1989.65 .29878 .513 .628 .88 1470.98 .11912 .368 .84 .89 1975.93 3.29577 .5530 .633 .90 1460.41 3.16714 3.403 .85 .92 1962.40 .29279 .548 .637 .92 1461.91 .16492 .420 .85 .92 1962.40 .29279 .548 .637 .92 1461.91 .16492 .420 .85 .96 1935.88 .28688 .583 .646 .96 1447.15 .16051 .435 .86 .96 1935.88 .28688 .583 .646 .96 1447.15 .16051 .435 .86 .96 1935.88 .28688 .583 .646 .96 1447.15 .16051 .455 .86 .96 1935.88 .28888 .583 .447 .94 1454.49 .16271 .438 .86 .96 1935.88 .28688 .583 .646 .96 1447.15 .16051 .455 .86 .96 1935.88 .28888 .583 .447 .94 1454.49 .16271 .438 .86 .96 1935.88 .28888 .583 .646 .96 1447.15 .16051 .455 .86 .96 1935.88 .28888 .583 .447 .94 1454.49 .16271 .438 .86 .96 1935.88 .28888 .583 .646 .96 1447.15 .16051 .455 .86 .96 .98 1439.88 .15833 .473 .86										.790
68 2138.10 .33003 .339 .585 .68 1557.22 .19235 .211 .80 .70 2122.26 3.32681 2.356 .589 .70 1548.80 3.1923 .211 .80 .72 2106.66 .32359 .373 .593 .72 1540.48 .18766 .246 .81 .74 2091.29 .32041 .391 .598 .74 1532.24 .18533 .263 .81 .78 2061.20 .31412 .426 .602 .76 1524.10 .18301 .281 .82 .80 2046.48 3.31101 .2443 .611 .80 1508.06 3.17842 3.316 .82 .82 2031.97 .30792 .460 .615 .82 1500.17 .17614 .333 .83 .84 2017.66 .30485 .478 .620 .84 1492.36 .17387 .351 .83 .86 2003.56 .301					.576					.794
70 2122.26 3.32681 2.356 .589 .70 1548.80 3.1900 3.228 .80 72 2106.66 .32359 .373 .593 .72 1540.48 .18766 .246 .81: .74 2091.29 .32041 .391 .598 .74 1532.24 .18533 .263 .810 .76 2076.13 .31726 .408 .602 .76 1524.10 .18301 .211 .82 .80 2046.48 3.31101 2.443 .611 .80 1508.06 3.17842 3.316 .82 .82 2031.97 .30792 .460 .615 .82 1500.17 .17614 .1874 .333 .83 .84 2017.66 .30485 .478 .620 .84 1492.36 .17387 .351 .83 .86 2003.56 .30180 .496 .624 .86 1484.63 .17162 .368 .84 .88 1989										
72 2106.66 .32359 .373 .593 .72 1540.48 .18766 .246 .81 .74 2091.29 .32041 .391 .598 .74 1532.24 .18533 .263 .816 .76 2076.13 .31726 .408 .602 .76 1524.10 .18301 .281 .82 .78 2061.20 .31412 .426 .607 .78 1516.14 .18071 .298 .82 .80 2046.48 3.31101 2.443 .611 .80 1508.06 3.17842 3.316 .82 .82 2031.97 .30792 .460 .615 .82 1500.17 .17614 .333 .83 .84 2017.66 .30485 .478 .620 .84 1492.36 .17387 .351 .83 .86 2003.56 .30180 .496 .624 .86 1484.63 .17162 .368 .84 .90 1975.93 3.295										
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76 2076.13 .31726 .408 .602 .76 1524.10 .18301 .281 .826 78 2061.20 .31412 .426 .607 .78 1516.14 .18071 .208 .82 .80 2046.48 3,31101 2.443 .611 .80 1508.06 3.17842 3.316 .82 .82 2031.97 .30792 .460 .615 .82 1500.17 .17614 .333 .83 .84 2017.66 .30485 .478 .620 .84 1492.36 .17387 .351 .83 .86 2003.56 .30180 .496 .624 .86 1484.63 .17162 .368 .84 .88 1989.65 .29878 .513 .628 .88 1476.98 .16937 .385 .84 .90 1975.93 3.29577 2.530 .633 .90 1460.41 3.16714 .3493 .85 .92 1962.40 .2										.812
$\begin{array}{cccccccccccccccccccccccccccccccccccc$.820
80 2046.48 3,31101 2.443 .611 .80 1508.06 3.17842 3.316 .82 .82 2031.97 .30792 .460 .615 .82 1500.17 .17614 .333 .83 .84 2017.66 .30485 .478 .620 .84 1492.36 .17387 .351 .83 .86 2003.56 .30180 .496 .624 .86 1484.63 .17162 .368 .84 .88 1980.65 .20878 .513 .628 .88 1470.98 .16937 .385 .84 .90 1975.93 3.29577 2.530 .633 .90 1460.41 3.16714 3.403 .85 .92 1962.40 .20279 .548 .637 .92 1461.91 .16492 .420 .85 .94 1940.05 .28688 .583 .646 .96 1447.15 .16051 .435 .86 .98 1922.89 .2										.825
82 2031.97 .30792 .460 .615 .82 1500.17 .17614 .333 .83 .84 2017.66 .30485 .478 .620 .84 1492.36 .17387 .351 .83 .86 2003.56 .30180 .496 .624 .86 1484.63 .17162 .368 .84 .88 1989.65 .29878 .513 .628 .88 1470.98 .16937 .385 .84 .90 1975.93 3.29577 2.530 .633 .90 1469.41 3.16714 3.403 .85 .92 1962.40 .20279 .548 .637 .92 1469.41 3.16714 3.403 .85 .94 1494.05 .28082 .565 .641 .94 1454.49 .16271 .438 .86 .96 1935.88 .28688 .583 .646 .96 1447.15 .16051 .455 .86 .98 1922.89 .283										.820
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$.833
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$.84		.17387		.838
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$							1484.63	.17162	.368	.842
.92 1962.40 .29279 .548 .637 .92 1461.91 .16492 .420 .85 .94 1949.05 .28082 .565 .641 .94 1454.49 .16271 .438 .86 .96 1935.88 .28688 .583 .646 .96 1447.15 .16051 .455 .86 .98 1922.89 .28306 .600 .650 .98 1439.88 .15833 .473 .86	.88	1989.65	.29878	.513						.847
.94 1949.05 .28082 .565 .641 .94 1454.49 .16271 .438 .866 .96 1935.88 .28688 .583 .646 .96 1447.15 .16051 .455 .866 .98 1922.89 .28396 .600 .650 .98 1439.88 .15833 .473 .866	.90		3.29577							.851
.96 1035.88 .28688 .583 .646 .96 1447.15 .16051 .455 .86 .98 1922.89 .28396 .600 .650 .98 1439.88 .15833 .473 .866	.92									.855
.98 1922.89 .28396 .600 .650 .98 1439.88 .15833 .473 .860										.860
190 1921109 11109 1110 110						.96				
3.00 1910.08 3.28105 2.018 .055 4.00 1432.09 3.15015 3.490 .87.										
	3.00	1910.08	3.28105	2.018	.055	4.00	1432.09	3.15015	3.490	.073

	(Tan.	Mid.				Tan,	Mid.
Deg.	Radius	Logarithm	Off.	Ord.	Deg.	Radius	Logarithm	Off.	Ord.
D	R	Log R	t t	m	D	R	Log R	t t	m
0	6 -	6	2 400	.873	0	1146.28	2 0 7 0 2 0	4 262	
4.00	1432.69	3.15615	3.490	.877	5.00	1140.20	3.05929	4.362	1.091
.02	1425.50	.15183	.525	.881	.04	1137.10	.05583	·379 ·397	.095
.04	1411.52	.14969	.542	.886	.04	1132.70	.05411	.414	.104
.08	1404.60	.14755	.560	.890	.08	1128.24	.05240	.432	.108
.10	1397.76	3.14543	3.577	.895	.10	1123.82	3.05070	4.449	1.113
.12	1390.98	.14332	-595	.899	.12	1119.43	.04900	.467	.117
.14	1384.26	.14122	.612	.903	.14	1115.08	.04731	.484	.122
.16	1377.61	.13012	.629	.908	.16	1111.00	.04571	.501	.126
.18	1371.02	.13704	.647	.912	.18	1106.47	.04394	.510	.130
.20	1364.49	3.13497	3.664	.916	.20	1102.22	3.04227	4.536	1.135
.22	1358.03	.13291	.682	.921	.22	1098.00	.04060	-554	.139
.24	1351.31	.13076	.699	.925	.24	1093.81	.03894	.571	.143
.26	1345.28	.12881	.717	.929	.26	1089.66	.03729	.589	.148
.28	1339.00	.12678	.734	-934	.28	1085.53	.03564	.606	.152
.30	1332.77	3.12476	3.752	.938	.30	1081.44	3.03400	4.623	1.156
.32	1326.61	.12274	.769	.943	.32	1077.38	.03237	.641	.161
-34	1320.49	.12074	.786	-947	-34	1073.34	.03074	.658	.165
.36	1314.44	.11874	.804	.951	.36	1069.34	.02912	.676	.170
.38	1308.44	.11675	.821	.956	.38	1065.37	.02750	.693	.174
-40	1302.50	3.11478	3.839	.960	.40	1061.43	3.02589	4.711	1.178
.42	1296.61	.11281	.856	.964	.42	1057.51	.02429	.728	.183
.44	1290.77	.11085	.874	.969	-44	1053.63	.02269	.746	.187
.46 .48	1284.98	.10696	.891	.973 .978	.46 .48	1049.77	.02109	.763 .780	.191
.50	1279.25	3.10502	3.926	.982	.50	1043.94	3.01793	4.798	1.200
.52	1267.93	.10310	.943	.986	.52	1038.37	.01635	.815	.205
·52	1262.35	.10118	.961	.900	·54	1034.62	.01478	.833	.200
.56	1256.82	.09927	.978	.995	.56	1030.00	.01322	.850	.213
.58	1251.33	.09737	.996	.999	.58	1027.21	.01166	.868	.218
.60	1245.89	3.09548	4.013	1.004	.60	1023.55	3.01011	4.885	1.222
.62	1240.50	.09360	.031	.008	.62	1010.01	.00856	.902	.226
.64	1235.16	.09172	.048	.012	.64	1016.29	.00702	.920	.231
.66	1229.86	.08986	.065	.017	.66	1012.70	.00548	-937	.235
.68	1224.61	.08800	.083	.021	.68	1009.14	.00395	-955	.239
.70	1219.40	3.08615	4.100	1.026	.70	1005.60	3.00243	4.972	1.244
.72	1214.24	.08430	.118	.030	.72	1002.00	.00091	.990	.248
.74	1209.12	.08247	.135	.034	.74	998.60	2.99939	5.007	.253
.76	1204.04	.08064	.153	.039	.76	995.14	.99788	.024	.257
.78	1199.00	.07882	.170	.043	.78	991.68	.99638	.042	.261
.80	1194.01	3.07701	4.188	1.047	.80	988.28	2.99488	5.059	1.266
.82	1189.06	.07520	.205	.052	.82 .84	984.89 981.52	.99339	.077	.270
.84 .86	1184.15	.07341	.222	.056	.86	981.52	.99190	.094	.274
.88	1179.28	.06983	.257	.065	.88	974.66	.98885	.112	.283
.00	1169.66	3.06806	4.275	1.060	.90	974.00	2.98746	5.146	1.287
.92	1164.01	.06629	.292	.074	.90	971.34	.98599	.164	.202
.92	1160.10	.06453	.310	.078	.94	065.01	.98453	.181	.296
.96	1155.52	.06278	.327	.082	.94 .96	961.77	.98307	.199	.301
.98 .98	1150.88	.06103	.345	.087	.98	958.56	.98162	.216	.305
5.00	1146.28	3.05929	4.362	1.001	6.00	955.37	2.98017	5.234	1.300
						1 300.07		0,	

Deg. · D	Radius . R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg. D .	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
6.00	955-37	2.98017	5.234	1.309	7.00	819.02	2.91329	6.105	1.528
.02	952.20	.97873	.251	.314	.02	816.69	.91206	.122	-532
.04	949.05	.97729	.268	.318	.04	814.37	.91082	.140	.536
.06	945.92	.97585	.286	.322	.06	812.07	.90959	.157	.541
.08	942.81	.97442	.303	-327	.08	809.78	.90837	.175	∙545
.10	939.72	2.97300	5.321	1.331	.10	807.50	2.90714	6.192	1.550
.12	936.65	.97158	.338	•335	.12	805.23	.90592	.209	.554
.14	933.60	.97016	.356	.340	.14	802.98	.90471	.227	.558
.16	930.57	.96875	·373	·344	.16	800.74 708.51	.90349	.244	.563
.10	927.50	.96734 2.96594	.390	·349	.18	796.30	.90228	.262	.567
.20	924.50	.96455	5.408 •425	1.353	.20	794.10	2.90108	6.279	1.572
.24	g18.66	.96315	•443	·357 .362	.24	701.00	.89867	.296	.576 .580
.26	915.72	.96176	.460	.366	.26	789.73	.89748	.314	.584
.28	012.81	.96038	.478	.370	.28	787.56	.89628	.331 .349	.589
.30	909.92	2.95900	5.495	1.375	.30	785.40	2.89509	6.366	1.503
.32	906.48	.95736	.512	-379	.32	783.26	.89391	.384	.598
.34	004.18	.95625	.530	.384	.34	781.13	.89391	.401	.602
.36	001.34	.95489	.547	.380	.36	770.01	.80154	.418	.606
.38	898.52	.95353	.565	.392	.38	776.90	.89037	.436	.611
.40	805.71	2.95217	5.582	1.397	.40	774.81	2.88919	6.453	1.615
.42	892.92	.95081	.600	.401	.42	772.72	.88802	.471	.610
.44	890.15	.94947	.617	.405	.44	770.65	.88685	.488	.624
.46	887.40	.94812	.634	.410	.46	768.58	.88560	.505	.628
.48	884.67	.94678	.652	.414	.48	766.53	.88453	.523	.632
.50	881.95	2.94544	5.669	1.418	.50	764.49	2.88337	6.540	1.637
.52	879.24	.94411	.687	.423	.52	762.46	.88222	-558	.641
-54	876.56	.94278	.704	-427	-54	760.44	.88106	-575	.646
.56	873.89	.94146	.722	.432	.56	758.45	.87993	.593	.650
.58	871.24	.94014	.739	.436	.58	756.43	.87877	.610	.654
.60	868.6o	2.93882	5.756	1.440	.60	754.44	2.87763	6.627	1.659
.62	865.98	.93751	.774	-445	.62	752.47	.87649	.645	.663
.64	863.37	.93620	.791	•449	.64	750.50	.87535	.662	.667
.66 .68	860.78 858.21	.93489	.809 .826	·453	.66	748.54	.87422	.680	.672
.70	855.65	-93359	5.844	.458 1.462	.68	746.60 744.66	.87309 2.87196	.697	.676 1.680
.70	853.10	.03100	.861	.466	.70 .72	744.00	.87083	6.714 •732	.685
.74	850.58	.93100	.878	.471	.72	740.82	.86071		.680
.76	848.06	.02843	.896	.475	.76	738.91	.86859	·749 ·767	.604
.78	845.56	.02715	.913	.480	.78	737.02	.86748	.784	.698
.76 .80	843.08	2.92587	5.931	1.484	.76 .80	735.13	2.86636	6.802	1.702
.82	840.61	.92459	.948	.488	.82	733.25	.86525	.810	.707
.84	838.16	.92332	.965	•493	.84	731.38	.86415	.836	.711
.86	835.71	.92206	.983	-497	.86	729.53	.86304	.854	.715
.88	833.29	.92080	6.000	1.501	.88	727.68	.86194	.871	.720
.90	830.88	2.91954	6.018	1.505	.90	725.85	2.86084	6.889	1.724
.92	828.48	.91828	.035	.510	.92	724.01	.85974	.906	.729
.94	826.09	.91703	.053	.515	.94	722.19	.85865	.923	.733
.96	823.72	.91578	.070	.519	.96	720.38	.85756	.941	.737
.98	821.36	.91454	.087	.523	.98	718.57	.85647	.958	.742
7.00	819.02	2.91329	6.105	1.528	8.00	716.78	2.85539	6.976	1.746

Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
8.00	716.78	2.85539	6.976	1.746	9.00	637.27	2.80433	7.846	1.965
.02	714.99	.85430	.993	.750	.02	635.86	.80336	.863	.969
.04	713.22	.85322	7.010	·755	.04	634.46	.80240	.881	·9 7 3
.06	711.45	.85215	.028	·759	.06	633.06	.80145	.898	.978
.08	709.69	.85107	.045	.764	.08	631.67	.80049	.916	.982
.10	707.94	2.85000	7.063	1.768	.10	630.29	2.79954	7.933	1.987
.12	706.20	.84893	.080	.772	.12	628.91	.79859	.950	.991
.14	704.47	.84786	.098	.777	.14	627.53	.79764	.968	.995
.16	702.75 701.03	.84680 .84574	.115	.781 .785	.16 .18	626.17 624.81	.79669	.985	.999
.10	699.33	2.84468	.132 7.150	1.790	.10	623.45	.79574	8.002 8.020	2.004
.20	697.63	.84362	.167	·794	.20	622.10	2.79480 .79386		2.008
.24	695.94	.84302	.185	.794	.24	620.76		.037	.013
.24	694.25	.84152	.202	.803	.24	619.42	.79292 .79198	.055	.017
.28	692.58	.84047	.210	.803	.28	618.00	.79198	.000	.021
.30	690.91	2.83942	7.237	1.811	.30	616.76	2.70012	8.107	2.030
.32	689.26	.83838	.254	.816	.32	615.44	.78919	.124	.034
-34	687.61	.83734	.272	.820	.34	614.12	.78826	.142	.039
.36	685.96	.83630	.280	.825	.36	612.82	.78733	.150	.043
.38	684.33	.83527	.306	.829	.38	611.51	.78640	.176	.048
.40	682.70	2.83423	7.324	1.833	.40	610.21	2.78548	8.194	2.052
.42	681.00	.83320	.341	.838	.42	608.02	.78456	.211	.056
.44	679.47	.83217	-359	.842	.44	607.63	.78364	.220	.061
.46	677.87	.83115	.376	.847	.46	606.35	.78272	.246	.065
.48	676.27	.83012	.393	.851	.48	605.08	.78181	.263	.060
.50	674.69	2.82910	7.411	1.855	.50	603.80	2.78090	8.281	2.074
.52	673.11	.82808	.428	.860	.52	602.54	.77999	.298	.078
-54	671.53	.82707	.446	.864	.54	601.28	.77908	.316	.083
.56	669.97	.82605	.463	.868	.56	600.02	.77817	-333	.087
.58	668.41	.82504	.480	.873	.58	598.77	.77726	.350	.091
.60	666.86	2.82403	7.498	1.877	.60	597.53	2.77636	8.368	2.096
.62	665.33	.82303	.515	.881	.62	596.29	.77546	.385	.100
.64	663.77	.82202	·533	.886	.64	595.06	.77456	.403	.104
.66	662.24	.82102	.550	.890	.66	593.83	.77366	.420	.109
.68	660.72	.82002	.567	.895	.68	592.60	.77276	.437	.113
.70	659.21	2.81902	7.585	1.899	.70	591.38	2.77187	8.455	2.117
.72	657.70	.81803	.602	.903	.72	590.17 588.96	.77098	.472	.121
.74	656.19	.81703 .81604	.620	.908	.74 .76	587.76	.77009	.490	.126
.76 .78	654.70 653.21	.81505	.637	.912	.78	586.56	.76831	.507	.131
.70 .80	651.73	2.81407	.655 7.672	1.021	.70 .80	585.36	2.76743	.524 8.542	2.130
.80	650.25	.81308	.680	.925	.82	584.17	.76654		.144
.82	648.79	.81300	.707	.925	.84	582.99	.76566	·559 ·576	.148
.86	647.32	.81112	.724	.934	.86	581.81	.76478	.594	.152
.88	645.87	.81014	.742	.934	.88	580.64	.76390	.611	.157
.90	644.42	2.80017	7.759	1.943	.90	579.46	2.76303	8.620	2.161
.92	642.08	.80820	.776	-947	.92	578.30	.76215	.646	.166
.94	641.54	.80723	.794	.951	.94	577.14	.76128	.663	.170
.96	640.11	.80626	.811	.956	.96	575.99	.76041	.681	.174
.98	638.60	.80520	.820	.960	.98	574.83	.75954	.698	.179
9.00	637.27	2.80433	7.846	1.965	10.00	573.69	2.75867	8.716	2.183
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Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg. D	Radius R	Logarithma Log R	Tan. Off. t	Mid. Ord. m
0					0				
10.0	573.69	2.75867	8.716	2.183	15.0	383.06	2.58327	13.053	3.277
.I	568.02	.75436	.803	.205	ı.	380.54	.58040	.139	.299
.2	562.47	.75010	.889	.227	.2	378.05	-57755	.226	.321
٠3	557.02	.74587	.976	.234	-3	375.60	.57472	.312	-343
.4	551.68	.74169	9.063	.270	-4	373.17	.57191	-399	.365
-5	546.44	2.73754	9.150	2.293	-5	370.78	2.56912	13.485	3.387
.6	541.30	.73344	.237	.314	.6	368.42	.56634	.572	.409
.7	536.25	.72937	.324	.336	.7	366. 0 9	.56358	.658	.431
.8	531.30	·72534	.411	.358	.8	363.78	.56084	.744	-452
.9	526.44	.72135	.498	.380	.9	361.51	.55812	.831	·474
11.0	521.67	2.71740	9.585	2.402	16.0	359.26	2.55541	13.917	3.496
Ι.	516.99	.71348	.671	.423	.I	357.05	·55273	14.004	.518
.2	512.38	.70960	.758	.445	.2	354.86	.55006	.090	.540
-3	507.86	.70575	.845	.467	-3	352.70	·5474 <u>0</u>	.177	.562
-4	503.42	.70193	.932	.489	.4	350.56	-54476	.263	.584
-5	499.06	2.69815	10.019	2.511	.5	348.45	2.54214	14.349	3.606
.6	494.77	.69441	.106	•533	.6	346.37	-53953	.436	.628
.7	490.56	.69 0 69	.192	-555	.7	344.31	.53694	.522	.650
.8	486.42	.68701	.279	-577	.8	342.27	·534 <u>3</u> 7	.608	.672
.9	482.34	.68336	.366	.598	.9	340.26	.53181	.695	.694
12.0	478.34	2.67974	10.453	2.620	17.0	338.27	2.52927	14.781	3.716
.I	474.40	.67614	.540	.642	.I	336.31	.52674	.867	.738
.2	470.53	.67258	.626	.664	.2	334.37	.52423	.954	.760
-3	466.72	.66905	.713	.686	-3	332.45	.52173	15.040	.781
-4	462.96	.66555	.800	.708	-4	330.56	.51924	.1 26	.803
-5	459.28	2.66207	10.887	2.730	-5	328.69	2.51677	15.212	3.825
.6	455.65	.65863	•973	.752	.6	326.83	.51432	.299	.847
.7	452.07	.65521	11.060	.774	.7	325.00	.51188	.385	.869
.8	448.56	.65182	.147	.795	.8	323.18	.50945	.47 I	.891
.9	445.00	.64845	.234	.817	.9	321.39	.50704	.557	.913
13.0	441.68	2.64511	11.320	2.839	18.0	319.62	2.50464	15.643	3.935
.1	438.33	.64180	.407	.861	ı.	317.87	.50225	.730	957
.2	435.02	.63851	.494	.883	.2	316.14	.49988	.816	.979
-3	431.76	.63525	.580	.905	-3	314.43	.49752	.902	4.001
-4	428.56	.63201	.667	.927	•4	312.73	.49517	.988	.023
·5	425.40	2.62879	11.754	2.949	-5	311.06	2.49284	16.074	4.045
	422.28	.62560	.840	.971	.6	309.40	.49052	.160	.067
.7 .8	419.22	.62244	.927	.992	.7	307.76	.48821	.246	.089
	416.19	.61929	12.014	3.014	.8	306.14	.48591	-333	.III
.9	413.21	.61617	.100	.036	.9	304.53	.48363	.419	.133
14.0 .1	410.28	.61000	.274	3.058 .080	19.0	302.94	2.48136	16.505	4.155
.1	407.38	.60605	.360	.102	.I	301.37	.47910	.591	.177
	404.53	.60391		.102		299.82 298.28	.47686 .47462	.677	.199
-3	398.94	.600391	.447	.124	-3	296.75		.763	
-4	396.20	2.59791	·533 12.620	3.168	-4		.47240	16.935	.243 4.265
5	393.50	.59495	.706	.190	.5 .6	295.25 293.76	2.47019 .46799	17.021	.287
.7	393.50	.59495	.700	.211	.0	293.70	.46580	.107	.308
.8	388.21	.589200	.880	.233	.8	292.28	.46362	.107	.330
.9	385.62	.58616	.966		.0	280.37	.46145	.279	.352
.9 15.0	383.06	2.58327	13.053	.255 3.277	20.0	287.94	2.45930	17.365	4.374
-3.0	555.00	2.35327	20.000	3.2//	20.0	207.94	2.43930	-1.303	4.374

Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
20.0	287.94	2.45930	17.365	4.374	25.0	231.01	2.36363	21.644	5.476
.1	286.52	.45716	.451	.396	.1	230.11	.36193	.729	.498
.2	285.12	.45502	·537	.418	.2	229.21	.36023	.814	.520
-3	283.73	.45290	.623	.440	-3	228.32	-35854	.899	-542
-4	282.35	.45079	.708	.462	•4	227.43	.35685	.985	.564
5	280.99	2.44869	17.794	4.484	-5	226.55	2.35517	22.070	5.586
.6	279.64	.4466 o	.880	.506	.6	225.68	35350	.155	.608
.7	278.30	-44452	.966	.528	.7	224.82	.35184	.240	.630
.8	276.98	.44245	18.052	.550	.8	223.96	.35018	.325	.653
.9 21.0	275.67	.44039 2.43834	.138	.572	.9 26.0	222.27	.34853 2.34688	.410	.675 5.697
	274.37 273.08	.43630	.300	4.594 .616	.1	221.43	-34524	22.495 .58c	.710
.I .2	271.81	.43427	.309	.638	.1	220.60	.34361	.665	.719
.2	270.55	.43427	.481	.660	.3	210.78	.34199	.750	.763
.4	269.30	.43024	.567	.682	.4	218.06	.34037	.835	.785
·4 ·5	268.56	2.42824	18.652	4.704	.5	218.15	2.33875	22.020	5.807
.6	266.34	.42624	.738	.726	.6	217.34	.33715	23.005	.829
.7	265.62	.42426	.824	.748	.7	216.54	-33555	.000	.852
.8	264.42	.42220	.010	.770	.8	215.75	-33395	.175	.874
.9	263.22	.42033	.995	.792	.9	214.06	-33237	.260	.896
22.0	262.04	2.41837	10.081	4.814	27.0	214.18	2.33078	23.345	5.918
.1	260.87	.41643	.167	.836	ı.	213.41	.32921	.429	.940
.2	259.71	.41449	.252	.858	.2	212.64	.32764	.514	.962
.3	258.56	.41256	.338	.881	-3	211.87	.32608	.599	.984
.4	257.42	.41064	.423	.903	-4	211.11	.32452	.684	6.006
-5	256.29	2.40873	19.500	4.925	-5	210.36	2.32297	23.769	6.029
.6	255.17	.40683	.595	-947	.6	209.61	.32142	.853	.051
.7	254.06	.40494	.680	.969	.7	208.87	.31988	.938	.073
.8	252.96	.40306	.766	.991	.8	208.14	.31835	24.023	.095
.9	251.87	.40118	.851	5.013	.9	207.40	.31682	.108	.117
23.0	250.79	2.39931	19.937	5.035	28.0	206.68	2.31529	24.192	6.139
.1	249.72	.39746	20.022	.057	.1	205.96	.31378	.277	.161
.2	248.66	.39561	.108	.079	.2	205.24	.31227	.362	.184
-3	247.61	.39376	.193	.101	•3	204.53	.31076	.446	.206
-4	246.56	.39193	.279	.123	-4	203.83	.30926	.531	.228
-5	245.53	2.39010	20.364	5.145	-5	203.13	2.30776	24.615	6.250
.6	244.50	.38829	.450	.167	.6	202.43	.30627	.700	.272
.7	243.49	.38647	·535	.189	.7	201.74	.30479	.784	.294
.8	242.48	.38467	.620	.211	.8	201.05	.30331	.869	.316
.9	241.48	.38288	.706	.233	.9	200.37	.30184	.954	-339
24.0	240.49	2.38109	20.791	5.255	29.0	199.70	2.30037	25.038	6.361
I.	239.50	.37931	.877	.278	.1	199.02	.29891	.122	.383
.2	238.53	-37754	.962	.299	.2	198.36	.29745	.207	.405
-3	237.56	-37578	21.047	.321	-3	197.70	.29000	.376	.450
-4	236.60	.37402	.132	-343	-4	196.38	2.20311	25.460	6.472
.5 .6	235.65	2.37227		5.366	.5 .6	195.74	.20167	-545	.494
.7	234.71	.37053	.303	.410	.7	195.74	.20024	.620	.516
.8	233.77	.36707	.300	.432	.8	195.09	.28881	.713	.538
.9	231.02	.36535	-559	.454	.0	193.82	.28739	.798	.560
25.0	231.01	2.36363	21.644	5.476	30.0	193.19	2.28597	25.882	6.583
23.0	231.51	2.30303	1 -1.044	3.470	35.5	1 -939	1 -120397	3,	2.525

Deg. D	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m	Deg.	Radius R	Logarithm Log R	Tan. Off. t	Mid. Ord. m
0					0				
30.0	193.19	2.28597	25.882	6.583	35.0	166.28	2.22083	30.071	7.696
.1	192.56	.28456	.966	.605	т.	165.82	.21963	.154	.718
.2	191.94	.28315	26.050	.627	.2	165.36	.21843	.237	.740
.3	191.32	.28175	.135	.649	.3	164.91	.21724	.320	.763
.4	190.70	.28036	.219	.671	.4	164.46	.21605	.403	.785
-5	190.09	2.27896	26.303	6.694	-5	164.01	2.21486	30.486	7.807
.6	189.49	.27757	.387	.716	.6	163.56	.21368	.570	.830
.7	188.88	.27619	.471	.738	.7	163.12	.21250	.653	.852
.8	188.28	.27481	.556	.760	.8	162.68	.21133	.736	.874
.9	187.69	.27344	.640	.782	.9	162.24	.21016	.819	.897
31.0	187.10	2.27207	26.724	6.805	36.o	161.80	2.20899	30.902	7.919
.I	186.51	.27071	.808	.827	.I	161.37	.20782	.985	.942
.2	185.93	.26935	.892	.849	.2	160.94	.2 0 666	31.068	.964
-3	185.35	.26799	.976	.871	٠3	160.51	.20550	.151	.986
-4	184.77	.26664	27.060	.894	-4	160.08	.20435	.233	8.009
-5	184.20	2.26530	27.144	6.916	-5	159.66	2.20320	31.316	8.031
.6	183.63	.26395	.228	.938	.6	159.24	.20205	-399	.053
.7	183.07	.26262	.312	.960	.7	158.82	.20091	.482	.076
.8	182.51	.26128	.396	.983	.8	158.40	.19977	.565	.098
.9	181.40	.25996 2.25863	.480 27.564	7.005	.9	157.99 157.58	.19863	.648	.121
32.0	180.85	.25731	.648	7.027	37.0 .I		2.19749 .19636	.813	8.143
.I .2	180.30	.25731		.049	.1	157.17 156.76	.19523	.806	.188
.2	179.76	.25469	.731	.072	.2	156.35	.19523	.979	.210
.4	179.70	.25338	.899	.116	.4	155.95	.19411	32.061	.233
.5	178.68	2.25208	27.983	7.138	.5	155.55	2.10187	32.144	8.255
.6	178.15	.25078	28.067	.161	.6	155.15	.19076	.227	.277
.7	177.62	.24949	.150	.183	.7	154.75	.18964	.300	.300
.8	177.00	.24820	.234	.205	.8	154.36	.18854	.392	.322
.9	176.57	.24601	.318	.227	.9	153.97	.18743	.474	-345
33.0	176.05	2.24563	28.402	7.250	38.0	153.58	2.18633	32.557	8.367
.1	175.53	.24435	.485	.272	.1	153.19	.18523	.639	.390
.2	175.02	.24308	.569	.204	.2	152.80	.18413	.722	.412
-3	174.51	.24181	.652	.316	-3	152.42	.18304	.804	.434
.4	174.00	.24054	.736	.339	-4	152.04	.18195	.887	.457
-5	173.49	2.23928	28.820	7.361	.5	151.66	2.18086	32.969	8.479
.6	172.99	.23802	.903	.383	.6	151.28	.17978	33.051	.502
.7	172.49	.23677	.987	.406	.7	150.90	.17870	.134	.524
.8	172.00	.23552	29.070	.428	.8	150.53	.17762	.216	-547
.9	171.50	.23428	154	.450	.9	150.16	.17655	.298	.569
34.0	171.02	2.23303	29.237	7.473	39.0	149.79	2.17547	33.381	8.592
ı,	170.53	.23180	.321	·495	.I	149.42	.17441	.463	.614
.2	170.04	.23056	.404	.517	.2	149.05	.17334	-545	.636
-3	169.56	.22933	.487	-539	-3	148.69	.17228	.627	.659
-4	169.09	.22811	.571	.562	-4	148.33	.17122	.710	.681
-5	168.61	2.22688	29.654	7.584	-5	147.97	2.17016	33.792	8.704
.6	168.14	.22567	.737	.606	.6	147.61	.16911	.874	.726
.7	167.67	.22445	.821	.629	.7	147.25	.16805	.956	.749
.8	167.20	.22324	.904	.651	.8	146.89	.16701	34.038	.771
.9	166.74	.22203	.987	.673	.9	146.54	.16596	.120	.794
35.0	100.28	2.22083	30.071	7.696	40.0	146.19	2.16492	34.202	8.816

TABLE II. — TANGENT DISTANCES FOR A 1° CURVE FOR VARYING I's $T_D = T_{1^\circ}/D + C$ of Table III

	ı°	2°	3°	4°	5°	6°	7°	I
.00 0.00 5	0.00 I	00.01	150.04	200.08	250.16	300.28	350.44	.00
.02 1.00 5	I.00 I	01.01	151.04	201.08	251.16	301.28	351.44	.02
.04 2.00 5	2.00 I	02.01	152.04	202.09	252.17	302.28	352.45	.04
.06 3.00 5	3.00 I	03.01	153.04	203.09	253.17	303.29	353 - 45	.06
.08 4.00 5	4.00 I	04.01	154.04	204.09	254.17	304.29	354.46	.o8
		05.01	155.04	205.09	255.17	305.29	355.46	.10
.12 6.00 5	6.00	06.01	156.04	206.09	256.17	306.30	356.46	.12
		07.01	157.04	207.09	257.18	307.30	357 - 47	.14
		08.01	158.04	208.09	258.18	308.30	358.47	.16
		09.01	159.04	209.10	259.18	309.30	359.48	.18
		10.01	160.04	210.10	260.18	310.31	360.48	.20
		11.02	161.04	211.10	261.18	311.31	361.48	.22
		12.02	162.05	212.10	262.19	312.31	362.49	.24
-	-	13.02	163.05	213.10	263.19	313.32	363.49	.26
		14.02	164.05	214.10	264.19	314.32	364.50	.28
		15.02	165.05	215.10	265.19	315.32 316.32	365.50	.30
		1	166.05	1	266.19		366.50	.32
		17.02	167.05 168.05	217.11	267.20 268.20	317.33 318.33	367.51 368.51	.34 .36
.0-		19.02	169.05	219.11	269.20	319.33	369.52	.38
, <u> </u>		20.02	170.05	220.11	270.20	320.34	370.52	.40
		21.02	171.05	221.11	271.21	321.34	371.52	.42
		22.02	172.05	222.11	272.21	322.34	372.53	.44
121		23.02	173.05	223.12	273.21	323.35	373.53	.46
3 i i	-	24.02	174.06	224.12	274.21	324.35	374.54	.48
		25.02	175.06	225.12	275.21	325.35	375.54	50
		26.02	176.06	226.12	276.22	326.36	376.55	.52
	7.01 1	27.02	177.06	227.12	277.22	327.36	377 - 55	.54
		28.02	178.06	228.12	278.22	328.36	378.55	.56
.58 29.00 7	9.01 1	29.02	179.06	229.12	279.22	329.37	379.56	.58
.60 30.00 8	0.01	30.02	180.06	230.13	280.23	330.37	380.56	.60
.62 31.00 8	I.0I I	31.02	181.06	231.13	281.23	331.37	381.57	.62
	2.01 1	32.03	182.06	232.13	282.23	332.38	382.57	.64
.66 33.00 8	3.01	133.03	183.06	233.13	283.23	333.38	383.58	.66
.68 34.00 8	4.01	134.03	184.07	234.13	284.24	334.38	384.58	.68
	-	35.03	185.07	235.13	285.24	335.39	385 59	.70
1 1 1		136.03	186.07	236.14	286.24	336.39	386.59	.72
	1	137.03	187.07	237.14	287.24	337 - 39	387.59	74
		138.03	188.07	238.14	288.25	338.40	388.60	.76
		139.03	189.07	239.14	289.25	339.40	389.60	.78
		140.03	190.07	240.14	290.25	340.40	390.61	.80
		141.03	191.07	241.15	291.25	341.41	391.61	.82
4 4 1 1 1	- 1	142.03	192.07	242.15	292.26 293.26	342.41	392.62 393.62	.84 .86
		143.03	193.07	243.15 244.15	293.20	343.42 344.42	394.63	.88
		144.03	194.08	244.15	294.20	344.42	394.03	.90
		146.03	195.08	245.15	295.20	345.42	396.64	.92
	1	147.03	197.08	247.16	297.27	347.43	397.64	.94
		147.03	198.08	248.16	298.27	348.43	398.65	.96
		149.04	199.08	249.16	299.28	349.44	399.65	.98
	0.0I	150.04	200.08	250.16	300.28	350.44	400.66	1.00

TABLE II. — (Continued)

$\cdot I$	8°	9°	10°	110	12°	13°	14°	15°	I
.00	400.66	450.93	501.28	551.70	602.21	652.81	703.51	754.32	.00
.02	401.66	451.94	502.29	552.71	603.22	653.82	704.53	755.34	.02
.04	402.67	452.95	503.29	553.72	604.23	654.84	705.54	756.36	.04
.06	403.67	453.95	504.30	554.73	605.24	655.85	706.56	757.38	.06
.08	404.68	454.96	505.31	555.74	606.26	656.86	707.57	758.39	.08
.10	405.68	455.96	506.32	556.75	607.27	657.88	708.59	759.41	.10
.12	406.69	456.97	507.33	557.76	608.28	658.89	709.60	760.43	.12
.14	407.69	457.98	508.33	558.77	609.29	659.90	710.62	761.45	.14
.16	408.70	458.98	509.34	559.78	610.30	660.92	711.63	762.46	.16
.18	409.70	459.99	510.35	560.79	611.31	661.93	712.65	76,3.48	.18
.20	410.71	461.00	511.36	_561.80	612.32	662.94	713.67	764.50	.20
.22	411.71	462.00	512.37	562.81	613.33	663.96	714.68	765.52	.22
.24	412.72	463.01	513.37	563.82	614.35	664.97	715.70	766.53	.24
.26	413.72	464.02	514.38	564.83	615.36	665.98	716.71	767.55	.26
.28	414.73	465.02	515.39	565.84	616.37	667.00	717.73	768.57	.28
.30	415.73	466.03	516.40	566.85	617.38	668.01	718.74	769.59	.30
.32	416.74	467.04	517.41	567.86	618.39	669.02	719.76	770.61	.32
-34	417.74	468.04	518.41	568.87	619.40	670.04	720.78	771.62	-34
.36	418.75	469.05	519.42	569.88	620.42	671.05	721.79	772.64	.36
.38	419.75	470.06	520.43	570.89	621.43	672.07	722.81	773.66	.38
.40	420.76	471.06	521.44	571.90	622.44	673.08	723.82	774.68	.40
.42	421.76	472.07	522.45	572.91	623.45	674.09	724.84	775.70	.42
.44	422.77	473.08	523.46	573.92	624.46	675.11	725.86	776.72	-44
.46	423.78	474.08	524.46	574.93	625.47	676.12	726.87	777 - 73	.46
.48	424.78	475.09	525.47	575.94	626.49	677.13	727.89	778.75	.48
.50	425.79	476.10	526.48	576.95	627.50	678.15	728.90	779.77	.50
.52	426.79	477.10	527.49	577.96	628.51	679.16	729.92	780.79	.52
.54	427.80	478.11	528.50	578.97	629.52	680.18	730.94	781.81	-54
.56	428.80	479.12	529.51	579.98	630.54	681.19 682.21	731.95	782.83	.56 .58
.58	429.81	480.13	530.51	580.99	631.55		732.97	783.85	
.60	430.81	481.13	531.52	582.00	632.56	683.22	733.99	784.86	.60
.62	431.82	482.14	532.53	583.01	633.57	684.23	735.00	785.88	.62
.64 .66	432.83	483.15	533.54	584.02 585.03	634.58 635.60	685.25 686.26	736.02	786.90 787.92	.64 .66
	433.83	484.15	534.55			1	737.03		
.68 .70	434.84	485.16	535.56	586.04	636.61	687.28	738.05	788.94	.68
.70	435.84 436.85	486.17 487.18	536.57 537.57	587.05 588.06	637.62 638.63	688.29 689.31	739.07	789.96 790.98	.72
		488.18		1	}	1			
.74 .76	437.85 438.86	488.18	538.58 539.59	589.07 590.08	639.65	690.32	741.10 742.12	792.00	.74 .76
.78	439.87	490.20	540.60	591.09	641.67	692.35	743.13	794.04	.78
80	440.87	491.20	541.61	592, 10	642.68	693.36	744.15	795.05	.80
.82	441.88	492.21	542.62	593.11	643.70	694.38		796.07	82
.84	441.88	492.21	542.62	593.11	644.71	695.39	745.17 746.19	790.07	.84
.86	443.89	494.23	544.64	595.13	645.72	696.41	747.20	798.11	.86
.88	444.90	495.23	545.65	596.14	646.73	697.42	748.22	799.13	.88
.90	445.90	496.24	546.66	597.16	647.75	698.44	749.24	800.15	.90
.92	446.91	497.25	547.67	598.17	648.76	699.45	750.25	801.17	.92
.94	447.91	498.26	548.67	599.18	649.77	700.47	751.27	802.19	.94
.96	448.92	499.26	549.68	600.19	650.79	701.48	752.29	803.21	.96
.98	449.93	500.27	550.69	601.20	651.80	702.50	753.31	804.23	.98
1.00	450.93	501.28	551.70	602.21	652.81	703.51	754.32	805.25	1.00

I	16°	17°	18°	19°	20°	21°	22°	23°	I
.00	805.25	856.30	907.49	958.81	1010.29	1061.93	1113.73	1165.71	.00
.02	806.27	857.32	908.51	959.84	1011.32	1062.96	1114.77	1166.75	.02
.04	807.29	858.35	909.54	960.87	1012.35	1064.00	1115.81	1167.79	.04
.06	808.31	859.37	910.56	961.90	1013.39	1065.03	1116.85	1168.83	.06
.08	809.33	860.39	911.59	962.93	1014.42	1066.07	1117.88	1169.88	.08
.10	810.35	861.41	912.61	963.96	1015.45	1067.10	1118.92	1170.92 1171.96	.10
.12	811.37	862.44	913.64	964.98			1119.96		.12
.14	812.39	863.46 864.48	914.66	966.01	1017.51	1069.17	1121.00	1173.00	.14
.16 .18	813.41 814.43	865.51	915.69 916.72	967.04 968.07	1019.58	1070.21	1122.04	1174.04	.18
.20	815.45	866.53	917.74	969.10	1020.61	1072.27	1124.11	1176.13	.20
.22	816.47	867.55	918.77	970.13	1021.64	1073.31	1125.15	1177.17	.22
.24	817.49	868.57	919.79	971.16	1022.67	1074.35	1126.19	1178.21	24
.26	818.51	869.60	920.82	972.19	1023.70	1075.38	1127.23	1179.25	26
.28	819.53	870.62	921.84	973.21	1024.73	1076.42	1128.27	1180.30	.28
.30	820.55	871.64	922.87	974.24	1025.77	1077.45	1129.31	1181.34	.30
.32	821.57	872.67	923.90	975.27	1026.80	1078.49	1130.35	1182.38	.32
.34	822.59	873.69	924.92	976.30	1027.83	1079.52	1131.38	1183.43	-34
.36	823.61	874.71	925.95	977.33	1028.86	1080.56	1132.42	1184.47	.36
.38	824.63	875.74	926.97	978.36	1029.89	1081.59	1133.46	1185.51	.38
.40	825.66	876.76	928.00	979.39	1030.93	1082.63	1134.50	1186.55	.40
.42	826.68	877.78	929.03	980.42	1031.96	1083.66	1135.54	1187.60	.42
.44	827.70 828.72	878.81 879.83	930.05	981.45 982.48	1032.99	1084.70	1136.58	1188.64	.44
.46									l '
.48	829.74 830.76	880.85 881.88	932.11	983.50	1035.06	1086.77	1138.66	1190.73	.48
.50 .52	831.78	882.90	933.13 934.16	984.53 985.56	1030.09	1088.84	1139.70	1192.81	.52
-54	832.80	883.92	935.19	986.59	1038.16	1089.88	1141.78	1193.86	.54
56	833.82	884.95	935.19	987.62	1030.10	1090.92	1142.82	1194.90	56
.58	834.84	885.97	937.24	988.65	1040.22	1091.95	1143.86	1195.94	.58
.60	835.87	887.00	938.27	989.68	1041.25	1092.99	1144.90	1196.99	.60
.62	836.89	888.02	939.29	990.71	1042.29	1094.03	1145.94	1198.03	.62
.64	837.91	889.04	940.32	991.74	1043.32	1095.06	1146.98	1199.07	.64
.66	838.93	890.07	941.35	992.77	1044.35	1096.10	1148.02	1200.12	.66
.68	839.95	891.09	942.37	993.80	1045.39	1097.14	1149.06	1201.16	.68
.70	840.97	892.12	943.40	994.83	1046.42	1098.17	1150.10	1202.21	.70
.72	841.99	893.14	944.43	995.86	1047.45	1099.21	1151.14	1203.25	.72
-74	843.02	894.17	945.46	996.89	1048.49	1100.25	1152.18	1204.29	.74 .76
.76 .78	844.04 845.06	895.19 896.21	946.48 947.51	997.92 998.95	1049.52 1050.55	1101.28	1153.22	1205.34	.78
.80	846.08	897.24	947.51	990.93	1051.59	1103.36	1155.30	1207.43	.80
.82	847.10	898.26	949.57	1001.01	1052.62	1104.39	1156.34	1208.47	.82
.84	848.12	899.29	950.59	1002.04	1053.66	1104.39	1157.38	1209.52	.84
.86	849.15	900.31	951.62	1003.08	1054.69	1106.47	1158.42	1210.56	.86
.88	850.17	901.34	952.65	1004.11	1055.72	1107.51	1159.46	1211.60	.88
.90	851.19	902.36	953.68	1005.14	1056.76	1108.54	1160.50	1212.65	.90
.92	852.21	903.39	954.70	1006.17	1057.79	1109.58	1161.55	1213.69	.92
.94	853.24	904.41	955.73	1007.20	1058.83	1110.62	1162.59	1214.74	.94
.96	854.26	905.44	956.76	1008.23	1059.86	1111.66	1163.63	1215.78	.96
.98	855.28	906.46	957.79	1009.26	1060.89	1112.69	1164.67	1216.83	.98 1.00
1.00	856.30	907.49	958.81	1010.29	1061.93	1113.73	1165.71	1217.87	1.00

TABLE II. — (Continued)

I	24°	25°	26°	27°	28°	29°	30°	31 •	I
.00	1217.87	1270.23	1322.79	1375.57	1428.56	1481.79	1535.25	1588.97	.00
.02	1218.92	1271.28	1323.85	1376.62	1429.62	1482.86	1536.33	1590.05	.02
.04	1219.97	1272.33	1324.90	1377.68	1430.69	1483.92	1537.40	1591.13	.04
.06	1221.01	1273.38	1325.95	1378.74	1431.75	1484.99	1538.47	1592.20	.06
.08	1222.06	1274.43	1327.01	1379.80	1432.81	1486.06	1539.54	1593.28	.08
.10	1223.10	1275.48	1328.06	1380.86	1433.87	1487.12	1540.62	1594.36	.10
.12	1224.14	1276.53	1329.12	1381.91	1434.94	1488.19	1541.69	1595.44	.12
.14	1225.19	1277.58	1330.17	1382.97	1436.00	1489.26	1542.76	1596.51	.14
.16	1226.24	1278.63	1331.22	1384.03	1437.06	1490.33	1543.83	1597.59	.16
.18	1227.28	1279.68	1332.28	1385.09	1438.13	1491.39	1544.91	1598.67	.18
.20	1228.33	1280.73	1333.33	1386.15	1439.19	1492.46	1545.98	1599.75	.20
.22	1229.38	1281.78	1334.39	1387.21	1440.25	1493.53	1547.05	1600.82	.22
.24	1230.42	1282.83	1335.44	1388.27	1441.32	1494.60	1548.12	1601.90	.24
.26	1231.47	1283.88	1336.50	1389.32	1442.38	1495.67	1549.20	1602.98	.26
.28	1232.52	1284.93	1337.55	1390.38	1443.44	1496.73	1550.27	1604.06	.28
.30	1233.56	1285.98	1338.60	1391.44	1444.51	1497.80	1551.34	1605.14	.30
.32	1234.61	1287.03	1339.66	1392.50	1445.57	1498.87	1552.42	1606.22	.32
.34	1235.65	1288.08	1340.71	1393.56	1446.63	1499.94	1553.49	1607.30	.34
.36	1236.70	1289.13	1341.77	1394.62	1447.70	1501.01	1554.56	1608.37	.36
.38	1237.75	1290.18	1342.82	1395.68	1448.76	1502.08	1555.64	1609.45	.38
.40	1238.79	1291.23	1343.88	1396.74	1449.82	1503.15	1556.71	1610.53	.40
.42	1239.84	1292.28	1344.93	1397.80	1450.89	1504.21	1557.79	1611.61	.42
.44	1240.89	1293.33	1345.99	1398.86	1451.95	1505.28	1558.86	1612.69	.44
.46	1241.93	1294.39	1347.04	1399.92	1453.02	1506.35	1559.93	1613.77	.46
.48	1242.98	1295.44	1348.10	1400.98	1454.08	1507.42	1561.01	1614.85	.48
.50	1244.03	1296.49	1349.15	1402.04	1455.15	1508.49	1562.08	1615.93	.50
.52	1245.08	1297.54	1350.21	1403.10	1456.21	1509.56	1563.16	1617.01	.52
.54	1246.12	1298.59	1351.26	1404.16	1457.27	1510.63	1564.23	1618.09	-54
.56	1247.17	1299.64	1352.32	1405.22	1458.34	1511.70	1565.31	1619.17 1620.25	.56 .58
.58	1248.22	1300.69	1353.38	1406.28	1459.40	1512.77			.60
.60	1249.27	1301.74	1354.43	1407.34	1460.47	1513.84	1567.46	1621.33	1
.62	1250.31	1302.80	1355.49	1408.40	1461.53	1514.91	1568.53	1622.41	.62
.64 .66	1251.36 1252.41	1303.85	1356.54	1409.46	1463.66	1517.05	1570.68	1624.57	.66
								1625.65	.68
.68 .70	1253.46	1305.95	1358.66	1411.58	1464.73 1465.80	1518.12	1571.76	1626.73	.70
.70	1254.50	1308.06	1360.77	1413.70	1466.86	1520.26	1573.91	1627.81	.72
		1309.11	1361.83	1414.76	1467.93	1521.33	1574.98	1628.89	.74
.74 .76	1256.60 1257.65	1309.11	1362.88	1414.70	1467.93	1522.40	1576.06	1629.97	.76
.78	1258.70	1311.21	1363.94	1416.88	1470.06	1523.47	1577.13	1631.05	.78
.80	1259.75	1312.27	1365.00	1417.94	1471.12	1524.54	1578.21	1632.14	.80
.82	1260.79	1313.32	1366.05	1418.01	1472.19	1525.61	1579.28	1633.21	.82
.84	1261.84	1314.37	1367.11	1420.07	1473.26	1526.68	1580.36	1634.30	.84
.86	1262.89	1315.42	1368.17	1421.13	1474.32	1527.76	1581.44	1635.38	.86
.88	1263.94	1316.48	1369.22	1422.19	1475.39	1528.83	1582.51	1636.46	.88
.90	1264.99	1317.53	1370.28	1423.25	1476.45	1529.90	1583.59	1637.54	.90
.92	1266.04	1318.58	1371.34	1424.31	1477.52	1530.97	1584.67	1638.62	.92
.94	1267.09	1319.63	1372.39	1425.38	1478.59	1532.04	1585.74	1639.70	.94
.96	1268.14	1320.69	1373.45	1426.44	1479.66	1533.11	1586.82	1640.79	.96
.98	1269.18	1321.74	1374.51	1427.50	1480.72	1534.18	1587.90	1641.87	.98
1.00	1270.23	1322.79	1375.57	1428.56	1481.79	1535.25	1588.97	1642.95	1.00

TABLE II. — (Continued)

1642.95 1697.20 1751.73 1866.55 1861.68 1917.11 1972.88 202 1644.04 1698.29 1752.82 1807.65 1862.78 1918.23 1974.00 203 1646.20 1700.46 1755.01 1899.85 1864.99 1920.45 1975.11 203 1646.20 1700.46 1755.01 1899.85 1864.99 1920.45 1976.23 203 1646.20 1700.46 1757.20 1812.05 1867.21 1922.68 1978.73 203 1048.36 1702.64 1757.20 1812.05 1867.21 1922.68 1978.73 203 124 1650.53 1704.82 1759.39 1814.25 1869.85 1923.79 1979.59 203 1865.27 1706.99 1761.58 1815.35 1870.53 1926.01 1981.83 203 1818.165.270 1706.99 1761.58 1816.45 1871.63 1927.13 1982.95 203 1653.78 1708.08 1762.67 1818.65 1873.85 1929.35 1985.19 204 1655.03 1710.26 1764.86 1819.75 1874.95 1930.47 1986.31 204 1657.03 1711.35 1765.95 1820.85 1876.66 1931.58 1987.13 204 1659.20 1713.53 1768.14 1823.06 1878.27 1933.81 1989.95 204 2	9° I 8.98 .00 0.10 .02 1.23 .04 2.35 .06 3.48 .08 4.60 .10 5.73 .12 6.86 .14 7.98 .16
02 1644.04 1698.29 1752.82 1807.65 1862.78 1918.23 1974.00 202 .04 1645.12 1699.37 1753.92 1808.75 1864.89 1919.34 1975.11 203 .06 1646.20 1700.46 1755.01 1809.85 1864.99 1920.45 1976.23 203 .08 1647.28 1701.55 1756.10 1810.95 1866.10 1921.56 197.35 203 .10 1648.36 1702.64 1757.20 1812.05 1867.21 1922.68 1978.47 203 .12 1649.45 1703.73 1758.29 1813.15 1868.31 1923.79 1979.59 203 .14 1650.53 1704.82 1759.39 1814.25 1869.42 1924.90 1980.71 203 .20 1651.61 1705.91 1766.48 1815.35 1870.53 1927.13 1980.71 203 .20 1653.78 1708.98 1762.67 1817.55 1872.74	0.10 .02 .04 .04 .06 .06 .08 .10 .12 .12 .12 .12 .12 .13 .14 .16 .16 .16 .16 .16 .16 .16 .16 .16 .16
1645.12	1.23 .04 2.35 .06 3.48 .08 4.60 .10 5.73 .12 6.86 .14 7.98 .16
.06 1646.20 1700.46 1755.01 1809.85 1864.99 1920.45 1976.23 203 .08 1647.28 1701.55 1756.10 1810.95 1866.10 1921.56 1977.35 203 .10 1648.36 1702.64 1757.20 1812.05 1867.21 1922.68 1978.47 203 .12 1649.45 1703.73 1758.29 1813.15 1868.31 1923.79 1979.59 204 .14 1650.53 1704.82 1759.39 1814.25 1869.42 1924.90 1980.71 203 .16 1651.61 1705.91 1760.48 1815.35 1870.53 1926.01 1081.83 203 .18 1652.70 1706.99 1761.58 1816.45 1871.63 1927.13 1982.95 203 .20 1653.78 1708.08 1762.67 1817.55 1872.74 1928.24 1984.07 .21 1654.86 1709.17 1763.77 1818.65 1873.85 1929.35 1985.19 204 .22 1655.05 1710.26 1764.86 1819.75 1874.95 1930.47 1986.31 204 .26 1657.03 1711.35 1765.95 1820.85 1876.06 1931.58 1987.43 204 .28 1658.11 1712.44 1767.05 1821.96 1877.17 1932.69 1988.55 204 .30 1659.20 1713.53 1768.14 1823.36 1878.27 1933.81 1987.43 204 .30 1659.20 1713.53 1768.14 1823.36 1878.27 1933.81 1989.67 204 .32 1660.28 1714.62 1769.24 1824.16 1879.38 1934.92 1990.79 204 .34 1661.36 1715.71 1770.34 1825.26 1880.49 1936.04 1991.91 204 .35 1662.45 1716.80 1771.43 1826.36 1881.60 1937.15 1993.03 204 .40 1664.62 1718.98 1773.62 1828.56 1883.81 1939.38 1995.28 205 .42 1665.70 1720.07 1777.72 1829.67 1884.92 1940.49 1996.40 205 .44 1666.79 1721.16 1775.81 1830.77 1886.03 1941.61 1997.52 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	2.35 .06 3.48 .08 4.60 .10 5.73 .12 6.86 .14 7.98 .16
1647.28	3.48 .08 4.60 .10 5.73 .12 6.86 .14 7.98 .16
10	4.60 .10 5.73 .12 6.86 .14 7.98 .16
1.12 1649.45 1703.73 1758.29 1813.15 1868.31 1923.79 1979.59 203 1.14 1650.53 1704.82 1759.39 1814.25 1869.42 1924.90 1980.71 203 1.16 1651.61 1705.91 1760.48 1815.35 1870.53 1926.01 1981.83 203 2.00 1653.78 1708.08 1762.67 1817.55 1872.74 1928.24 1984.07 204 2.21 1654.86 1709.17 1763.77 1818.65 1873.85 1929.35 1985.19 204 2.24 1655.95 1710.26 1764.86 1819.75 1874.95 1930.47 1986.31 204 2.26 1657.03 1711.35 1765.95 1820.85 1876.06 1931.58 1987.43 204 2.28 1658.11 1712.44 1767.05 1821.96 1877.17 1932.69 1988.55 204 3.30 1659.20 1713.53 1768.14 1823.06 1878.27 1933.81 1989.67 204 3.34 1661.36 1715.71 1770.34 1825.26 1880.49 1936.04 1991.91 204 3.34 1661.35 1716.80 1771.43 1825.26 1880.49 1936.04 1991.91 204 3.36 1662.45 1716.80 1771.43 1825.26 1880.49 1936.04 1991.91 204 3.36 1662.53 1717.89 1772.53 1827.46 1882.71 1938.26 1994.15 205 3.38 1663.57 1720.07 1774.72 1829.67 1884.92 1990.49 1996.40 205 4.42 1665.76 1722.25 1776.91 1831.87 1881.14 1942.72 1998.64 205 4.48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	5.73 .12 6.86 .14 7.98 .16
16	7.98 .16
18 1652.70 1706.99 1761.58 1816.45 1871.63 1927.13 1982.95 203 204 204 1653.78 1708.08 1762.67 1817.55 1872.74 1928.24 1984.07 204 204 1655.95 1710.26 1764.86 1819.75 1874.95 1930.47 1985.19 204 205	
20 1653.78 1708.08 1762.67 1817.55 1872.74 1928.24 1984.07 204	
22 1654.86 1709.17 1763.77 1818.65 1873.85 1929.35 1985.19 204 24 1655.95 1710.26 1764.86 1819.75 1874.95 1930.47 1986.31 204 26 1657.03 1711.35 1765.95 1820.85 1876.06 1931.58 1987.43 204 28 1658.11 1712.44 1767.05 1821.96 1877.17 1932.69 1988.55 204 30 1659.20 1713.53 1768.14 1832.96 1878.27 1933.81 1989.67 204 32 1660.28 1714.62 1769.24 1824.16 1879.38 1934.92 1990.79 204 34 1661.36 1715.71 1770.31 1825.26 1880.49 1936.04 1991.91 204 38 1662.45 1716.80 1771.43 1825.26 1880.40 1937.15 1993.03 204 40 1664.62 1718.98 1772.53 1827.46 1882.71 <t< th=""><th>9.11 .18</th></t<>	9.11 .18
24 1655.95 1710.26 1764.86 1819.75 1874.95 1930.47 1986.31 204 26 1657.03 1711.35 1765.95 1820.85 1876.06 1931.58 1987.43 204 28 1658.11 1712.44 1767.05 1821.96 1877.17 1932.69 1988.55 204 30 1659.20 1713.53 1768.14 1823.06 1877.17 1933.81 1989.67 204 32 1660.28 1714.62 1769.21 1824.16 1879.38 1934.92 1990.79 204 34 1661.36 1715.71 1770.34 1825.26 1880.49 1936.04 1991.91 204 36 1662.45 1716.80 1771.43 1826.36 1881.60 1937.15 1993.03 204 40 1664.62 1718.98 1773.62 1828.56 1883.81 1939.38 1995.28 205 42 1666.79 1721.16 1775.81 1830.77 1884.92 <t< th=""><th>0.24 .20</th></t<>	0.24 .20
.26 1657.03 1711.35 1765.95 1820.85 1876.06 1931.58 1987.43 204 .28 1658.11 1712.44 1767.05 1821.96 1877.17 1932.69 1988.55 204 .30 1659.20 1713.53 1768.21 1823.06 1878.27 1933.81 1989.67 204 .32 1660.28 1714.62 1769.24 1824.16 1879.38 1934.92 1990.79 204 .34 1661.36 1715.71 1770.34 1825.26 1880.49 1936.04 1991.91 204 .36 1662.45 1716.80 1771.43 1826.36 1881.60 1937.15 1993.03 204 .38 1663.53 1717.89 1772.53 1827.46 1882.71 1938.26 1994.15 205 .40 1664.62 1718.98 1773.62 1829.67 1884.92 1990.49 1996.40 205 .42 1666.79 1721.16 1775.81 1830.77 1886.33	1.36 .22
.28 1658.11 1712.44 1767.05 1821.96 1877.17 1932.69 1988.55 204 .30 1659.20 1713.53 1768.14 1823.06 1878.27 1933.81 1989.67 204 .32 1660.28 1714.62 1769.24 1824.16 1879.38 1934.92 1990.79 204 .34 1661.36 1715.71 1770.34 1825.26 1880.49 1936.04 1991.91 204 .36 1662.45 1716.80 1771.43 1826.36 1881.60 1937.15 1993.03 204 .38 1663.53 1717.89 1772.53 1827.46 1882.71 1938.26 1994.15 205 .40 1664.62 1718.98 1773.62 1828.56 1883.81 1939.38 1995.28 205 .42 1665.70 1720.07 1774.72 1829.67 1884.92 1940.49 1996.40 205 .44 1666.99 1721.16 1775.81 1830.77 1886.03 1941.61 1997.52 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	2.49 .24
.30 1659.20 1713.53 1768.14 1823.06 1878.27 1933.81 1989.67 204 .32 1660.28 1714.62 1769.24 1824.16 1879.38 1934.92 1990.79 204 .34 1661.36 1715.71 1770.34 1825.26 1880.49 1936.04 1991.91 204 .36 1662.45 1716.80 1771.43 1826.36 1881.60 1937.15 1993.03 204 .38 1663.53 1717.89 1772.53 1827.46 1882.71 1938.26 1994.15 205 .40 1664.62 1718.98 1773.62 1829.67 1884.92 1990.49 1996.40 205 .42 1666.9 1721.16 1775.81 1830.77 1886.03 1941.61 1997.52 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25	
.32 1660. 28 1714. 62 1769. 24 1824. 16 1879. 38 1934. 92 1990. 79 204 .34 1661. 36 1715. 71 1770. 34 1825. 26 1880. 49 1936. 04 1991. 91 204 .36 1662. 45 1716. 80 1771. 43 1826. 36 1881. 60 1937. 15 1993. 03 204 .38 1663. 53 1717. 89 1772. 53 1827. 46 1882. 71 1938. 26 1991. 15 205 .40 1664. 62 1718. 98 1773. 62 1828. 56 1883. 81 1939. 38 1995. 28 205 .42 1665. 70 1720. 07 1774. 72 1829. 67 1884. 92 1940. 49 1996. 40 205 .44 1666. 79 1721. 16 1775. 81 1830. 77 1886. 03 1941. 61 1997. 52 205 .46 1667. 87 1722. 25 1776. 91 1831. 87 1887. 14 1942. 72 1998. 64 205 .48 1668. 96 1723. 34 1778.	4.74 .28
.34 1661.36 1715.71 1770.34 1825.26 1880.49 1936.04 1991.91 204 .36 1662.45 1716.80 1771.43 1826.36 1881.60 1937.15 1993.03 204 .38 1663.53 1717.89 1772.53 1827.46 1882.71 1938.26 1994.15 205 .40 1664.62 1718.98 1773.62 1828.56 1883.81 1939.38 1995.28 205 .42 1665.70 1720.07 1774.72 1829.67 1884.92 1940.49 1996.40 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	
.36 1662.45 1716.80 1771.43 1826.36 1881.60 1937.15 1993.03 204 .38 1663.53 1717.89 1772.53 1827.46 1882.71 1938.26 1994.15 205 .40 1664.62 1718.98 1773.62 1828.56 1883.81 1939.38 1995.28 205 .42 1665.70 1720.07 1774.72 1829.67 1884.92 1940.49 1996.40 205 .44 1666.79 1721.16 1775.81 1831.87 1887.14 1942.72 1998.64 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	
.38 1663.53 1717.89 1772.53 1827.46 1882.71 1938.26 1994.15 205 .40 1664.62 1718.98 1773.62 1828.56 1883.81 1939.38 1995.28 205 .42 1665.79 1720.07 1774.72 1829.67 1884.92 1940.49 1996.40 205 .44 1666.79 1721.16 1775.81 1830.77 1886.03 1941.61 1997.52 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	8.13 .34 9.26 .36
.40 1664.62 1718.98 1773.62 1828.56 1883.81 1939.38 1995.28 205 .42 1665.70 1720.07 1774.72 1829.67 1884.92 1940.49 1996.40 205 .44 1666.79 1721.16 1775.81 1830.77 1886.03 1941.61 1997.52 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	0.38 .38
.42 1665.70 1720.07 1774.72 1829.67 1884.92 1940.49 1996.40 205 .44 1666.79 1721.16 1775.81 1830.77 1886.03 1941.61 1997.52 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	1.51 .40
.44 1666.79 1721.16 1775.81 1830.77 1886.03 1941.61 1997.52 205 .46 1667.87 1722.25 1776.91 1831.87 1887.14 1942.72 1998.64 205 .48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	2.64 .42
.48 1668.96 1723.34 1778.00 1832.97 1888.25 1943.84 1999.76 205	3.77 .44
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	4.90 .46
FO 1670 04 1704 42 1770 70 1924 69 1990 26 1944 07 2000 99 200	6.03 .48
	7.15 . 50
	8.38 .52
	9.41 .54
	0.54 . 56 1.67 .58
	1.67 2.80 .60
17577. 17575 15575 155775 155775 155775	
200	3.93 .62 5.06 .64
	6.19 .66
.68 1679.81 1734.25 1788.98 1844.00 1899.34 1955.00 2010.99 206	7.32 .68
10. 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8.45 .70
	9.58 .72
	o.71 . 74
	1.84 .76
	2.97 .78
	1.10 .80
	5.24 .82
	5.37 .84 7.50 .86
	·
12 13 14 14 14 14 14 14 14 14 14 14 14 14 14	3.63 .88
	9.76 .90 9.89 .92
	2.03 .94
.96 1695.02 1749.54 1804.35 1859.46 1914.89 1970.64 2026.72 208	
1.00 1697.20 1751.73 1806.55 1861.68 1917.11 1972.88 2028.98 208	1.29 .98

TABLE II. — (Continued)

I	40°	41°	42°	43°	44°	45°	46°	47°	I
.00	2085.42	2142.23	2199.41	2256.97	2314.93	2373.30	2432.09	2491.32	.00
.02		2143.37	2200.55	2258.12	2316.09	2374.47	2433.27	2492.51	.02
.04		2144.51	2201.70	2259.28	2317.26	2375.64	2434 . 45	2493.70	.04
.06		2145.65	2202.85	2260.44	2318.42	2376.81	2435.63	2494.89	.06
.08		2146.79	2204.00	2261.59	2319.58	2377.99	2436.71	2496.08	.08
.10		2147.93	2205.15	2262.75	2320.75	2379.16	2438.00	2497.27	.10
.12	1	2149.07	2206.29	2263.90	2321.91	2380.33	2439.18	2198.46	.12
.14		2150.21	2207.44	2265.06	2323.08	2381.50	2440.36	2499.65	.14
.16		2151.35	2208.59	2266.22	2324.24	2382.68 2383.85	2441.54	2500.84	.16 .18
		2152.49	2209.74	2267.37	2325.40		2442.72	2502.03	
.20		2153.63	2210.89	2268.53	2326.57	2385.02	2443.90	2503.22	.20
.22	2097.89	2154.78	2212.04	2269.69	2327.73	2386.20	2445.08	2504.41	.22
.24 .26	2099.02	2155.92 2157.06	2213.19	2270.84	2328.90	2387.37 2388.54	2446.27	2505.60 2506.80	.24
	1		2214.33	2272.00	2330.06		2447.45	1	1
.28	2101.29	2158.20	2215.48	2273.16	2331.23	2389.72	2448.63	2507.99	.28
.30 .32	2102.43	2159.34	2217.78	2274.31 2275.47	2332.40	2390.89	2449.82 2451.00	2509.18 2510.37	.30
1									
.34 .36	2104.70	2161.63 2162.77	2218.93	2276.63	2334.73 2335.89	2393.24 2394.41	2452.18 2453.36	2511.56 2512.75	.34 .36
.38	2106.97	2163.91	2221.23	2278.95	2337.06	2395.59	2454.55	2513.95	.38
.40	2108.10	2165.05	2222.38	2280.10	2338.23	2396.76	2455 · 73	2515.14	.40
.42	2109.24	2166.20	2223.53	2281.26	2339.39	2397.94	2456.91	2516.33	1 1
44	2110.37	2167.34	2224.68	2282.42	2340.56	2399.11	2458.10	2517.53	.42
.46	2111.51	2168.48	2225.84	2283.58	2341.73	2400.29	2459.28	2518.72	.46
.48	2112.64	2169.63	2226.99	2284.74	2342.89	2401.47	2460.47	2519.91	.48
.50	2113.78	2170.77	2228.14	2285.90	2344.06	2402.64	2461.65	2521.11	.50
.52	2114.92	2171.91	2229.29	2287.06	2345.23	2403.82	2462.84	2522.30	.52
.54	2116.05	2173.06	2230.44	2288,22	2346.40	2404.99	2464.02	2523.49	.54
.56	2117.19	2174.20	2231.59	2289.38	2347.56	2406.17	2465.21	2524.69	.56
.58	2118.32	2175.34	2232.74	2290.54	2348.73	2407.35	2466.39	2525.88	.58
60	2119.46	2176.49	2233.90	2291.70	2349.90	2408.52	2467.58	2527.08	.60
.62	2120.60	2177.63	2235.05	2292.86	2351.07	2409.70	2468.76	2528.27	.62
.64	2121.74	2178.78	2236.20	2294.02	2352.24	2410.88	2469.95	2529.47	.64
.66	2122.87	2179.92	2237.35	2295.18	2353.41	2412.05	2471.13	2530.66	.66
.68	2124.01	2181.07	2238.51	2296.34	2354.58	2413.23	2472.32	2531.86	.68
.70	2125.15	2182.21	2239.66	2297.50	2355.74	2414.41	2473.51	2533.05	.70
.72	2126.29	2183.36	2240.81	2298.66	2356.91	2415.59	2474.69	2534.25	.72
.74	2127.42	2184.50	2241.97	2299.82	2358.08	2416.76	2475.88	2535.44	.74
.76	2128.56	2185.65	2243.12	2300,98	2359.25	2417.94	2477.07	2536.64	.76
.78	2129.70	2186.79	2244.27	2302.14	2360.42	2419.12	2478.25	2537.83	.78
.80	2130.84	2187.94	2245.43	2303.30	2361.59	2420.30	2479.44	2539.03	.80
.82	2131.98	2189.09	2246.58	2304.47	2362.76	2421.48	2480.63	2540.23	.82
.84	2133.11	2190.23	2247.73	2305.63	2363.93	2422.66	2481.82	2541.43	.84
.86	2134.25	2191.38	2248.89	2306.79	2365.10	2423.84	2483.00	2542.62	.86
.88	2135.39	2192.52	2250.04	2307.95	2366.27	2425.01	2484.19	2543.82	.88
.90	2136.53	2193.67	2251.20	2309.12	2367.44	2426.19	2485.38	2545.02	.90
.92	2137.67	2194.82	2252.35	2310.28	2368.61	2427.37	2486.57	2546.21	.92
.94	2138.81	2195.97	2253.50	2311.44	2369.78	2428.55	2487.76	2547.41	.94
.96 .98	2139.95	2197.11	2254.66	2312.60	2370.96	2429.73	2488.95	2548.61	.96
	2141.09	2198.26	2255.81	23 ^I 3.77	2372.13	2430.91	2490.13	2549.81	.98
1.00	2142.23	2199.41	2256.97	2314.93	2373.30	2432.09	2491.32	2551.00	1.00

TABLE II. — (Continued)

I	48°	49°	50°	51°	52°	53°	54°	55°	I
00	2551.00	2611.15	2671.78	2732.90	2794.54	2856.70	2919.40	2982.67	.00
.02	2552.20	2612.36	2672.99	2734.13	2795.77	2857.95	2920.66	2983.94	.02
.04	2553.40	2613.57	2674.21	2735.36	2797.0I	2859.20	2921.92	2985.21	.04
.06	2554.60	2614.78	2675.43	2736.59	2798.25	2860.44	2923.18	2986.48	.06
.08	2555.80	2615.98	2676.65	2737.81	2799.49	2861.69	2924.44	2987.75	.08
.10	2557.00	2617.19	2677.86	2739.04	2800.73	2862.94	2925.70	2989.02	.10
.12	2558.20	2618.40	2679.09	2740.27	2801.97	2864.19	2926.96	2990.30	.12
.14	2559.40	2619.61	2680.31	2741.50	2803.21	2865.44	2928.23	2991.57	.14
.16	2560.60	2620.82	2681.53	2742.73	2804.45	2866.69	2929.49	2992.84	.16
.18	2561.80	2622.03	2682.74	2743.96	2805.69	2867.94	2930.75	2994.12	.18
.20	2563.00	2623.24	2683.96	2745.19	2806.93	2869.20	2932.01	2995.39	.20
22	2564.20	2624.45	2685.18	2746.42	2808.17	2870.45	2933.27	2996.66	.22
.24	2565.40	2625.66	2686.40	2747.65	2809.41	2871.70	2934.53	2997.94	.24
.26	2566.60	2626.87	2687.62	2748.88	2810.65	2872.95	2935.80	2999.21	.26
28	2567.80	2628.08	2688.84	2750.11	2811.89	2874.20	2937.06	3000.48	28
.30	2569.00	2629.29	2690.06	2751.34	2813.13	2875.45	2938.32	3001.76	.30
.32	2570.20	2630.50	2691.28	2752.57	2814.37	2876.70	2939.59	3003.03	.32
-34	2571.40	2631.71	2692.50	2753.80	2815.61	2877.96	2940.85	3004.31	.34
.36	2572.60	2632.92	2693.73	2755.03	2816.85	2879.21	2942.11	3005.58	.36
.38	2573.80	2634.13	2694.95	2756.26	2818.10	2880.46	2943.38	3006.86	.38
.40	2575.0I	2635.34	2696.17	2757.49	2819.34	2881.71	2944.64	3008.13	.40
.42	2576.21	2636.56	2697.39	2758.73	2820.58	2882.97	2945.90	3009.41	.42
-44	2577.41	2637.77	2698.61	2759.96	2821.82	2884.22	2947.17	3010.68	-44
.46	2578.61	2638.99	2699.83	2761.19	2823.06	2885.47	2948.43	3011.96	.46
.48	2579.82	2640.19	2701.06	2762.42	2824.31	2886.73	2949.70	3013.24	.48
.50	2581.02	2641.40	2702.28	2763:65	2825.55	2887.98	2950.96	3014.51	.50
-52	2582.22	2642.62	2703.50	2764.89	2826.79	2889.24	2952.23	3015.79	.52
-54	2583.43	2643.83	2704.72	2766.12	2828.04	2890.49	2953.49	3017.07	-54
.56	2584.63	2645.04	2705.95	2767.35	2829.29	2891.74	2954.76	3018.35	.56
.58	2585.83	2646.26	2707.17	2768.59	2830.52	2893.00	2956.03	3019.62	.58
.60	2587.04	2647.47	2708.39	2769.82	2831.77	2894.26	2957.29	3020.90	.60
.62	2588.24	2648.68	2709.62	2771.05	2833.01	2895.51	2958.56	3022.18	.62
.64	2589.44	2649.90	2710.84	2772.29	2834.26	2896.77	2959.83	3023.46	.64
.66	2590.65	2651.11	2712.06	2773.52	2835.50	2898.02	2961.09	3024.74	.66
.68	2591.85	2652.33	2713.29	2774.76	2836.75	2899.28	2962.36	3026.02	.68
.70	2593.06	2653.54	2714.51	2775.99	2837.99	2900.53	2963.63	3027.29	.70
.72	2594.26	2654.76	2715.74	2777.23	2839.24	2901.79	2964.90	3028.57	.72
.74	2595 - 47	2655.97	2716.96	2778.46	2840.48	2903.05	2966.16	3029.85	.74
76	2596.67	2657.18	2718.19	2779.70	2841.73	2904.30	2967.43	3031.13	.76
.78	2597.88	2658.40	2719.41	2780.93	2842.98	2903.56	2968.70	3032.41	.78
.80	2599.08	2659.62	2720.64	2782.17	2844.22	2906.82	2969.97	3033.69	.80
.82	2600.29	2660.83	2721.86	2783.41	2845.47	2908.07	2971.24	3034.97	.82
.84 .86	2601.50	2662.05	2723.09	2784.64	2846.72	2909.33	2972.51	3036.25	.84
	2602.70	2663.26	2724.32	2785.88	2847.96	2910.59	2973.78	3037.54	
.88	2603.91	2664.48	2725.54	2787.11	2849.21	2911.85	2975.05	3038.82	.88
.90	2605.12	2665.69	2726.77	2788.35	2850.46	2913.11	2976.31	3040.10	.90
.92	2606.32	2666.91	2727.99	2789.59	2851.71	2914.37	2977.58	3041.38	.92
.94	2607.53	2668.13	2729.22	2790.82	2852.95	2915.63	2978.86	3042.66	.94
.96 .98	2608.74	2669.34	2730.45	2792.06	2854.20	2916.88	2980.13	3043.94	.96 .98
	2609.94	2670.56	2731.68	2793.30	2855.45	2918.14	2981.48	3045.23	
1.00	2611.15	2671.78	2732.90	2794.54	2856.70	2919.40	2982.67	3046.51	1.00

TABLE II. — (Continued)

I	56°	57°	58°	59°	60°	61°	62°	63°	I
.00									.00
	3046.51	3110.95	3176.00	3241.68	3308.01	3375.02	3442.72	3511.14	.00
.02	3047.79 3049.07	3112.24 3113.54	3178.61	3243.00 3244.32	3309.35 3310.38	3377.72	3444.08 3445.44	3513.88	.02
.06	3050.36	3114.83	3179.92	3245.64	3312.02	3379.06	3446.81	3415.26	.06
.08	3051.64	3116.13	3181.23	3246.96	3313.35	3380.41	3448.17	3516.64	.08
.10	3052.92	3117.42	3182.54	3248.28	3314.69	3381.76	3449.53	3518.02	.10
.12	3054.21	3118.72	3183.85	3249.61	3316.02	3383.11	3450.89	3519.39	.12
.14	3055.49	3120.02	3185.15	3250.93	3317.36	3384.46	3452.26	3520.77	.14
.16	3056.78	3121.31	3186.46	3252.25	3318.69	3385.81	3453.62	3522.15	.16
.18	3058.06	3122.61	3187.77	3253.57	3320.03	3387.16	3454.98	3523.53	.18
.20	3059.35	3123.91	3189.08	3254.89	3321.36	3388.51	3456.35	3524.90	.20
.22	3060.63	3125.20	3190.39	3256.22	3322.70	3389.85	3457.71	3526.28	.22
.24	3061.92	3126.50	3191.70	3257.54	3324.03	3391.21	3459.07	3527.66	.24
.26	3063.20	3127.80	3193.01	3258.86	3325.37	3392.56	3460.44	3529.04	.26
.28	3064.49	3129.10	3194.32	3260.19	3326.71	3393.91	3461.80	3530.42	.28
.30	3065.78	3130.40	3195.63	3261.51	3328.05	3395.26	3463.17	3531.80	.30
.32	3067.06	3131.69	3196.95	3262.83	3329.38	3396.61	3464.53	3533.18	.32
.34	3068.35	3132.99	3198.26	3264.16	3330.72	3397.97	3465.90	3534.56	34
.36	3069.64	3134.29	3199.57	3265.48	3332.06	3399.31	3467.27	3535.94	.36
.38	3070.92	3135.59	3200.88	3266.81	3333.40	3400.66	3468.63	3537 - 32	.38
.40	3072.21	3136.89	3202.19	3268.14	3334.74	3402.02	3470.00	3538.70	.40
.42	3073.50	3138.19	3203.51	3269.46	3336.08	3403.37	3471.37	3540.09	.42
.44 .46	3074.79 3076.08	3139.49 3140.79	3204.82 3206.13	3270.79 3272.11	3337.41 3338.75	3404.72 3406.08	3472.73 3474.10	3541.47 3542.85	.44
. 1									1
.48	3077.36	3142.09 3143.39	3207.44 3208.76	3273.44 3274.76	3340.09 3341.43	3407.43 3408.78	3475.47 3476.84	3544.23 3545.62	.48
.50 .52	3078.65 3079.94	3144.69	3210.07	3276.09	3342.77	3410.14	3478.20	3547.00	.50 .52
.54	3081.23	3146.00	3211.39	3277.42	3344.11	3411.49	3479.57	3548.38	
.56	3082.52	3147.30	3212.70	3278.75	3345.46	3412.85	3480.94	3549.76	.54 .56
.58	3083.81	3148.60	3214.01	3280.07	3346.80	3414.20	3482.31	3551.15	.58
.60	3085.10	3149.90	3215.33	3281.40	3348.14	3415.56	3483.68	3552.53	.60
.62	3086.39	3151.20	3216.64	3282.73	3349.48	3416.91	3485.05	3553.92	.62
.64	3087.68	3152.51	3217.96	3284.06	3350.82	3418,27	3486.42	3555.30	.64
.66	3088.97	3153.81	3219.27	3285.39	3352.16	3419.62	3487.79	3556.69	.66
.68	3090,26	3155.11	3220.59	3286.72	3353.51	3420.98	3489.16	3558.07	.68
.70	3091.55	3156.42	3221.91	3288.04	3354.85	3422.34	3490.53	3559.46	.70
.72	3092.84	3157.72	3223.22	3289.37	3356.19	3423.69	3491.90	3560.84	.72
.74	3094.13	3159.02	3224.54	3290.70	3357 - 53	3425.05	3493.27	3562.23	.74
.76	3095.43	3160.33	3225.86	3292.03	3358.88	3426.41	3494.65	3563.62	.76
.78	3096.72	3161.64	3227.17	3293.36	3360.22	3427.77	3496.02	3565.01	.78
.80	3098.01	3162.94	3228.49	3294.69	3361.57	3429.12	3497.39	3566.39	.80
.82	3099.30	3164.24	3229.81	3296.03	3362.91	3430.48	3498.77	3567.78	.82
.84 .86	31co.6o 31o1.89	3165.55 3166.85	3231.13 3232.45	3297.36 3298.69	3364.26 3365.60	3431.84	3500.14 3501.51	3569.17 3570.56	.84 .86
.88 .90	3103.18 3104.48	3168.16 3169.46	3233.76 3235.08	3300.02 3301.35	3366.94 3368.29	3434.57 3435.92	3502.89 3504.26	3571.95 3573.33	.88 .90
.92	3104.48	3170.77	3236.40	3302.68	3369.64	3437.28	3505.63	3574.72	.90
.94	3107.06	3172.08	3237.72	3304.02	3370.98	3438.64	3507.01	3576.11	.94
.96	3107.00	3172.08	3239.04	3305.35	3372.33	3440.00	3508.38	3577.50	.94
.98	3109.65	3174.69	3240.36	3306.68	3373.67	3441.36	3509.76	3578.89	.98
1.00	3110.95	3176.00	3241.68	3308.01	3375.02	3442.72	3511.14	3580.28	1.00

TABLE II. - (Continued)

I	64°	65°	66°	67°	68°	69°	70°	71°	I
.00	3580.28	3650.19	3720.88	3792.37	3864.70	3937.88	4011.94	4086.92	.00
.02	3581.67	3651.60	3722.30	3793.81	3866.15	3939 - 35	4013.43	4088.43	.02
.04	3583.06	3653.00	3723.72	3795.25	3867.61	3940.82	4014.93	4089.94	.02
.06	3584.46	3654.41	3725.15	3796.69	3869.06	3942.30	4016.42	4091.45	.06
.08	3585.85	3655.82	3726.57	3798.13	3870.52	3943.77	4017.91	4092.96	.08
.10	3587.24	3657.22	3727.99	3799.57	3871.98	3945.25	4019.40	4094.47	.10
.12	3588.63	3658.63	3729.41	3801.01	3873.43	3946.72	4020.89	4095.98	. 12
.14	3590.02	3660.04	3730.84	3802.45	3874.89	3948.19	4022.39	4097.49	.14
.16	3591.42	3661.45	3732.26	3803.89	3876.35	3949.67	4023.88	4099.00	.16
.18	3592.81	3662 86	3733.69	3805.33	3877.81	3951.15	4025.37	4100.51	.18
.20	3594.20	3664.26	3735.11	3806.77	3879.27	3952.62	4026.86	4102.03	.20
.22	3595.60	3665.67	3736.54	3808.21	3880.72	3954.10	4028.36	4103.54	.22
.24	3596.99	3667.08	3737.96	3809.65	3882.18	3955.57	4029.85	4105.05	.24
.26	3598.39	3668.49	3739 - 39	3811.10	3883.67	3957.05	4031.35	4106.57	.26
. 28	3599.78	3669.88	3740.81	3812.54	3885.10	3958.53	4032.84	4108.08	.28
.30	3601.17	3671.31	3742.24	3813.98	3886.56	3960.00	4034.34	4109.59	.30
.32	3602.57	3672.72	3743.67	3815.42	3888.02	3961.48	4035.84	4111.11	.32
.34	3603.96	3674.13	3745.09	3816.87	3889.48	3962.96	4037.33	4112.62	-34
.36	3605.36	3675.55	3746.52	3818.31	3890.94	3964.44	4038.83	4114.14	.36
.38	3606.76	3676.96	3747.95	3819.76	3892.40	3965.92	4040.33	4115.65	.38
.40	3608.15	3678.37	3749.38	3821.20	3893.87	3967.40	4041.82	4117.17	.40
.42	3609.55	3679.78	3750.81	3822.65	3895.33	3968.88	4043.32	4118.69	.42
.44	3610.95	3681.20	3752.24	3824.09	3896.79	3970.36	4044.82	4120.20	-44
.46	3612.34	3682.61	3753.66	3825.54	3898.25	3971.84	4046.32	4121.72	.46
.48	3613.74	3684.02	3755.09	3826.98	3899.73	3973.32	4047.82	4123.24	.48
.50	3615.14	3685.43	3756.52	3828.43	3901.18	3974.80	4049.32	4124.76	.50
. 52	3616.54	3686.85	3757.95	3829.88	3902.64	3976.28	4050.82	4126.28	.52
-54	3617.94	3688.26	3759.38	3831.32	3904.11	3977.76	4052.32	4127.80	.54
.56 .58	3619.34	3689.68	3760.81 3762.24	3832.77	3905.57	3979.24	4053.82	4129.31	.56
.60	3620.74	3691.09	3763.68	3834.22	3907.04	3980.73	4055.32	4130.83	.58 .60
	3622.14	3692.51		3835.67	3908.50	3982.21	4056.82	4132.35	1
.62 .64	3623.54	3693.92 3695.34	3765.11 3766.54	3837.12 3838.56	3909.97	3983.69 3985.18	4058.32 4059.82	4133.87	.62
.66	3624.93 3626.34	3696.76	3767.97	3840.01	3911.43	3986.66	4059.82	4136.92	.66
									1
.68 .70	3627.74 3629.14	3698.17 3699.59	3769.41 3770.84	3841.46 3842.91	3914.37 3915.83	3988.15 3989.63	4062.83	4138.44	.68
.70	3630.54	3701.01	3772.27	3844.36	3917.30	3991.12	4065.83	4141.48	.72
1	3631.94	3702.42	3773.71	3845.81	3918.77	3992.60	4067.34	4143.00	.74
.74	3633.34	3702.42	3775.14	3847.26	3920.24	3994.00	4068.84	4144.53	.76
.78	3634.74	3705.26	3776.57	3848.71	3921.70	3995.57	4070.34	4146.05	.78
.80	3636.15	3706.68	3778.01	3850.17	3923.17	3997.06	4071.85	4148.57	.80
.82	3637.55	3708.10	3779 - 44	3851.62	3924.64	3998.55	4073.36	4149.10	.82
.84	3638.95	3709.52	3780.88	3853.07	3926.11	4000.03	4074.86	4150.62	.84
.86	3640.36	3710.93	3782.31	3854.52	3927.58	4001.52	4076.37	4152.15	.86
.88	3641.76	3712.35	3783.75	3855.97	3929.05	4003.01	4077.87	4153.67	.88
.90	3643.16	3713.77	3785.19	3857.43	3930.68	4004.50	4079.38	4155.20	.90
.92	3644.57	3715.19	3786.62	3858.88	3931.99	4005.99	4080.89	4156.73	.92
. 94	3645.97	3716.61	3788.06	3860.33	3933.46	4007.48	4082.39	4158.25	.94
. 96	3647.38	3718.04	3789.50	3861.79	3934.94	4008.96	4083.90	4159.78	.96
. 98	3648.78	3719.46	3790.93	3863.24	3936.41	4010.45	4085.41	4161.31	. 98
1.00	3650.19	3720.88	3792.37	3864.70	3937.88	4011.94	4086.92	4162.83	1.00

TABLE II. — (Continued)

I	72°	73°	74°	75°	76°	77°	78°	I
.00	4162.83	4239.72	4317.60	4396.52	4476.50	4557.56	4639.78	.00
.02	4164.36	4241.27	4319.17	4398.11	4478.10	4559.20	4641.44	.02
.04	4165.89	4242.81	4320.74	4399.69	4479.72	4560.84	4643.09	.04
.06	4167.42	4244.36	4322.31	4401.28	4481.33	4562.47	4644.75	.06
.08	4168.95	4245.91	4323.88	4402.87	4482.94	4564.10	4646.41	.08
.10	4170.48	4247.46	4325.45	4404.46	4484.55	4565.74	4648.06	.10
.12	4172.01	4249.01	4327.02	4406.06	4486.16	4567.37	4649.72	. 12
.14	4173.54	4250.56	4328.59	4407.65	4487.78	4569.01	4651.38	.14
.16	4175.07	4252.11	4330.16	4409.24	4489.39	4570.65	4653.04	.16
. 18	4176.60	4253.66	4331.73	4410.83	4491.01	4572.28	4654.70	. 18
.20	4178.13	4255.21	4333.30	4412.42	4492.62	4573.92	4656.36	.20
.22	4179.66	4256.77	4334.87	4414.02	4494.23	4575.56	4658.02	.22
.24	4181.20	4258.32	4336.45	4415.63	4495.85	4577.19	4659.68	.24
.26	4182.73	4259.87	4338.02	4417.21	4497.47	4578.83	4661.34	.26
.28	4184.26	4261.42	4339.59	4418.80	4499.09	4580.47	4663.01	.28
.30	4185.80	4262.98	4340.97	4420.39	4500.70	4582.11	4664.67	.30
.32	4187.33	4264.53	4342.74	4421.99	4502.32	4583.75	4666.33	.32
.34	4188.87	4266.09	4344.32	4423.59	4503.94	4585.39	4668.00	.34
.36	4190.40	4267.64	4345.89	4425.18	4505.55	4587.03	4669.66	.36
.38	4191.93	4269.19	4347 - 47	4426.78	4507.17	4588.67	4671.32	.38
.40	4193.47	4270.85	4349.04	4428.38	4508.79	4590.31	4672.99	.40
.42	4195.01	4272.31	4350.62	4429.97	4510.41	4591.96	4674.65	.42
.44	4196.54	4273.86	4352.19	4431.57	4512.03	4593.60	4676.32	.44
.46	4198.08	4275.42	4353.77	4433.17	4513.65	4595.24	4677.99	.46
.48	4199.62	4276.98	4355.35	4434.77	4515.27	4596.89	4679.65	.48
.50	4201.15	4278.53	4356.93	4436.37	4516.89	4598.53	4681.32	.50
.52	4202.69	4280.09	4358.51	4437.97	4518.51	4600.18	4682.99	.52
-54	4204.23	4281.65	4360.08	4439.57	4520.14	4601.82	4684.66	.54
. 56	4205.77	4283.21	4361.66	4441.17	4521.76	4603.47	4686.32	.56
. 58	4207.31	4284.77	4363.24	4442.77	4523.38	4605.19	4687.99	.58
.60	4208.85	4286.33	4364.81	4444.37	4525.01	4606.76	4689.67	.60
.62	4210.39	4287.89	4366.40	4445.97	4526.63	4608.40	4691.33	.62
.64	4211.93	4289.45	4367.98	4447.58	4528.25	4610.05	4693.00	.64
.66	4213.47	4291.01	4369.56	4449.18	4529.88	4611.70	4694.68	.66
.68	4215.01	4292.57	4371.15	4450.78	4531.50	4613.35	4696.35	.68
.70	4216.55	4294.13	4372.73	4452.39	4533.13	4614.99	4698.02	.70
.72	4218.09	4295.69	4374.31	4453.99	4534.76	4616.64	4699.69	.72
.74	4219.63	4297.25	4375.90	4455.59	4536.38	4618.29	4701.37	.74
.76	4221.18	4298.82	4377.48	4457.20	4538.01	4619.94	4703.04	.76
.78	4222.72	4300.38	4379.06	4458.81	4539.64	4621.59	4704.71	.78
.80	4224.26	4301.94	4380.65	4460.41	4541.27	4623.24	4706.39	.80
.82	4225.81	4303.51	4382.23	4462.02	4542.89	4624.90	4708.06	.82
.84	4227.35	4305.07	4383.82	4463.62	4544.52	4626.55	4709.74	.84
.86	4228.90	4306.64	4385.40	4465.23	4546.15	4628.20	4711.41	.86
.88	4230.44	4308.20	4386.99	4466.84	4547.78	4629.85	4713.09	.88
.90	4231.98	4309.77	4388.58	4468.45	4549.41	4631.51	4714.77	.90
.92	4233.53	4311.33	4390.16	4470.05	4551.04	4633.16	4716.45	.92
.94	4235.08	4312.90	4391.75	4471.66	4552.67	4634.81	4718.12	.94
.96	423 6 .62	4314.46	4393.34	4473.27	4554.31	4636.47	4719.80	.96
.98	4238.17	4316.03	4394.93	4474.88	4555.94	4638.12	4721.48	.98
1.00	4239.72	4317.60	4396.52	4476.50	4557.56	4639.78	4723.16	1.00

TABLE II. — (Continued)

I	79°	80°	81°	82°	83°	84°	85°	I
.00	4723.16	4807.85	4893.58	4980.71	5069.17	5159.00	5250.26	.00
.02	4724.84	4809.45	4895.31	4982.47	5070.95	5160.80	5252.10	.02
.04	4726.52	4811.16	4897.04	4984.22	5072.73	5162.62	5253.94	.04
.06	4728.20	4812.86	4898.78	4985.98	5074.52	5164.43	5255.78	.06
.08	4729.88	4814.57	4900.51	4987.74	5076.30	5166.25	5257.62	.08
.10	4731.56	4816.27	4902.24	4989.49	5078.09	5168.06	5259.46	.10
. 12	4733.25	4817.98	4903.97	4991.25	5079.87	5169.88	5261.30	. 12
.14	4734.93	4819.69	4905.70	4993.01	5081.66	5171.69	5263.15	.14
.16	4736.61	4821.40	4907.44	4994.77	5083.45	5173.50	5264.99	. 16
.18	4738.29	4823.10	4909.17	4996.53	5085.23	5175.32	5266.84	. 18
.20	4739.98	4824.81	4910.90	4998.29	5087.02	5177.14	5268.68	.20
.22	4741.66	4826.52	4912.64	5000.05	5088.81	5178.95	5270.53	.22
.24	4743.35	4828.23	4914.37	5001.82	5090.60	5180.77	5272.38	.24
.26	4745.03	4829.94	4916.11	5003.58	5092.39	5182.59	5274.22	.26
.28	4746.72	4831.65	4917.83	5005.34	5094.18	5184.41	5276.07	.28
.30	4748.41	4833.36	4919.58	5007.10	5095.97	5186.23	5277.92	.30
.32	4750.09	4835.08	4921.32	5008.87	5097.76	5188.05	5279.77	.32
-34	4751.78	4836.79	4923.06	5010.63	5099.55	5189.87	5281.62	.34
. 36	4753 - 47	4838.50	4924.80	5012.40	5101.34	5191.69	5283.47	.36
.38	4755.16	4840.22	4926.54	5014.16	5103.14	5193.51	5285.32	.38
.40	4756.85	4841.93	4928.28	5015.93	5104.93	5195.33	5287.17	.40
.42	4758.54	4843.64	4930.02	5017.70	5106.73	5197.15	5289.02	.42
.44	4760.23	4845.36	4931.76	5019.46	5108.52	5198.98	5290.87	.44
.46	4761.92	4847.08	4933.50	5021.23	5110.32	5200.80	5292.73	.46
.48	4763.61	4848.79	4935.24	5023.00	5112.11	5202.62	5294.58	.48
.50	4765.30	4850.51	4936.98	5024.77	5113.91	5204.45	5296.42	.50
. 52	4766.99	4852.22	4938.73	5026.5.1	5115.70	5206.27	5298.29	-52
.54	4768.69	4853.94	4940.47	5028.31	5117.50	5208.10	5300.13	.54
.56	4770.38	4855.66	4942.21	5030.08	5119.30	5209.93	5302.00	.56
. 58	4772.07	4857.38	4943.96	5031.85	5121.10	5211.75	5303.86	.60
.60	4773.76	4859.10	4945.70	5033.62	5122.90	5213.58	5305.71	•
.62	4775.46	4860.82	4947 - 45	5035.39	5124.70	5215.41	5307.57	.62
.64 .66	4777.15	4862.54	4949.19	5037.17 5038.94	5126.50 5128.30	5217.24 5219.07	5309.43 5311.29	.66
	4778.85	4864.26	4950.94					1
.68	4780.55	4865.98	4952.68	5040.71	5130.10	5220.90	5313.15	.68
.70 .72	4782.24	4867.70 4869.42	4954.43 4956.18	5042.49 5044.26	5131.90 5133.70	5222.73 5224.56	5315.01 5316.87	.72
	4783.94					5226.39	5318.73	74
.74 .76	4785.64	4871.14 4872.87	4957 · 93 4959 · 68	5046.04 5047.81	5135.51 5137.31	5228.22	5310.73	.76
.78	4787.33 4789.03	4874.59	4961.63	5049.59	5139.12	5230.06	5322.46	.78
.80		4876.31	4963.18	5051.37	5140.92	5231.89	5324.32	.80
	4790.73		4964.93	5053.14	5142.73	5233.72	5326.18	.82
.82 .84	4792.43 4794.13	4878.04 4879.76	4966.68	5053.14	5142.73	5235.72	5328.05	.84
.86	4794.13	4881.49	4968.43	5056.70	5146.34	5237.39	5329.91	.86
.88	4797.53	4883.22	4970.18	5058.48	5148.15	5239.23	5331.78	.88
.90	4797 - 53	4884.94	4975.16	5060.26	5149.95	5241.07	5333.65	.90
.92	4800.93	4886.67	4973.69	5062.04	5151.76	5242.90	5335.51	.92
	4802.64	4888.40	4975.44	5063.82	5153.57	5244.74	5337.38	.94
.94 .96	4804.34	4890.13	4973.44	5065.60	5155.38	5246.58	5339.25	.96
.98	4806.04	4891.85	4978.95	5067.38	5157.19	5248.42	5341.12	.98
1.00	4807.85	4893.58	4980.71	5069.17	5159.00	5250.26	5342.99	1.00

TABLE II. — (Continued)

I	86°	87°	88°	8 9°	90°	91°	92°	I
.00	5342.99	5437.24	5533.06	5630.51	5729.65	5830.53	5933.23	.00
.02	5344.85	5439.14	5534.99	5632.48	5731.65	5832.57	5935 - 30	.02
.04	5346.73	5441.04	5536.92	5634.44	5733.65	5834.61	5937 - 37	.04
.06	5348.60	5442.94	5538.86	5636.41	5735.65	5836.64	5939 - 45	.06
.08	5350.46	5444.84	5540.79	5638.38	5737.65	5838.68	5941.52	. 08
.10 .12	5352.34	5446.75 5448.65	5542.73 5544.67	5640.35 5642.32	5739.66 5741.66	5840.72 5842.76	5943.60	.IO .I2
	5354.21							
.14	5356.09 5357.96	5450.55 5452.46	5546.60 5548.54	5644.29 5646.26	5743.67 5745.67	5844.80 5846.84	5947.75 5949.83	.14
.18	5357.90	5454.37	5550.48	5648.23	5747.68	5848.88	5951.91	.18
.20	5361.71	5456.27	5552.42	5650.20	5749.69	5850.93	5953.99	.20
.22	5363.59	5458.18	5554.36	5652.18	5751.69	5852.97	5956.07	.22
.24	5365.46	5460.09	5556.30	5654.15	5753.70	5855.01	5958.15	.24
.26	5367.34	5462.00	5558.24	5656.12	5755.71	5857.05	5960.23	.26
.28	5369.22	5463.91	5560.18	5658.10	5757.72	5859.10	5962.31	.28
.30	5371.10	5465.81	5562.12	5660.07	5759.73	5861.15	5964.40	.30
.32	5372.98	5467.72	5564.06	5662.05	5761.74	5863.20	5966.48	.32
.34	5374.86	5469.64	5566.0I	5664.03	5763.75	5865.24	5968.56	.34
.36	5376.74	5471.55	5567.95	5666.00	5765.76	5867.29	5970.65	.36
.38	5378.62	5473.46	5569.90	5667.98	5767.78	5869.34	5972.74	.38
.40	5380.50	5475.37	5571.84	5669.96	5769.79	5871.38	5974.82	.40
.42	5382.38	5474.29	5573.79	5671.94	5771.80	5873.44	5976.91	.42
-44	5384.26	5479.20	5575.73	5673.92	5773.82	5875.49	5979.00	.44
.46	5386.15	5481.12	5577.68	5675.90	5775.84	5877.54	5981.09	.46
.48	5388.03	5483.03	5579.63	5677.88	5777.85	5879.60	5983.18	.48
.50 .52	5389.92 5391.80	5484.95 5486.86	5581.58 5583.53	5679.87 5681.85	5779.87 5781.89	5881.65 5883.71	5985.27 5987.36	.50 .52
		5488.78	5585.48	5683.83				
.54 .56	5393.69 5395.57	5490.70	5587.43	5085.82	5783.91 5785.93	5885.76 5887.82	5989.46 5991.55	.54 .56
.58	5397.46	5492.62	5589.38	5687.80	5787.95	5889.87	5993.64	.58
.60	5399.35	5494.54	5591.33	5689.79	5789.97	5891.93	5995.74	.60
.62	5401.24	5496.46	5593.29	5691.78	5791.99	5893.98	5997.83	.62
.64	5403.13	5498.38	5595.24	5693.76	5794.01	5896.05	5999.93	.64
.66	5405.02	5500.30	5597.19	5695.75	5796.03	5898.10	6002.02	.66
.68	5406.91	5502.22	5599.15	5697.74	5798.06	5900.16	6004.12	.68
.70	5408.80	5504.14	5601.10	5699.73	5800.08	5902.23	6006.22	.70
.72	5410.69	5506.07	5603.06	5701.72	5802.11	5904.29	6008.32	.72
74	5412.58	5507.99	5605.01	5703.71	5804.13	5906.35	6010.42	.74
.76 .78	5414.47	5509.92 5511.84	5606.97 5608.93	5705.70	5806.16	5908.41	6012.52	.76 .78
.80	5416.37			5707.69	5808.19	5910.48	6014.62	.78
.82	5418.26	5513.77	5610.89	5709.68	5810.21	5912.54	6016.72	.82
.82 .84	5420.16 5422.05	5515.69 5517.62	5612.85 5614.81	5711.68 5713.67	5812.24 5814.27	5914.61 5916.67	6018.83 6020.93	.82
.86	5423.95	5519.55	5616.77	5715.67	5816.30	5918.74	6023.04	.86
.88	5425.84	5521.48	5618.73	5717.66	5818.33	5920.81	6025.14	.88
.90	5427.74	5523.40	5620.69	5719.66	5820.37	5922.87	6027.25	.90
.92	5429.64	5525.33	5622.65	5721.65	5822.40	5924.94	6029.35	.92
.94	5431.54	5527.26	5624.62	5723.65	5824.43	5927.01	6031.46	.94
.96	5433.44	5529.19	5626.58	5725.65	5826.47	5929.08	6033.57	.96
.98	_5435.34	5531.13	5628.55	5727.65	5828.50	5931.15	6035.68	.98
1.00	5437.24	5533.06	5630.51	5729.65	5830.53	5933.23	6037.79	1.00

TABLE II. — (Continued)

I	93°	94°	95°	96°	97°	98°	99°	I
.00	6037.79	6144.30	6252.82	6363.42	6476.19	6591.21	6708.56	.00
.02	6039.90	6146.45	6255.01	6365.66	6478.47	6593.53	6710.93	.02
.04	6042.01	6148.60	6257.20	6367.89	6480.75	6595.86	6713.30	.04
.06	6041.12	6150.75	6259.39	6370.13	6483.03	6598.18	6715.67	.06
.08 .10	6046.25 6048.35	6152.90 6155.06	6261.59 6263.78	6372.36 6374.60	6485.31 6487.59	6600.51 6602.84	6718.05	.08
.10	6050.47	6157.21	6265.98	6376.84	6489.87	6605.16	6722.80	.10
.14	6052.58	6159.37	6268.16	6379.08	6492.16	6607.49	6725.18	.14
.16	6054.70	6161.52	6270.37	6381.32	6494.44	6609.83	6727.56	.16
.18	6056.82	6163.68	6272.57	6383.56	6496.73	6612.16	6729.93	.18
.20	6058.96	6165.84	6274.77	6385.80	6499.01	6614.49	6732.32	.20
.22	6061.05	6168.00	6276.97	6388.04	6501.30	6616.82	6734.70	.22
.24	6063.17	6170.15	6279.17	6390.29	6503.59	6619.17	6737.08	.24
.26	6065.29	6172.32	6281.37	6392.53	6505.88	6621.49	6739.46	.26
.28	6067.42	6174.48	6283.57	6394.77	6508.17	6623.83	6741.85	.28
.30 .32	6069.55 6071.66	6176.64 6178.80	6285.78 6287.98	6397.02 6399.27	6510.46 6512.75	6626.16 6628.50	6744.23 6746.62	.30
		6180.96						1
·34 ·36	6073.78 6075.91	6183.13	6290.18 6292.39	6401.52 6403.76	6515.04	6630.84 6633.18	6749.∞ 6751.39	.34 .36
.38	6078.03	6185.29	6294.60	6406.01	6519.63	6635.52	6753.78	.38
.40	6080.16	6187.46	6296.80	6408.26	6521.92	6637.86	6756.17	.40
.42	6082.28	6189.63	6299.01	6410.52	6524.22	6640.21	6758.56	.42
-44	6084.41	6191.79	6301.22	6412.77	6526.62	6642.55	6760.96	.44
.46	6086.54	6193.96	6303.43	6415.02	6528.81	6644.90	6763.35	.46
.48	6088.67	6196.13	6305.64	6417.28	6531.11	6647.24	6765.74	.48
.50	6090.80	6198.30	6307.85	6419.53	6533.41	6649.59	6768.14	.50
.52	6092.93	6200.47	6310.07	6421.79	6535.71	6651.93	6770.53	.52
·54 ·56	6095.06 6097.19	6202.64 6204.81	6312.28 6314.49	6424.04 6426.30	6538.02	6654.28 6656.63	6772.93	.54 .56
.58	6099.32	6206.99	6316.71	6428.56	6542.62	6658.98	6777.73	.58
.60	6101.46	6209.16	6318.92	6430.82	6544.93	6661.33	6780.12	.60
.62	6103.59	6211.34	6321.14	6433.08	6547.23	6663.69	6782.53	.62
.64	6105.73	6213.51	6323.36	6435.34	6549.54	6666.04	6784.93	.64
.66	6107.86	6215.69	6325.58	6437.60	6551.85	6668.39	6787.33	.66
.68	6110.00	6217.87	6327.80	6439.86	6554.15	6670.75	6789.73	.68
.70	6112.14	6220.04	6330.02	6442.13	6556.46	6673.10	6792.14	.70
.72	6114.28	6222.22	6332.24	6444.39	6558.77	6675.46	6794.55	.72
.74 .76	6116.42 6118.55	6224.40 6226.58	6334.46 6336.68	6446.66 6448.93	6561.08 6563.39	6677.82 6680.18	6796.95 6799.36	.74 .76
.70	6120.70	6228.77	6338.90	6451.19	6565.71	6682.54	6801.77	.78
.80	6122.84	6230.95	6341.13	6453.46	6568.02	6684.90	6804.18	.80
.82	6124.98	6233.13	6343.35	6455.73	6570.34	6687.26	6806.59	.82
.84	6127.12	6235.31	6345.58	6458.00	6572.65	6689.62	6809.00	.84
.86	6129.27	6237.50	6347.81	6460.27	6574.97	6691.99	6811.41	.86
.88	6131.42	6239.69	6350.04	6462.54	6577.29	6694.35	6813.83	.88
.90	6133.56	6241.87	6352.26	6464.81	6579.60	6696.72	6816.24	.90
.92	6135.70	6244.06	6354.49	6467.09	6581.92	6699.08	6818.66	.92
.94	6137.85	6246.25	6356.72	6469.36	6584.24	6701.45	6821.07	.94
.96 .98	6140.00 6142.15	6248.44 6250.63	6358.96 6361.19	6471.64 64 73.91	6586.56 6588.89	6703.82 6706.19	6823.49 6825.91	.96 .98
1.00	6144.30	6252.82	6363.42	6476.19	6591.21	6708.56	6828.33	1.00
1.00	0144.30	0252.02	0303.42	04/0.19	0591.21	0700.50	0020.33	1.00

TABLE III. — TANGENT DISTANCE CORRECTIONS $T_D = T_1 \circ / D + \text{tabular correction}$

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I D	2°	4°	6°	8°	10°	12°	14°	16°	18°	20°	D_I
ů	0.00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.01	0.01	i
2	.00	.00	.01	.01	.01	.02	.02	.02	.02	.03	2
4	.00	.01	.01	.02	.03	.03	.04	.04	. 05	.05	4
6	.01	.01	.02	.03	.04	. 05	.05	.06	.07	.08	6
8	.01	.02	.03	. 0.1	.05	.06	.07	.08	.09	.10	8
10	0.01	0.02	0.04	0.05	0.06	0.08	0.09	0.10	0.11	0.13	10
12	.01	.03	.04	.06	.08	.09	.II	.12	.14	.15	12
14	.01	.03	.05	.07	.09	.II	.13	14	.16	.18	14
16	.02	04	.06	.08	.10	.12	.14	.16	.18	.20	16
18	.02	.04	.07	.09	.II	.14	.16	. 18	.21	.23	18
20	0.02	0.05	0.07	0.10	0.13	0.15	0.18	0.21	0.23	0.26	20
22	.02	.05	.08	.II	.14	.17	.20	. 23	. 25	. 29	22
24	.02	.06	.09	.12	.15	.18	,22	. 25	. 28	.31	24
26	.03	.06	.10	.13	.17	.20	.24	. 27	.30	.34	26
28	.03	.07	.11	.14	. 18	.22	.25	.29	-33	.36	28
30	0.03	0.07	0.11	0.15	0.19	0,23	0.27	0.31	0.35	0.39	30
32	.03	.08	.12	.16	.21	.25	.29	.33	.38	.42	32
34	.03	.08	.13	.18	. 22	. 27	.31	.36	.40	. 45	34
36	.04	.09	.14	.19	.23	.28	-33	. 38	.43	-47	36
38	.04	.09	15	. 20	. 25		- 35	.40	- 45	.50	38
40	0.04	0.10	0.15	0.21	0.26	0.32	0.37	0.42	0.47	0.53	40
42	.04	.10	.16	.22	.28	.33	.39	.45	.50	. 56	42
44	.04	.II	.17	.23	.29	-35	.41	.47	.53	.59	44
46	.05	.12	.18	.24	.31	.37	.43	.49	.56	.62	46
48	.05	.12	.19	. 26	.32	. 39	-45	.52	.59	.65	48
50	0.05	0.13	0.20	0.27	0.34	0.40	0.47	0.54	0.61	0.68	50
52	.05	.13	.21	.28	.35	.42	.50	-57	.64	.71	52
54	.06	.14	.22	.29	.37	.44	.52	.62	.67	.74	54
56 58	,06	.15	.23	.30	.38	.48	.54 .56	.64	.70	.77	56 58
60	0.06	0.16	0.24	0.33	0.42	0.50	0.58	0.67	0.75	0.84	60
62	.07	16	-25	-34		.52	61	.70	.79	.87	62
64	.07	.17	.23	.36	.43 .45	.54	.64	.73	.82	.91	64
66	.07	.18	,28	.37	.47	.56	.66	.75	.85	.95	66
68	.07	.18	.29	.39	.49	.59	.69	.78	.88	.98	68
70	0.08	0.19	0.30	0.40	0.50	0.61	0.71	0.81	0.91	1.02	70
72	.08	.20	.31	.42	.52	.63	.74	.84	.95	1.06	72
74	.08	,21	.32	.43	.54	.65	.77	.87	.99	1.10	74
76	.09	.21	.33	.45	.56	.68	.79	.91	1.02	1.14	76
78	.09	.22	.34	.46	.58	.70	.82	-94	1.06	1.18	78
80	0.09	0.23	0.36	0.48	0.60	0.73	0.84	0.97	1.10	I.22	80
82	.09	.24	.37	.50	.63	.75	.88	1.01	1.14	1.27	82
84	.10	. 25	. 38	.52	.65	.78	.91	1.05	1.18	1.31	84
86	.10	.25	.40	-53	.67	.81	.95	1.08	1.22	1.36	86
88	.11	.26	.41	-55	.70	.84	.98	1.12	1.26	1.41	88
90	0.11	0.27	0.42	0.57	0.72	0.87	1.02	1.16	1.31	1.45	90
92	.11	.28	-44	-59	.75	.90	1.05	1.20	1.36	1.50	92
94	.12	. 29	.46	.61	.77	.93	1.09	1.24	1.40	1.56	94
96	.12	.30	-47	.64	.80	.96	1.13	1.29	1.45	1.62	96
98	.13	.31	.49	.66	.83	1.00	1.17	1.34	1.51	1.68	98
100	0.13	0.33	0.51	0.68	0.86	1.03	1.21	1.38	1.56	1.74	100

TABLE IV. — External Distances for a 1° Curve $E_D = E_{1^{\rm o}}/D \ ({\rm approx.})$

I	o°	10°	20°	30°	40°	50°	60°	70°	8o°	90°
.0	.0	21.9	88.4	202.I	367.7	592.3	886.4	1265.0	1749.9	2373.3
.a	.0	22.8	90.2	04.9	71.6	97.5	93.I	73.5	60.9	87.5
.4	.0	23.7	92.0	07.7	75.5	602.7	99.8	82.1	71.9	2401.8
.6	.I	24.6	93.8	10.5	79.4	07.9	906.5	90.8	83.0	16.1
.8	.I	25.5	95.7	13.4	83.4	13.1	13.3	99.5	94.1	30.5
1.0	.2	26.5	97.6	216.2	387.4	618.4	920.1	1308.2	1805.3	2444.9
.2	.3	27.5	99.5	19.1	91.4	23.7	27.0	17.0	16.6	59.5
.4	.4	28.5	101.4	22.0	95.4	29.0	33.9	25.8	27.9	74.2
.6	.6 .7	29.5 30.5	103.3	25.0 27.9	99.5 403.5	34.4 39.8	40.8 47.8	34.7 43.6	39·3 50·7	88.8
.8 2.0									1862.2	2503.6
	9	31.6	107.2	230.9	407.6	645.2	954.8	1352.6		2518.5
.2	1.1	32.6	9.2 11.2	33.9 36.9	11.8	50.6 56.1	61.8 68.8	61.6 70.6	73.8 85.4	33.4
.4 .6	I.3 I.5	33.7	13.3	39.9	20.I	61.6	75.9	70.0	97.0	48.5 63.6
						67.1		88.9	1908.7	
.8	I.7 2.0	35.9 37.1	15.3 117.4	43.0 246.1	24.3 428.5	672.7	83.I 990.2	1398.0	1900.7	78.7
3.0	2.2	38.2	19.5	49.2	32.7	78.2	97.4	1407.3	32.4	2594.0 2609.4
	2.5	39.4	21.6	52.3	37.0	83.9	1004.7	16.5	44.3	24.8
.4 .6	2.8	40.6	23.7	55.4	41.3	89.5	12.0	25.9	56.3	40.3
.8	3.2	41.8	25.8	58.6	45.6	95.2	19.3	35.3	68.3	55.9
4.0	3.5	43.0	128.0	261.8	450.0	700.9	1026.6	1444.6	1980.4	2671.6
.2	3.9	44.3	30.2	65.0	54.3	06.6	34.0	54.1	92.5	87.4
.4	4.2	45.5	32.4	68.2	58.7	12.4	41.4	63.6	2004.7	2703.3
.6	4.6	46.8	34.6	71.5	63.2	18.2	48.9	73.2	17.0	19.2
.8	5.0	48.1	36.9	74.8	67.6	24.0	56.4	82.8	29.3	35.2
5.0	5.5	49.4	139.1	278.I	472.I	729.9	1063.9	1492.4	2041.7	2751.3
.2	5.9	50.8	41.4	81.4	76.6	35.7	71.5	1502.1	54.2	67.5
.4	6.4	52.1	43.7	84.7	81.1	41.6	79.I	11.8	66.7	83.8
.6	6.8	53 - 5	46.0	88.I	85.6	47.6	86.8	21.7	79.3	2800.I
.8	7.3	54.9	48.4	91.5	90.2	53.6	94.5	31.5	91.9	16.6
6.0	7.9	56.3	150.7	294.9	494.8	759.6	1102.2	1541.4	2104.6	2833.2
. 2	8.4	57 - 7	53.I	98.3	99.4	65.6	09.9	51.3	17.4	49.8
.4	8.9	59.2	55.5	301.7	504.I	71.7	17.7	61.3	30.3	66.5
.6	9.5	60.6	57.9	05.2	08.8	77.8	25.6	71.3	43.2	83.4
.8	10.1	62.1	60.4	08.7	13.5	83.9	33.5	81.4	56.2	2900.3
7.0	10.7	63.6	162.8	312.2	518.2	790.I	1141.4	1591.6	2169.2	2917.3
. 2	11.3	65.2	65.3	15.8	22.9	96.3	49.3	1601.8	82.4	34.4
.4	12.0	66.7	67.8	19.3	27.7	802.5	57.3	12.0	95.5	51.6
.6	12.6	68.3	70.3	22.9	32.5	08.8	65.4	22.3	2208.8	68.9
.8	13.3	69.8	72.8	26.5	37.4	15.2	73.4	32.6	22.I	86.3
8.0	14.0	71.4	175.4	330.1	542.2	821.4	1181.6	1643.0	2235.5	3003.8
.2	14.7	73.0	78.0	33.8	47.I	27.7	89.7	63.5	48.9	21.4
.4	15.4	74.7	80.6	37.5	52.0	34.I	97.9	64.0	62.5	39.1
.6	16.2	76.3	83.2	41.2	57.0	40.5	1206.1	74.5	76.1	56.8
.8	16.9	78.0	85.8	44.9	61.9	47.0	14.4	85.1	89.8	74.7
9.0	17.7 18.5	79.7 81.4	188.5 91.2	348.6 52.4	566.9 72.0	853.5 60.0	1222.7 31.1	1695.8 1706.5	2303.5 17.3	3092.7 3110.8
.2				ı	'	1	1		1	28.9
.4 .6	19.3 20.2	83.I 84.8	93.9 96.6	56.2 60.0	77.0 82.1	66.5 73.1	39.5 48.0	17.3 28.1	31.2 45.1	28.9 47.2
.8	21.0	86.6	99.4	63.9	87.2	79.7	56.4	39.0	59.2	65.6
10.0	21.0	88.4	202.I	367.7	592.3	886.4	1265.0	1749.9	2373.3	3184.1
$\frac{10.0}{I}$	0°	10°	202.1	307.7 30°	40°	50°	60°	70°	80°	90°
4		10	20	30	40	30	1 00	/-	1 00	30

TABLE V. — Long Chords and Actual Arcs

Degree	Actual	۱ ـ		-					Degree
of	arc, one	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of
curve	station								curve
0.2	100.000	200.0	300.0	400.0	500.0	600.0	700.0	800.0	0.2
.4	.000	00.0	00.0	00.0	00.0	00.0	699.9	799.9	.4
.6	.000	00.0	00.0	00.0	499.9	599.9	699.8	799.8	.6
.8	.001	00.0	00.0	00.0	99.9	99.8	99.7	99.6	.8
1.0	100.001	200.0	300.0	399.9	499.8	599.7	699.6	799.4	1.0
.2	.002	00.0	00.0	99.9	99.8	99.6	99.4	99.1	. 2
.4	.002	00.0	299.9	99.9	99.7	99.5	99.2	98.8	.4
.6	.003	00.0	99.9	99.8	99.6	99.3	98.9	98.4	.6
.8	.004	00.0	99.9	99.8	99.5	99.1	98.6	97.9	.8
2.0	100.005	200.0	299.9	399.7	499.4	598.9	698.3	797.4	2.0
.2	,006	00.0	99.9	99.6	99.3	98.7	97.9	96.9	.2
.4	.007	00.0	99.8	99.6	99.1	98.5	97.5	96.3	.4
.6	.009	00.0	99.8	99.5	99.0	98.2	97.I	95.7	.6
.8	.010	199.9	99.8	99.4	98.8	97.9	96.7	95.0	.8
3.0	100.011	199.9	299.7	399.3	498.6	597.6	696.2	794.3	3.0
.2	.013	99.9	99.7	99.2	98.4	97.3	95.6	93.5	.2
.4	.015	99.9	99.6	99.1	98.2	96.9	95.1	92.6	.4
.6	.016	99.9	99.6	99.0	98.0	96.6	94.5	91.7	.6
.8	.018	99.9	99.6	98.9	97.8	96.2	93.9	90.8	.8
4.0	100,020	199.9	299.5	398.8	497.6	595.7	693.2	789.8	4.0
.2	.022			98.7		95.3	92.5	88.8	
.4	.022	99.9 99.9	99.5 99.4	98.5	97.3 97.1	95.3	92.5	87.7	. 2 . 4
.6	.025	99.9	99.4	98.4	96.8	94.9	91.0	86.5	.6
.8	1		1	98.2	96.5		90.2	1	.8
5.0	.029 100.032	99.8 199.8	99.3 299.2	398.1	496.2	93.9 593.4	689.4	85.3 784.1	5.0
.2	.034	99.8	99.2	97.9	95.9	92.8	88.5	82.8	.2
		99.8	99.1	97.8	95.6	92.3	87.6	81.5	.4
.4 .6	.037	99.8	99.1	97.6	95.0	92.3	86.7	80.1	.6
.8	.043	99.0	99.0	97.4	94.9	91.1	85.7	78.7	.8
6.0	100.046	199.7	298.9	397.3	494.5	590.4	684.7	777.2	6.0
.2						89.8			
.4	.049	99.7 99.7	98.8 98.8	97.1 96.9	94.2 93.8	89.1	83.7 82. 7	75.6 74.0	. 2
.6	.052 .055	99.7	98.7	96.7	93.6	88.5	81.6	72.4	.6
.8			98.6	96.5		87.7	80.4	70.7	.8
7.0	.059 100.062	99.6 199.6	298.5	396.3	93.0 492.6	587.0	679.3	769.0	7.0
.2	.066	99.6	98.4	96.1	92.I	86.3	78.1	67.2	.2
.4	.070	99.6	98.3	95.8	91.7	85.5	76.9	65.4	.4
.6	.073	99.6	98.2	95.6	91.7	84.7	75.6	63.5	.6
.8	.073	99.5	98.1	95.4	90.8	83.9	74.3	61.6	.8
8.0	100.081	199.5	298.1	395. I	490.3	583. I	673.0	759.7	8.0
.2	.085	99.5	98.0	94.9	89.8	82.2	71.7	57.7	.2
.4	.085	99.5 99.5	98.0	94.6	89.3	81.4	70.3	55.6	.4
.6	.094	99.4	97.9	94.4	88.8	80.5	68.9	53.5	.6
.8	.098	99.4	97.6	94.1	88.3	79.6	67.4	51.4	.8
9.0	100.103	199.4	297.5	393.9	487.7	578.6	666.0	749.2	9.0
.2	.108	99.4	97.4	93.6	87.2	77.7	64.4	46.9	.2
-4	.112	99.3	97.3	93.3	86.6	76.7	62.9	44.6	.4
.6	.112	99.3	97.3	93.0	86.1	75.7	61.3	42.3	.6
.8	.122	99.3	97.1	92.7	85.5	74.7	59.7	39.9	.8
10.0	100.127	199.2	297.0	392.4	484.9	573.7	658.1	737.5	10.0
Degree	Actual arc		3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree
Degree	Actual arc	z ota.	3 Sta.	4 Jia.	3 Dia.	o Dia.	/ Dia.	o ota.	Degree

								,	
Degree of curve	Actual arc, one station	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree of curve
10.0	100.127	199.2	297.0	392.4	484.9	573.7	658.1	737.5	10.0
. 2	.132	99.2	96.8	92.1	84.3	72.6	56.5	35.I	.2
.4	.137	99.2	96.7	91.8	83.7	71.6	54.8	32.5	.4
.6	.143	99.1	96.6	91.5	83.1	70.5	53.0	30.0	.6
.8	. 148	99. I	96.5	91.2	82.4	69.4	51.3	27.4	.8
11.0	100.154	199.1	296.3	390.8	481.8	568.2	649.5	724.8	11.0
.2	.159	99.0	96.2	90.5	81.1	67.1	47.7	22.I	. 2
.4	. 165	99.0	96. I	90.2	80.4	65.9	45.8	19.4	.4 .6
.6	.171	99.0	95.9	89.8	79.7	64.8	44.0	16.6	.8
.8	. 177	98.9	95.8	89.5	79.0	63.5	42.I	13.8	
12.0	100.183	198.9	295.6	389.I	478.3	562.3	640. I	710.9	12.0
. 2	.189	98.9	95.5	88.7	77.6	61.1	38.2	08.1	. 2
.4	. 195	98.8	95.3	88.4	76.9	59.8	36.2	05.1	.4
.6	. 202	98.8	95.2	88.0	76.2	58.5	34.2	702.2	.6
.8	. 208	98.8	95.0	87.6	75.4	57.2	32.I	699.2	.8
13.0	100.215	198.7	294.9	387.2	474.6	555.9	630.1	696. I	13.0
.2	.222	98.7	94.7	86.8	73.9	54.6	28.0	93.0	.2
-4	. 228	98.6	94.6	86.5	73.I	53.2	25.8	89.9	.4
.6	. 235	98.6	94.4	86.0	72.3	51.9	23.7	86.7	.6
.8	. 242	98.5	94.2	85.6	71.5	_50.5	21.5	83.5	.8
14.0	100.249	198.5	294.I	385.2	470.6	549. I	619.3	680.3	14.0
.2	. 256	98.5	93.9	84.8	69.8	47.6	17.0	77.0	. 2
.4	. 264	98.4	93.7	84.4	69.0	46.2	14.8	73.7	.4
.6	.271	98.4	93.5	83.9	68.1	44.7	12.5	70.3	.6
.8	. 279	98.3	93.4	83.5	67.3	43.2	10.2	66.9	.8
15.0	100.286	198.3	293.2	383.I	466.4	541.7	607.8	663.5	15.0
.2	. 294	98.2	93.0	82.6	65.5	40.2	05.4	60.0	.2
.4	.302	98.2	92.8	82.2	64.6	38.7	03.0	56.5	.4
.6	.310	98.2	92.6	81.7 81.2	63.7 62.8	37.I	600.6 598.2	53.0	.6
.8	.318	98.1	92.4			35.6		49.4	.8
16.0	100.326	198.1	292.3	380.8	461.9	534.0	595.7	645.8	16.0
.2	-334	98.0	92.I	80.3	60.9	32.4	93.2	42.2	.2
.4	.342	98.0	91.9	79.8	60.0	30.7	90.7 88.1	38.5	.4
.6	.351	97.9	91.7	79.3	59 0	29. I	1	34.8	.6
.8	-359	97.9	91.5	78.8	58.0	27.5	85.5	31.1	.8
17.0	100.368	197.8 97.8	291.3 91.1	378.3 77.8	457.I 56.I	525.8 24.1	582.9 80.3	627.3	17.0 .2
.2	.376			1	_				ì
.4 .6	.385	97.7 97.6	90.8 90.6	77.3 76.8	55.I 54.I	22.4	77.7 75.0	19.6 15.8	.4 .6
.8	.394 .403	97.6	90.0	76.3	53.0	18.9	72.3	11.9	.8
18.0	100.412	197.5	290.2	375.7	452.0	517.2	569.6	608.0	18.0
			<u> </u>				66.8		
.2	.422	97.5	90.0	75.2	51.0 49.9	15.4 13.6	64.1	04.0 600.0	.2
.6	.431 .440	97 · 4 97 · 4	89.6	74.7 74.1	48.9	13.0	61.3	596.0	.4 .6
.8		97.3	89.3	73.6	47.8	10.0	58.5	92.0	.8
19.0	.450 100.460	197.3	289.1	373.0	446.7	508.1	555.6	587.9	19.0
.2	.469	97.2	88.9	72.5	45.6	06.3	52.8	83.8	.2
.4	.479	97.I	88.6	71.9	44.5	04.4	49.9	79.7	.4
.4 .6	.479	97.1	88.4	71.9	44.5	02.5	47.0	75.5	.6
.8	.499	97.0	88.2	70.7	42.3	500.6	44.I	71.3	.8
20.0	100.510	197.0	287.9	370.2	44I.I	498.7	54I.I	567.1	20.0
Degree	Actual arc	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree
Degree	nctual arc	Z Did.	J Dia.	4014.	o Dia.	J Dia.	, ora.	J Dia.	Degree

TABLE VI. - MIDDLE ORDINATES

Degree	1 -		T .			1			Da
of curve	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree of curve
0.2	.04	.17	.39	.70	1.09	1.57	2.14	2.79	0.2
.4	.09	-35	.78	I.40	2.18	3.14	4.28	5.58	-4
. 6 . 8	.13 .17	.52	1.18	2.09	3.27	4.7I 6.28	6.41	8.38	.6
1.0	.22	.87	1.96	2.79	4.36	1	8.55	11.17	.8
.2	.26	1.05	2.36	3.49 4.19	5.45 6.54	7.85 9.42	10.69	13.96 16.75	1.0
.4	.30	1.22	2.75	4.89	7.63	10.99	14.96	19.53	.4
.6	.35	1.40	3.14	5.58	8.72	12.56	17.09	22.32	6
.8	.39	1.57	3.53	6.28	9.81	14.13	19.22	25.10	.8
2.0	.44	I.75	3.93	6.98	10.90	15.69	21.36	27.88	2.0
. 2	. 48	1.92	4.32	7.68	11.99	17.26	23.48	30.66	.2
.4 .6	.52	2.09	4.71	8.37	13.08	18 83	25.61	33.43	-4
	.57	2.27	5.10	9.07	14.17	20.39	27.74	36.21	.6
.8 3.0	.61 .65	2.44	5.50 5.89	9.77	15.25	21.95	29.86	38.98	.8
.2	.70	2.79	6.28	10.46	16.34	23.52 25.08	31.98	41.74	3.0
.4	.74	2.97	6.67	11.86	18.51	26.64	36.22	44.30	.4
.6	.78	3.14	7.06	12.55	19.60	28.20	38.34	50.01	.6
.8	.83	3.32	7.46	13.25	20.68	29.75	40.45	52.76	.8
4.0	.87	3.49	7.85	13.94	21.77	31.31	42.56	55.50	4.0
. 2	.92	3.66	8.24	14.64	22.85	32.86	44.66	58.24	.2
.4	. 96	3.84	8.63	15.33	23.93	34.41	46.77	60.97	-4
. 6	1.00	4.01	9.02	16.03	25.01	35.96	48.87	63.69	.6
. 8 5.0	1.05	4.19	9.42	16.72	26.09	37.51	50.96	66.42	.8
.2	1.09	4.36	9.81	17.42	27.17 28.25	39.06 40.60	53.05	69.13	5.0
.4	1.14	4.71	10.59	18.80	29.33	42.15	55.14	71.84	. 2
.6	1.22	4.89	10.98	19.49	30.40	43.69	57.23 59.31	74.54 77.23	.4 .6
. 8	I.27	5.06	11.37	20.19	31.48	45.22	61.38	79.92	.8
6.0	1.31	5.23	11.76	20.88	32.55	46.76	63.46	82.60	6.0
. 2	1.35	5.41	12.15	21.57	33.63	48.29	65.52	85.27	. 2
.4	1.40	5.58	12.54	22.26	34.70	49.82	67.58	87.93	.4
.6	1.44	5.76	12.93	22.95	35 77	51.35	69.64	90.59	.6
.8	1.48	5.93	13.32	23.64	36.84	52.88	71.70	93.23	.8
7.0	I.53 I.57	6.11	13.71 14.10	24.33 25.02	37.91 38.97	54.40 55.92	73.74	95. 87 98.50	7.0
.4	1.62	6.45	14.49	25.71	40.04	57.44	75.79 77.82	101.12	.2
.6	1.66	6.63	14.49	26.39	41.10	58.95	77.82	101.12	.4 .6
.8	1.70	6.80	15.27	27.08	42.17	60.46	81.88	106.33	.8
8.0	1.75	6.98	15.66	27.77	43.23	61.97	83.90	108.92	8.0
.2	1.79	7.15	16.05	28.45	44.29	63.47	85.92	111.50	.2
.4	1.83	7.32	16.44	29.14	45.35	64.97	87.92	114.06	.4
.6	1.88	7.50	16.83	29.82	46.40	66.47	89.92	116.62	.6
.8 9.0	1.92	7.67	17.22	30.51	47.46	67.97	91.92	119.17	.8
9.0	1.97 2.00	7.85 8.02	17.61 18.00	31.19	48.51 49.56	69.46 70.95	93.91	121.71	9.0
.4	2.05	8.19	18.38	32.56	50.61	72.43	95.89	124.23	.2
.6	2.10	8.37	18.77	32.50	51.66	72.43	97.87 99.83	126.75 129.25	.4 .6
.8	2.14	8.54	19.16	33.92	52.71	75.39	101.80	131.74	.8
10.0	2.18	8.72	19.55	34.60	53.75	76.86	103.75	134.22	10.0
Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

TABLE VI. — (Continued)

Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree
of curve	2.18	8.72	19.55	34.60	53.75	76.86	103.75	134.22	of curve
.2	2.23	8.89	19.94	35.28	54.79	78.33	105.70	136.68	.2
.4	2.27	9.06	20.32	35.96	55.83	79.79	107.64	139.14	.4
.6	2.31	9.24	20.71	36.63	56.87	81.25	109.57	141.58	.6
.8	2.36	9.41	21.10	37.31	57.91	82.71	111.49	144.00	.8
11.0	2.40	9.59	21.48	37.99	58.94	84.16	113.41	146.41	11.0
.2	2.44	9.76	21.87	38.66	59.98	85.61	115.32	148.81	.2
.4	2.49	9.93	22.25	39.34	61.01	87.05	117.21	151.20	.4
.6 .8	2.53	10.11	22.64	40.01 40.68	62.04 63.06	88.49	119.11	153.57	.6 .8
12.0						89.92		155.93	12.0
	2.62	10.45	23.41	41.36	64.09	91.36	122.87	158.27	
.2	2.66 2.71	10.63	23.80	42.70	65.11 66.13	92.78 94.20	124.73 126.59	160.59 162.91	.2
.6	2.75	10.00	24.57	43.37	67.14	95.62	128.43	165.21	.6
.8	2.80	11.15	24.95	44.03	68.16	97.03	130.27	167.49	.8
13.0	2.84	11.32	25.33	44.70	69.17	98.43	132.10	169.75	13.0
.2	2.88	11.49	25.72	45 - 37	70.18	99.83	133.92	172.01	.2
-4	2.93	11.67	26.10	46.03	71.19	101.23	135.73	174.24	-4
.6	2.97	11.84	26.48	46.70	72.19	102.62	137.53	176.46	.6
.8	3.01	12.01	26.87	47.36	73.20	104.00	139.33	178.67	.8
14.0	3.06	12.19	27.25	48.02	74.20	105.38	141.11	180.85	14.0
.2	3.10	12.36	27.63 28.01	48.69	75.20	106.76	142.88	183.02 185.17	.2
.6	3.15	12.53 12.71	28.40	49.35 50.01	76.19 77.18	108.12	144.64	187.31	.4 .6
.8	3.23	12.88	28.78	50.66	78.17	110.85	148.14	189.43	.8
15.0	3 28	13.05	29.16	51.32	79.16	112.20	149.87	191.53	15.0
.2	3.32	13.23	29.54	51.98	80.14	113.54	151.59	193.62	.2
.4	3.36	13.40	29.92	52.63	81.12	114.88	153.30	195.68	-4
.6	3.41	13.57	30.30	53.29	82.10	116.22	155.00	197.73	.6
.8	3.45	13.74	30.68	53.94	83.08	117.55	156.69	199.76	.8
16.0	3.50	13.92	31.06	54.59	84.05	118.87	158.37	201.77	16.0
.2	3.54	14.09	31.44	55.24	85.02	120.19	160.03	203.77	.2
.6	3.58	14.26 14.44	31.82 32.20	55.89 56.54	85.99 86.95	121.50	161.69	205.74	.4 .6
.8	3.67	14.61	32.57	57.19	87.91	121.10	164.96	209.64	.8
17.0	3.72	14.78	32.95	57.83	88.87	125.39	166.59	211.55	17.0
.2	3.76	14.95	33.33	58.48	89.83	126.68	168.20	213.46	.2
.4	3.80	15.13	33.71	59.12	90.78	127.96	169.79	215.33	.4
.6	3.85	15.30	34.08	59.76	91.73	129.23	171.38	217.20	.6
.8	3.89	15.47	34.46	60.40	92.67	130.49	172.95	219.03	.8
18.0	3.94_	15 64	34.84	61.04	93.62	131.75	174.52	220.86	18.0
.2	3.98	15.82	35.21	61.68	94.55	133.01	176.07	222.65	.2
.6	4.02	15.99 16.16	35.59 35.96	62.32 62.96	95.49 96.42	134.25	177.60	224.43	.6
.8	4.11	16.33	36.34	63.59	97.35	136.72	180.64	227.93	.8
19.0	4.16	16.51	36.71	64.22	98.28	130.72	182.15	229.65	19.0
. 2	4.20	16.68	37.09	64.85	99.20	139.17	183.64	231.35	.2
-4	4.24	16.85	37.46	65.48	100.12	140.38	185.11	233.03	.4
.6	4.29	17.02	37.83	66.11	101.03	141.58	186.57	234.69	.6
.8	4.33	17.19	38.20	66.74	101.95	142.78	188.02	236.33	.8
20.0	4.37	17.37	38.58	67 37	102.86	143.97	189.46	237.94	20.0
Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

CHAPTER II

THE SPIRAL

The railroad spiral is a curve of varying radius connecting a main or central curve with a tangent or connecting the two branches of a compound curve. If it is a true spiral its change in "degree" is proportionate to its length. Thus at the point of junction with the tangent (T.S. in Fig. 22) the degree is zero; at the junction with the main or central curve of degree D (S.C. in Fig. 22) it is D; at its midpoint it is $\frac{1}{2}D...$ etc. The radius is closely inversely as the length. Knowing the degree of the central curve the first quantity to determine is the length L, the second is Δ , the central angle consumed by the spiral. If these two can be conveniently chosen the other functions can be had from tables.

The length of the spiral is determined as follows: For curves of 6° or over on which track is canted 8 inches, L=240 feet as a minimum.

For curves flatter than 6° likely sometime to limit speed, $L = \frac{587}{\sqrt{D}}$ feet,

D being the degree of the central curve. For minor curves not likely to limit speed, $L=\frac{2}{3}SE$ or 30 E in feet, in which S is speed in miles per hour and E is the difference in elevation of the two rails in inches.

If the maximum allowable cant is 6 inches, $L = \frac{380}{\sqrt{D}}$ feet for curves

flatter than 4.5° likely to limit speed. For curves of 4.5° and over the minimum length will be 180 feet.

For minor curves, $L = \frac{2}{3} SE$ or 30 E, as above.

It will be well to select lengths that are round numbers of feet not less than the required minimums and such that the resulting Δ may be whole degrees or a whole number of tenths of a degree divisible by 3. This is merely for convenience in computing.

$$\Delta = \frac{LD}{200}.$$

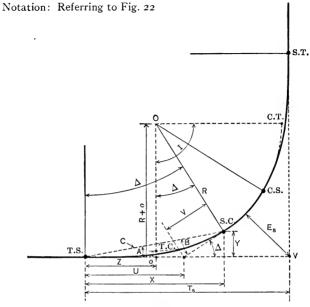


FIG. 22.

T. S. = Tangent-Spiral.

S. C. = Spiral-Curve.

C. S. = Curve-Spiral.

S. T. = Spiral-Tangent.

T. C. = Tangent-Curve.

C. T. = Curve-Tangent.

 Δ = central angle of the spiral.

A = deflection angle T. S. to S. C.

B = deflection angle S. C. to T. S.

C = the long chord of the spiral.

X = abscissa with T. S. as origin.

Y = ordinate with T. S. as origin.

U =spiral long tangent.

V =spiral short tangent.

o = curve offset.

Z = distance on tangent from T. S. to T. C. of the offset curve.

 T_s = tangent distance of the spiraled curve.

 E_{δ} = external distance of the spiraled curve.

R = radius of central curve.

The Chord Spiral. — If the spiral be laid out by equal chords it is approximately true that the deflection angles from the tangent at the T. S. to the several chord points are as the squares of the chord numbers, and the final deflection A of the long chord is one-third the central angle Δ .

If the spiral be divided into N chords, the deflection angle for the first chord will closely approximate $\frac{\Delta}{3 N^2}$ and the angles that the several chords (produced) will make with the tangent will be approximately

1, 7, 19, 37, 61, 91, 127, 169, 217, 271, etc., times
$$\frac{\Delta}{3 N^2}$$

The chord spiral is a curve passing through the chord points of a series of equal chords for which the relations of the preceding paragraph are exactly true. It is not a curve of uniformly varying radius or degree, but differs from such a curve by an inappreciable amount.

The spiral may be divided into any number of chords. Tables for a division into ten chords have been devised by Mr. Jenks B. Jenkins for the American Railway Engineering Association, and have been approved as good practice by that association.

Table VIII gives values for the quantities noted below. Excepting o and Z the linear quantities vary as L and hence the tabular quantities are coefficients by which the L's of any given cases are to be multiplied to find the functions C, X, Y, U, and V. The use of the table to get o and Z will be evident from the table headings.

Referring to Fig. 22, the tabulated quantities are Δ , A, \overline{L} , \overline{L} , \overline{L} , \overline{L}

 $\frac{U}{L}$, $\frac{V}{L}$, coefficients for o and Z. The following formulas give these quantities:

$$\Delta = \frac{LD}{200}, A = \frac{1}{3}\Delta - 0.000000825\Delta^{3}, B = \Delta - A.$$

$$\frac{C}{I} = \cos 0.3\Delta + 0.004 \operatorname{exsec} \frac{3}{4}\Delta \operatorname{(approx.)}.$$

$$X = C \cos A$$
.

$$Y = C \sin A$$
.

$$Z = X - R\sin\Delta.$$

$$U = C \frac{\sin B}{\sin \Delta}.$$

$$V = C \frac{\sin A}{\sin \Delta}.$$

$$o = Y - R \text{ vers } \Delta.$$

Exactly,
$$X = \frac{L}{10} \left(\cos \frac{\Delta}{300} + \frac{7\Delta}{300} + \cos \frac{19\Delta}{300} + \cos \frac{37\Delta}{300} + \cos \frac{61\Delta}{300} + \cos \frac{61\Delta}{300} + \cos \frac{127\Delta}{300} + \cos \frac{169\Delta}{300} + \cos \frac{217\Delta}{300} + \cos \frac{271\Delta}{300} \right)$$
. Exactly, $Y = \frac{L}{10} \left(\sin \frac{\Delta}{300} + \sin \frac{7\Delta}{300} + \dots \right)$. Exactly, $\tan A = \frac{Y}{V}$.

The following formulas give the tangent distance and external distance of the curve:

$$T_8 = (R + o) \tan \frac{1}{2} I + Z$$

 $E_8 = (R + o) \operatorname{exsec} \frac{1}{2} I + o.$

The central δ subtended by any portion, l feet, of the spiral is the average "degree" of the portion multiplied by $\frac{l}{100}$. The average "degree" is the initial and final degree of the portion divided by 2. The degree at any point distant l feet from the T.S. is $\frac{l}{L}D$. The degree at the end of any chord p (p being the number of the chord) is $\frac{p}{10}D$ for the 10-chord spiral or $\frac{p}{N}D$ for the N-chord spiral.

For precise computation of positions of points on line, A should be computed from $A=\frac{1}{3}\Delta-0.00000825~\Delta^3$ or taken from Table VIII, or Tables IX to XXIII. The deflection a_1 for the first chord is always $\frac{\Delta}{300}$ for the 10-chord spiral.

For field use the deflection from the T. S. to any chord point should be taken as a_1 times the square of the number of the chord point to be located so long as δ does not exceed 15°. A may be taken as $1/3 \Delta$ for $\Delta \equiv 15^\circ$. When Δ is more than 15° one or more intermediate transit points should be used. Such points should be so chosen that the δ from the T. S. to the first intermediate point shall not exceed 15°, and so that δ from any occupied point to the next transit point less the δ from the T. S. to the occupied point shall not exceed 15°. With this procedure the deflections from the tangent at any intermediate point may be taken as in Table VII, which gives the coefficients by which a_1 is to be multiplied to give deflections to points both forward and back as indicated. This procedure is not exact but results in angular errors less than can be measured by the transit. It is probable that 90 or more per cent of the cases in practice will involve Δ s of less than 10° and an error of 3 seconds or less than 0.001° if A is taken as $\frac{1}{3}\Delta$.

For $\Delta=15^{\circ}$ the error is 10 seconds or less than 0.003°. If it is desired to find the deflection from the T.S. to any point to which the δ exceeds 15° it may be done by finding the δ and then the corresponding A from Table VIII. If convenient spirals have been chosen, Tables IX to XXIII may be used.

To Select and Lay Out the Spiral. — Knowing I and D, determine L and Δ ; from Table VIII find coefficients for and determine o and Z and substitute in the equation for T_s . Knowing the P. I. the station of the T. S. can be found. There are now four ways of locating the curve.

I. The curve may be run from the T. S. to the S. C. by deflection angles and chord measurements, using Table VII for multiples of a_1 and setting on intermediate points if necessary as advised in the preceding article. To lay out by 5 chords use the deflection coefficients for every second point computing a_1 as for 10 chords.

2. The tangent may be continued from the T.S. for Z feet, o laid off and the curve D run in for the full central angle I, using an offset back sight for the direction of the offset tangent, locating the S.C. at a distance corresponding to Δ , and which will be nearly L-Z, and the C.S. at a distance from the S.C. corresponding to $I-2\Delta$, and offsetting o to the forward tangent and proceeding, locating the spirals later by deflection angles, or by offsets as in 4 below, when staking out for construction.

3. Measure U from the T. S.; establish a transit point, turn the angle Δ and measure V and establish the S. C.; run the spiral by deflections from either end; continue the central curve to the C. S.; lay out V and U to get the S. T. and run in the final spiral by deflections from either end.

4. Many times it will be sufficiently exact after running the central curve as in 2, to bisect the offset o for a point on the spiral and then set over such points as may be desired from tangent and curve respectively, making the offsets from the tangent half proportional to the cube of the distance from T.S. and from the curve half proportional to the cube of the distance from the S.C. Thus the quarter points would be offset 1/8 of $\frac{1}{2}o$ or o/16 from tangent and curve respectively.

Time may be saved if a spiral that can be found in one of the Tables IX to XXIII can be chosen. Thus if a 1.5-degree curve is to be connected and the speed to be considered is 90 miles an hour or less, Table X gives all required quantities for the necessary spiral which is 500 feet long. It may be laid out in ten chords of 50 feet each, for which deflection angles are found under the A column. If pluses are to be

located they may be interpolated between the tabular values which are given for each 10 feet on the spiral. But if the speed considered is only 65 miles an hour Table XIII may be used, the length of the spiral being 200 feet. It may be laid out in 10 chords of 20 feet for which the deflection angles or coordinates are given in the table or it may be laid out by 5 chords of 40 feet. Pluses may be interpolated as indicated above. If the speed is 60 miles an hour, Table XIV may be used and the length of spiral will be found to be 150 feet. It may be laid out in 10 chords of 15 feet interpolating in the table, or better, by 5 chords of 30 feet, with quantities taken directly from the table. Thus each table is good for many different spiral lengths connecting curves of various degrees. Any table may be used in which the degree of the central curve can be found in the column headed D provided the speed for which the table is adapted is that for which the curve is to be spiraled or the track canted. Shorter spirals found in tables for slower maximum speed than that for which the track is canted may be used but are not recommended except where it is necessary materially to save cost of construction or to fit cramped situations in cities or on high embankments or in deep cuts when relining old track.

Spiraling a Compound Curve. — The length of spiral to connect the two branches of a compound curve may be found just as for a

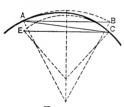


Fig. 23.

tangent and simple curve by substituting the difference of "degrees" $(D_1 - D_2)$ in the equation for length. It is also practically true that the deflections at the junction points with the two branches to the various chord points of the spiral are the same as for corresponding chord points of the spiral between tangent and simple curve of degree $(D_1 - D_2)$ if the deflections are considered as turned from equivalent

chord points on the respective curves rather than from the tangent. Thus in Fig. 23, the deflection from chord AB to chord AC of the spiral is $\frac{1}{3} \Delta$ (Δ being the central angle for spiral of length L connecting a tangent and $(D_1-D_2)^\circ$ curve) if arc AB=L, and from chord CE to chord CA it is the same. These relations are closely approximate. The deflection from the tangent at A is, if D_2 be the degree of the larger radius curve and D_1 of the shorter, $\frac{LD_2}{200}+\frac{1}{3}\Delta-C$, when $\Delta=$

 $\frac{(D_1 - D_2) L}{200}$ and C is the correction to be used when necessary or when Δ is more than 15°. Or the curve may be considered as part of a spiral from a tangent to the curve of degree D_2 and the deflection coefficients of Table VII may be used.

Illustrative Example. — A 4° curve is to connect with an 8° curve the offset coming at Sta. 464 of the 4° curve. $D_2=4^\circ;\ D_1=8^\circ;\ D_1-D_2=4^\circ;\ L=\frac{600}{\sqrt{D_1-D_2}}=300.\ \Delta=\frac{(D_1+D_2)}{2}\times\frac{L}{100}=18^\circ.$ For computing o and Z we use $D=D_1-D_2=4^\circ,\ \text{and}\ L=300,\ \text{whence}\ \Delta=6^\circ,\ \text{and}\ \text{from}$ the tables for $D=4,\ L=300,\ \text{and}\ \Delta=6^\circ$ we find o=2.62 and Z=149.92. Therefore C. S. = Sta. 464 — 149.92 ft. = Sta. 462 + 50.08. If the 300 feet is part of a spiral connecting a tangent and an 8° curve and covers a difference of 4° in its length the whole spiral would be $L_8=\frac{8\,L}{D_1-D_2}=2\,L=600\,\text{feet}$ covering a Δ of 24°. Therefore Sta. 462 + 50.08 = C. S. is the fifth chord point of the spiral. Since the central angle consumed by the spiral to be run is 18° and the central angle up to the fifth point of the 600-foot spiral is 6°, the difference is 12° or less than 15° and it will be proper to use Table VII with the transit at the fifth chord point. Hence the deflections to the several chord points are 16, 34, 54, 76, and 100 times a_1 , which is $\frac{\Delta}{300}=0.08^\circ$ or:

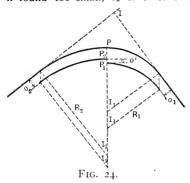
The chords are 60 feet and the deflections from tangent at A to the corresponding points on the 4° curve extended would be:

Setting up on the S. C., the compounding point with the 8° curve, the deflection from the long chord of the spiral to the tangent is from Table VII, 125 \times a_1 or 10°. It is also $\frac{LD_1}{200} - 2^{\circ}$ or, stated otherwise,

the angle between the long chord of $\frac{L}{100}$ stations of curve D_2 and the chord of the spiral is 2° , which is the deflection angle of a 300-foot spiral connecting a tangent and $4^{\circ} = (D_1 - D_2)$ degree curve.

Considering the whole spiraled curve, and referring to Fig. 24, in which R_1 is the shorter radius and R_2 is the longer radius, the compound curve is supposed connected first directly to the tangents. To introduce the spirals, the arc of R_1 must be thrown in along the line of common radius $PP_1 = o_1 \sec I_1$. The arc of R_2 must be thrown $PP_2 = o_2 \sec I_2$. $PP_1 - PP_2$ must equal o', the proper offset for the connecting spiral. Therefore determine L_2 to find o_2 and PP_2 ; to

 PP_2 add o' previously found and find a trial value for $o_1 = \frac{PP_2 + o'}{\sec I_1}$; if found too small, o_2 or o' or both may be increased, which will



necessitate increase in L_2 or L' or both; if found too large no harm will result unless in relining track the shift is too great. The tangent distances are increased by $o_2 \tan \Delta_2$ and $o_1 \tan \Delta_1$, respectively.

To lessen the movement of existing track the following procedure may be had: Conceive the larger radius curve moved outward along the common radius line, and the smaller radius curve moved inward, each by $\frac{1}{2} \rho'$, the

proper offset for the chosen spiral; find new radii for the curves such that

$$R_{2}' = R_{2} - \frac{\frac{1}{2}o'\cos I_{2} + o_{2}}{\text{vers } I_{2}}.$$

$$R_{1}' = R_{1} - \frac{o_{1} - \frac{1}{2}o'\cos I_{1}}{\text{vers } I_{1}}.$$

Both tangent points will be moved toward the vertex by

$$t_2 = (R_2 - R_2' + \frac{1}{2} o') \sin I_2$$

 $t_1 = (R_1 - R_1' - \frac{1}{2} o') \sin I_1$.

TABLE VII. — Coefficients of a_1 for Deflection Angles to Chord Points

Deflection				Tran	sit at c	hord-p	oint nu	ımber			
angle to chord-point number	о Т. S.	I	2	3	4	5	6	7	8	9	10 S. C.
o T. S.	o	2	8	18	32	50	72	98	128	162	200
1	1	0	5	14	27	44	65	90	119	152	189
2	4	4	0	8	20	36	56	80	108	140	176
3	9	10	7	0	II	26	45	68	95	126	161
4	16	18	16	10	0	14	32	54	80	110	144
5 6	25	28	27	22	13	0	17	38	63	92	125
6	36	40	40	36	28	16	0	20	44	72	104
7	49	54	55	52	45	34	19	0	23	50	81
8	64	70	72	70	64	54	40	22	0	26	56
9	81	88	91	90	85	76	63	46	25	0	29
10 S. C.	100	108	112	112	108	100	88	72	52	28	0

TABLE VIII. — GENERAL FUNCTIONS — TEN-CHORD SPIRAL

		C	X	Y	U	V	o=mL	-nD	Z=mL	-nD	
Δ	A	$\frac{C}{L}$	\overline{L}	L	Ī	L	m	n	m	n	Δ
ů.o	0.000	1.00000	1.00000	.00000	.66667	.33333	.00000	.0000	.50000	.0000	0.0
Ι.	.033	.00000	.00000	.00058	.66667	.33333	.00015	.0000	. 50000	.0001	.1
.2	.067	.00000	.00000	.00116	.66667	.33333	.00029	.0000	. 50000	.0003	.2
.3	.100	.00000	.00000	.00175	.66667	.33333	.00044	.0000	.50000	.0004	.3
.4	. 133	.00000	.00000	.00233	.66667	.33333	.00058	.0000	. 50000	.0005	.4
.5	. 167	.00000	0.99999	.00291	.66667	.33334	.00073	.0000	.50000	.0006	- 5
.6	.200	.00000	.99999	.00349	.66667	33334	.00087	.0000	.50000	.0008	.6
.7	. 233	.99999	.99999	.00407	.66667	.33334	.00102	.0000	.50000	.0009	.7
.8	. 267	.99999	.99998	.00465	.66667	33334	.00116	.0000	.50000	.0010	.8
.9	.300	•99999	.99998	.00524	.66668	-33334	.00131	.0000	.50000	.0011	.9
1.0	.333	.99999	.99997	.00582	.66668	.33334	.00145	.0000	.50000	.0013	1.0
. 1	.367	.99998	.99996	.00640	.66668	.33335	.00160	.0000	.49999	.0014	. 1
.2	.400	.99998	.99996	.00698	.66668	.33335	.00175	.0000	.49999	.0015	. 2
.3	.433	.99998	.99995	.00756	.6 6668	.33335	.00189	.0000	-49999	.0017	.3
.4	.467	.99997	.99994	.00814	.66669	.33335	.00204	.0000	. 49999	.0018	.4
.5	.500	.99997	.99993	.00873	.66669	.33336	.00218	.0000	.49999	.0019	.5
.6	.533	.99997	.99992	.00931	.66669	.33336	.00233	.0000	-49999	.0020	.6
.7	.567	.99996	.99991	.00989	.66670	. 33336	.00247	.0000	. 49999	.0022	.7
.8	.600	.99996	.99990	.01047	.66670	.33337	.00262	.0000	. 49998	.0023	.8
.9	.633	-99995	.99989	.01105	.66671	.33337	.00276	.0000	49998	.0024	.9
2.0	.667	.99995	.99988	.01163	.66671	-33337	.00291	.0000	.49998	.0025	2.0
. т	.700	.99994	.99987	.01222	.66671	.33338	.00305	.0000	. 49998	.0027	.т
.2	.733	-99994	.99985	.01280	.66672	.33338	.00320	.0001	.49998	.0028	.2
-3	.767	-99993	.99984	.01338	.66672	. 33338	.00335	.0001	-49997	.0029	.3
.4	.800	.99992	.99983	.01396	.66673	.33339	.00349	.0001	-49997	.0031	.4
.5	.833	.99992	.99981	.01454	.66673	.33339	.00364	.0001	-49997	.0032	.5
.6	.867	.99991	.99980	.01512	.66674	. 33340	.00378	.0001	-49997	.0033	.6
.7	.900	.99990	.99978	.01571	.66674	.33340	.00393	.0001	.49996	.0034	.7
.8	.933	.99990	.99976	.01629	.66675	.33341	.00407	.0001	.49996	.0036	.8
.9		.99989		.01687	.66676	-33342	.00422	.0001	.49996	.0037	.9
3.0	1.000	.99988	.99973	.01745	.66676	-33342	.00436	.0001	-49996	.0038	3.0
.1	1.033	.99987	.99971	.01803	.66677	-33343	.00451	.0001	-49995	.0039	. 1
. 2	1.067	.99986		.01861	.66678	-33343	.00465	10001	-49995	.0041	.2
.3	1.100	.99985	1	.01919	.66678	-33344	.00480	.0001	-49995	.0042	.3
.4	1.133	.99985	1	.01978	.66679	.33345		.0001	-49994	.0043	.4
5	1.167	.99984	.99963	.02036	.66680	·33345	.00509	.0001	-49994	.0045	.5 .6
.6	1.200	.99983	1	.02094	.66681	.33346	.00524	.0001	-49994	.0046	
.7	1.233	.99982		.02152	.66681	.33347	.00538	0002	-49993	.0047	.7
.8	1.267 1.300	.99981	.99956	.02210	.66682	·33347	.00553	.0002	·49993	.0048	.8 .9
.9		.99980				.33348			-49993		
4.0	I.333	-99979	.99952	.02326	.66684	•33349	.00582	.0002	.49992	.0051	4.0
. І	1.367	.99978		.02384	.66685	.33350	.00596	.0002	.49992	.0052	. 1
.2	1.400			.02443	.66686	.33351	.00611	.0002		.0053	.2
.3	1.433	1		.02501	.66686	.33351	.00625	.0002	1	.0055	.3
.4	1.467			.02559	.66687	.33352	.00640	.0002	.49991	.0056	.4
.5	1.500			.02617	.66688	.33353	.00654	.0002	.49990	.0057	·5
.6	1.533			.02675	.66689	-33354	.00669	.0002	.49990	.0059	
.7	1.567			.02733	.66690	-33355	.00683	.0002	.49989	.0060	.7
.8	1.600	1		.02791	.66691	.33356	.00698	.0003	.49989	.0061	.8
.9	1.633			.02849	.66692	-33357	.00713	.0003	.49988	.0062	.9 5.0
5.0	1.667	.99967	.99924	.02907	,66693	.33358	.00727	.0003	.49988	.0064	ט.ט

TABLE VIII. - (Continued)

		0	37	77	7.7	77		ъ.			
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$	o=mL	-nD	Z=mI	J-nD	Δ
L.							m	n	m	n	
5.0	1.667	.99967	.99924	.02907	.66693	·33358	.00727	.0003	.49988	.0064	5.0
. 1	1.700	.99965	.99921	.02965	.66695	.33359	.00742	.0003	.49987	.0065	. 1
. 2	1.733	.99964	.99918	.03023	.66696	.33360	.00756	.0003	.49987	.0066	. 2
.3	1.767	.99962	.99915	.03082	.66697	.33361	.00771	.0003	.49986	.0067	.3
-4	1.800	.99961	.99912	.03140	.66698	. 33362	.00785	.0003	.49986	.0069	.4
-5	1.833	.99960	.99908	.03198	.66699	. 33363	.00800	.0003	. 49985	.0070	.5
.6	1.867	-99958	.99905	.03256	.66700	.33364	.00814	,0003	. 49985	.0071	.6
.7	1.900	.99957	.99902	.03314	.66702	. 33365	.00829	.0004	. 49984	.0073	.7
.8	1.933	.99955	.99898	.03372	.66703	.33366	.00843	.0004	.49984	.0074	.8
.9	1.967	-99953	.99895	.03430	.66704	.33367	.00858	.0004	49983	.0075	.9
6.0	2.000	.99952	.99891	.03488	.66705	.33369	.00872	.0004	.49982	.0076	6.0
.1	2.033	.99950	.99887	.03546	.66707	.33370	.00887	.0004	.49982	.0078	.1
. 2	2.067	.99949	.99884	.03604	.66708	.33371	.00901	.0004	.49981	.0079	.2
.3	2.100	.99947	. 99880	.03662	.66709	.33372	.00916	,0004	.49981	.0080	-3
.4	2.133	.99945	.99876	.03720	.66711	.33373	.00930	.0005	.49980	.0081	.4
-5	2.167	.99944	.99872	.03778	.66712	-33375	.00945	.0005	-49979	.0083	.5
.6	2.200	.99942	.99868	.03836	.66713	.33376	.00959	.0005	49979	.0084	.6
.7	2.233	.99940	.99864	.03894	.66715	-33377	.00974	.0005	. 49978	.0085	.7
.8	2.267	.99938	.99860	.03952	.66716	.33379	.00989	.0005	.49977	.0086	.8
.9	2.300	.99936	.99856	.04010	.66718	.33380	.01003	.0005	-49977	.0088	.9
7.0	2.333	.99935	.99852	. 04068	.66719	.33381	.01018	.0005	.49976	.0089	7.0
Ι.	2.367	.99933	.99847	.04126	.66721	.33383	.01032	.0006	.49975	.0090	. r
.2	2.400	.99931	.99843	.04184	.66722	.33384	.01047	.0006	-49975	.0091	.2
.3	2.433	.99929	.99839	.04242	.66724	.33385	.01061	.0006	-49974	.0093	.3
.4	2.467	.99927	.99834	.04300	.66725	. 33387	.01076	.0006	-49973	.0094	.4
.5	2.500	.99925	.99830	.04358	.66727	. 33388	.01090	.0006	.49972	.0095	- 5
.6	2.533	.99923	.99825	.04416	.66729	. 33390	.01105	,0006	.49972	.0097	.6
.7	2.567	.99921	.99821	.04474	.66730	.33391	.01119	.0007	.49971	.0098	.7
.8	2.600	.99919	.99816	.04532	.66732	-33393	.01134	.0007	. 49970	.0099	.8
.9	2.633	.99917	.99811	.04590	.66734	-33394	.01148	.0007	.49969	.0100	.9
8.0	2.666	.99914	.99806	.04648	.66735	.33396	.01163	.0007	.49969	.0102	8.0
. г	2.699	.99912	.99801	.04706	.66737	.33398	.01177	.0007	.49968	.0103	. 1
.2	2.733	.99910	.99797	.04764	.66739	-33399	.01192	.0007	. 49967	.0104	. 2
.3	2.766	. 99908	.99792	.04822	.66741	.33401	.01206	.0008	.49966	.0105	.3
.4	2.799	.99906	.99786	.04880	.66742	. 33402	.01221	.0008	.49965	.0107	.4
-5	2.833	.99903	.99781	.04937	.66744	. 33404	.01235	.0008	.49965	.0108	.5
.6	2.866	.99901	.99776	.04995	.66746	.33406	.01250	.0008	.49964	.0109	.6
.7	2.899	.99899	.99771	.05053	.66748	. 33407	.01264	.0008	. 49963	.0110	.7
.8	2.933	.99897	.99766	.05111	.66750	. 33409	.01279	.0009	. 49962	.0112	.8
.9	2.966	.99894	.99760	.05169	.66752	.33411	.01293	.0009	.49961	.0113	.9
9.0	2.999	.99892	.99755	.05227	.66754	.33413	.01308	.0009	.49960	.0114	19.0
.1	3.033	.99889	.99749	.05285	.66756	.33414	.01322	.0009	.49959	.0116	. 1
.2	3.066	.99887	.99744	.05343	.66758	.33416	.01337	.0009	-49959	.0117	.2
-3	3.099	.99884	.99738	.05400	.66760	.33418	.01351	.0010	.49958	.0118	٠3
-4	3.133	.99882	.99733	.05458	.66762	.33420	.01366	.0010	- 49957	.0119	.4
.5	3.166	.99879	.99727	.05516	.66764	. 33422	.01381	.0010	.49956	.0120	.5
.6	3.199	.99877	.99721	.05574	.66766	.33424	.01395	.0010	-49955	.0122	.6
.7	3.232	.99874	.99715	.05632	.66768	.33425	.01410	.0010	49954	.0123	.7
.8	3.266	.99872	.99709	.05690	.66770	. 33427	.01424	.0011	49953	.0124	.8
.9	3.299	.99869	.99704	.05747	.66772	.33429	.01439	.0011	. 49952	.0126	.9
10.0	3.332	.99866	.99698	.05805	.66774	.33431	.01453	.0011	. 49951	.0127	10.0

		- 1	1		**						
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	<u>V</u>	o=mL	-nD	Z=mL	-nD	Δ
_		L	L	L	L	\overline{L}	m	n	m	n	-
10.0	3.332	.99866	. 99698	.05805	.66774	.33431	.01453	.0011	.49951	.0127	10.0
.т	3.366	.99864	.99691	.05863	.66776	.33433	.01468	.0011	. 49950	.0128	. 1
.2	3.399	.99861	.99685	.05921	.66779	.33435	.01482	.0012	.49949	.0129	.2
.3	3.432	.99858	.99679	.05979	.66781	.33437	.01497	.0012	. 49948	.0131	.3
.4	3.466	.99856	.99673	.06036	.66783	.33439	.01511	.0012	-49947	.0132	.4
.5	3.499	.99853	.99667	.06094	.66785	.33441	.01526	.0012	.49946	.0133	.5
.6	3.532	.99850	.99660	.06152	.66787	.33443	.01540	.0012	49945	.0134	.6
.7	3.566	.99847	.99654	.06210	.66790	.33446	.01555	.0013	.49944	.0136	.7
.8	3.599	.99844	.99647	.06267	.66792	.33448	.01569	.0013	.49943	.0137	.8
.9	3.632	.99841	.99641	.06325	.66794	.33450	.01584	.0013	.49942	.0138	.9
11.0	3.666	.99838	.99634	.06383	.66797	.33452	.01598	.0013	49941	.0139	11.0
.1	3.699	.99835	.99627	.06441	.66799	33454	.01612	.0014			
.2	3.732	.99832	.99621	.06498	.66802	.33456	.01612	.0014	. 49940 . 49939	.0141	.I
.3	3.765	.99829	.99614	.06556	.66804	.33459	.01641	.0014	· 49939	.0142	.3
	3.799	.99826	.99607	.06614	.66806	.33461	.01656				1
.4	3.799	.99823	.99600	.06671	.66809	.33463	.01050	.0014	.49936	.0144	.4
.5 .6	3.865	.99820	.99593	.06729	.66811	.33465	.01685	.0015	· 49935 · 49934	.0146	.5 .6
	3.899	.99817	.99586	.06787	,66814	.33468					
.7 .8	3.932	.99814	.99579	.06844	.66816	.33400	.01699	.0015	·49933 ·49932	.0148	.7 .8
.9	3.965	.99811	.99572	.06902	.66819	.33472	.01714	.0016	.49932	.0149	.9
12.0											
	3.999	.99808	.99565	.06960	.66822	-33475	.01743	.0016	.49929	.0152	12.0
.1	4.032	.99804	.99557	.07017	.66824	.33477	.01757	.0016	.49928	.0153	.I
.2	4.065	.99801	.99550	.07075	.66827	•33479	.01772	.0016	.49927	.0154	.2
.3	4.098	.99798	•99543	.07133	.66830	.33482	.01786	.0017	.49926	.0156	-3
.4	4.132	.99795	.99535	.07190	.66832	. 33484	.01801	.0017	.49925	.0157	-4
.5	4.165	.99791	.99528	.07248	.66835	.33487	.01815	.0017	.49923	.0158	.5
.6	4.198	.99788	.99520	.07305	.66838	.33489	.01830	.0018	.49922	.0159	.6
.7	4.232	.99785	.99513	.07363	.66840	-33492	.01844	.0018	.49921	.0160	.7
.8	4.265	.99781	.99505	.07421	.66843	-33494	.01859	.0018	.49920	.0162	.8
.9	4.298	.99778	.99497	.07478	.66846	-33497	.01873	.0018	.49918	.0163	.9
13.0	4.331	.99774	.99489	.07536	.66849	.33499	.01888	.0019	.49917	.0164	13.0
Ι.	4.365	.99771	.99481	.07593	.66852	.33502	.01902	.0019	.49916	.0165	.1
.2	4.398	.99767	.99474	.07651	.66854	.33504	.01917	.0019	.49915	.0167	.2
.3	4.431	.99764	.99467	.07708	.66857	.33507	.01931	.0020	-49913	.0168	.3
.4	4.465	.99760	-99457	.07766	.66860	.33510	.01946	.0020	.49912	.0169	.4
.5	4.498	.99757	.99449	.07823	.66863	.33512		.0020	.49911	.0170	.5
.6	4.531	.99753	.99441	.07881	.66866	.33515	.01974	.0020	.49909	.0172	1
.7	4.564	.99749	•99433	.07938	.66869	.33518	.01989	.0021	.49908		.7
.8	4.598	.99746	.99425	.07996	.66872	.33520	.02003	.0021	-49907	.0174	.8
.9	4.631	.99742	.99416	.08053	.66875	·33523	.02018	.0021	.49905	.0175	.9
14.0	4.664	.99738	.99408	.08111	.66878	-33526	.02032	.0022	.49904	.0177	14.0
Ţ,	4.698	.99735	.99399	.08168	.66881	.33529	.02047	.0022	.49903	.0178	.1
.2	4.731	.99731	.99391	.08226	.66884	·33531	.02061	.0022	.49901	.0179	.2
.3	4.764	.99727	.99382	.08283	.66887	• 3 3534	.02076	.0023	.49900	.0180	-3
.4	4.797	.99723	· 9 9374	.08340	.66890	.33537	.02090	.0023	. 49898	.0182	.4
.5	4.831	.99719	.99365	.08398	.66893	-33540		.0023	.49897	.0183	.5
.6	4.864	.99715	.99356	.08455	.66897	.33543	.02119	.0024	.49896	.0184	.6
.7	4.897	.99711	-99347	.08513	.66900	.33546		.0024	. 49894	.0185	.7
.8	4.930	.99708	-99339	.08570	.66903	-33549			.49893	.0186	.8
.9	4.964	.99704	.99330	.08627	.66906	-33552			.49891	.0188	.9
15.0	4.997	.99700	.99321	.08685	. 66909	-33555	.02177	.0025	.49890	.0189	15.0

		C	X	Y	U	V	o=mL	-nD	Z=mL	-nD	
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	L	m	n	m	п	Δ
15.0	4.997	.99700	.99321	.08685	.66909	.33555	.02177	.0025	.49890	.0189	15.0
.r	5.030	.99696	.99312	.08742	.66913	.33558	.02191	.0025	.49888	.0190	. 1
.2	5.064	.99692	.99302	.08799	.66916	.33561	.02206	.0026	. 49887	.0191	. 2
-3	.5.097	. 99687	.99293	.08857	.66919	.33564	.02220	.0026	.49885	.0193	-3
-4	5.130	. 99683	.99284	.08914	.66923	.33567	.02235	.0026	. 19884	.0194	.4
.5	5.163	.99679	.99275	.08971	,66926	.33570	.02249	.0027	.49882	.0195	.5
.6	5.197	. 99675	.99265	.09028	.66929	.33573	.02264	.0027	.49881	.0196	.6
. 7	5.230	.99671	.99256	. c9o86	.66933	. 33576	.02278	.0027	.49879	.0198	.7
.8	5.263	.99667	.99246	.09143	.66936	.33579	.02292	.0028	.49878	.0199	.8
.9	5.296	. 99662	.99237	.09200	.66940	.33582	.02307	.0028	.49876	.0200	.9
16.0	5.330	.99658	.99227	.09257	.66943	33585	.02321	.0028	.49875	.0201	16.0
.1	5.363	.99654	.99218	.09315	.66947	.33588	.02336	.0029	.49873	.0202	. I
.2	5.396	.99650	.99208	.09372	.66950	.33592	.02350	.0029	.49872	.0204	.2
.3	5.429	.99645	.99198	.09429	.66954	.33595	.02365	.0029	.49870	.0205	.3
.4	5.463	.99641	.99188	. 09486	.66957	.33598	.02379	.0030	.49868	. 0206	-4
.5	5.496	.99637	.99178	.09543	.66961	.33601	.02393	.0030	.49867	.0207	.5 .6
.6	5.529	.99632	.99169	.09600	.66964	.33605	.02408	.0030	. 19865	.0209	
.7	5.563	.99628	.99159	.09658	.66968	.33608	.02422	.0031	.49863	.0210	.7
.8	5.596	.99623	.99148	.09715	.66972 .66975	.33611	.02437	.0031	.49362 .49860	.0211	.8
.9	5.629	.99619	.99138	.09772			.02451	.0032			
17.0	5.662	.99614	.99128	.09829	.66979	.33618	.02466	.0032	. 49859	.0213	17.0
I.	5.696	.99610	.99118	.09886	.66983	.33621	.02180	.0032	.49857	.0215	.I
.2	5.729	.99605	.99108	.09943	.66986	.33625	.02494	.0033	.49855	.0216	.2
.3	5.762	.99601	.99097	.10000	.66990	.33628	.02509	.0033	.49853	.0217	-3
.4	5.796	.99596	.99087	.10057	.66994	.33632	.02523	.0033	. 49852	.0218	.4
·5	5.829	.99591	.99076	.10114	.66998	.33635	.02538	.0034	.49850	.0220	·5
	5.862	.99587	.99066		.67002	.33639	.02552	1			
·7	5.896	.99582	.99055	.10228	.67005	.33642	.02567	.0035	. 49847	.0222	.7
.9	5.929 5.962	.99577	.99044	.10205	.67003	. 33649	.02595	.0035	.49843	.0223	9.
18.0							.02510	.0036	.49841	.0226	18.0
	5.995	.99568	.99023	.10399	.67017	.33653					
ı.	6.028	.99563	.99012	.10456	.67021	.33657	.02624	.0036	.49840	.0227	. I . 2
.2	6.062	.99558	.99001	.10513	.67025	.33660 .33664	.02639	.0037	. 49838 . 49836	.0220	.3
-3		.99553		.10570			.02667	.0037	. 49834	.0230	
.4	6.128	.99548	98979 .98968	.10627	.67033	.33667	.02682	.0037	.49833	.0230	·4 ·5
·5	6.194	.99538	.98957	.10741	.67041	.33675	.02696	.0038	.49831	.0233	.6
.7	6.228	.99533		.10798		.33679	.02711	,0039	. 49829	.0234	.7
.8	6.261	.99533	.98935	.10790	.67049	.33682	.02725	.0039	.49827	.0235	.8
.9	6.294	.99523		.10912		.33686		.0039	.49825	.0236	.9
19.0	6.328			,10968	.67058	.33690	.02754	.00.10	.49823	.0238	19.0
1.	6.361			.11025	.67062	.33694	.02768	.co40	.49821	. 0239	. г
.2	6.394			.11023		.33697	.02783	.0041	.4982C	.02.10	.2
.3	6.427			.11139		.33701		.0041	.49818	.0241	.3
.4	6.461		1 .	.11196		.33705		.0041	.49816	.0212	.4
-5	6.494			.11252		.33709		.0042	.49814	.0244	.5
.6	6.527			.11309		.33713	1 -	.0042	.49812	.0245	.6
.7	6.560	1		.11366		.33717		.0043	.49810	.0246	.7
.8	6.594		.98819	.11423		.33721		.0043	.49808	.0247	.8
.9	6.627			.11479		.33725		.0044	.49806	.0248	.9
20.0	6.660		The same of the sa	.11536	.67100	.33729	.02898	.0044	.49804	.0250	20.0

		-									
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$	o=mL	-nD	Z=mL	-nD	Δ
			L	L	L	L	m	n	m	n	
20.0	6.660	.99466	.98795	.11536	.67100	.33729	.02898	.0044	.49804	.0250	20°.0
.1	6.693	.99461	.98783	.11593	.67105	.33733	.02912	.0044	.49802	.0251	.1
.2	6.727	.99456	.98771	.11649	.67109	-33737	.02926	.0045	.49800	.0252	.2
.3	6.759	.99450	.98759	.11706	.67114	.33741	.02941	.0045	.49798	.0253	-3
.4	6.793	.99445	.98747	.11763	.67118 .67123	33745	.02955	.0046	.49796	.0254	.4
·5	6.826	.99439 .99434	.98734 .98722	.11819	.67123	·33749 ·33753	.02969	.0046	.49794 .49792	.0256	·5 ·6
	6.892	.99434	.98710	.11932	.67132	.33757	.02998	.0047	.49790	.0258	
.7 .8	6.926	.99428	.98697	.11932	.67136	.33762	.02998	.0047	.49798	.0259	.7 .8
.9	6.959	.99417	.98685	.12046	.67141	.33766	.03027	.0048	.49786	.0260	.9
21.0	6.992	.99412	.98672	.12102	.67145	.33770	.03041	.0048	.49784	.0262	21.0
.1	7.026	.99406	.98660	.12159	.67150	-33774	.03056	.0049	.49782	.0263	. І
.2	7.059	.99400	.98647	.12215	.67155	.33778	.03030	.0049	.49780	.0264	.2
.3	7.092	.99395	.98634	.12272	.67159	.33783	.03084	.0050	.49778	.0265	.3
.4	7.125	.99389	.98622	.12328	.67164	.33787	.03099	.0050	.49776	.0266	.4
.5	7.158	.99383	.98609	.12385	.67169	.33791	.03113	.0051	49774	.0267	.5
.6	7.192	.99378	.98596	.12441	.67173	.33796	.03127	.0051	.49772	.0269	.6
.7	7.225	.99372	.98583	.12497	.67178	.33800	.03142	.0052	.49770	.0270	.7
.8	7.258	.99366	.98570	.12554	.67183	.33804	.03156	.0052	.49768	.0271	.8
.9	7.291	.99360	. 98557	.12610	.67188	.33809	.03170	.0053	.49765	.0272	.9
22.0	7.324	-99354	.98544	.12667	.67193	.33813	.03185	.0053	.49763	.0273	22.0
.ı	7.358	.99349	.98531	.12723	.67197	.33818	.03199	.0054	.49761	.0275	. 1
.2	7.391	.99343	.98517	.12779	.67202	.33822	.03213	.0054	.49759	.0276	.2
.3	7.424	.99337	.98504	.12836	.67207	.33827	.03228	.0055	.49757	.0277	-3
.4	7.458	.99331	.98491	.12892	.67212	.33831	.03242	.0055	.49755	.0278	- 4
·5	7.491	.99325	.98477 .98464	.12948	.67217 .67222	.33836	.03256	.0056 .0056	.49752	.0279	.5 .6
	7.524			.13061	.67227	.33845	1		.49750		
.7 .8	7.557 7.590	.99313	.98450 .98437	.13001	.67232	.33849	.03285	.0057	.49748 .49746	.0282	·7 .8
.9	7.623	.99301	. 98423	.13173	.67237	.33854	.03299	.0058	.49744	.0284	.9
23.0	7.657	.99295	.98409	.13230	.67242	.33859	.03328	.0058	.49741	.0285	23.0
Ι.	7.690	.99288	.98396	.13286	.67247	.33863	.03342	.0059	+49739	.0286	.1
.2	7.723	.99282	.98382	.13342	.67252	.33868	.03357	.0059	.49739	.0288	.2
.3	7.756	.99276	.98368	.13398	.67258	.33873	.03371	.0060	49735	.0289	.3
.4	7.789	.99270	.98354	.13454	.67263	.33877	.03385	.0060	.49732	.0290	.4
.5	7.822	.99264	.98340	.13510	.67268	.33882	.03400	.0061	.49730	.0291	.5
.6	7.856	.99257	.98326	.13567	.67273	.33887	.03414	.0061	.49728	.0292	.6
.7	7.889	.99251	.98312	.13623	.67278	.33892	.03428	.0062	.49725	.0293	.7
.8	7.922	.99245	.98298	.13679	.67284	. 33896	.03443	.0062	.49723	.0295	.8
.9	7.955	.99238	.98283	.13735	.67289	.33901	.03457	.0063	.49721	.0296	.9
24.0	7.989	.99232	.98269	.13791	.67294	.33906	.03471	.0063	.49718	.0297	24.0
Ι.	8.022	.99226	.98255	.13847	.67300	.33911	.03485	.0064	.49716	.0298	. 1
.2	8.055	.99219	.98240	.13903	.67305	.33916	.03500	.0064	.49714	.0299	.2
.3	8.088	.99213	.98226	.13959	.67310	.33921	.03514	.0065	.49711	.0300	.3
.4	8.121 8.154	.99206 .99200	.98211 .98197	.14015	.67316 .67321	.33926 .33931	.03528	.0065	.49709	.0302	.4
.5 .6	8.188	.99200	.98197	.14071	.67327	.33931	.03543	,0066	.49707	.0303	.5 .6
.7	8.221	.99193	.98167	.14183	.67332	.33941	.03571	.0067	.49704	.0305	.7
.8	8.254	.99180	.98153	.14103	.67338	.33941	.03571	.0067	.49699	.0305	.8
.9	8.287	.99174	.98138	.14295	.67343	.33951	.03600	.0068	.49697	.0307	.9
25.0	8.321	.99167	.98123	.14350	.67349	.33956	.03614	.0068	.49695	.0309	25.0
20.0	0.321	.99107	.90123	.14350	.07349	+33930	.03014	.0000	.49093	.0309	20.

		-						D	Z=mI		
Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$	o=mL	-nD	Z=mL	nD	Δ
		L	L	L			m	n	m	n	
25.0	8.321	.99167	.98123	.14350	.67349	.33956	.03614	.0068	.49695	.0309	25°.0
.I	8.354	.99160	.98108	.14406	.67354	. 33961	.03628	.0069	.49692	.0310	. 1
.2	8.387	.99154	.98093	.14462	.67360	. 33966	.03643	.0069	. 49690	.0311	. 2
-3	8.420	.99147	.98078	.14518	.67365	.33971	.03657	.0070	.49687	.0312	.3
-4	8.453	.99140	.98063	.14574	.67371	.33976	.03671	.0071	.49685	.0313	-4
·5	8.486	.99133	.98048	.14629	.67377	.33982	.03685	.0071	.49682	.0314	.5
.6	8.519	.99127	. 98033	. 14685	.67382	. 33987	.03700	.0072	.49680	.0315	.6
.7	8.553	.99120	.98017	.14741	.67388	.33992	.03714	.0072	.49677	.0317	.7
.8	8.586 8.619	.99113	.98002	.14797 .14852	.67394	.33997	.03728	.0073	.49675 .49672	.0318	.8
.9										.0319	.9
26.0	8.652	. 99099	.97971	.14908	.67405	.34008	.03757	.0074	.49670	.0320	26.0
ı.	8.685	.99092	.97956	. 14964	.67411	.34013	.03771	.0074	.49667	.0321	.I
.2	8.719	.99085	.97940	.15019	.67417 .67423	.34018	.03785	.0075	.49665 .49662	.0322	.2
.3	8.752	.99078	.97925	.15075			- 1	- 1		.0323	-3
.4	8.785 8.818	.99071	.97909	.15131 .15186	.67429 .67435	.34029	.03814	.0076	.49660 .49657	.0325	-4
·5 .6	8.851	.99004	.97878	.15242	.67441	.34040	.03842	.0077	.49654	.0327	.5 .6
	8.884	.99050	.97862	.15297	.67447	.34045	.03857	.0078	.49652	.0328	
.7 .8	8.917	.99030	.97846	.15297	.67452	.34051	.03871	.0078	.49649	.0320	.7 .8
.9	8.951	.99036	.97830	.15408	.67458	.34056	.03885	.0079	.49647	.0330	.9
27.0	8.984	.99029	.97814	.15464	.67465	.34062	.03899	.0080	.49644	.0331	27.0
	9.017	.99022	.97798	.15519	.67471	.34067	.03913	.0080	.49641	.0333	.1
. I . 2	9.017	.99022	.97782	.15519	.67471	.34007	.03913	.0081	.49639	.0333	.1
.3	9.083	.99007	.97766	.15630	.67483	.34079	.03942	.0081	.49636	.0335	3
.4	9.116	.99000	97749	.15686	.67489	.34084	.03956	,0082	.49633	.0336	.4
.5	9.149	.98993	.97733	.15741	.67495	.34090	.03970	.0082	.49631	.0337	-5
.6	9.183	.98985	.97717	.15796	.67501	.34095	.03985	.0083	.49629	.0338	.6
.7	9.216	.98978	.97700	.15852	.67507	.34101	.03999	.0084	.49625	.0339	.7
.8	9.249	.98971	.97684	.15907	.67514	.34107	.04013	.0084	.49623	.0340	.8
.9	9.282	. 98963	.97667	.15962	.67520	.34113	.04027	.0085	.49620	.0342	.9
28.0	9.315	.98956	.97651	.16018	.67526	.34118	.04041	.0085	.49617	.0343	28.0
Ι.	9.348	.98948	.97634	.16073	.67532	.34124	.04056	.0086	.49615	.0344	т.
.2	9.381	.98941	.97617	.16128	.67539	.34130	.04070	.0087	.49612	.0345	.2
.3	9.415	. 98933	.97601	.16183	.67545	.34136	.04084	.0087	.49609	.0346	.3
.4	9.448	. 98926	.97584	.16239	.67551	.34141	.04098	.0088	.49606	.0347	-4
.5	9.481	.98918	.97567	. 16294	.67558	.34147	.04113	.0088	.49604	.0348	- 5
.6	9.514	.98911	.97550	.16349	.67564	.34153	.04127	.0089	.49601	.0349	.6
.7	9.547	.98903	.97533	.16404	.67571	.34159	.04141	,0090	.49598	.0351	.7
.8	9.580	.98895	.97516	.16459	.67577	.34165	.04155	.0090	+49595	.0352	.8
.9	9.613	.98888	.97499	.16514	.67584	.34171	.04169	.0091	.49592	.0353	.9
29.0	9.647	98880	.97482	.16569	.67590	.34177	.04184	.0092	.49590	.0354	29.0
.I	9.680	.98872	.97465	.16624	.67597	.34183	.04198	.0092	.49587	.0355	.I
.2	9.713	.98865	.97447	.16679	.67603	.34189	.04212	.0093	.49584	.0356	.2
.3	9.746	.98857	.97430	.16734	.67610	.34195	,04226	.0093	.49581	.0357	-3
.4	9.779	.98849	.97413	.16789	.67616	.34201	.04240	.0094	.49578	.0358	-4
.5 .6	9.812 9.845	.98841	·97395	.16844	.67623 .67630	.34207	.04254	.0095	.49575 .49573	.0359	.5 .6
		1	.97378			.34213					1
.7 .8	9.878 9.911	.98826	.97360	.16954	.67636 .67643	.34219	.04283	.0096	.49570 .49567	.0362	.7 .8
.0	9.911	.98810	.97343 .97325	.17064	.67650	.34225	.04297	.0097	.49564	.0364	.9
30.0	9.943	98802	.97307	.17119	.67657	.34238	.04325	.0098	.49561	.0365	30.0
30.0	9.970	90002	.9/307	.1/119	.07037	134430	.04323	.0090	.49301	.0303	55.5

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ı	Δ	A	$\frac{C}{L}$	$\frac{X}{L}$	$\frac{Y}{L}$	$\frac{U}{L}$	$\frac{V}{L}$	o=mL	-nD	Z=m1	-nD	Δ
					L	L	L	m	n	m	n	
3(o.o	9.978	.988c2	.97307	.17119	.67657	.34238	.04325	.0098	.49561	.0365	30.0
	. I	10.011	.98794	.97290	.17174	.67663	.34244	.04339	.0098	.49558	.0366	.1
	.2	10.044	.98786	.97272	.17229	.67670	.34250	.04354	.0099	· 49555	.0367	.2
1	.3	10.077	.98778	.97254	.17283	.67677	.34257	.04368	.0100	.49552	.0368	-3
1	.4	10.110	.98770	. 97236	.17338	.67684	. 34263	.04382	.0100	.49549	.0369	-4
ł	.5	10.143	.98762	.97218	.17393	.67691	.34269	.04396	.0101	. 49546	.0371	5
1	.6	10.176	.98754	.97200	.17448	.67698	.34276	.04410	.0102	·49543	.0372	.6
ı	.7	10.209	.98745	.97182	. 17502	.67705	.34282	.04424	.0102	. 49540	.0373	.7
ı	.8	10.242	.98737	.97164	.17557	.67712	.34288	.04439	.0103	49537	.0374	.8
١	.9	10.276	.98729	.97146	.17612	.67719	.34295	.04453	.0104	-49534	.0375	.9
33	١.٥	10.309	.98721	.97127	. 17666	.67726	.34301	.04467	.0104	.49531	. 0376	31.0
ı	.I	10.342	.98713	.97109	. 17721	.67733	.34308	.04481	.0105	. 49528	.0377	. І
ŀ	.2	10.375 10.408	.98704	.97091	.17776	.67740 .67747	.34314	.04495	.0106	49525	.0378	.2
	•3		.98696	.97072			- 1			.49522	.0379	-3
	.4	10.441	.98688	.97054	.17885	.67754 .67761	.34327	.04523	.0107	.49519	.0380	.4
ı	·5 .6	10.474	.98680	.97035	.17939	.67768	·34334 ·34340	.04538	8010.	.49516	.0381	·5 .6
							- 1	- 1	- 1		- 1	1
	.7 .8	10.540 10.573	.98663	.96998	.18048	.67775 .67783	·34347 ·34353	.04566	.0109	.49510	.0384 .0385	.7 .8
	.9	10.607	.98646	.96960	. 18157	.67790	.34360	.04594	.0110	.49504	.0386	.9
٠,	.0	10.640		.96942	.18212	.67797	34367	.04608	.0111	.49501		32.0
32			.98637								.0387	
	.I	10.673 10.706	.98629	.96923	.18266	.67804 .67812	·34373 ·34380	.04622	.0112	.49498	.0388	ı.
	.3	10.739	.98612	.96885	.18375	.67819	.34387	.04650	.0112	· 49495 · 49491	.0389 .0390	.2
		10.772	.98603	.96866	.18429	.67826	34394	.04665	.0114	.49488		
	·4 ·5	10.805	.98595	.96847	. 18483	.67834	.34400	.04679	.0114	.49485	.0391	.4 .5
	.6	10.838	.98586	.96828	.18538	.67841	.34407	.04693	.0115	.49482	.0393	.6
	.7	10.871	.98577	.96808	. 18592	.67849	.34414	.04707	.0116	. 49479	.0394	-7
	.8	10.904	.98569	.96789	.18646	.67856	.34421	.04721	.0116	.49476	.0395	.8
l	.9	10.937	.98560	.96770	.18700	.67864	.34428	.04735	.0117	.49473	.0397	.9
33	.0	10.970	.98551	.96750	.18754	.67871	.34435	.04749	.0118	.49469	.0398	33.0
	л.	11.003	.98543	.96731	.18809	.67879	.34442	.04763	.0118	.49466	.0399	.1
ì	.2	11.036	.98534	.96712	.18863	67886	.34448	.04777	.0119	.49463	.0400	.2
ŀ	.3	11.069	.98525	.96692	.18917	.67894	.34455	.04791	.0120	.49460	.0401	-3
	.4	11.103	.98516	.96672	.18971	.67901	.34462	.04805	.0121	.49457	.0402	.4
i	.5	11.136	.98507	.96653	.19025	.67909	. 34469	.04820	.0121	49453	.0403	-5
ı	.6	11.169	.98499	.96633	.19079	.67917	.34477	.04834	.0122	.49450	.0404	.6
	.7	11.202	.98490	.96613	. 19133	.67925	. 34484	.04848	.0123	-49447	.0405	.7
	.8	11.235	.98481	.96593	.19187	.67932	.34491	.04862	.0123	.49443	.0406	.8
1	.9	11.268	.98472	.96574	.19241	.67940	.34498	.04876	.0124	.49440	.0407	.9
34	1.0	11.301	.98463	.96554	.19295	.67948	.34505	.04890	.0125	-49437	.0408	34.0
ı	. I	11.334	.98454	.96534	.19349	.67956	.34512	.04904	.0126	.49434	.0409	. 1
ı	.2	11.367	.98445	.96514	.19403	.67963	.34519	.04918	.0126	.49430	.0410	.2
	٠3	11.400	.98436	.96494	.19457	.67971	-34527	.04932	.0127	.49427	.0411	-3
ŀ	.4	11.433	.98427	.96473	.19510	.67979	-34534	.04946	.0128	.49424	.0412	-4
ĺ	.5	11.456	.98417	.96453	.19564	.67987	.34541	.04960	.0128	.49420	.0413	-5
1	.6	11.499	.98408	.96433	.19618	.67995	.34548	.04974	.0129	.49417	.0415	.6
	.7	11.532	.98399	.96413	.19672	.68003	.34556	.04988	.0130	.49414	.0416	.7 .8
1	.8	11. 5 65 11. 5 98	.98390 .98381	.96392	. 19726 . 19779	.68011	.34563 .34570	.05002	.0131	.49410	.0417	.8
١.,	.9 5.0	11.631	.98371	.96351	.19779	.68027	.34578	.05030	.0131	.49404	.0419	35.0
13	υ.υ	11.031	.90371	.90351	.19033	.00027	.34570	.05030	.0132	.49404	.0419	30.0

		C	X	Y	U	V	o=mL	-nD	Z=mL	-nD	
Δ	A	$\frac{C}{L}$	\overline{L}	$\frac{Y}{L}$	L	\bar{L}	m	n	m	n	Δ
35°.0	11.631	.98371	.96351	. 19833	.68027	.34578	.05030	.0132	. 49404	.0419	35.0
1.	11.664	.98362	. 96331	.19887	.68035	.34585	.05044	.0133	.49400	.0420	т.
.2	11.698	.98353	.96310	.19940	.68043	.34593	.05058	.0133	.49397	.0421	.2
.3	11.731	.98344	.96290	.19994	.68051	. 34600	.05072	.0134	-49393	.0422	-3
.4	11.764	. 98334	.96269	.20047	.68059	. 34608	.05086	.0135	.49390	.0423	-4
-5	11.797	.98325	.96248	.20101	.68068	.34615	.05100	.0136	.49387	.0424	-5
.6	11.830	.98315	.96227	.20155	.68076	.34623	.05115	.0136	.49383	.0425	.6
.7	11.863	.98306	.96207	. 20208	.68084	. 34630	.05129	.0137	. 49380	.0426	.7
.8	11.896	.98297	.96186	. 20262	. 68092	. 34638	.05143	.0138	.49376	.0427	.8
.9	11.929	.98287	.96165	. 20315	.68101	. 34645	.05157	.0139	-49373	.0428	.9
36.0	11.961	.98278	.96144	.20368	.68109	.34653	.05171	.0139	.49369	.0429	36.0
т.	11.994	.98268	.96123	.20422	.68117	.34661	.05185	.0140	.49366	.0430	т.
.2	12.027	.98259	.96102	. 20475	.68126	.34668	.05199	.0141	.49362	.0431	.2
.3	12.061	.98249	.96080	.20529	.68134	. 34676	.05213	.0142	.49359	.0432	.3
.4	12.094	.98239	.96059	.20582	.68142	.34684	.05227	.0142	.49355	. 0433	.4
.5	12.127	.98230	.96038	.20635	.68151	.34692	.05241	.0143	. 49352	.0434	.5
.6	12.159	.98220	.96017	.20689	.68159	. 34699	.05255	.0144	. 49348	.0435	.6
.7	12.192	.98210	.95995	.20742	.68168	.34707	.05269	.0145	. 49345	.0436	.7
.8	12.226	.98201	.95974	.20795	.68176	.34715	.05282	.0145	.49341	.0437	.8
.9	12.259	.98191	.95952	.20848	.68185	. 34723	.05296	.0146	. 49338	.0438	.9
37.0	12.292	.98181	.95931	. 20901	.68194	.34731	.05310	.0147	. 49334	.0439	37.0
1.	12.324	.98171	.95909	. 20955	.68202	.34739	.05324	.0148	.49330	.0440	. 1
.2	12.358	.98162	.95887	.21008	.68211	-34747	.05338	.0149	.49327	.0441	.2
.3	12.391	.98152	. 95866	.21061	.68219	.34754	.05352	.0149	. 49323	.0442	.3
.4	12.424	.98142	.95844	.21114	.68228	. 34762	.05366	.0150	.49320	.0443	.4
.5	12.456	.98132	.95822	.21167	.68237	.34770	.05380	.0151	.49316	.0444	.5
.6	12.489	.98122	.95800	.21220	.68246	.34779	.05394	.0152	.49312	.0445	.6
.7	12.523	.98112	.95778	.21273	.68254	.34787	.05408	.0152	. 49309	.0446	.7
.8	12.556	.98102	.95756	.21326	.68263	-34795	.05422	.0153	.49305	.0447	.8
.9	12.588	.98092	.95734	.21379	.68272	34803	.05436	.0154	. 49302	.0448	.9
38.0	12.621	.98082	.95712	.21432	.68281	.34811	.05450	.0155	.49298	.0449	38.0
Ι.	12.654	.98072	.95690	.21485	.68290	.34819	.05464	.0156	. 49294	.0450	1.
.2	12.687	.98062	.95668	.21537	.68299	.34827	.05478	.0156	.49291	.0451	.2
.3	12.720	.98052	.95646	.21590	. 68307	.34835	.05492	.0157	.49287	.0452	-3
.4	12.753	.98042	.95623	.21643	.68316	.34844	.05506	.0158	.49283	.0453	.4
- 5	12.786	.98032	.95601	.21696	.68325	.34852	.05520	.0159	. 49279	.0454	-5
.6	12.819	. 98022	.95578	.21749	.68334	.34860	.05534	.0159	. 49276	.0455	.6
.7	12.852	. 98011	.95556	. 21801	. 68343	. 34869	.05548	.0160	.49272	.0456	.7
.8	12.885	.98001	.95533	. 21854	.68353	.34877	.05561	.0161	. 49268	.0457	.8
.8	12.918	.97991	.95511	.21907	. 68362	.34885	.05575	.0162	. 49265	.0458	.9
39.0	12.951	.97981	.95488	.21959	.68371	.34894	.05589	.0163	.49261	.0459	39.0
т.	12.984	.97970	.95466	.22012	.68380	.34902	.05603	.0163	. 49257	.0460	.1
.2	13.017	.97960	-95443	.22065	.68389	.34911	.05617	.0164	.49253	.0461	.2
.3	13.050	.97950	.95420	.22117	.68398	.34919	.05631	.0165	.49250	.0462	-3
.4	13.083	.97939	.95397	.22170	.68408	.34928	.05645	.0166	.49246	.0463	.4
.5	13.116	. 97929	.95374	.22222	.68417	.34936	.05659	.0167	.49242	.0464	.5
.6	13.149	.97919	.95351	. 22275	.68426	-34945	.05673	.0168	.49238	.0465	.6
.7	13.182	.97908	.95328	. 22327	.68435	-34953	. 05687	.0168	. 49234	.0466	
.8	13.215	.97898	.95305	. 22379	. 68445	.34962	.05701	.0169	. 49231	.0467	.8
.9	13.247	.97887	. 95282	.22432	.68454	-34970	.05714	.0170	.49227	.0468	
40.0	13.281	.97877	. 95259	. 22484	.68464	-34979	.05728	.0171	.49223	.0469	40.0

TABLE IX. — Spiral Functions for Change of 0.2° per 100 Feet Suitable for Speeds of 104 Miles an Hour or Less and Curves of 1° or Less

	1			URVES			E33			
L	D	Δ	A	Z	0	С	X	Y	U	V
	•	0	•							
10	0.02	0.001	0.000	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.04	.004	.001	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.06	.009	.003	15.00	.00	30.00	30.00	.00	20.00	10.00
40	.08	.016	.005	20.00	.00	40.00	40.00	.00	26.67	13.33
50	.10	.025	.008	25.00	.00	50.00	50.00	.oı	33.33	16.67
60	.12	.036	.012	30.00	.00	60.00	60.00	.01	40.00	20.00
70	.14	.049	.016	35.00	.00	70.00	70.00	.02	46.67	23.33
80	.16	.064	.021	40.00	.01	80.00	80.00	.03	53.33	26.67
90	. 18	.081	.027	45.00	.01	90.00	90.00	.04	60.00	30.00
100	.20	.100	.033	50.00	.01	100.00	100.00	.06	66.67	33.33
10	.22	.121	.0.10	55.00	.02	10.00	10.00	.08	73.33	36.67
20	.24	.144	.048	60.00	.03	20.00	20.00	.10	80.00	40.00
30	26	.169	.056	65.00	.03	30.00	30.00	.13	86.67	43.33
40	. 28	.196	.065	70.00	.04	40.00	40.00	.16	93.33	46.67
50	.30	.225	.075	75.00	.05	50.00	50.00	.20	100.00	50.00
60	.32	.256	.085	80.00	.06	60.00	60.00	.24	06.67	53.33
70	.34	.289	.096	85.00	.07	70.00	70.00	.28	13.33	56.67
80	.36	324	.108	90.00	.08	80.00	80.00	.34	20.00	60.00
		-	.120	95.00	.10	90.00	90.00	.40	26.67	
90 200	.38	.361	.133	100.00	.10	200.00	200.00	.40	133.33	63.33 66.67
10	.40	.441	.133	105.00	.13	10.00	10.00	.54	40.00	70.00
			.161	110.00	_	20,00	20.00	.62	1 '	
20	.44	.484	.101	115.00	.15	30.00	30.00	.02	46.67	73.33 76.67
30	.46	.529	.170	120.00	.18	40.00	40.00	.80	53.33 60.00	80.00
40	.48	.576					'	1		
50	.50	.625	.208	125.00	.23	50.00	50.00	.91	66.67	83.33
60	.52	. 676	. 225	130.00	.26	60.00	60.00	1.02	73.33	86.67
70	-54	.729	.243	135.00	. 29			1.14	80.00	90.00
8o	.56	. 784	.261	140.00	.32	80.00	79.99	1.28	86.67	93.34
90	.58	.841	.280	145.00	-35	90.00	89.99	1.42	93.33	96.67
300	.60	.900	.300	150.00	-39	300.00	99.99	1.57	200.00	100.00
10	.62	.961	.320	155.00	.43	10.00	309.99	1.73	06.67	103.34
20	.64	1.024	.341	160.00	.48	20,00	19.99	1.91	13.33	106.67
30	.66	1.089	. 363	165.00	. 52	29.99	29.99	2.09	20.00	110.00
40	.68	1.156	. 385	170.00	.57	39.99	39.99	2.29	26.67	113.34
50	.70	1.225	.408	175.00	.62	49.99	49.98	2.49	33.34	116.67
60	.72	1.296	.432	180.00	.68	59.99	59.98	2.71	40.01	120.01
70	.74	1.369	.456	185.00	.74	69.99	69.98	2.95	46.67	123.34
80	.76	1.444	.481	189.99	.80	79.99	79.98	3.19	53.34	126.67
90	.78	1.521	1.507	194.99	.86	89. 9 9	89.97	3.45	60.01	130.01
400	.80	1.600	-533	199.99	.93	99.99	99.97	3.72	266.68	133.34
10	.82	1.681	.560	204.99	1.00	409.98	409.96	4.01	73.35	136.68
20	.84	1.764	. 588	209.99	1.08	19.98	19.96	4.31	80.02	140.01
30	.86	1.849	.618	214.99	1.16	29.98	29.96	4.63	86,68	143.35
40	.88	1.936	.645	219.99	1.24	39.98	39.95	4.96	93 35	146.68
50	.90	2.025	.675	224.99	1.33	49.98	49.94	5.30	300.02	150.02
60	.92	2.116	.705	229.99	1.42	59.97	59.94	5.66	06.69	153.35
70	.94	2.209	.736	234.99	1.51	69.97	69.93	6.04	13.36	156.69
80	.96	2.304	.768	239.98	1.61	79.97	79.92	6.43	20.03	160.02
90	.98	2,401	.800	244.98	1.71	89.96	89.91	6.84	26.70	163.36
500	1.00	2.500	.833	249.98	1.82	499.96	499.91	7.27	333.37	166.70
		1 333	1	1 .5.55		1			1	

TABLE X. — Spiral Functions for a Change of 0.3° per 100 Feet. Suitable for Speeds of 91 Miles an Hour or Less, or Curves of 1.5° or Less

L	D	Δ	A	Z	0	С	X	Y	U	V
	•	•	-					_		
10	0.03	0.001	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.06	.006	.002	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.09	.013	.005	15.00	.00	30.00	30.00	.00	20.00	10.00
40	.12	.024	.008	20.00	.00	40.00	40.00	.00	26.67	13.33
50	.15	.037	.013	25.00	.00	50.00	50.00	.01	33 33	16.67
60	.18	.054	.018	30.00	.00	60.00	60.00	.02	40.00	20.00
70	.21	.073	.025	35.00	.01	70.00	70.00	.03	46.67	23.33
8o	. 24	.096	.032	40.00	.01	80.00	80.00	.04	53.33	26.67
90	. 27	.121	.041	45.00	.02	90.00	90.00	.06	60.00	30.00
100	.30	. 150	.050	50.00	.02	100.00	100.00	.09	66.67	33.33
10	.33	.181	.061	55.00	.03	110.00	110.00	.12	73.33	36.67
20	.36	.216	.072	60.00	.04	120.00	120.00	.15	80.00	40.00
30	-39	.253	. 085	65.00	.05	130.00	130.00	.19	86.67	43.33
40	.42	. 294	.098	70.00	.06	140.00	140.00	.24	93.33	46.67
50	-45	-337	.113	75.00	.07	150.00	150.00	.29	100.00	50.00
60	.48	.384	.128	80.00	.09	160.00	160.00	.36	106.67	53.33
70	.51	-433	. 145	85.00	.11	170.00	170.00	.43	113.33	56.67
80	-54	.486	.162	90.00	.13	180.00	180.00	.51	120.00	60.00
90	.57	.541	.181	95.00	.15	190.00	190.00	.60	126.67	63.33
200	.60	. 600	.200	100.00	.17	200.00	200.00	.70	133.33	66.67
10	.63	.661	.221	105.00	.20	210.00	210.00	.81	140.00	70.00
20	.66	.726	.242	110.00	.23	220.00	220.00	.93	146.67	73.33
30	.69	-793	. 265	115.00	.27	230.00	230.00	1.06	153.33	76.67
40	.72	.864	.288	120.00	.30	240.00	240.00	1.21	160.00	80.00
50	.75	.937	.313	125.00	.34	250.00	250.00	1.36	166.67	83.34
60	.78	1.014	.338	130.00	.38	260.00	259.99	1.53	173.34	86.67
70	.81	1.093	. 365	135.00	.43	269.99	269.99	1.72	180.00	90.00
80	.84	1.176	.392	140.00	.48	279.99	279.99	1.92	186.67	93.34
90	.87	1.261	.421	145.00	.53	289.99	289.99	2.13	193.34	96.67
300	.90	1.350	.450	150.00	.59	299.99	299.98	2.36	200.01	100.01
10	.93	1.441	.481	155.00	.65	309.99	309.98	2.60	206.67	103.34
20	.96	1.536	.512	160.00	.71	319.99	319.98	2.86	213.34	106.67
30	.99	1.633	-545	165.00	-79	329.99	329.97	3.14	220.0I	110.01
40	1.02	1.734	.578	170.00	.86	339.99	339.97	3.43	226.68	113.34
50	1.05	1.837	.613	175.00	.93	349.99	349.96	3.74	233.35	116.68
60	1.08	1.944	.648	180.00	1.02	359.98	359.96	4.07	240.02	120.01
70	1.11	2.053	.685	184.99	1.11	369.98	369.95	4.42	246.68	123.35
80	1.14	2.166	.722	189.99	1.20	379.98	379.94	4.79	253.35	126.68
90	1.17	2.281	.761	194.98	1.29	389.97	389.94	5.18	260.02	130.02
400	1.20	2.400	.800	199.98	1.40	399.97	399.93	5.58	266.69	133.36
10	1.23	2.521	.841	204.98	1.50	409.96	409.92	6.01	273.36	136.69
20	1.26	2.646	.882	209.98	1.62	419.96	419.91	6.46	280.03	140.03
30	1.29	2.773	.925	214.98	1.74	429.96	429.90	6.94	286.70	143.37
40	1.32	2.904	.968	219.98	1.86	439.95	439.89	7.43	293.37	146.70
50	1.35	3.037	1.013	224.98	1.98	449.95	449.87	7.95	300.04	150.04
60	1.38	3.174	1.058	229.97	2.13	459.94	459.86	8.49	306.72	153.38
70	1.41	3.313	1.105	234.97	2.27	469.93	469.84	9.06	313.39	156.72
80	1.44	3.456	1.152	239.96	2.41	479.92	479.83	9.65	320.06	160.06
90	1.47	3.601	1.201	244.96	2.57	489.92	489.81	10.27	326.74	163.40
500	1.50	3.750	1.250	249.96	2.72	499.90	499.79	10.91	333.41	166.74

TABLE XI. — Spiral Functions for a Change of 0.4° per 100 FEET. Suitable for Speeds of 83 Miles an Hour or Less, or Curves of 2.0° or Less

L	D	Δ	A	Z	0	С	X	Y	U	V
	۰	•								
10	0.04	0.002	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.08	.008	.003	10.00	.00	20.00	20.00	.00	13.33	6.67
30_	.12	.018	.006	15.00	.00	30.00	30.00	.00	20.00	10.00
40	.16	.032	.011	20.00	.00	40.00	40.00	.01	26.67	13.33
50	.20	.050	.016	25.00	.00	50.00 60.00	50.00 60.00	.02	33.33	16.67
60	.24	.072	.024	30.00	.01			.03	40.00	20.00
70	. 28	.098	. 033	35.00	.01	70.00	70.00	.04	46.67	23.33
80	.32	. 128	.043	40.00	.0I .02	80.00 90.00	80.00 90.00	. o6 . o8	53.33 60.00	26.67 30.00
90	. 36		.054							
100	.40	.200	.067	50.00	.03	100.00	100.00	.12	66.67	33.33
10	-44	.242	.081	55.00	.04	110.00	110.00	. 16	73.33	36.67
20	. 48	.288	.096	60.00	. 05	120.00	120.00	.20	80.00	40.00
30	.52	.338	.113	65.00	.06	130.00	130.00	.26	86.67	43.33
40	.56	.392	.131	70.00	.08	140.00	140.00	.32	93.33	46. 6 7
50	.60	.450	.150	75.00	.10	150.00	150.00	-39	100.00	50.00
60	.64	.512	.171	80.00	.12		160.00	.48		53.33
70	. 68	.578	. 193	85.00	. 14	170.00	170.00	.57	113.33	56.67
80	.72 .76	.648	.216	90.00	. 17	180.00	180.00	.68 .80	120.00	60.00
90		.722	.241	95.00						63.33
200	.80	.800	. 267	100.00	23	200.00	200.00	.93	133.33	66.67
10	.84	.882	. 294	105.00	. 27	210.00	210.00	1.08	140.00	70.00
20	.88	.968	. 323	110.00	.31	220.00	219.99	1.24	146.67	73.33
30	.92	1.058	-353	115.00	-35	230.00	229.99	1.41	153.34	76.67
40	.96	1.152	. 384	120.00	.40	240.00	239.99	1.61	160.00	80.00
50	I.00	1.250	.417	125.00	.46	250.00	249.99	1.82	166.67	83.34
60	1.04	1.352	.451	130.00	.51	259.99	259.98	2.04	173.34	86.67
70	1.08	1.458	.486	135.00	-57	269.99	269.98	2.29	180.01	90.01
80	I.12 I.16	1.568	.523 .561	140.00	.64 .71	279.99 289.99	279.98	2.55	186.67	93.34 96.67
90 300		1.800	.600	144.99			289.97	2.84	193.34	
1	1.20			149.99	.79	299.99	299.97	3.14	200.01	100.01
10	I.24	1.922	.641	154.99	.86	309.98	309.97	3.47	206.68	103.34
20	1.28 1.32	2.048 2.178	.683	159.99 164.99	.95 1.05	319.98	319.96	3.81	213.35	106.68
30	-				}	329.98	329.95	4.18		
40	1.36	2.312	.771 .817	169.99	1.14	339.98	339.95	4.57	226.68	113.35
50 60	1.44	2.450 2.592	.864	174.98	1.25	349.97 359.97	349.94 359.93	4.99	233.36	116.69
70	1.44			184.98	1 -			5.43		
80	1.40	2.738 2.888	.913 .963	189.98	1.48	369.96 379.96	369.91 379.90	5.89 6.38	246.69 253.37	123.36 126.70
90	1.56	3.042	1.014	194.98	1.72	389.95	389.89	6.90	260.04	130.03
400	1.60	3.200	1.067	199.97	1.86	399.94	399.88		266.71	133.37
10	1.64							7.44		
20	1.68	3.362 3.528	1.121	204.97	2.00	409.94 419.93	409.86	8.02 8.61	273.38 280.06	136.71
30	1.72	3.528	I.233	214.96	2.15 2.3I	419.93	429.82	9.25	286.73	143.39
40	1.76	3.872	1.291	219.96	2.48	439.91	439.80	9.23	293.41	145.39
50	1.70	4.050	1.350	224.95	2.40	439.91	439.80	10.60	300.08	150.07
60	1.84	4.030	1.330	229.95	2.83	459.89	459.75	11.32	306.76	153.41
70	1.88	4.418	1.473	234.95	3.02	469.88	469.72	12.07	313.43	156.75
80	1.92	4.608	I.533	239.94	3.02	479.87	479.69	12.86	313.43	160.10
90	1.96	4.802	1.601	244.93	3.42	489.85	489.66	13.68	326.79	163.44
500	2.00	5.000	1.667	249.93	3.63	499.84		ļ ———		166.79
900	2.00	5.000	1.007	249.93	3.03	1 499.84	499.62	14.54	333.47	100.79

TABLE XII. — SPIRAL FUNCTIONS FOR A CHANGE OF 0.5° PER 100
FEET. SUITABLE FOR SPEEDS OF 77 MILES AN HOUR OR
LESS, OR CURVES OF 2.0° OR LESS

L	D	Δ	A	Z	0	С	X	Y	U	V
	۰	0	•							
10	0.05	0.002	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.10	.010	.003	10.00	.00	20.00	20.00	.00	13.33	6.67
30	. 15	.025	.008	15.00	.00	30.00	30.00	.00	20.00	10.00
40	.20	.040	.013	20.00	.00	40.00	40.00	.01	26.67	13.33
50	. 25	.062	.021	25.00	.00	50.00	50.00	.02	33.33	16.67
60	.30	.090	. 030	30.00	.01	60.00	60.00	.03	40.00	20,00
70	.35	.122	.041	35.00	.01	70.00	70.00	.05	46.67	23.33
80	.40	. 160	.053	40.00	.02	80.00	80.00	.07	53.33	26.67
90	. 45	. 202	. 067	45.00	.03	90.00	90.00	.11	60.00	30.00
100	. 50	. 250	.083	50.00	. 04	100.00	100.00	.15	66.67	33.33
10	- 55	. 302	.10I	55.00	.05	110.00	110.00	. 19	73.33	36.67
20	.60	. 360	.120	60.00	. 06	120.00	120.00	. 25	80.00	40.00
30	.65	. 422	.141	65.00	.08	130.00	130.00	.32	86.67	43.33
40	.70	. 490	. 163	70.00	. 10	140.00	140.00	. 40	93.33	46.67
50	.75	. 562	.187	75.00	. 12	150.00	150.00	49	100.00	50.00
60	.80	. 640	.213	80.00	.15	160.00	160.00	.60	106.67	53.33
70	.85	.722	.241	85.00	. 18	170.00	170.00	.71	113.33	56.67
80	.90	.810	. 270	90.00	. 21	180.00	180.00	.85	120.00	60.00
90	- 95	. 902	.301	95.00	. 25	190.00	189.99	1.00	126.67	63.33
200	I.00	1.000	.333	100.00	. 29	200.00	199.99	1.16	133.34	66.67
10	.05	1.102	. 367	105.00	.34	210.00	209.99	1.35	140.00	70.00
20	. 10	1.210	. 403	110.00	. 39	220.00	219.99	1.55	146.67	73.34
30	. 15	1.322	.441	115.00	- 44	230.00	229.99	1.77	153.34	76.67
40	. 20	I.440	.480	120.00	. 50	239.99	239.99	2.01	160.01	80.00
50	.25	1.562	.521	125.00	.57	249.99	249.98	2.27	166.67	83.34
60	. 30	1.690	. 563	129.99	.64	259.99	259.98	2.56	173.34	86.67
70	. 35	1.822	.607	134.99	.72	269.99	269.97	2.86	180.01	90.01
80	.40	1.960	. 653	139.99	.80	279.99	279.97	3.19	186.68	93.34
90	- 45	2.102	.701	144.99	. 88	289.98	289.96	3.55	193.35	96.68
300	I.50	2.250	.750	149.99	. 98	299.98	299.96	3.93	200.02	100.01
10	- 55	2.402	.801	154.99	1.08	309.98	309.95	4.33	206.69	103.35
20	.60	2.560	.853	159.98	1.19	319.97	319.94	4.76	213.36	106.69
30	.65	2.722	. 907	164.98	1.31	329.97	329.93	5.23	220.02	110.02
40	.70	2.890	.963	169.98	1.43	339.96	339.92	5.72	226.70	113.36
50	.75	3.062	1.021	174.98	1.56	349.96	349.90	6.23	233.37	116.70
60	.80	3.240	1.080	179.97	1.70	359.95	359.88	6.78	240.04	120.03
70	.85	3.422	1.141	184.97	1.84	369.94	369.87	7.37	246.71	123.38
80	.90	3.610	1.203	189.97	2.00	379.94	379.85	7.98	253.39	126.71
90	. 95	3.802	1.267	194.96	2.16	389.93	389.83	8.63	260.06	130.05
400	2.00	4.000	1.333	199.96	2.33	399.92	399.81	9.30	266.74	133.40

TABLE XIII. — SPIRAL FUNCTIONS FOR A CHANGE OF 0.75° PER 100 FEET. SUITABLE FOR SPEEDS OF 67 MILES AN HOUR OR LESS, OR CURVES OF 3.0° OR LESS

L	D	Δ	A	z	o	С	X	Y	U	V
	-		-							
10	0.075	0.004	0.001	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	. 150	.015	.005	10.00	.00	20.00	20.00	.00	13.33	6.67
30	. 225	.034	.012	15.00	.00	30.00	30.00	.01	20.00	10.00
40	.300	.o6c	.020	20.00	.00	40.00	40.00	.01	26.67	13.33
50	.375	.094	.031	25.00	.01	50.00	50.00	.03	33.33	16.67
60	. 450	. 135	.045	30.00	.01	60.00	60.00	.05	40.00	20.00
70	. 525	. 184	.061	35.00	.02	70.00	70.00	.07	46.67	23.33
8o	.600	. 240	.080	40.00	.03	80.00	80.00	.11	53.33	26.67
90	.675	.304	.101	45.00	.04	90.00	90.00	. 16	60.00	
100	.750	.375	. 125	50.00	.06	100.00	100.CO	.22	66.67	33.33
10	.825	. 454	. 151	55.00	.07	110.00	110.00	. 29	73.33	36.67
20	.900	.540	.180	60.00	.09	120.00	120.00	. 38	80.00	40.00
30	.975	.634	.211	65.00	.12	130.00	130.00	. 48	86.67	43.33
40	1.050	.735	.245	70.00	.15	140.00	140.00	.60	93.33	46.67
50	1.125	.844	.281	75.00	. 18	150.00	150.00	.74	100.00	50.00
60	1.200	.960	. 320	80.00	.22	160.00	160.00	.89	106.67	53.33
70	1.275	1.084	.361	85.00	. 27	170.00	169.99	1.07	113.33	56.67
80	1.350	1.215	.405	90.00	. 32	180.00	179.99	1.27	120.00	60.00
90	1.425	1.354	.451	95.00	.37	189.99	189.99	1.50	126.67	63.34
200	1.500	1.500	. 500	100.00	.44	199.99	199.99	1.75	133.34	66.67
10	1.575	1.654	.551	104.99	.51	209.99	209.98	2.02	140.01	70.01
20	1.650	1.815	.605	109.99	. 58.	219.99	219.98	2.32	146.67	73.34
30	1.725	1.984	.661	114.99	.66	229.99	229.97	2.65	153.34	76.68
40	1.800	2.160	.720	119.99	.73	239.99	239.97	3.02	160.01	80.01
50	1.875	2.344	.781	124.99	.85	249.98	249.96	3.41	166.68	83.34
60	1.950	2.535	. 845	129.99	.96	259.98	259.95	3.84	173.35	86.68
70	2.025	2.734	.911	134.98	1.07	269.97	269.94	4.30	180.02	90.02
80	2.100	2.940	.980	139.98	1.20	279.97	279.93	4.79	186.69	93.36
90	2.175	3.154	1.051	144.98	1.33	289.96	289.91	5.32	193.37	96.69
300	2.250	3.375	1.125	149.97	1.47	299.96	299.90	5.86	200.04	100.03
10	2.325	3.604	1.201	154.97	1.63	309.95	309.88	6.50	206.71	103.37
20	2.400	3.840	1.280	159.97	1.79	319.94	319.86	7.15	213.38	106.71
30	2.475	4.084	1.361	164.96	1.96	329.93	329.83	7.84	220.06	110.04
40	2.550	4.335	1.445	169.96	2.14	339.92	339.81	8.57	226.73	113.39
50	2.625	4.594	1.531	174.95	2.34	349.90	349.78	9.35	233.41	116.74
60	2.700	4.860	1.620	179.94	2.54	359.88	359.74	10.17	240.09	120.09
70	2.775	5.134	1.711	184.93	2.76	369.87	369.70	11.04	246.77	123.43
80	2.850	5.415	1.805	189.93	2.99	379.85	379.67	11.97	253.45	126.78
90	2.925	5.704	1.901	194.92	3.24	389.83	389.62	12.93	260.14	130.12
400	3.000	6.000	2.000	199.91	3.49	399.81	399.56	13.95	266.82	138.34
	1		ł		1	1		l		

TABLE XIV. — Spiral Functions for a Change of 1.0° per 100 Feet. Suitable for Speeds of 61 Miles an Hour or Less, or Curves of 4.0° or Less

L	D	7	A	Z	0	С	X	Y	U	î.
	۰	•	•						:	
10	0.10	0.005	0.002	5.00	0 00	10.00	10.00	.00	6.67	3.33
20	. 20	.020	.007	10.00	.00	20.00	20.00	.00	13 33	6.66
30	. 30	. 045	.015	15.00	.00	30.00	30.00	.01	20.00	10.00
40	.40	.080	.027	20.00	.00	40.00	40.00	.02	26.67	13.33
50	. 50	.125	.042	25.00	.01	50.00	50.00	.01	33.33	10.67
60	.60	.180	.060	30.00	.02	60.00	60.00	.06	40.00	20.00
70	.70	. 245	.082	35.00	.03	70.00	70.00	.10	46.67	23.33
80	.80	. 320	.107	40.00	.03	80.00	80.00	. 15	53.33	26.67
90	.90	.405	. 135	45.00	.05	90.00	90.00	.21	60.00	30.00
100	1.00	.500	. 167	50.00	.07	100.00	100.00	.29	66.67	33.33
10	1.10	.605	. 202	55.00	.10	110.00	110.00	.39	73.33	36.67
20	I.20	.720	. 240	60.00	.13	120.00	120.00	.50	80.00	40.00
30	1.30	.845	. 282	65.00	.16	130.00	130.∞	.64	86.67	43.33
40	1.40	.980	. 327	70.00	. 20	140.00	140.00	.80	93.34	46.67
50	1.50	1.125	.375	75.00	. 25	150.00	149.99	. 98	100.00	50.00
60	1.60	1.280	. 427	80.00	. 30	160.00	159.99	1.19	106.67	53.34
70	1.70	I.445	.482	85.00	. 36	169.99	169.99	I.43	113.34	56.67
80	1.80	1.620	. 540	90.00	.42	179.99	179.99	1.70	120.00	60.00
90	1.90	1.805	.602	94.99	. 50	189.99	189.98	1.99	126.67	63.34
200	2.00	2.000	.667	99.99	. 58	199.99	199.98	2.33	133.34	66.67
10	2.10	2.205	.735	104.99	.67	209.99	209.97	2.69	140.CI	70.01
20	2.20	2.420	.807	109.99	.77	219.98	219.96	3.10	146.68	73.35
30	2.30	2.645	.882	114.99	.89	229.98	229.95	3.54	153.35	76.68
40	2.40	2.880	.960	119.98	1.01	239.97	239.94	4.02	160.02	80.02
50	2.50	3.125	1.042	124.98	I.14	249.97	249.93	4.54	166.69	83.36
60	2.60	3.380	1.127	129.97	1.28	259.96	259.91	5.11	173.37	86.70
70	2.70	3.645	1.215	134.97	1.43	269.95	269.89	5.72	180.04	90.03
80	2.80	3.920	1.307	139.97	1.60	279.94	279.87	6.38	186.71	93.37
90	2.90	4.205	I.402	144.96	1.77	289.93	289.85	7.09	193.39	96.72
300	3.00	4.500	1.500	149.95	1.96	299.92	299.82	7.85	200.06	100.06
10	3.10	4.805	1.602	134.95	2.16	309.90	309.78	8.66	206.74	103.40
20	3.20	5.120	1.707	159.94	2.38	319.89	319.75	9.53	213.42	106.75
30	3.30	5 - 445	1.815	164.93	2.61	329.87	329.70	10.44	220.10	110.09
40	3.40	5.780	1.927	169.92	2.86	339.85	339.66	II.42	226.79	113.44
50	3.50	0.125	2.042	174.91	3.12	349.82	349.60	12.46	233 - 47	116.80
60	3.60	6.480	2.160	179.89	3.39	359.80	359.54	13.56	240.16	120.15
70	3.70	6.845	2.282	184.88	3.68	369.77	369.47	14.71	246.85	123.50
80	3.80	7.220	2.407	189.87	3.99	379.73	379.40	15.94	253 - 54	126.86
90	3.90	7.605	2.535	194.85	4.31	389.70	389.32	17.23	260.24	130.22
400	4.00	8.000	2.667	199.84	4.65	399.66	399.22	18.59	266.94	133.58
	1							1		

TABLE XV. — SPIRAL FUNCTIONS FOR A CHANGE OF 13° PER 100 FEET. SUITABLE FOR A SPEED OF 55 MILES AN HOUR OR LESS, OR CURVES OF 4.0° OR LESS

L	D	7	A	Z	0	С	X	Y	U	V
_	•	•	•							
10	0.133	0.007	0.002	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	. 267	.027	.009	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.400	.060	.020	15.00	.00	30.00	30.00	.CI	20.00	10.00
40	- 533	.107	.036	20.00	.01	40.00	40.00	.02	26.67	13.33
50	.667	.167	.056	25.00	.01	50.00	50.00	.05	33.33	16.67
60	.800	. 240	.080	30.00	.02	60.00	60.00	.08	40.00	20.00
70	.933	.327	.109	35.00	.03	70.00	70.00	.13	46.67	23.33
8o	1.067	.427	. 142	40.00	.05	80.00	80.00	. 20	53.33	26.67
· 9o	1.200	.540	. 180	45.00	.07	90.00	90.00	. 28	60.00	30.00
100	1.333	.667	,222	50.00	. 10	100.00	100.00	. 39	66.67	33.33
10	1.467	.807	. 269	55.00	. 13	110.00	110.00	. 52	73.33	36.67
10	1.600	.960	.320	60.00	. 17	120.00	120.00	.67	80.00	40.00
30	1.733	1.127	.376	65.00	.21	130.00	129.99	.85	86.67	43.34
40	1.867	1.307	.436	70.00	. 27	140.00	139.99	1.06	93.34	46.67
50	2,000	1.500	. 500	74.99	-33	150.00	149.99	1.31	100.00	50.00
60	2.133	1.707	. 569	79.99	.40	159.99	159.99	1.59	106.67	53.34
70	2.267	1.927	. 642	84.99	.48	169.99	169.98	1.91	113.34	56.67
8o	2.400	2.160	.720	89.99	-57	179.99	179.97	2.26	120.01	60.01
90	2.533	2.407	.802	94.99	.66	189.98	189.97	2.66	126.68	63.34
200	2.667	2.667	.889	99.98	.78	199.98	199.96	3.10	133.35	66.68
10	2.800	2.940	.980	104.98	.90	209.97	209.94	3.59	140.02	70.02
20	2.933	3.227	1.076	109.98	1.03	219.97	219.93	4.12	146.69	73-35
30	3.067	3.527	1.176	114.97	1.18	229.95	229.91	4.71	153.36	76.69
40	3.200	3.840	1.280	119.97	1.34	239.95	239.89	5.35	160.04	80.03
50	3 - 333	4.167	1.389	124.96	1.51	249.94	249.87	6.05	166.72	83.38
60	3.467	4.507	I.502	129.95	1.70	259.93	259.84	6.81	173.39	86.72
70	3.600	4.860	1.620	134.95	1.91	269.91	269.81	7.62	180.07	90.06
80	3 733	5.227	1.742	139.94	2.13	279.90	279.77	8.50	186.75	93.41
90	3.867	5.607	1.869	144.94	2.36	289.88	289.72	9.43	193.43	96.76
300	4.000	6.000	2.000	149.92	2.61	299.86	299.67	10.46	200.12	100.11

TABLE XVI. — SPIRAL FUNCTIONS FOR A CHANGE OF 1.5° PER 100 FEET. SUITABLE FOR SPEEDS OF 53 MILES AN HOUR OR LESS, OR CURVES OF 4.5° OR LESS

L	D	Δ	A	Z	o	c	X	Y	U	V
	•	۰								
10	0.15	0.008	0.002	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.30	. 030	.010	10.00	.00	20.00	20.00	.00	13.33	6.67
30	- 45	.068	.022	15.00	.00	30.00	30.00	.01	20.00	10.00
40	.60	.120	. 0.10	20,00	.01	40.00	40.00	.03	26.67	13.33
50	.75	. 188	.062	25.00	.01	50.00	50.00	.05	33.33	16.67
6о	.90	. 270	.090	30.00	.02	60.00	60.00	.09	40.00	20.00
70	1.05	. 368	.122	35.00	.04	70.00	70.00	.15	46.67	23.33
80	1.20	.480	.160	40.00	.06	80.00	80.00	.22	53.33	26.67
90	1.35	.608	.202	45.00	.08	90.00	90.00	.32	60.00	30.CO
100	1.50	.750	. 250	50.00	. 11	100.00	100.00	.44	66.67	33.33
10	1.65	.908	.302	55.00	. 15	110.00	110.00	.58	73.33	36.67
20	1.80	1.080	.360	60.00	.13	120.00	120.00	.75	80.00	40.00
30	1.95	1.268	.422	65.00	.24	130.00	129.99	.96	86.67	43.34
						_		_		46.67
40	2.10	1.470	. 490 . 562	69.99	.30	140.00	139.99	1.20	93.34 100.00	50.00
50 60	2.25	1.000	.640	74.99 79.99	.45	149.99 159.99	149.99	I.47 I.79	106.67	53.34
								Name		
70	2.55	2.168	.722	84.99	-54	169.99	169.97	2.14	113.34	56.67
80	2.70	2.430	.810	89.99	.64	179.99	179.97	2.54	120.01	60.01
90	2.85	2.708	.902	94.98	-75	189.98	189.96	2.99	126.68	63.35
200	3.00	3.000	1.000	99.98	.87	199.98	199.95	3.49	133.35	66.68
10	3.15	3.308	1.102	104.98	1.01	209.97	209.93	4.04	140.02	70.02
20	3.30	3.630	1.210	109.97	1.16	219.96	219.91	4.64	146.70	73.36
30	3.45	3.968	1.322	114.96	1.33	229.95	229.89	5.30	153.37	76.70
40	3.60	4.320	1.440	119.96	1.51	239.94	239.87	6.03	160.05	80.04
50	3.75	4.688	1.562	124.95	1.70	249.93	249.83	6.81	166.73	83.39
60	3.90	5.070	1.690	129.94	1.92	259.91	259.80	7.66	173.41	86.73
70	4.05	5.468	1.822	134.93	2.15	269.89	269.76	8.58	180.09	90.08
8o	4.20	5.880	1.960	139.92	2.39	279.87	279.71	9.55	186.77	93.43
90	4.35	6.308	2.102	144.91	2.66	289.85	289.65	10.61	193.46	96.78
300	4.50	6.750	2.250	149.90	2.94	299.82	299.59	11.77	200.15	100.13
1										

TABLE XVII. — Spiral Functions for a Change of 2.0° per 100 Feet. Suitable for a Speed of 48 Miles an Hour OR Less, and Curves of 6.0° or Less

L	D	Δ	A	z	o	С	X	Y	U	V
	•	•	•							
10	0.20	0.010	0.003	5.00	0.00	10.00	10.00	0.00	6.97	3.33
20	.40	.040	.013	10.00	.00	20.00	20.00	.00	13.33	6.67
30	.60	.090	.030	15.00	.00	30.00	30.00	.02	20.00	10.00
40	.80	.160	.053	20.00	.01	40.00	40.00	.04	26.67	13.33
50	1.00	.250	.083	25.00	.02	50.00	50.00	.07	33.33	16.67
6o	.20	.360	.120	30.00	.03	60.00	60.00	.13	40.00	20.00
70	.40	.490	. 163	35.00	.05	70.00	70.00	.20	46.67	23.33
80	.60	.640	.213	40.00	.07	80.00	80.00	.30	53.33	26.67
90	.80	.810	.270	45.00	.11	90.00	90.00	.42	60.00	30.00
100	2.00	1.000	-333	50.00	.14	100.00	100.00	. 58	66.67	33.33
10									<u>_</u>	36.67
20	.20	I.210 I.440	.403	55.00 59.99	.19	110.00	109.99	1.00	73.33 80.00	40.00
30	.60	1.690	.563	64.99	.34	129.99	129.99	1.28	86.67	43.34
_										
40	.80	1.960	.653	69.99	.40	139.99	139.98	1.60	93.34	46.67
50 60	3.00	2.250 2.560	.750	74.99 79.98	.49 .60	149.99	149.98	1.96 2.38	100.01	50.01
00	.20	_	.853			159.99	159.97		100,08	53.34
70	.40	2.890	.963	84.98	.71	169.98	169.96	2.86	113.35	56.68
8 o	.60	3.240	1.080	89.98	.85	179.97	179.94	3.39	120.02	60.02
90	.80	3.610	1.203	94.97	1.00	189.97	189.93	3.99	126.69	63.36
200	4.00	4.000	1.333	99.96	1.16	199.96	199.90	4.65	133.37	66.70
10	.20	4.410	1.470	104.96	1.35	209.95	209.88	5.38	140.04	70.04
20	.40	4.840	1.613	109.95	1.55	219.93	219.84	6.19	146.72	73.38
30	.60	5.290	1.763	114.94	1.77	229.91	229.80	7.07	153.40	76.73
40	.80	5.760	1.920	119.93	2.01	239.89	239.76	8.03	160.09	80.08
50	5.00	6.250	2.083	124.91	2.27	249.87	249.70	9.08	166.77	83.43
60	.20	6.760	2.253	129.90	2.55	259.84	259.64	10.21	173.46	86.78
70	.40	7.290	2.430	134.88	2.86	269.81	269.57	11.44	180.15	90.14
8o	.60	7.840	2.613	139.86	3.19	279.77	279.48	12.75	186.85	93.50
90	.80	8.410	2.802	144.84	3.54	289.73	289.38	14.17	193.55	96.87
300	6.00	9.000	2.999	149.81	3.92	299.68	299.26	15.68	200.26	100.24

TABLE XVIII. — SPIRAL FUNCTIONS FOR A CHANGE OF 2.5°
PER 100 FEET. SUITABLE FOR SPEEDS OF 45 MILES AN
HOUR OR LESS, AND CURVES OF 7.5° OR LESS

L	D	Δ	A	Z	0	С	X	Y	U	V
		•	•							
10	0.25	0.012	0.004	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.50	.050	.017	10.00	.00	20.00	20.00	.01	13.33	6.67
30	.75	.112	.037	15.00	.00	30.00	30.00	.02	20.00	10.00
40	1.00	. 200	.067	20.00	.01	40.00	40.00	.05	26.67	13.33
50	.25	. 312	. 104	25.00	.02	50.00	50.00	.09	33.33	16.67
6 o	.50	. 450	.150	30.00	.04	60.00	60.00	. 16	40.CO	20.00
70	.75	.612	. 20.1	35.00	.c6	70.00	70.00	.21	46.67	23.33
8o	2.00	. 800	. 267	40.00	.09	80.00	80.00	.37	53.33	26.67
90	.25	1.012	- 337	45.00	.13	90.00	90.00	53	60.00	30.00
100	. 50	1.250	.417	50.00	. 18	100.00	100.00	.73	66.67	33.34
10	.75	1.512	.504	54.99	.24	110.00	109.99	.97	73.34	36.67
20	3.00	1.800	.600	59.99	.31	120.00	119.99	1.26	80.00	40.00
30	. 25	2.112	. 704	64.99	.40	129.99	129.98	1.60	86.67	43.34
40	.50	2.450	.817	69.98	.50	139.99	139.97	2.00	93.34	46.67
50	- 75	2.812	.937	74.98	.61	149.98	149.96	2.45	100.01	50.01
60	4.00	3.200	1.067	79.98	.74	159.98	159.95	2.98	106.68	53.35
70	.25	3.612	I.204	84.97	.89	169.97	169.93	3.57	113.36	56.69
8o	.50	4.050	1.350	89.96	1.06	179.96	179.91	4.24	120.03	60.03
90	.75	4.512	1.504	94.95	1.25	189.95	189.88	4.99	126.71	63.37
200	5.00	5.000	1.667	99.94	1.45	199.93	199.85	5.81	133.39	66.72
10	.25	5.512	1.837	104.93	1.68	209.91	209.81	6.73	140.07	70.06
20	.50	6.050	2.017	109.92	1.93	219.89	219.76	7.74	146.76	73.41
30	.75	6.612	2.204	114.90	2.21	229.87	229.70	8.84	153.44	76.76
40	6.00	7.200	2.400	119.89	2.51	239.83	239.62	10.04	160.13	80.12
50	.25	7.812	2.604	124.86	2.84	249.80	249.54	11.35	166.83	83.48
60	.50	8.450	2.816	129.84	3.19	259.75	259.44	12.76	173.53	86.85
70	.75	9.112	3.036	134.81	3.57	269.70	269.32	14.29	180.24	90.22
80	7.00	9.800	3.266	139.78	3.98	279.64	279.19	15.93	186.96	93.60
90	.25	10.512	3.503	144.75	4.42	289.57	289.03	17.69	193.68	96.98
300	7.50	11.250	3.749	149.71	4.89	299.49	298.85	19.58	200.41	100.37

TABLE XIX. — SPIRAL FUNCTIONS FOR A CHANGE OF 3.0° PER 100 FEET. SUITABLE FOR SPEEDS OF 41 MILES AN HOUR OR LESS, AND CURVES OF 9.0° OR LESS

L	D	Δ	A	z	0	С	X	Y	U	V
	•	•	•							
10	0.30	0.015	0.005	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.60	.060	.020	10.00	.00	20.00	20.00	.01	13.33	6.67
30	.90	.135	.045	15.00	.01	30.00	30.00	.02	20.00	10.∞
40	1.20	.240	.080	20.00	.01	40.00	40.00	.06	26.67	13.33
50	.50	.375	.125	25.00	.03	50.00	50.00	.11	33.33	16.67
60	.80	. 540	. 180	30.00	.05	60.∞	60.00	.19	40.00	20.00
70	2.10	.735	. 245	35.00	.07	70.00	70.00	.30	46.67	23.33
80	.40	.960	.320	40.00	.11	80.00	80.00	.45	53.34	26.67
90	.70	1.215	. 405	45.00	.16	90.00	90.00	.64	60.00	30.00
100	3.00	1.500	. 500	49.99	.22	100.00	99.99	.87	66.67	33.34
10	.30	1.815	.605	54.99	.29	109.99	109.99	1.16	73.34	36.67
20	.60	2.160	.720	59.99	.36	119.99	119.98	1.51	80.01	40.01
30	.90	2.535	.845	64.98	.48	129.99	129.98	1.92	86.67	43.34
40	4.20	2.940	.980	69.98	.60	139.98	139.96	2.39	93.35	46.68
50	.50	3.375	1.125	74.97	.74	149.98	149.95	2.94	100.02	50.02
60	.80	3.840	1.280	79.97	.89	159.97	159.93	3.57	106.69	53.36
70	5.10	4.335	1.445	84.96	1.07	169.96	169.90	4.28	113.37	56.70
80	.40	4.860	1.620	89.95	1.27	179.94	179.87	5.08	120.05	60.04
90	.70	5.415	1.805	94.93	1.49	189.92	189.83	5.98	126.73	63.39
200	6.00	6.000	2.000	99.92	1.74	199.90	199.78	6.98	133.41	66.74
10	. 30	6.615	2.205	104.90	2.02	209.88	209.72	8.06	140.10	70.09
20	. 60	7.260	2.420	109.88	2.32	219.85	219.65	9.26	146.79	73.45
30	.90	7.935	2.645	114.86	2.65	229.81	229.56	10.59	153.49	76.81
40	7.20	8.640	2.879	119.83	3.01	239.76	239.46	12.04	160.19	80.17
50	.50	9.375	3.124	124.80	3.40	249.71	249.34	13.60	166.90	83.55
60	.80	10.140	3.379	129.77	3.82	259.64	259.19	15.30	173.62	86.93
70	8.10	10.935	3.644	134.73	4.28	269.57	269.03	17.11	180.35	90.32
80	.40	11.760	3.919	139.69	4.77	279.48	278.83	19.08	187.08	93.71
90	. 70	12.615	4.203	144.64	5.30	289.39	288.61	21.20	193.83	97.12
300	9.00	13.500	4.498	149.58	5.86	298.70	298.35	23.47	200.59	100.54

TABLE XX. — SPIRAL FUNCTIONS FOR A CHANGE OF 4.0° PER 100 FEET. SUITABLE FOR SPEEDS OF 35 MILES AN HOUR OR LESS, OR CURVES OF 10.0° OR LESS

L	D	Δ	A	Z	0	C	X	Y	U	V
	-		•			-				
10	0.40	0.020	0.007	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	.80	. 080	.027	10.00	.00	20.00	20.00	.01	13.33	6.67
30	1.20	.180	. 060	15.00	.01	30.00	30.00	.03	20.00	10.00
40	.60	.320	. 107	20.00	.02	40.00	40.00	.07	26.67	13.33
50	2.00	.500	.167	25.00	.04	50.00	50.00	.15	33.33	16.67
60	.40	. 720	.240	30.00	.06	60.00	60.00	.25	40.00	20.00
70	.80	.980	.327	35.00	.10	70.00	70.00	.40	46.67	23.33
8o	3.20	1.280	.427	39.99	.15	80.00	80.00	.60	53.33	26.67
90	.60	1.620	. 540	44.99	.21	90.00	89.99	.85	60.00	30.00
100	4.00	2.000	. 667	49.99	. 29	99.99	99.99	1.16	66.67	33.34
10	. 40	2.420	.807	54.98	. 39	109.99	109.98	1.55	73.33	36.67
20	.80	2.880	.960	59.98	.50	119.99	119.97	1.84	80.01	40.01
30	5.20	3.380	1.127	64.97	.64	129.98	129.95	2.56	86.68	43.35
40	.60	3.920	1.307	69.96	.80	139.97	139.93	3.19	93.36	46.69
50	6.00	4.500	1.500	74.95	.98	149.96	149.91	3.93	100.03	50.03
60	.40	5.120	1.707	79.94	1.19	159.94	159.87	4.76	106.71	53.37
70	.80	5.780	1.927	84.92	1.43	169.92	169.83	5.71	113.40	56.72
8o	7.20	6.480	2.160	89.90	1.77	179.90	179.77	6.78	120.08	60.08
90	.60	7.220	2.407	94.88	1.99	189.87	189.70	7.97	126.77	63.43
200	8.00	8.000	2.667	99.86	2.32	199.83	199.61	9.30	133.47	66.79
10	.40	8.820	2.939	104.83	2.68	209.78	209.51	10.76	140.18	70.16
20	.80	9.680	3.222	109.79	3.09	219.72	219.38	12.38	146.89	73.54
30	9.20	10.580	3.526	114.75	3.52	229.66	229.22	14.11	153.61	76.92
40	.60	11.520	3.839	119.70	4.00	239.57	239.03	16.03	160.34	80.31
250	10.00	12.500	4.165	124.65	4.52	249.48	248.82	18.12	167.09	83.72

TABLE XXI. — Spiral Functions for a Change of 5.0° per 100 Feet. Suitable for Speeds of 32 Miles an Hour or Less, or Curves of 12.5° or Less

L	D	Δ	A	Z	0	c	X	Y	U	v
	•	•	•			-				
10	0.50	0.025	0.008	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	1.00	.100	.033	10.00	ૂે.00	20.00	20,00	.01	13.33	6.67
30	.50	.225	.075	15.00	.01	30.00	30.00	.04	20.00	10.00
40	2.00	.400	.133	20.00	.02	40.00	40.00	.09	26.67	13.33
50	.50	.625	.208	25.00	.05	50.00	50.00	.18	33.33	16.67
60	3.00	.900	. 300	30.00	.08	60.00	60.00	.31	40.00	20.00
70	.50	1.225	. 408	34.99	.13	70.00	70.00	.50	46.67	23.33
80	4.00	1.600	.533	39.99	.19	80.00	79.99	.74	53 - 34	26.67
90	.50	2.025	.675	44.99	.27	90.00	89.99	1.06	60.00	30.00
100	5.00	2.500	.833	49.98	.36	99.99	99.98	1.45	66.67	33.34
10	.50	3.025	1.008	54.97	.48	109.99	109.97	1.93	73.34	36.68
20	6.00	3.600	1.200	59.97	.63	119.98	119.95	2.51	80.02	40.02
30	.50	4.225	1.408	64.95	.80	129.97	129.93	3.19	86.69	43.36
40	7.00	4.900	1.633	69.94	1.00	139.96	139.90	3.99	93.37	46.70
50	.50	5.625	1.875	74.92	1.20	149.94	149.86	4.90	100.05	50.05
60	8.00	6.400	2.133	79.90	1.48	159.91	159.80	5.94	106.74	53.40
70	.50	7.225	2.408	84.88	1.78	169.88	169.73	7.13	113.43	56.75
8o	9.00	8.100	2.699	89.85	2.11	179.84	179.64	8.46	120.13	60.12
90	.50	9.025	3.008	94.82	2.48	189.79	189.53	9.95	126.83	63.48
200	10.00	10.000	3.332	99.78	2.90	199.73	199.40	11.61	133.55	66.86
10	.50	11.025	3.674	104.73	3.35	209.66	209.23	13.41	140.27	70.25
20	11.00	12.100	4.032	109.67	3.82	219.57	219.04	15.42	147.01	73.65
30	.50	13.225	4.406	114.61	4.40	229.46	228.79	17.62	153.76	77.06
40	12.00	14.400	4.797	119.54	5.99	239.34	238.50	20.02	160.54	80.49
250	12.50	15.625	5.205	124.46	5.64	249.18	248.16	22.62	167.32	83.94

TABLE XXII.—Spiral Functions for a Change of 7.5°

PER 100 FEET. SUITABLE FOR A SPEED OF 26 MILES AN

HOUR OR LESS, OR A CURVE OF 18.0° OR LESS

20 I.50 .1500 .050 10.00 .00 20.00 20.00 .02 13 30 2.25 .3375 .113 15.00 .01 30.00 30.00 .06 20 40 3.00 .6000 .200 20.00 .03 40.00 40.00 .14 26 50 3.75 .9375 .313 25.00 .07 50.00 50.00 .27 33 60 4.50 1.3500 .450 29.99 .12 60.00 60.00 .47 40 70 5.25 1.8375 .613 34.99 .19 70.00 69.99 .75 46	00 10.00 67 13.33
20 I.50 .1500 .050 10.00 .00 20.00 20.00 .02 13 30 2.25 .3375 .113 15.00 .01 30.00 30.00 .06 20 40 3.00 .6000 .200 20.00 .03 40.00 40.00 .14 26 50 3.75 .9375 .313 25.00 .07 50.00 50.00 .27 33 60 4.50 1.3500 .450 29.99 .12 60.00 60.00 .47 40 70 5.25 1.8375 .613 34.99 .19 70.00 69.99 .75 46	33 6.67 00 10.00 67 13.33
30 2.25 .3375 .113 15.00 .01 30.00 30.00 .06 20. 40 3.00 .6000 .200 20.00 .03 40.00 40.00 .14 26. 50 3.75 .9375 .313 25.00 .07 50.00 50.00 .27 33. 60 4.50 1.3500 .450 29.99 .12 60.00 60.00 .47 40. 70 5.25 1.8375 .613 34.99 .19 70.00 69.99 .75 46.	33 6.67 00 10.00 67 13.33
40 3.00 .6000 .200 20.00 .03 40.00 40.00 .14 26. 50 3.75 .9375 .313 25.00 .07 50.00 50.00 .27 33. 60 4.50 1.3500 .450 29.99 .12 60.00 60.00 .47 40. 70 5.25 1.8375 .613 34.99 .19 70.00 69.99 .75 46.	67 13.33
50 3.75 .9375 .313 25.00 .07 50.00 50.00 .27 33. 60 4.50 1.3500 .450 29.99 .12 60.00 60.00 .47 40. 70 5.25 1.8375 .613 34.99 .19 70.00 69.99 .75 46.	.
60 4.50 1.3500 .450 29.99 .12 60.∞ 60.∞ .47 40. 70 5.25 1.8375 .613 34.99 .19 70.∞ 69.99 .75 46.	33 16.67
70 5.25 1.8375 .613 34.99 .19 70.∞ 69.99 .75 46.	
	20.00
	67 23.34
80 6.00 2.4000 .800 39.98 .28 79.99 79.99 1.12 53.	34 26.67
90 6.75 3.0375 1.013 44.97 .40 89.99 89.97 1.59 60.	01 30.01
100 7.50 3.7500 1.250 49.96 .54 99.98 99.96 2. 18 66.	68 33.35
10 8.25 4.5375 1.513 54.94 .71 109.97 109.93 2.90 73.	36 36.69
20 9.00 5.4000 1.800 59.92 .94 119.95 119.89 3.77 80.	04 40.03
30 9.75 6.3375 2.113 64.90 1.19 129.93 129.84 4.78 86.	72 43.38
40 10.50 7.3500 2.450 69.86 1.49 139.90 139.77 5.98 93.	41 46.74
50 11.25 8.4375 2.812 74.83 1.83 149.86 149.68 7.35 100.	11 50.10
60 12.00 9.6000 3.199 79.78 2.22 159.80 159.55 8.92 106.	83 53.48
70 12.75 10.8375 3.612 84.73 2.66 169.73 169.40 10.67 113.	55 56.86
80 13.50 12.1500 4.049 89.66 3.15 179.64 179.20 12.66 120.	29 60.26
90 14.25 13.5375 4.511 94.59 3.51 189.54 188.95 14.89 127.	63.68
200 15.00 15.000 4.997 99.50 4.32 199.40 198.64 17.37 133.	82 67.11
10 15.75 16.5375 5.509 104.40 4.99 209.23 208.27 19.86 140.	52 70.57
20 16.50 18.1500 6.045 109.27 5.73 219.03 217.82 22.72 147.	45 74.05
30 17.25 19.8375 6.607 114.13 6.54 228.79 227.28 25.91 154.	31 77.56
240 18.00 21.6000 7.192 118.97 7.41 238.51 236.63 30.01 161.	22 81.11

TABLE XXIII. — Spiral Functions for a Change of 10.0°
PER 100 FEET. SUITABLE FOR SPEEDS OF 22 MILES AN
HOUR OR LESS, OR CURVES OF 25.0° OR LESS

·	1 _	1	1	Ī	1			1		
L	D	Δ	A	Z	0	C	X	Y	U	V
	۰	•	•							
10	1.00	0.050	0.017	5.00	0.00	10.00	10.00	0.00	6.67	3.33
20	2.00	.200	.067	10.00	.01	20.00	20.00	.02	13.33	6.67
30	3.00	.450	. 150	15.00	.02	30.00	30.co	.c8	20.00	10.00
40	4.00	.800	.267	20.00	.05	40.00	40.00	.19	26.67	13.33
50	5.00	1.250	.417	24.99	.09	50.00	50.00	.36	33.33	16.67
60	6.00	1.800	.600	29.98	.16	60.00	59.99	.63	40.00	20.00
70	7.00	2.450	.817	34.98	.25	69.99	69.99	.98	46.67	23.34
8o	8.00	3.200	1.067	39.96	.37	79.99	79.97	1.49	53.34	26.67
90	9.00	4.050	1.350	44.95	-53	89.98	89.96	2.12	60.02	30.01
100	10.00	5.000	1.667	49.92	.72	99.97	99.92	2.91	66.69	33.36
10	11.00	6.050	2.017	54.89	.98	109.95	109.88	3.87	73.38	36.71
20	12.00	7.200	2.400	59.86	1.25	119.92	119.81	5.02	80.07	40.06
30	13.00	8.450	2.816	64.81	1.59	129.88	129.72	6.38	86.77	43.42
40	14.00	9.800	3.266	69.76	1.98	139.82	139.59	7.97	93.48	46.80
50	15.00	11.250	3.749	74.69	2.43	149.74	149.43	9.78	100.20	50.19
60	16.00	12.80C	4.265	79.61	2.95	159.65	159.21	11.87	106.95	53.59
70	17.00	14.450	4.814	84.52	3.53	169.53	168.93	14.21	113.72	57.01
8o	18.00	16,200	5.396	89.40	4.18	179.37	178.57	16.87	120.45	60.47
90	19.00	18.050	6.012	94.26	4.91	189.18	188.13	19.78	127.34	63.94
200	20.00	20,000	6.660	99.11	5.71	198.93	197.59	23.07	134.20	67.46
10	21.00	22.050	7.341	103.92	6.69	208.64	206.93	26.60	141.11	71.01
20	22.00	24.200	8.055	108.71	7.56	218.28	216.13	30.59	148.07	74.62
30	23.00	26.450	8.802	113.46	8.51	227.86	225.17	34.77	155.09	78.27
40	24.00	28.800	9.580	118.18	9.76	237.35	234.04	39.50	162.18	82.00
250	25.∞	31.250	10.392	122.86	10.99	246.75	242.70	44.67	169.36	85.79
	1				1		-			

CHAPTER III

LOGARITHMS AND TRIGONOMETRIC FUNCTIONS

TABLE XXIV. — Common Logarithms of Numbers

USE OF THE TABLE OF LOGARITHMS The logarithm of a number is the exponent denoting the power to

which some fixed base number must be raised to equal the number whose logarithm is considered. There are two base numbers in use. but almost all operations are performed by one system, known as Common Logarithms, in which the base is 10. The logarithm of 1 in any system is o because any number raised to the o power is I. Thus $\frac{x^1}{x^1} = x^{1-1} = x^0 = 1$. The logarithm of 10 in the common system is 1; of 100, 2; of 1000, 3; etc., since $10^1 = 10$, $10^2 = 100$, $10^3 = 1000$, etc. Numbers between I and IO, IO and IOO, IOO and IOOO, etc., will have fractional logarithms. Thus, the logarithm of 8 is 0.90309; of 13 is 1.11394; of 126 is 2.10037, etc., since $10^{0.90309} = 8$, $10^{1.11394} = 13$, $10^{2.10037}$ = 126, etc. The fraction is called the mantissa and is always the same for the same sequence of figures and is incommensurable, being given to 3, 5, 6, 7, or 10 decimal places, according to the precision required. Thus $\log 1.263 = 0.10140$; $\log 12.63 = 1.10140$; and $\log 126.3 =$ 2.10140, all of 5 decimal places. The whole number, called the characteristic, varies. The characteristic is always I less than the number of digits to the left of the decimal point of the number whose logarithm is being found. In the tables only the mantissas are given. The whole number must be known by the computer from the number of digits in the number whose logarithm is wanted.

To find the logarithm of a number look in the table for the mantissa and prefix the proper characteristic, determined from the number of digits to the left of the decimal point in the number in question. Thus, on page 76, line 27, we find the mantissa for the sequence 1263 in the fifth column to be 0.10140; then for 1.263 the log is 0.10140; for 12.63 and 126.3 as given above.

In the table the first three figures of a four-figure number appear in the first column, the fourth figure at the heads of the 10 numbered columns. The first two figures of the mantissa appear in the second column, the last three in the column under the fourth digit of the number whose logarithm is sought. If the first two figures change in going across the page, that fact is indicated by an asterisk; which, to economize space, stands for the first two figures of the second column in the *line below the asterisk*. Thus, the logarithm of 1445 (see p. 76) is 3.15987, while that of 1446 is 3.16017. For numbers of 3 figures or less, the mantissa is found in the column headed 0, since the mantissas for 1, 10, 100, or for 2, 20, 200, or for 15, 150, 1500, etc., are respectively the same.

The logarithm of a number of more than four figures is found as indicated in the following example: What is the log of 382.568? On page 81, line 33, columns 2 and 7, find log 382.5 to be 2.58263. Note that log 382.6 is 2.59274, a difference of 11 in the log for a difference of I in the last place of the sequence in the number. Assuming that the log increases in proportion to the number, the log of 382.568 may be said to be $\frac{68}{100}$ of 11 larger than log 382.5 since 382.568 is $\frac{68}{100}$ of 1 in the last place (the place of the 5) greater than 382.5. To facilitate this computation, a table of proportional parts is found alongside the log Thus, in the case just given, for a difference of II we find, from the table of proportional parts, that an increase of 0.6 of one in the last place of the number makes a difference in the log of 6.6, an increase of 0.08 in the number increases the log by 0.88, found by moving the decimal point I digit to the left in the tabular value for 0.8, so that an increase of 0.68 of 1 in the last place increases the log of 382.5 by 6.6 + 0.88, or 7.48; or, since we make the fifth figure the nearest whole number, we find $\log 382.568 = 2.58263 + 7 = 2.58270$.

To find the number corresponding to a given logarithm we reverse the process. Thus, the number corresponding to the logarithm 2.58270 is found as follows: The next smaller mantissa is 0.58263 for the sequence 3825 and it is smaller than 0.58270 by 7. The difference for a whole unit in the last place is 11 and in the table of proportional parts under 11 find 6.6, corresponding to 0.6 of 1 in the last place of the number, as the next smaller difference to 7, leaving still a difference of 7-6.6=0.4 to be used, which, by moving the decimal point one digit to the left, is found to correspond most nearly to 0.04 of 1 in the last place of the number. Therefore, the whole number is 382.564. But we found that 2.58270 is the logarithm of 382.568. We see by this that this table cannot be depended on to give more than a sequence of 5 significant

figures correctly. This is true of all tables of logarithms: that as many significant figures in sequence may be correctly determined as there are decimal places in the tabular mantissas. A 5-place table gives five significant figures, a 6-place table, six significant figures, etc.

To multiply a by b we add the logarithms of a and b, written $\log a$ and $\log b$, and find the number corresponding to the sum.

To divide a by b, we subtract $\log b$ from $\log a$ and find the number corresponding to the difference.

It may often occur in computations that the fifth place in a resulting logarithm, found by adding two or more logarithms, may be in error by one unit, thus making the quantity determined certain to one less significant figure than the number of places in the logarithm.

To find the product a^2b^3 . Find the logarithm of a and multiply it by 2; find the logarithm of b and multiply it by 3; add the two results for the logarithm of the product and find the corresponding number. Thus:

```
What is the product 1.2^2 \times 4.3^3?

p. 76, line 21, col. 2, log 1.2 = 0.07918 \times 2 = 0.15836

p. 82, line 31, col. 2, log 4.3 = 0.63347 \times 3 = 1.90041

p. 76, line 15, col. 6 and 7 = 2.05877 = \log 114.49.

Ans.
```

This example, checked by a 7-place table, gives the same result to the fifth significant figure even though both logarithms were multiplied and then added.

The following example, worked by 5-place and 7-place logarithms, shows the uncertainty of the last figure in computations made by any set of tables, by showing the uncertainty of the fifth figure in the computations made with the 5-place tables. Required the product $1.65^2 \times 1.8^3$.

$$\begin{array}{c} 5\text{-Place} \\ \text{Log 1.65} = 0.21748 \times 2 = 0.43496 \\ \text{Log 1.8} = 0.25527 \times 3 = \underbrace{0.76581}_{1.20077} = \log 15.877. \quad \text{Ans.} \\ 7\text{-Place} \\ \text{Log 1.65} = 0.2174839 \times 2 = 0.4349678 \\ \text{Log 1.8} = 0.2552725 \times 3 = \underbrace{0.7658175}_{1.2007853} = \log 15.8776. \quad \text{Ans.} \end{array}$$

Thus 15.878 is nearer right than 15.877, although the error of the latter is only about 0.6 of one in the last place and the error of the former is

about 0.4 of one in the last place. Greater differences can occur so that the fifth place is not certain within I unit.

Logarithms of fractions. The logarithm of $I = \frac{10}{10} = I0^{1-1} = I0^0$ is 0.00000. Similarly the logarithm of 0.1 = $\frac{1}{10}$ = 100-1 is -1.00000; the logarithm of $\frac{1}{100}$ is -2; of $\frac{1}{1000}$ is -3; etc. Therefore, if the sequence is all fractional the characteristic is minus and with a numerical value expressed by the number of the place on the right of the decimal point in which the first significant figure appears. Thus the logarithm of 0.00126 is -3 + 0.10037, usually written $\overline{3}.10037$. The mantissa is not minus, only the characteristic is minus. This sometimes gives the beginner trouble, but need not if he remembers that the mantissa is always plus, while the characteristic is plus or minus according as the number corresponding is equal to or greater than I or is less than I, and that in general the two must be treated separately. The following examples will make the use of the signs clear:

Required the product 43.0×0.43 .

Required the product 43.0×0.43^2 .

Log
$$43.0 = 1.63347$$
 Log $0.43^2 = \overline{1}.63347 \times 2$ Log $0.43^2 = \overline{1}.26694$ Log $7.951 = 0.90041$ Log $0.43^2 = \overline{1}.26694 = \overline{1}.26694$

Required the product 43.0 \times 0.43\frac{1}{2}.

Log
$$0.43^{\frac{1}{2}} = \overline{1}.816735$$
 found thus: Add 10 to the characteristic and subtract 10 before dividing by 2, getting
$$1.45021 = 1.45021$$
 Log $0.43^{\frac{1}{2}} = \overline{1}.816735 - 5$, or $\overline{1}.816735$.

Instead of adding and subtracting 10 in the preceding example, only enough may be added and subtracted to make the negative characteristic divisible by the divisor. Thus: In the foregoing example add and subtract I, getting $\frac{\overline{1.63347} - 1 + 1}{2} = \frac{\overline{2} + 1.63347}{2} = \overline{1.816735}$, before, without the necessity of considering the 4 and -5. If the 1/3 power has been required, the divisor would have been 3, and 2 should be added and subtracted getting $\frac{\overline{1.63347} - 2 + 2}{2} = \frac{\overline{3} + 2.63347}{2}$

= 1.877823 +. This work need not be written out in full in an exam-

ple, as the computer can see the figures mentally. Thus, he knows the characteristic will be $\overline{\mathbf{I}}$ so he writes this down and then imagines a 2, or whatever number is to be added, at the left of the decimal and at once writes down the quotient after the $\overline{\mathbf{I}}$. In handling very small numbers when the negative characteristic is large, it may be necessary to write out the operation to guard against error.

In making the tables, when the remainder after the fifth figure was more than 0.5, the fifth figure was increased by 1; when less than 0.5, the fifth figure was not changed.

When the computer is finding a logarithm, and the operation brings a 5 in the place following the last place of the table (as the sixth place when using the tables of this book) and the 5 is followed by ciphers, a good rule to adopt is to make the last place the nearest *even* number. Thus in getting log 0.43^{1/2} in the example above we add 5 in the sixth place. This rule will tend to balance inaccuracies in a long series of computations.

To divide 3.68×4.21 we find (page 81) log 3.68 = 0.56585 (page 82) log 4.21 = 0.62428

Now to subtract, we may add and subtract

10 from the log 3.68, getting 10.56585 - 10 0.62428

 $\frac{0.02428}{9.94157 - 10} = \overline{1.94157}$

or, we may add the arithmetical complement of log 4.21 instead of subtracting the log 4.21. That is, we may multiply by $\frac{1}{4.21}$ instead

of dividing by 4.21. The logarithm of $\frac{1}{4.21}$ is 0.00000 - 0.62428, or

1.37572 and is called the arithmetical complement of the log 4.21. It is the logarithm of the reciprocal of 4.21. In a series of operations, where several factors are to be multiplied and the product divided by the product of several factors, the arithmetical complements of the divisor factors are used to avoid the double operation of two additions and one subtraction, since the arithmetical complements may be written down from the logs almost as readily as the logs themselves. Each digit of the mantissa of the log is subtracted from 9 except the last, which is subtracted from 10. The characteristic is negative and one greater than the characteristic of the log when the log characteristic is positive; and is positive and one less than the characteristic of the log if that characteristic is negative. Thus:

Log 8.364 is 0.92241; its complement is **7.07759** Log 83.64 is 1.92241; its complement is **2.07759** Log 836.4 is 2.92241; its complement is $\overline{3}$.07759 Log 0.8364 is $\overline{1}$.92241; its complement is 0.07759 Log 0.08364 is $\overline{2}$.92241; its complement is 1.07759

Instead of thinking of the characteristic by the rule above, the log may be subtracted from 10 instead of zero when a characteristic of 9 in the complement will correspond to $\overline{1}$; 8 to $\overline{2}$, etc. And the computer can as readily think of 9 as indicating that the first significant figure of the result is in the first or tenths' place of the decimal; 8, that it is in the second or hundredths' place, etc., and this will cause no confusion unless very large quantities are being dealt with, so that the 8 or 9 might sometimes be a positive characteristic not standing in the place of a $\overline{2}$ or $\overline{1}$; but this difficulty is not likely to arise in using 5- or 6-place tables, since such tables would not be used with such large numbers.

When the first figures are small. When the first three figures of a number of five or more places are between 100 and 110 inclusive use pages 94 and 95, which give 7-place logarithms for five digits directly.

N	L	0	ı	2	3	4	5	6	7	8	9	1	PP	
100	00	000	043	087	130	173	217	260	303	346	389			
101		432	475	518	561	604	647	689	732	775	817	44	43	42
102	١.	860	903	945	988	*030	*072	*115	*157	*199	*242	- 12	40	***
103	01	284	326	368	410	452	494	536	578	620	662	I 4.4	4.3	4.2
104	02	703	745 160	· 787	828	870 281	912	953	995	*036	*078	2 8.8 3 I3.2	8.6 12.9	8.4
105 106	02	119 531	572	612	243 6 5 3	694	325 735	366 776	407 816	449 857	490 898	4 17.6	17.2	16.8
107		938	979	*019	*060	*100	*141	*181	*222	*262	*302	5 22.0	21.5 25.8	2I.0 25.2
108	0,3		383	423	463	503	543	583	623	663	703	7 30.8	30.I	29.4
109		743	782	822	862	902	941	981	*021	*060	*100	8 35.2	34·4 38.7	33.6
110	04	139	179	218	258	297	336	376	415	454	493	9 39.6	30.7	37.8
111		532	571	610	650	689	727	766	805	844	883	41	40	39
112		922	961	999	*038	*077	*115	*154	*192	*231	*269	41	40	39
113	05	308	346	385	423	461	500	538	576	614	652	1 4.1	4.0	3.9
114	- 6	690	729	767	805	843	881	918	956	994	*032	2 8.2 3 I2.3	8.0	7.8 II.7
115	o 6		108	145	183	221	258	296	333	371	408	4 16.4	16.0	15.6
		446 810		521 893	558	595	633	670	707	744	781	5 20.5	20.0	19.5
117	07	188	856 225	262	930	967 335	*004 372	*041 408	*078 445	*115 482	*151 518	7 28.7	28.0	23.4 27.3
110	٠,	555	591	628	661	700	737	773	800	846	882	8 32.8	32.0	31.2
120		918	954	990	*027	*063	*099	*135	*171	*207	*243	9 36.9	36.0	35.I
121	08	279	314	350	386	422	458	493	529	565	600	38	37	36
122	•0	636	672	707	743	778	814	849	884	920	955	**	31	30
123		991	*026	*061	*096	*132	*167	*202	*237	*272	*307	1 3.8	3.7	3.6
124	09	342	377	412	447	482	517	552	587	621	656	2 7.6 3 II.4	7.4 II.I	7.2
125		691	726	760	795	830	864	899	934	968	*003	4.15.2	14.8	14.4
126	10	037	072	100	140	175	209	243	278	312	346	5 19.0	18.5	18.0 21.6
127		380	415	449	483	517	551	585	619	653	687	7 26.6	25.9	25.2
128		721	755	789 126	823 160	857	890	924	958	992	*025	8 30.4	29.6	28.8
129 130	11	059	093			193	227	261	294	$\frac{327}{661}$	361	9 34.2	33.3	32.4
(394	428	461	494	528	561	594	628		694	35	34	33
131 132	т 2	727 057	760 090	793 123	826	860 189	893	926	959 287	992 320	*024	""	34	33
133	12	385	418	450	156 483	516	548	254 581	613	646	352 678	1 3.5	3.4	3.3
134		710	743	775	808	840	872	905	937	969	*001	2 7.0 3 IO.5	6.8 10.2	6.6 9.9
135	13	033	066	098	130	162	194	226	258	290	322	4 14.0	13.6	13.2
136	,	354	386	418	450	481	513	545	577	600	640	5 17.5 6 21.0	17.0 20.4	16.5 19.8
137		672	704	735	767	799	830	862	893	925	956	7 24.5	23.8	23.I
138		988	*019	*051	*082	*114	*145	*176	*208	*239	*270	8 28.0	27.2	26.4
139	14	301	333	364	395	426	457	489	520	551	582	9 31.5	30.6	29.7
140		613	644	675	706	737	768	799	829	860	891	32	31	30
141		922	953	983	*014	*045	*076	*106	*137	*168	*198	""	01	50
142	15	229	259 564	290	320 625	351	381 685	412 715	442 746	473 776	503 806	I 3.2 2 6.4	3.I 6.2	3.0 6.0
. 1		534 836	866	594	- 1	655	987	*017	*047	*077	*107	2 6.4	9.3	9.0
144	τ6	137	167	897	927	957 256	286	316	346	376	406	4.12.8	12.4	12.0
146	10	435	465	495	524	554	584	613	643	673	702	5 I6.0 6 I9.2	15.5 18.6	15.0 18.0
147		732	761	701	820	850	879	900	938	967	997	7 22.4	21.7	21.0
148	17	026	056	085	114	143	173	202	231	260	289	8 25.6 0 28.8	24.8 27.9	24.0 27.0
149		319	348	377	406	435	464	493	522	_55I	580	9:20.0	27.9	27.0
150	17	609	863	667	696	725	754	782	811	840	869			
N	L	0		2	3	4	5	6	7	8	9		PΡ	

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150	17 60		667	696	725	754	782	811	840	869	29 28
151	89		955	984	*013	*041	*070	*099	*127	*156	
152 153	18 18. 46		241 526	270 554	298 583	327 611	355 639	384 667	412 696	44I 724	1 2.9 2.8 2 5.8 5.6
154	75		808	837	865	893	Q2I	949	977	*005	3 8.7 8.4
155	19 03		080	117	145	173	201	220	257	285	4 II.6 II.2 5 I4.5 I4.0
156	31		368	396	424	451	479	507	535	562	6 17.4 16.8
157	59		645	673	700	728	756	783	811	838	7 20.3 19.6 8 23.2 22.4
158	86		921	948	976	*003	*030	*058	*085	*112	9 26.I 25.2
159	20 140		194	222	249	276	303	330	358	385	
160	41:		466	493	520	548	575	602	629	656	27 26
161 162	68; 95:		737 *005	763 *032	790 *059	817 *085	844 *112	871 *139	898 *165	925 *192	I 2.7 2.6
163	21 21	245	272	299	325	352	378	405	431	458	2 5.4 5.2
164	48	1	537	564	590	617	643	669	696	722	3 8.1 7.8 4 10.8 10.4
165	74	775	801	827	854	880	906	932	958	985	5 13.5 13.0
166	22 01	1	o 63	089	115	141	167	194	220	246	6 16.2 15.6 7 18.9 18.2
167 168	27:		324	350	376	401	427	453	479	505	7 18.9 18.2 8 21.6 20.8
169	53 78		583 840	608 866	634 891	660 917	686 943	712 968	737 994	763 *019	9 24.3 23.4
170	23 04		096	121	147	172	198	223	249	274	
171	300		350	376	401	426	452	477	502	528	25
172	55		603	629	654	679	704	729	754	779	I 2.5
173	80		855	880	905	930	955	980	*005	*030	2 5.0
174	24 05		105	130	155	180	204	229	254	279	3 7.5 4 10.0
175	30.		353	378	403	428	452	477	502	527	5 12.5
176	55		100	625	650	674	699	724	748	773	
177	79°		846 091	871	895 139	920 164	944 188	969 212	993 237	*018 261	8 20.0
179	28		334	358	382	406	431	455	479	503	9 22.5
180	52		575	600	624	648	672	696	720	744	04 00
181	768	_	816	840	864	888	912	935	959	983	24 23
182	26 00	031	055	079	102	126	150	174	198	22I	I 2.4 2.3
183	24.		293	316	340	364	387	411	435	458	2 4.8 4.6 3 7.2 6.9
184	48:		529	553	576	600	623	647	670	694	4 9.6 9.2
185 186	71 95		764 998	788 *021	811 *045	834 *o 68	858 *091	881 *114	905 *138	928 *161	5 12.0 11.5 6 14.4 13.8
187	27 18		231	254	277	300	323	346	370	393	7 16.8 16.1
188	410	439	462	485	508	531	554	577	600	623	8 19.2 18.4 9 21.6 20.7
189	640	669	692	715	738	761	784	807	830	852	2
190	87		921	944	967	989	*012	*035	*0 58	*081	22 21
191	28 10		149	171	194	217	240	262	285	307	
192 193	339		375 601	398 623	421 646	443 668	466	488	511	533	I 2.2 2.I 2 4.4 4.2
193	550 780		825	847	870	802	691	713	735 959	758 081	3 6.6 6.3
194	29 00		048	070	092	115	914 137	937 159	181	203	4 8.8 8.4 5 II.O IO.5
196	220		270	292	314	336	358	380	403	425	6 13.2 12.6
197	44		491	513	535	557	579	601	623	645	7 15.4 14.7 8 17.6 16.8
198	66		710	732	754	776	798	820	842	863	9 19.8 18.9
199	88.	-1	929	951	973	994	*016	*038	*060	*081	
200	30 10		146	168	190	211	233	255	276	298	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	L	0	-1	2	3	4	5	6	7	8	9	PP
200	30	103	125	140	168	190	211	233	255	276	298	
201		320	341	363	384 600	406 621	428 643	449 664	471 685	492	514	22 21
202		535 750	557 771	578 792	814	835	856	878	899	707	728	I 2.2 2.I 2 4.4 4.2
204		963	984	*006	*027	*048	*069	*091	*112	*133	*154	3 6.6 6.3
205	31	175	197	218	239	260	281	302	323	345	366	4 8.8 8.4 5 II.0 IO.5
206		387	408	429	450	471	492	513	534	555	576	6 13.2 12.6
207		597 806	618 827	639 848	66 o 86 o	681 890	702 911	723 931	744	765	785	7 15.4 14.7 8 17.6 16.8
200	32	015	035	056	077	098	118	130	100	973 181	994 201	9 19.8 18.9
210		222	243	263	284	305	325	346	366	387	408	
211		428	449	409	490	510	531	552	572	593	613	20
212		634	654	675	695	715	736	756	777	797	818	I 2.0
213		838	858	879 082	899	919	940	960	980	*001	*C2I	2 4.0 3 6.0
214	33	04I 244	264	284	304	325	345	163 365	385	203	224 425	4 8.0
216		445	465	486	506	526	546	566	586	606	626	5 10.0 6 12.0
217		646	666	686	706	726	746	766	786	806	826	7 14.0 8 16.0
218	2.4	o11 846	866 064	885 084	001	925	945	965	985 183	*005	*025	9 18.0
220	34	212	262	282	301	321	143 341	361	380	203	120	
221		439	459	479	198	518	537	557	577	596	616	19
222		635	655	674	694	713	733	753	772	792	811	I 1.9
223		830	850	869	889	908	928	947	967	986	*005	2 3.8 3 5.7
224	35	025	044	064	083	102	I 2 2	141	160	180	199	4 7.6
225		218 411	238 430	257 449	276 468	295 488	315	334 526	353 545	372 564	392 583	5 9.5 6 II.4
227		603	622	641	660	679	608	717	736	755	774	7 13.3
228		793	813	832	851	870	889	908	927	946	965	8 15.2 9 17.1
229		984	*003	*02I	*010	*019	*078	*097	*116	*135	*154	
230	36	173	192	211	229	248	267	286	305	324	342	18
231		361 549	380 568	399 586	418 605	436 624	455 642	474 661	493 680	511 608	717	1 1.8
232 233		736	754	773	791	810	829	847	866	884	903	2 3.6 3 5.4
234		922	940	959	977	996	*011	*033	*051	*070	*088	4 7.2
235	37	107	125	144	162	181	199	218	236	254	273	5 9.0 6 10.8
236		291	310	328	346	365	383	101	420	438	457	7 12.6
237 238		475 658	493 676	511	530 712	548 731	566 749	585 767	603 785	621 803	639 822	8 14.4 9 16.2
239		840	858	876	894	912	931	949	967	985	*003	
240	38	C 2 I	039	057	075	093	II2	130	148	166	184	17
241		202	220	238	256	274	292	310	328	346	364	1 1.7
242 243		382 561	399 578	417 596	435 614	453 632	47I 650	489 668	5 9 7 686	525 703	543 721	2 3.4
243		739	757	775	792	810	828	846	863	881	899	3 5.1 4 6.8
245		917	934	952	970	987	*005	*023	*011	*058	*076	5 8.5 6 10.2
246	39	091	III	129	146	164	182	199	217	235	252	7 11.9
247		270	287	305	322	340	358	375	393	410	428	8 13.6 9 15.3
248		445	463 637	480 655	498 672	515 690	533	550 724	568 742	585 759	602 777	9 1 13.3
250	30	794	811	829	846	863	881	898	915	933	950	
N	L			2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
250	39 794		829	846	863	881	898	915	933	950	
251	967	985	*002	*019	*037	*054	*071	*088	*106	*123	18
252	40 140		175	192	381	226	243	261	278	295	I 1.8
253	312		346	364	"	398	415	432	449	466	2 3.6 3 5.4
254 255	483 654	500 671	518	535 705	552 722	739	586 756	603 773	620 700	807	4 7.2
256	824	841	858	875	892	909	926	943	960	976	5 9.0 6 10.8
257	993	*010	*027	*044	*061	*078	*095	*111	*128	*145	7 12.6
258	41 162	179	196	212	,229	246	263	280	296	313	8 14.4 9 16.2
259	330	347	363	380	397	414	430	447	464	481	9 10.2
260	497	514	531	547	564	581	597	614	631	647	17
261	664	681	697	714	73 I	747	764	780	797	814	
262	830	847	863	880	896	913	929	946	963	979	I 1.7 2 3.4
263	996	*012	*029	*045	*062	*078	*095	*111	*127	*144	3 5.1 4 6.8
264 265	42 160	177	193	210	226	243 406	259	275	292	308	4 6.8
266	325 488	341 504	357 521	374 537	390 553	570	423 586	439 602	455 619	472 635	5 8.5 6 10.2
267	651	667	684	700	716	732	749	765	781	797	7 11.9
268	813	830	846	862	878	894	911	927	043	959	8 13.6 9 15.3
269	975	991	*008	*024	*040	*056	*072	*088	*104	*120	7 - 3.3
270	43 136	152	169	185	201	217	233	249	265	281	16
271	297	313	329	345	361	377	393	400	425	441	
272	457	473	489	505	521	537	553	569	584	600	I 1.6 2 3.2
273	616	632	648	664	680	696	712	727	743	759	3 4.8
274 275	775 933	791 949	807 965	823 981	838 996	854 *012	870 *028	886 *044	902 *059	917 *075	4 6.4 5 8.0
276	44 091	107	122	138	154	170	185	201	217	232	6 9.6
277	248	264	279	205	311	326	342	358	373	380	7 11.2 8 12.8
278	404	420	436	451	467	483	498	514	529	545	9 14.4
279	560	576	592	607	623	638	654	669	685	700	
280	716	731	747	762	778	793	809	824	840	855	15
281	871	886	902	917	932	948	963	979	994	*010	I 1.5
282 283	45 025 179	040	056 200	225	086	102	117 271	133 286	301	163	2 3.0
284	332	194	362	378	240 393	255 408	423	Į.	454	317 469	3 4.5 4 6.0
285	332 484	347 500	515	530	393 545	561	576	439 591	454 606	621	5 7.5
286	637	652	667	682	697	712	728	743	758	773	6 9.0 7 10.5
287	788	803	818	834	849	864	879	894	909	924	8 12.0
288	939	954	969	984	*000	*015	*030	*045	*060	*075	9 13.5
289	46 090	105	120	135	150	165	180	195	210	225	
290	240	255	270	285	300	315	330	345	359	374	14
29I 292	389	404	419 568	434 583	449 598	464	479 627	494 642	509 657	523 672	1 1.4 2.8
293	538 687	553	716	731	746	761	776	790	805	820	2 2.8 3 4.2
204	835	850	864	879	894	000	923	938	953	967	4 5.6
295	982	997	*012	*026	*041	*056	*070	*085	*100	*114	5 7.0 6 8.4
296	47 129	144	159	173	188	202	217	232	246	261	7 9.8
297	276	290	305	319	334	349	363	378	392	407	8 II.2 9 I2.6
298	422	436	451	465	480	494	500	524	5 3 8 683	553 698	9 12.0
299	567	582	596	611	625	640	654	813	828	842	
300	47 712	727	741	756	770	784	799			_	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	L	0	ı	2	3	4	5	6	7	8	9	PP
300	47	712	727	741	756	770	784	799	813	828	842	
301		857	871	885	900	914	929	943	958	972	986	
302	48	100	015	029	044	058	073	087	101	116	130	
303		144	159	173	187	202	216	230	244	259	273	15
304 305		287 430	302	316 458	330 473	344 487	359 501	373 515	387	401	416	1 1.5
305		572	444 586	601	615	629	643	657	530 671	544 686	558 700	2 3.0
307		714	728	742	756	770	785	799	813	827	841	3 4.5 4 6.0
308		855	869	883	897	911	926	940	954	968	982	5 7.5 6 9.0
309		996	*010	*024	*038	*052	*066	*080	*094	*108	*122	7 10.5
310	49	136	150	164	178	192	206	220	234	248	262	8 12.0 9 13.5
311 312		276 415	290 429	304 443	318 457	332 471	346 485	36 o 499	374 513	388 527	402 541	9 13.3
313		554	568	582	596	610	624	638	651	665	679	
314		693	707	721	734	748	762	776	790	803	817	
315		831	845	859	872	886	900	914	927	941	955	14
316		969	982	996	*010	*024	*037	*051	*065	*079	*092	1 1.4
317 318	50	106 243	120 256	133	147 284	161 297	174 311	188 325	338	352	229 365	2 2.8 3 4.2
319		379	393	406	420	433	447	461	474	488	501	4 5.6
320		515	529	542	556	569	583	596	610	623	637	5 7.0 6 8.4
321		651	664	678	691	705	718	732	745	759	772	7 9.8
322		786	799	813	826	840	853	866	880	893	907	8 II.2 9 I2.6
323		920	934	947	961	974	987	*001	*014	*028	*041	
324 325	51	055 188	o68	081	095 228	108	255	135 268	148	162 295	175 308	
326		322	335	348	362	375	388	402	415	428	441	
327		455	468	481	495	508	521	534	548	561	574	13
328		587	601	614	627	640	654	667	680	693	706	I I.3 2 2.6
329 330		720	733	746	759	772	786	799	812	825	838	3 3.9
		851	865	878	891 *022	904	917	930 *061	943	957 *o88	970	4 5.2 5 6.5
33I 332	52	983	996	*000	153	*035 166	*048	192	*075 205	218	231	6 7.8
333	3-	244	257	270	284	297	310	323	336	349	362	7 9.1 8 10.4
334		375	388	401	414	427	440	453	466	479	492	9 11.7
335		504	517	530	543	556	569	582	595	608	621	
336		763	776	780	673 802	686 815	827	711	724 853	737 866	750 879	
337 338		802	905	017	930	943	956	969	982	994	*007	12
339	53	020	033	046	058	071	084	097	110	122	135	I I.2
340		148	161	173	186	199	212	224	237	250	263	2 2.4
341		275	288	301	314	326	339	352	364	377	390	3 3.6 4 4.8
342 343		403 529	415 542	428 555	567	453 580	466 593	479 605	491 618	504 631	517 643	5 6.0
344		656	668	681	604	706	719	732	744	757	769	
345		782	794	807	820	832	845	857	870	882	895	8 9.6
346		908	920	933	945	958	970	983	995	*008	*020	9 10.8
347	54	033	045	058	070	083	095	108	120	133	145	
348 349		158 283	170 295	183 307	195 320	332	345	233 357	245 370	382	394	
350	5,1	407	419	432	444	456	469	481	494	506	518	
N	L	0	1	2	3	4	5	6	7	8	9	PP
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350	54 407	419	432	444	456	469	481	494	506	518	
351	531	543	555	568 691	580	593 716	605	617	630	642	
352 353	654 777	790	802	814	704 827	839	728 851	741 864	753 876	765 888	13
354	900	913	925	937	949	962	974	986	998	*011	
355	55 023	035	047	060	072	084	096	108	121	133	2 2.6
356	145	157	169	182	194	206	218	230	242	255	3 3.9 4 5.2
357 358	267 388	279 400	291 413	303 425	315 437	328 449	340 461	35 ² 473	364 485	376	4 5.2 5 6.5 6 7.8
359	509	522	534	546	558	570	582	594	606	497 618	6 7.8 7 9.1
360	630	642	654	666	678	691	703	715	727	739	8 10.4
361	751	763	775	787	799	811	823	835	847	859	9 11.7
362 363	871 991	883 *003	895 *015	907 *027	919	931	943 *062	955	967 * o 86	979	
364	56 110	122	134	146	*038	*050 170	182	*074	205	*098 217	
365	229	241	253	265	277	289	301	312	324	336	12
366	348	360	372	384	396	407	419	431	443	455	I I.2
367	467	478	490	502	514	526	538	549	561	573	2 2.4 3 3.6
368 369	585 70 3	597 714	608 726	620 738	750	644 761	773	785	679 797	691 8 0 8	4 4.8
370	820	832	844	855	867	879	801	902	914	926	5 6.0 6 7.2
371	937	949	961	972	984	996	*008	*010	*031	*043	7 8.4
372	57 054	066	078	089	101	113	124	136	148	159	8 9.6 9 10.8
373	171	183	194	206	217	229	241	252	264	276	
374 375	287 403	299 415	310 426	322 438	334 449	345 461	357 473	368 484	380 496	392 507	
376	519	530	542	553	565	576	588	600	611	623	
377	634	646	657	669	68 o	692	703	715	726	738	11
378	749	761	772 887	784	795	807	818	830	841	852	I I.I 2 2.2
379 380	86 ₄ 978	990	*001	898 *013	910 *024	921 *035	933	944 *058	955 *070	967 *081	3 3.3
381	58 092	104	115	127	138	149	*047 161	172	184	195	4 4.4 5 5.5 6 6.6
382	206	218	229	240	252	263	274	286	297	309	6 6.6
383	320	331	343	354	365	377	388	399	410	422	7 7.7 8 8.8
384	433	444	456	467	478	490	501	512	524	535	9 9.9
385 386	546 659	557 670	569 681	580 692	591 704	602 715	726	737	636 749	760	
387	771	782	794	805	816	827	838	850	861	872	
388	883	894	906	917	928	939	950	961	973	984	10
389 390	995	*006	*017	*028	*040	*051	*062	*073	*084	*095	1 1.0
391	59 <u>106</u> 218	118	129	140	262	162	173	184	195	207	2 2.0 3 3.0
391	329	340	240 351	251 362	373	273 384	395	295 4 0 6	306 417	318 428	4 4.0
393	439	450	461	472	483	494	506	517	528	539	5 5.0 6 6.0
394	550	561	572	583	594	605	616	627	638	649	7 7.0 8 8.0
395 396	660 770	780	682 701	693 802	704 813	715 824	726 835	737 846	748 857	759 868	9 9.0
397	879	800	901	Q12	923	934	945	956	966	977	
398	988	999	*010	*021	*032	*043	*054	*065	*076	*o86	
399	60 097	108	119	130	141	152	163	173	184	195	
400	60 206	217	228	239	249	260	271	282	293	304	
N	L O	11	2	3	4	5	6	7	8	9	PP

N	L	0	1	2	3	4	5	6	7	8	9	PP
400	60	206	217	228	239	249	260	271	282	293	304	
401		314	325	336	347	358 466	369	379 487	390 498	401 500	412 520	
402 403		423 531	433 541	444 552	455 563	574	477 584	595	606	617	627	V
404		638	649	660	670	681	692	703	713	724	735	
405		746	756	767	778	788	799	810	821	831	842	44
406 407		853	863 970	874 081	885 991	895 *002	906 *013	917 *023	927 *034	938 *045	949 *055	11
407	61	959 066	077	087	098	100	119	130	140	151	162	I I.I 2 2.2
409		172	183	194	20.1	215	225	236	247	257	268	3 3.3
410		278	289	300	310	321	331	342	352	363	374	4 4.4 5 5.5 6 6.6
411 412		384 490	395 500	405 511	416 521	426 532	437 542	448 553	458 563	469 574	479 584	
413		595	606	616	627	637	648	658	669	679	690	7 7.7 8 8.8
414		7∞	711	721	731	742	752	763	773	784	794	9 9.9
415 416		805	920	826	836	847 951	857 962	868 972	982	888 993	899 *003	
417	62	909 014	024	930	941 045	055	066	076	086	097	107	
418		118	128	138	149	159	170	180	190	201	211	
419		221	232	242	252	263	273	284	294	304	315	
420		325	335	346	356	366	377	387	397	408	418 521	10
42I 422		428 531	439 542	449 552	459 562	469 572	480 583	49 0 593	500	511	624	1 1.0
423		634	644	655	665	675	685	696	706	716	726	2 2.0 3 3.0
424		737	747	757	767	778	788	798	808	818	829	4 4.0
425 426		839 941	849 951	859 961	870 972	880 982	992	900 *002	910 *012	92I *022	*033	5 5.0 6 6.0
427	63	043	053	063	073	083	094	104	114	124	134	7 7.0 8 8.0
428		144	155	165	175	185	195	205	215	225	236	9 9.0
429 430		246	256	266	276	286	296	306	317	327 428	337 438	
43I		347 448	357 458	367 468	377 478	387 488	397 498	508	518	528	538	1
431		548	558	568	579	589	599	609	619	629	639	
433		649	659	669	679	689	699	709	719	729	739	
434		749	759	769 860	779 879	789 880	799 899	809	819	929	939	9
435 436		849 949	859 959	969	979	988	998	*008	*018	*028	*038	1 0.9
437	64	048	058	o 68	078	088	098	108	118	128	137	2 1.8
438		147	157	167 266	177	187	197 296	207	316	326	237	
439 440		345	355	365	276 375	385	395	306	414	424	335 434	4 3.6 5 4.5 6 5.4
441		343 444	454	464	473	483	493	503	513	523	532	7 6.3
442		542	552	562	572	582	591	601	611	621	631	8 7.2 9 8.1
443	1	640	650	660	670	680	689	699	709	719 816	729 826	
444 445		738 836	748 846	758 856	768 865	777 875	787 885	797 895	807	914	924	
446		933	943	953	963	972	982	992	*002	*011	*021	
447	65	031	040	050	060	070	079	089	099	108	118	
448 449		128	137 234	147 244	157 254	167	176 273	186	196	302	312	1
450	65	321	331	341	350	360	369	379	389	398	408	
N	L		1	2	3	4	5	6	7	8	9	PP

N	L	0	1	2	3	4	5	6	7	8	9	PP
450	65	321	331	341	350	360	369	379	389	398	40 8	
45I		418	427	437	447	456	466	475	485	495	504	
452		514	523	533	543	552	562	571	581	591	600	
453		610	619	629	639	648	658	667	677	686	696	
454		706	715	725	734	744	753	763	772 868	782	792	
455 456		8 01 896	906	916	925	839	849 944	858 954	963	877 973	887 982	10
		992	*001	*011	*020	935 *o30	*039	*049	*058	*o68	*077	10
457 458	66		001	106	115	124	134	143	153	162	172	I I.O 2 2.0
459		181	191	200	210	210	229	238	247	257	266	3 3.0
460		276	285	295	304	314	323	332	342	351	361	4 4.0
461		370	380	389	398	408	417	427	436	445	455	5 5.0 6 6.0
462		464	474	483	492	502	511	521	530	539	549	7 7.0 8 8.0
463		558	567	577	586	596	605	614	624	633	642	8 8.0 9 9.0
464		652	661	671	68o	689	699	708	717	727	736	9 9.0
465		745	755	764	773	783	792	801	811	820	829	
466		839	848	857	867	876	885	894	904	913	922	
467 468		932 025	941 934	950 043	960 052	969 062	978 071	987 080	997 089	*006 099	*015 108	
469		117	127	136	145	154	164	173	182	191	201	
470		210	210	228	237	247	256	265	274	284	293	
471		302	311	321	330	339	348	357	367	376	385	9
471		394	403	413	422	43I	440	449	459	468	477	1 0.9
473		486	495	504	514	523	532	541	550	560	569	2 1.8 3 2.7
474		578	587	596	605	614	624	633	642	651	660	4 3.6
475	١ ١	669	679	688	697	706	715	724	733	742	752	5 4.5
476		761	770	779	788	797	806	815	825	834	843	6 5.4 7 6.3
477		852	861	870	879	888	897	906	916	925	934	8 7.2
478	68	943	952	961	970 0 61	979	988	997 088	*006	*015	*024	9 8.1
479 480		034	043	052		160	160	178	187		115	
		124	133	142	151			260		196 287	205	
481 482		215 305	224 314	233 323	332	25I 34I	260 350	359	278 368	377	296 386	
483		395	404	413	422	431	440	449	458	467	476	
484		485	494	502	511	520	529	538	547	556	565	
485		574	583	592	601	610	619	628	637	646	655	8
486	l	664	673	681	690	699	708	717	726	735	744	1 o.8
487		753	762	771	780	789	797	806	815	824	833	2 1.6
488		842	851	860	869	878	886	895 984	904	913 *002	922 *011	3 2.4 4 3.2
489 490		931	028	949	958	966	975 064	073	993 082	090	099	5 4.0
	09	020		037		055	152	161	170	179	188	6 4.8 7 5.6
49 I 49 2		108	205	214	135	144 232	241	249	258	267	276	8 6.4
493	1	285	294	302	311	320	329	338	346	355	364	9 7.2
494	1	373	381	390	399	408	417	425	434	443	452	1
495		461	469	478	487	496	504	513	522	531	539	
496		548	557	566	574	583	592	601	600	618	627	i
497	1	636	644	653	662	671	679	688	697	705	714	ļ
498		723 810	732 819	740	749 836	758	767	775 862	784 871	793 880	888	1
499 500	60	897	906	914	923	932	854 940	949	958	966	975	1
N	109 L	0	900	2	3	4	5	6	7	8	9/3	PP
I N	1 -	U		2	ا ا	1 4	0	0	1 '		1 9	

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500	69	897	906	914	923	932	940	949	958	966	975	
501		984	992	*001	*010	*018	*027	*036	*044	*053	*062	\
502	70	070	079	088	096	105	114	122	131	140	148	
503 504		157 243	165 252	174 260	183 260	191 278	286	209	303	312	234 321	
504		329	338	346	355	364	372	381	389	398	406	
506		415	424	432	441	449	458	467	475	484	492	9
507		501	509	518	526	535	544	552	561	569	578	1 0.9
508 50 9		586 672	595 680	68g	612	706	629 714	638 723	646 731	655 740	663 749	2 1.8
510		757	766	774	783	791	800	808	817	825	834	3 2.7 4 3.6
511		842	851	859	868	876	885	893	902	010	919	4 3.0 5 4.5 6 5.4
512		927	935	944	952	961	969	978	986	995	*003	7 6.3
513	71	012	020	029	037	0.16	054	063	071	079	088	8 7.2 9 8.1
514 515		096	189	113	122 206	130	139	147 231	155	164 248	172 257	,,
516		265	273	282	290	299	307	315	324	332	341	
517		349	357	366	374	383	391	399	408	416	425	
518		433	441	450	458	466	475	483 567	492	500	508	- 3.
519 520		517	525 600	533	$\frac{542}{625}$	550 634	559 642	650	575 659	667	592	
52 I		684	602	700	700	717	$\frac{042}{725}$	734	742	750	759	8
522		767	775	784	792	800	809	817	825	834	842	1 0.8
523		850	858	867	875	883	892	900	908	917	925	2 I.6 3 2.4
524		933	941	950	958	966	975	983	991	999	*008	4 3.2
525 526	72	010	024 107	032	04I 123	132	057	148	974 156	165	090	5 4.0 6 4.8
527		181	189	198	206	214	222	230	239	247	255	7 5.6 8 6.4
528		263	272	280	288	296	304	313	321	329	337	9 7.2
529 530		346	354	362	370	378	387	395	403	411	419	
531		<u>428</u> 509	436 518	444 526	452	460 542	469 550	477 558	485 567	493 575	583	
531		591	599	607	534 616	624	632	640	648	656	665	
533		673	681	689	697	705	713	722	730	738	746	
534		754	762	770	779	787	795	803	811	819	827	_
535 536		835	843 925	852 933	860 941	868	876 957	884 965	892 973	900	908	7
537		997	*006	*014	*022	*030	*038	*046	*054	*062	*070	I 0.7 2 I.4
538	73	078	086	094	102	III	119	127	135	143	151	3 2.1
539		159	167	175	183	191	199	207	215	223	231	5 3.5
540		239	247	255	263	272	280	288	296	304	312	
541 542		320 400	328 408	336	344 424	352 432	360 440	368 448	376 456	384	392 472	8 5.6
543		480	488	496	50.1	512	520	528	536	544	552	9 6.3
544		560	568	576	584	592	600	608	616	624	632	
545 546		640 710	648 727	656 735	743	672 751	759	687	775	703	711 791	
547		799	807	815	823	830	838	846	854	862	870	
548		878	886	894	902	910	918	926	933	941	949	
549		957	965	973	981	989	997	*005	*013	*020	*028	
<u>550</u>	_	036	044	052	060	o 68	076	084	00)2	000	107	
N	L	. 0	1	2	3	4	5	6	7	8	9	PP

2	LO	1	2	3	4	5	6	7	8	9	PP
550	74 036	044	052	060	o 68	076	084	092	099	107	
551	115	123	131	139	147	155	162	170	178	186	
552 553	194 273	202 280	210 288	218 296	225 304	233 312	24I 320	249 327	257 335	265 343	
554	351	359	367	374	382	390	398	406	414	421	
555	429	437	445	453	461	468	476	484	492	500	
556	507	515	523	53 I	539	547	554	562	570	578	
557	586	593	601	609	617	624	632	640	648	656	
558	663	671	679	687	695	702	710	718	726	733	
559 560	741 819	749 827	757	764 842	772 850	780 858	865	796	803	811	
561	896	904	834 Q12	920	927	935		950	958	966	
562	974	981	989	920	*005	*012	943	*028	*035	*043	8
563	75 051	059	o 66	074	082	089	097	105	113	120	1 0.8
564	128	136	143	151	159	166	174	182	189	197	2 1.6 3 2.4
565	205	213	220	228	236	243	251	259	266	274	4 3.2
566	282	289	297	305	312	320	328	335	343	351	4 3.2 5 4.0 6 4.8 7 5.6 8 6.4
567 568	358 435	366 442	374 450	381 458	389 465	397 473	404 481	412	420 496	427 504	7 5.6
569	511	519	526	534	542	549	557	565	572	580	8 6.4 9 7.2
570	587	595	603	610	618	626	633	641	648	656	, , ,
571	664	671	679	686	694	702	709	717	724	732	
572	740	747	755	762	770	778	785	793	800	808	
573	815	823	831	838	846	853	861	868	876	884	
574 575	891 967	899 974	906 982	914 989	921 997	929 *005	937 *012	944 *020	952 *027	959 *035	
576	76 042	050	057	065	072	080	087	095	103	110	
577	118	125	133	140	148	155	163	170	178	185	
578	1 193	200	208	215	223	230	238	245	253	260	
579 580	268	275	283	290	298	305	313	320	328	335	7
	343	350	358	365	373	380	388	395	403	410	
581 582	418 492	425 500	433 507	440 515	448 522	455 530	462 537	470 545	477 552	485 559	I 0.7 2 I.4
583	567	574	582	589	597	604	612	619	626	634	3 2.1
584	641	649	656	664	671	678	686	693	701	708	4 2.8 5 3.5 6 4.2
585	716	723	730	738	745	753	760	768	775	782	6 4.2
586	790	797	805	812	819	827	834	842	849	856	7 4.9 8 5.6
587 588	864 938	871 945	879 953	886 960	893 967	901 975	908	916	923 997	930	8 5.6 9 6.3
589	77 012	019	026	034	041	048	056	063	070	078	
590	085	093	100	107	115	122	129	137	144	151	
591	159	166	173	181	188	195	203	210	217	225	
592	232	240	247	254	262	269	276	283	201	298	
593	305	313	320	327	335	342	349	357	364	371	
594 595	379 452	386 459	393 466	401 474	408 481	415 488	422	430 503	437 510	444 517	
596	525	532	539	546	554	561	568	576	583	590	
597	597	605	612	619	627	634	641	648	656	663	
598	670	677	685	692	699	706	714	721	728	735	
599	743	750	757	764	772	779	786	793	801	808	
600	77 815	822	830	837	844	851	859	866	873	880	
N	LO	ı	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
600	77 815	822	830	837	844	851	859	866	873	880	
601	887	895	902	909	916	924	931	938	945	952	
602	960	967	974	981	988	996	*003	*010	*017	*025	1
603= 604	78 032	039	046	053	061	068	075	082	o 89	097	
605	104 176	111	100	125	132	140 211	147 210	154	233	168	
606	247	254	262	269	276	283	290	297	305	312	8
607	319	326	333	340	347	355	362	369	376	383	1 0.8
608	390	398	405	412	419	426	433	440	447	455	2 1.6
609 610	462	469	476	483	490	497	504	512	519	526	3 2.4 4 3.2
611	533 604	540	618	554 625	633	569 640	576 647	583 654	590 661	597 668	5 4.0
612	675	682	680	696	704	711	718	725	732	739	
613	746	753	760	767	774	781	789	796	803	810	8 6.4
614	817	824	831	838	845	852	859	866	873	880	9 7.2
615	888	895	902	909	916	923	930	937	944	951	
616	958	965	972	979	986	993	*000	*007	*014	*021	
618	79 029 099	106	043	050	057	064 134	141	148	085	162	
619	169	176	183	190	197	204	211	218	225	232	
620	239	246	253	260	267	274	281	288	295	302	7
621	309	316	323	330	337	344	351	358	365	372	1
622 623	379	386	393	400	407	414	421	428	435	442	I 0.7 2 I.4
624	449 518	456	463 532	470	477 546	484	491 560	498 567	505	581	3 2.1
625	588	525 595	602	539 6 0 0	616	553 623	630	637	574 644	650	4 2.8 5 3.5
626	657	664	671	678	685	692	699	706	713	720	6 4.2
627	727	734	741	748	754	761	768	775	782	789	7 4.9 8 5.6
628 629	796 865	803 872	810 879	817 886	824 893	900	906	844	920	858	9 6.3
630	934	941	948	955	962	969	975	913	980	927	
631	80 003	G10	017	024	030	037	9/3	051	058	065	
632	072	079	085	002	099	106	113	1 20	127	134	
633	140	147	154	161	168	175	182	188	195	202	
634	209	216	223	229	236	243	250	257	264	271	
635 636	277 346	284 353	291 359	298 366	3 0 5	312 380	318	3 2 5 3 9 3	332	339	6
637	414	421	428	434	3/3 44I	448	455	462	468	475	I 0.6 2 I.2
638	482	489	496	502	509	516	523	530	536	543	3 1.8
639	550	557	564	570	577	584	591	598	604	611	4 2.4
640	618	625	632	638	645	652	659	665	672	679	6 3.6
641	686	693	699	706	713	720	726	733	740	747	7 4.2 8 4.8
642	754 821	828	767 835	774 841	781 848	787 855	794 862	801 868	808	814	9 5.4
644	88g	895	902	909	016	922	929	936	943	949	
645	956	963	969	976	983	990	929	*003	*010	*017	
646	81 023	030	037	043	050	057	064	070	077	084	
647	090	097	104	III	117	124	131	137	144	151	
648 64 9	158	164	238	178 245	184 251	191 258	198	204 271	211	218	
650	81 291	208	305	311	318	325	331	338	345	351	
N	L O	1	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
650	81 291	298	305	311	318	325	331	338	345	351	
651	3 5 8	305	371	378	385	391	398	405	411	418	
652 653	425	431 498	438	445	451 518	458	465	471	478	485	
654	491 558	564	505 571	511 578	584	525 501	531 598	538 6 0 4	544 611	551	
655	624	631	637	644	651	657	664	671	677	684	
656	690	697	704	710	717	723	730	737	743	750	\
657	757	763	770	776	783	790	796	803	809	816	
658	823	829	836	842	849	856	862	869	875	882	
659	889	895	902	908	915	921	928	935	941	948	
660	954	961	968	974	981	987	994	*000	*007	*014	_
661 662	82 020 086	027	033	040	046	053	060	066	073	079	7
663	151	158	164	105	178	184	125	132	204	145 210	I 0.7
664	217	223	230	236	243	240	256	263	260	276	2 I.4 3 2.1
665	282	289	295	302	308	315	321	328	334	341	4 2.8
666	347	354	360	367	373	380	387	393	400	406	5 3.5 6 4.2
667	413	419	426	432	439	445	452	458	465	471	7 4.9
668 669	478	484	491	497	504 569	510	517	523 588	530	536	8 5.6 9 6.3
670	543 607	614	620	627	633	575 640	646	653	595 659	666	
671	672	679	685	692	608	705	711	718	724		
672	737	743	750	756	763	769	776	782	789	730 795	
673	802	808	814	821	827	834	840	847	853	860	
674	866	872	879	885	892	898	905	911	918	924	
675	930	937	943	950	956	963	969	975	982	988	ĺ
676	995	*001	*008	*014	*020	*027	*033	*040	*046	*052	
677 678	83 0 59	129	136	078 142	085	155	097 161	168	174	181	
679	187	193	200	206	213	210	225	232	238	245	
680	251	257	264	270	276	283	289	296	302	308	6
681	315	321	327	334	340	347	353	359	366	372	1 0.6
682	378	385	391	398	404	410	417	423	429	436	2 1.2
683	442	448	455	461	467	474	480	487	493	499	3 1.8
684	506	512	518	525	531	537	544	550	556	563	4 2.4 5 3.0 6 3.6
685 686	569 632	575 639	582 645	588 651	594 658	664	670	613	683	626 680	
687	696	1	708	715	721	727	734	740	746	753	7 4.2 8 4.8
688	759	765	771	778	784	790	797	803	809	816	9 5.4
689	822		835	841	847	853	860	866	872	879	
690			897	901	910	916	923	929	935	942	
691	948		960	967	973	979	985	992	998	*004	1
692 693	84 011	080	023	029	036	105	C48	055	123	130	
694	136		148	155	161	167	173	180	186	102	
695	198		211	217	223	230	236	242	248	255	1
696	201		273	280	286	292	298	305	311	317	
697	323		3 36	342	348	354	361	367	373	379	
698	386		398	404	410	417	423	429	435	442	
699 70 0	84 510		460 522	<u>466</u> 528	473	479 541	485	553	497	504 566	
		-			535		547		559		
N	L O	1	2	3	4	5	6	7	8	9	PP

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700	84	510	516	522	528	535	541	547	553	559	566	
701		572	578	584	590	597	665	600	615	621	628	
702 703		634 696	640 702	646 7 0 8	652 714	658	726	733	677 739	745	689 751	
704	-	757	763	770	776	782	788	794	800	807	813	
705		819	825	831	837	844	850	856	862	868	874	
706		880	948	954	899 960	905	911	917	924 985	930	936	7
707 708	85	942 003	000	954	022	028	973	040	046	991 052	997 058	I 0.7
709		065	071	077	083	o 89	095	101	107	114	120	2 I.4 3 2.1
710		126	132	138	144	150	156	163	169	175	181	4 2.8
711 712		187 248	193 254	199 260	205	211	217	224 285	230	236	242 303	5 3.5 6 4.2
713		309	315	321	327	333	339	345	352	358	364	7 4.9 8 5.6
714		370	376	382	388	394	400	406	412	418	425	9 6.3
715		431	437	443	449	455	461	467	473	479	485	
716 717		49I 552	497 558	503 564	509	516	522	528 588	534 594	540	54 ⁰ 606	
718		612	618	625	631	637	643	649	655	661	667	
719		673	679	685	691	697	703	700	715	721	727	
720		733	739	745	751	757	763	769	775	781	788	6
72 I 72 2		794 854	800 860	8 o 6 866	812 872	818 878	824 884	830 890	836 896	942	848 908	1 0.6
723		914	920	926	932	938	944	950	956	962	968	2 1.2
724		974	980	986	992	998	*004	*010	*016	*022	*028	3 1.8 4 2.4
725 726	86	034	040	046 106	052	058	064	130	076 136	082	088	5 3.0 6 3.6
727		094	150	165	171	177	183	189	195	201	147 207	7 4.2
728		213	219	225	231	237	243	249	255	261	267	8 4.8 9 5.4
729		273	279	285	291	297	303	308	314	320	326	
730		332	338	344	350	356	362	368	374	380	386	
731 732		392 451	398 457	404 463	410 469	415 475	42I 48I	427 487	433 493	439 499	445 504	
733		510	516	522	528	534	540	546	552	558	564	
734		570	576	581	587	593	599	605	611	617	623	_
735 736		629	635 604	641 700	646 705	652 711	658	723	729	735	682 741	5
737		747	753	759	764	770	776	782	788	794	800	I 0.5 2 I.0
738		806	812	817	823	829	835	841	847	853	859	3 1.5 4 2.0
739		864	870	876	882	888	894	900	906	911	917	5 2.5
740		$\frac{923}{982}$	929 988	935	941	947	953 *011	958	964 *023	970 *020	976 *035	6 3.0 7 3.5
741 742	87	040	900	994 052	999 058	*005	070	075	081	087	093	8 4.0
743		099	105	III	116	122	128	134	140	146	151	9 4.5
744		157	163	169	175	181	186	192	198	204	210	
745 746		216	22I 280	227 286	233 291	239 297	245 3 0 3	300	256 315	262 320	326	
747		332	338	344	349	355	361	367	373	379	384	
748		300	396	402	408	413	419	425	431	437	442	
749 750	٥.	448	454	460	466	471	477	483	489	495	500	
	_	506	512	518	523	529	535	541	547	552	558	
N	L	0	1	2	3	4	5	6	7	8	9	PP

N	LO	1	2	3	4	5	6	7	8	9	PP
750	87 506	512	518	523	529	535	541	547	552	558	
751	564	570	576	581	587	5 93	599	604	610	616	
752 753	622 679	628	633 691	639 697	703	651 7 0 8	656 714	720	668 726	674 731	
754	737	743	749	754	760	766	772	777	783	780	
755	795	800	806	812	818	823	829	835	841	846	
756	852	858	864	869	875	881	887	892	898	904	
757	910	915	921	927	933	938	944	950	955	961	
758 759	967 88 0 24	973 030	978 036	984 041	990 047	996 05 3	*001	*007	*013	*018 076	
760	081	087	093	098	104	110	116	121	127	133	•
761	138	144	150	156	161	167	173	178	184	190	6
762	195	201	207	213	218	224	230	235	241	247	1 0.6
763	252	258	264	270	275	281	287	292	298	304	2 1.2 3 1.8
764 765	309 366	315 372	32I 377	326 383	332 389	338 39 5	343	349 4 0 6	355 412	360 417	
766	423	429	434	440	446	451	457	463	468	474	5 3.0
767	480	485	491	497	502	508	513	519	525	530	7 4.2
768	536	542	547	553	559	564	570	576	581	587	8 4.8 9 5.4
769	593	598	604	610	615	621	627	632	638	643	9 3.4
770	649	655	660	666	672	677	683	689	694	700	
77I 772	705 762	711 767	717 773	722 779	728 784	734 790	739 795	745 801	750 807	756 812	
773	818	824	829	835	840	846	852	857	863	868	
774	874	880	885	891	897	902	908	913	919	925	
775	930	936	941	947	953	958	964	969	975	981	
776	986	992	997	*003	*009	*014	*020	*025	*031	*037	
777 778	89 042 098	048	053 100	059	064	126	131	081	087	148	
779	154	159	165	170	176	182	187	193	198	204	
780	209	215	221	226	232	237	243	248	254	260	5
781	265	271	276	282	287	293	298	304	310	315	1 0.5
782 783	321 376	326 382	332 387	33 7 393	343 398	348 4 0 4	354 409	360 415	36 5 421	371 426	2 I.O 3 I.5
784	432	437	443	448	454	459	465	470	476	481	4 2.0
785	487	492	498	504	509	515	520	526	531	537	5 2.5 6 3.0
786	542	548	553	559	564	570	575	581	586	592	7 3.5
787 788	597	658	609 664	614 660	620 675	625 680	686	636 691	642	702	8 4.0 9 4.5
789	653 7 0 8	713	719	724	730	735	741	74 6	752	757	
790	763	768	774	779	785	790	796	801	807	812	
791	818	823	829	834	840	845	851	856	862	867	
792	873	878	883	889	894	900	905	911	916	922	
793	927	933	938	944	949 *004	955 *000	960 *015	966 *020	971 *026	977	
794 795	982 90 0 37	988 0 42	993 048	998 053	059	064	069	075	080	*031 086	
796	091	097	102	108	113	119	124	129	135	140	
797	146	151	157	162	168	173	179	184	189	195	
798	200	200	211 266	217	222	227	233	238	244	249	
799 800	90 309	314		$\frac{271}{325}$	331	336	287	$\frac{293}{347}$	298 352	358	
800 N	L 0	314	320	325	4	5	342 6	7	8	9	PP
N	i L O	' '	- 2	3	4	1 0	0	1_'	0	9	1 PP 1

N	L	0	1	2	3	4	5	6	7	8	9	PP
800	90 3	309	314	320	325	331	336	342	347	352	358	
801		363	369	374	38 o	385	390	396	401	407	412	
802 803		117 172	423 477	428 482	434 488	439 493	445 499	450 504	455 509	461 515	466 520	
804		526	53I	536	542	547	553	558	563	560	574	
805	5	580	585	590	596	601	607	612	617	623	628	
806		534	639	644	650	655	660	666	671	677	682	
807 808		587 741	693 747	698 752	703 757	7 0 9 763	714	720 773	725 779	730 784	736 789	
809		795	800	806	811	816	822	827	832	838	843	
810	8	349	854	859	865	870	875	881	886	891	897	
811		02	907	913	918	924	929	934	940	945	950	6
812 813	91 0	056	961 014	966 020	972 025	977 030	982 036	988	993 0 46	052	*004 057	I 0.6
814	-	062	068	073	078	084	089	094	100	105	110	3 1.8
815		116	121	126	132	137	142	148	153	158	164	4 2.4 5 3.0 6 3.6
816		169	174	180	185	190	196	201	206	212	217	6 3.6
817 818		222	228 281	233 286	238 291	243 297	249 302	254 3 0 7	259 312	265 318	270 323	8 4.8
819		328	334	339	344	350	355	360	365	371	376	9 5.4
820	3	381	387	392	397	403	408	413	418	424	429	
821		134	440	445	450	455	461	466	47 I	477	482	
822 823		187 540	492 545	498 551	503 556	508 561	514 566	519 572	524 577	529 582	535 587	N.
824		93	598	603	600	614	619	624	630	635	640	.9
825		45	651	656	661	666	672	677	682	687	693	
826		598	703	709	714	719	724	730	735	740	745	
827 828		303	756 808	761 814	766 819	772 824	777 829	782 834	787 840	793 845	798 850	
829		355	861	866	871	876	882	887	892	897	903	
830	_	800	913	918	924	929	934	939	944	950	955	5
831 832	92 C	060	965 018	971	976 028	981	986 038	991	997	*002	*007 059	1 0.5
833		065	070	023	080	033 085	030	044	049 101	106	111	2 I.O
834		17	122	127	132	137	143	148	153	158	163	3 I.5 4 2.0
835		69	174	179	184	189	195	200	205	210	215	5 2.5 6 3.0
836 837		273	226	23 I 283	236	241	247 298	252 304	257 300	262 314	267 319	7 3.5
838	3	324	330	335	340	293 345	350	355	361	366	371	8 4.0 9 4.5
839	3	376	381	387	392	397	402	407	412	418	423	
840		128	433	438	443	449	454	459	464	469	474	
841 842		180	485 536	490	495 547	500 552	505	511 562	516 567	52I 572	526 578	
843		83	588	542 593	598	552 603	557 6 0 9	614	619	624	629	
844	6	534	639	645	650	655	660	665	670	675	681	
845		586	691	696	701	706	711	716 768	722	727	732 783	
846 847		88	742 793	747 799	75 ² 80 ₄	758 800	763 814	810	773 824	778 829	834	
848	8	340	845	850	855	860	865	870	875	881	886	
849	8	391	896	901	906	911	916	921	927	932	937	
850	929		947	952	957	962	967	973	978	983	988	
N	L	0	1	2	3	4	5	6	7	8	9	PP

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850	92 942	947	952	957	962	967	973	978	983	988	
851	993	998	*003	*008	*013	*018	*024	*029	*034	*039	
852	93 044	049	054	059	064	069	075	080	085	090	
853	095	100	105	161	115 166	120	125	131	136 186	141	
854 855	146	151 202	156 207	212	217	17I 222	227	232	237	192 242	
856	247	252	258	263	268	273	278	283	288	293	6
857	298	303	308	313	318	323	328	334	339	344	1 0.6
858	349	354	359	364	369	374	379	384	389	394	2 1.2
859	399	404	400	414	420	425	430	435	440	445	3 I.8 4 2.4
860 861	450	455	460	465	470	475	480	485	490	495	5 3.0
862	500 551	505 556	510 561	515 566	520 571	526 576	531 581	536 586	541 591	546 596	6 3.6 7 4.2
863	601	606	611	616	621	626	631	636	641	640	8 4.8
864	651	656	661	666	671	676	682	687	692	697	9 5.4
865	702	707	712	717	722	727	732	737	742	747	
866	752	757	762	767	772	777	782	787	792	797	
867 868	802 852	807 857	812	817 867	822 872	827 877	832 882	837 887	842 802	847 897	
869	902	907	912	917	922	927	932	937	942	947	
870	952	957	962	967	972	977	982	987	992	997	
871	94 002	007	012	017	022	027	032	037	042	047	5
872	052	057	062	067	072	077	082	o 86	001	o 96	I 0.5 2 I.0
873	101	106	161	116	121	126	131	136	141	146	3 1.5
874 875	151 201	156	211	216	17I 22I	176 226	231	236	240	245	4 2.0 5 2.5 6 3.0
876	250	255	260	265	270	275	280	285	290	295	6 3.0
877	300	305	310	315	320	325	330	335	340	345	7 3.5 8 4.0
878	349	354	359	364	369	374	379	384	389	394	9 4.5
879 880	399 448	453	458	414	419	424	429	433	438	443	
881	498	503	507	512	517	522	527	532	537	542	
882	547	552	557	562	567	571	576	581	586	591	
883	596	601	606	611	616	621	626	630	635	640	
884	645	650	655	660	665	670	675	680	685	689	4
885 886	694 743	699 748	704 753	709 758	714	719	724 773	729 778	734 783	738	_
887	792	797	802	807	812	817	822	827	832	836	1 0.4 2 0.8
888	841	846	851	856	861	866	871	876	880	885	3 I.2 4 I.6
889	890	895	900	905	910	915	919	924	929	934	5 2.0
890	939	944	949	954	959	963	968	973	978	983	6 2.4 7 2.8
891 892	988 95 036	993	998 0 46	*002 051	*007	*012 061	*017	*022 071	*027 075	*032 080	8 3.2
893	085	000	095	100	105	100	114	119	124	129	9 3.6
894	134	139	143	148	153	158	163	168	173	177	
895	182	187	192	197	202	207	211	216	221	226	
896	231	236	240	245	250	255	260	265	318	274	Į
897 898	279 328	332	289 337	294 342	299 347	303 352	308	313	366	323 371	
899	376	381	386	390	395	400	405	410	415	419	
900	95 424	429	434	439	444	448	453	458	463	468	
N	L O	ı	2	3	4	5	6	7	8	9	PP

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900	95 424	429	434	439	444	448	453	458	463	468	
901	47		482	487	492	497	501	506	511	516	
902 903	521 560		530	535 583	540	545	550	554	559 607	564	
904	61		626	631	636	641	646	650	655	660	
905	66		674	679	684	689	694	698	703	708	
906	713		722	727	732	737	742	746	751	756	
907 908	761 800		770	775 823	780 828	785 832	789 837	794 842	799 847	804	
909	856		866	871	875	880	885	890	895	899	
910	902	909	914	918	923	928	933	938	942	947	_
911	952		961	966	971	976	980	985	990	995	5
912 913	999 96 0 47		*009	*014	*019	*023 071	*028 076	*033	*038	*042	I 0.5 2 I.0
914	095		104	100	114	118	123	128	133	137	3 1.5
915	142	147	152	156	161	166	171	175	180	185	4 2.0 5 2.5
916	190		199	204	200	213	218	223	227	232	6 3.0
917 918	237 284		246	251	303	308	265	317	275 322	280 327	7 3.5 8 4.0
919	332	1 =	341	346	350	355	360	365	369	374	9 4.5
920	379		388	393	398	402	407	412	417	421	
921	426		435	440	445	450	454	459	464	468	
922	473 520	1	483	487	492	497	501	506	511	515	
923 924	567	1 0 0	530	534 581	539 586	544 591	548	553	558	562	
925	614		577 624	628	633	638	642	647	652	656	
926	661	1	670	675	680	685	689	694	699	703	
927	708		717	722	727	731	736	741	745	750	
928 929	755 802	759 806	764	769 816	774 820	778 825	783 830	788 834	792 839	797 844	
930	848		858	862	867	872	876	881	886	890	
931	895		904	909	914	918	923	928	932	937	4
932	942	946	951	956	960	965	970	974	979	984	1 0.4 2 0.8
933	988		997	*002	*007	*011	*016	*021	*025	*030	3 1.2
934 935	97 035 081		044	049 005	100	058	063	067	072	123	4 I.6 5 2.0
936	128		137	142	146	151	155	160	165	169	5 2.0 6 2.4 7 2.8
937	174		183	188	192	197	202	206	211	216	8 3.2
938 939	220 267		230 276	234 280	239 285	243 290	248	253	257 304	262 308	9 3.6
940	313		322	327	331	336	340	345	350	354	
941	359		368	373	377	382	387	391	396	400	
942	405	410	414	419	424	428	433	437	442	447	
943	451		460	465	470	474	479	483	488	493	
944 945	497 543		506	511	516 562	520 566	525 571	529 575	534 580	539 585	
945	5 43		598	557 6 0 3	607	612	617	621	626	630	
947	635	640	644	649	653	658	663	667	672	676	<u> </u>
948	681	685	690	695	699	704	708	713	717	722	
949	727		736	740 786	745	749	754 800	759 804	763 809	768 813	
950	97 772				791	795					
N	L 0	1	2	3	4	5	6	7	8	9	PP

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950	97 772	777	782	786	791	795	800	804	809	813	
951	818	823	827	832	836	841	845	850	855	859	
952	864	868	873	877	882	886	891	896	900	905	
953	909	914	918	923 068	928	932	937	941	946	950	
954 955	955	959 005	964 009	014	973 019	978 023	982 028	987 032	991 937	996 041	
956	046	050	055	059	064	068	073	078	082	087	
957	091	096	100	105	109	114	118	123	127	132	\
958	137	141	146	150	155	159	164	168	173	177	
959	182	186	191	195	200	204	200	214	218	223	
960	227	232	236	241	245	250	254	259	263	268	5
961 962	2 7 2 318	277 322	281 327	286 331	290 336	295 340	299 345	304 349	308 354	313 358	
963	363	367	372	376	381	385	390	394	399	403	I 0.5 2 I.0
964	408	412	417	421	426	430	435	439	444	448	3 1.5
965	453	457	462	466	471	475	480	484	489	493	4 2.0 5 2.5
966	498	502	507	511	516	520	525	529	534	538	6 3.0
967	543	547	552	556	561	565	570	574	579	583	7 3.5 8 4.0
968 969	588 632	592 637	597 641	601 646	650	655	659	664	623	628 673	9 4.5
970	677	682	686	691	695	700	704	700	713	717	
971	722	726	731	735	740	744	749	753	758	762	
971	767	771	776	780	784	789	793	798	802	807	
973	811	816	820	825	829	834	838	843	847	851	
974	856	86 o	865	869	874	878	883	887	892	896	
975	900	905	909	914	918	923	927	932	936	941	
976	945	949	954	958	963	967	972 *016	976 *021	981	985	
977 978	989 99 9 34	994 038	998 043	*003 047	*007 052	*012 056	061	C65	*025 060	*029 074	
979	078	083	087	092	096	100	105	100	114	118	
980	123	127	131	136	140	145	149	154	158	162	4
981	167	171	176	180	185	189	193	198	202	207	
982	211	216	220	224	229	233	238	242	247	251	1 0.4 2 0.8
983	255	260	264	269	273	277	282	286	291	295	3 I.2 4 I.6
984 985	300 344	3 0 4 348	308 352	313	317 361	322 366	326 370	330	335 379	339 383	
986	388	392	396	401	405	410	414	419	423	427	5 2.0
987	432	436	441	445	449	454	458	463	467	471	7 2.8 8 3.2
988	476	480	484	489	493	498	502	506	511	515	9 3.6
989	520	524	528	533	537	542	546	550	555	559	
990	564	568	572	577	581	585	590	594	599	603	
99 I 992	607 651	612	616	621	625	629	634	638	642	647 601	
993	695	699	704	708	712	717	721	726	730	734	
994	739	743	747	752	756	760	765	769	774	778	
995	782	787	791	795	800	804	808	813	817	822	
996	826	830	835	839	843	848	852	856	861	865	
997	870	874	878	883	887	891	896 939	900	904	909	
998 999	913 957	917 961	922	926	930	935	939	944	940	952 996	
1000	∞ 937	004	000	013	017	022	026	030	035	039	
N	L O	<u> </u>	2	3	4	5	6	7	8	9	PP
N	LU	<u> </u>	1 2	0	4	1 2			_ •	_ 9	PP

N	L	0	1	2	3	4	5	6	7	8	9
1000	000	0000	0434	0869	1303	1737	2171	2605	3039	3473	3907
1001		4341	4775	5208	5642	6076	6510	6943	7377	7810	8244
1002		8677	9111	9544	9977	*0411	*0844	*1277	*1710	*2143	*2576
1003	100	3009	3442	3875	4308	474I	5174	5607	6039	6472	6905
1004		7337	7770	8202	8635	9067	9499	9932	*0364	*0796	*1228
1005	002	1661	2093	2525	2957	3389	3821	4253	4685	5116	5548
1006		5980	6411	6843	7275	7706	8138	8569	9001	9432	9863
1007	003	0295	0726	1157	1588	2010	2451	2882	3313	3744	4174
1008		4605	5036	5467	5898	6328	6759	7190	7620	8051	8481 *2784
1009		8912	9342	9772	*0203	*0633	*1063	*1493	*1924	*2354	
1010	004	3214	3644	4074	4504	4933	5363	5793	6223	6652	7082
1011		7512	7941	8371	8800	9229	9659	*0088	*0517	*0947	*1376
1012	005	1805	2234	2663	3092	3521	3950	4379	4808	5237	5666
1013		6094	6523	6952	7380	7809	8238	8666	9094	9523	9951
1014	006	0380	0808	1236	1664	2092	2521	2949	3377	3805	4233
1015		4660	5088	5516	5944	6372	6799	7227	7655	8082	8510
1016		8937	9365	9792	*0219	*0647	*1074	*1501	*1928	*2355	*2782
1017	007	3210	3637	4064	4490	4917	5344	5771	6198	6624	7051
1018	0	7478	7904	8331	8757	9184	9610	*0037	*0463	*0889	*1316
1019	008	1742	2168	2594	3020	3446	3872	4298	4724	5150	5576
1020		6002	6427	6853	7279	7704	8130	8556	8981	9407	9832
1021	000	0257	0683	1108	1533	1959	2384	2800	3234	3659	4084
1022		4509	4934	5359	5784	6208	6633	7058	7483	7907	8332
1023		8756	9181	9605	*0030	*0454	*0878	*1303	*1727	*2151	*2575
1024	010	3000	3424	3848	4272	4696	5120	5544	5967	6391	6815
1025		7239	7662	8086	8510	8933	9357	9780	*0204	*0627	*1050
1026	011	1474	1897	2320	2743	3166	3590	4013	4436	4859	5282
1027		5704	6127	6550	6973	7396	7818	8241	8664 *2887	9086	9509
1028		9931	*0354	*0776	*1198	*1621	*2043 6264	*2465 6685	7107	*3310 7529	*3732 7951
1029	012	4154	4576	4998	5420	l	-		<u> </u>		
1030		8372	8794	9215	9637	*0059	*0480	*0901	*1323	*1744	*2165
1031	013	2587	3008	3429	3850	4271	4692	5113	5534	5955	6376
1032		6797	7218	7639	8059	8480	8901	9321	9742	*0162	*0583
1033	014	1003	1424	1844	2264	2685	3105	3525	3945	4365	4785
1034		5205	5625	6045	6465	6885	7305	7725	8144	8564	8984 *3178
1035		9403	9823	*0243	*0662	*1082	*1501	*1920 6112	*2340 6531	*2759 6950	7369
1036	015	3598	4017	4436	4855	5274	5693 9881	*0300	*0718	*1137	*1555
1037	0.16	7788	8206	8625	3220	9462 3647	4065	4483	4901	5319	5737
1038	010	1974 6155	6573	6001	7400	7827	8245	8663	9080	9498	9916
1040	017	0333	0751	1168	1586	2003	2421	2838	3256	3673	4000
1041	",	4507	4924	5342	5759	6176	6593	7010	7427	7844	8260
1041		8677	9094	0511	9927	*0344	*0761	*1177	*1594	*2010	*2427
1043	018	2843	3259	3676	4002	4508	4925	5341	5757	6173	6589
1044		7005	7421	7837	8253	8669	9084	9500	9916	*0332	*0747
1045	010	1163	1578	1994	2410	2825	3240	3656	4071	4486	4902
1046	´	5317	5732	6147	6562	6977	7392	7807	8222	8637	9052
1047		9467	9882	*0296	*0711	*1126	*1540	*1955	*2369	*2784	*3198
1048	020	3613	4027	4442	4856	5270	5684	6000	6513	6927	7341
1049		7755	8169	8583	8997	9411	9824	*0238	*0652	*1066	*1470
1050	021	1893	2307	2720	3134	3547	3961	4374	4787	5201	5614
N	L	0	1	2	3	4	5	6	7	8	9

N	L	0	1	2	3	4	5	6	7	8	9
1050	021	1893	2307	2720	3134	3547	3961	4374	4787	5201	5614
1051		6027	6440	6854	7267	7680	8093	8506	8919	9332	9745
1052	022	0157	0570	0983	1396	1808	2221	2634	3046	3459	3871
1053		4284	4696	5100	5521	5933	6345	6758	7170	7582	7994
1054		8406	8818	9230	9642	*0054	*0466	*0878	*1289	*1701	*2113
1055	023	2525	2936	3348	3759	4171	4582	4994	5405	5817	6228
1056		6639	7050	7462	7873	8284	8695	9106	9517	9928	*0339
1057	024	0750	1161	1572	1982	2393	2804	3214	3625	4036	4446
1058 1059		4857 8960	5267 9370	5678 9780	6088 *0190	6498 *0600	*1010	7319 *1419	7729 *1829	8139 *2239	8549 *2649
1060	025	3059	3468	3878	4288	4697	5107	5516	5926	6335	6744
1061	-	7154	7563	7972	8382	8791	9200	9600	*0018	*0427	*0836
1062	026	1245	1654	2063	2472	2881	3289	3698	4107	4515	4924
1063		5333	5741	6150	6558	6967	7375	7783	8192	8600	9008
1064		9416	9824	*0233	*0641	*1049	*1457	*1865	*2273	*2680	*3088
1065	027	3496	3904	4312	4719	5127	5535	5942	6350	6757	7165
1066	_	757^{2}	7979	8387	8794	9201	9609	*0016	*0423	*0830	*1237
1067	028	1644	2051	2458	2865	3272	3679	4086	4492	4899	5306
1068		5713	6119	6526	6932	7339	7745	8152	8558	8964	9371
1069		9777	*0183	*0590	*0996	*1402	*1808	*2214	*2620	*3026	*3432
1070	029	3838	4244	4649	5055	5461	5867	6272	6678	7084	7489
1071	0.20	7895	8300	8706	9111	9516	9922	*0327	*0732	*1138	*1543
1072 1073	030	1948 5997	2353 6402	2758 68 07	3163 7211	3568 7616	3973 8020	4378 8425	4783 8830	5188 9234	5592 9638
1073	021	0043	0402	0851	1256	1660	2064	2468	2872	3277	3681
1074	031	4085	4489	4893	5296	5700	6104	6508	6012	7315	7719
1076		8123	8526	8930	9333	9737	*0140	*0544	*0947	*1350	*1754
1077	0.3.2	2157	2560	2963	3367	3770	4173	4576	4979	5382	5785
1078		6188	6590	6993	7396	7799	8201	8604	9007	9409	9812
1079	033	0214	0617	1019	1422	1824	2226	2629	3031	3433	3835
1080		4238	4640	5042	5444	5846	6248	6650	7052	7453	7855
1801		8257	8659	9060	9462	9864	*0265	*0667	*1068	*1470	*1871
1082	034	2273	2674	3075	3477	3878	4279	4680	5081	5482	5884
1083		6285	6686	7087	7487	7888	8289	8690	9091	9491	9892
1084	035	0293	0693	1004	1495	1895	2296	2696	3096	3497	3897
1085		4297 8298	4698	5098	5498	5898	6298	6698	7098 *1097	7498	7898 *1896
1087	026	2205	8698 2695	90 98	9498 3494	9898 3893	*0297 4293	*0697 4692	5001	*1496	5890
1087	0,0	6280	6688	7087	7486	7885	8284	8683	9082	5491 9481	9880
1089	037	0279	0678	1076	1475	1874	2272	2671	3070	3468	3867
1090		4265	4663	5062	5460	5858	6257	6655	7053	7451	7849
1091		8248	8646	9044	9442	9839	*0237	*0635	*1033	*1431	*1829
1092	o 38	2226	2624	3022	3419	3817	4214	4612	5009	5407	5804
1093		6202	6599	6996	7393	7791	8188	8585	8982	9379	9776
1094	039	0173	0570	0967	1364	1761	2158	2554	2951	3348	3745
1095		4141 8106	4538	4934 8898	5331	5727	6124 *0086	6520 *0482	6917 *0878	7313	7709 *1670
1096	040	2066	8502 2462	2858	9294	9690 3650	ı		4837	*1274	5628
1097	040	6023	6410	6814	3254 7210	7605	4045 8001	4441 8396	4837 8791	5232 9187	9582
1099		9977	*0372	*0767	*1162	*1557	*1952	*2347	*2742	*3137	*3532
1100	041	3927	4322	4716	5111	5506	5900	6295	6690	7084	7479
N	L	0		2	3	4	5	6	7	8	9

TABLE XXV. — LOGARITHMS OF SINES, TANGENTS, COSINES, AND COTANGENTS FOR EACH 0.01° OF THE QUADRANT

In this table whenever the trigonometric function is fractional, as it always is for sines and cosines, except when it is I, the logarithms have been increased by IO to avoid the negative characteristic. But where the function is greater than I, as are cotangents and tangents for certain parts of the circle, the logarithm is given without the IO. Thus in the column headed cot at the top of the page the logarithms are unaugmented; in all other columns they are augmented. This must be remembered in working with them.

To find the square root of the sine of 26.32° we find on page 151, line 33, the log sin to be 9.64678, which must be divided by 2 to give the logarithm of the square root; the operation is performed thus:

$$\frac{2)9.64678 - 10}{4.82339 - 5} = \overline{1}.82339.$$

Whence $\sqrt{\sin 26.32^{\circ}}$ = the number whose log is $\overline{1.82339}$ or 0.66587+. But to find the square root of the cotangent of 26.32° , page 151, line 33, we have $0.30569 \div 2 = 0.152845$, which corresponds to the number 1.4218+.

The numbering of the pages. — On each page there will be found four-degree numbers which are to be used as follows: the upper left-hand figure is used with the headings at the tops of the columns and the fractions running down the left side of the page. The lower right-hand figure is used with the headings at the bottoms of the columns, and fractions running up the right-hand side of the page. The upper right-hand figure is used with headings at the tops of the columns and fractions running up the right-hand side of the page. The lower left-hand figure is used with headings at the bottom of the page and fractions running down the left-hand side of the page. Generally stated the figures are used with the headings and fractions nearest them.

Example. — See pages 163-164. The log sin of 32.4° is found in the 2nd column, page 163, 41st line, to be 9.72902, while the log sin of 122.4° is found in the 7th column of the same page and line to be 9.92651. The log sin of 147.4° is found in the 2nd column on page 164, 41st line from the bottom, to be 9.73140, while the log sin 57.4° is found in the 7th column of the same page and line to be 9.92555.

When the function or angle sought is not in the table, as when the log sin of 14.436° or the angle whose sine is 9.34220 is wanted, we must interpolate between the tabular quantities. Thus:

- (a) Log sin 14.43° is found on page 127, line 44, to be 9.39654 with a tabular difference of 30 for a change of 0.01 given in the column headed d. Then the addition for 6 tenths of 0.01° is found by multiplying 30 × 0.6 = 18, and adding to 9.39654 giving 9.39672 as the required sine. When the quantities are less simple the proportional part given in the right-hand column of the page may be used. If the angle is 14.4362° the table of proportional parts is convenient even for the simple difference of 30. Thus, from the values in the right-hand column headed "30" we find 18 opposite 6; moving the decimal point one place to the left, we find 0.6 opposite 2; adding we get .000186, or .00019, to be added to the log sin 14.43° to give log sin 14.4362°. The figures are uncertain beyond five places and may be a fraction of one in error in the fifth place.
- (b) For the angle whose log sine is 9.34220 we find on page 124 the next smaller log sin = 9.34212 = log sin 12.70°; the difference is 9.34220 9.34212 = 8 in the last place. The tabular difference is 34. Looking in the column of proportional parts under 34 we find 6.8 next smaller number than 8 corresponding to 0.002 and leaving 1.2 unused; moving the decimal point one place to the left in the tabular quantities, the next smaller and nearest number is 1.02 opposite 3. Therefore the angle is 12.7023°. The last figure is uncertain.

For fractional angles near 0° and 90°, the differences are changing so rapidly that linear interpolation is not sufficiently exact. The right-hand columns of pages 99 to 104 show what to do. Thus to find the log sin 0.1246° we find (pages 76 and 99)

Log. 0.1246 =
$$\overline{1}$$
.09552
 $S = \underbrace{1.75812}_{7.33740}$

To find log cos and log cot we find log sin and tangents of complementary angles. Thus, to get log cos 89.367°, we get log sin 0.633°. Conversely, to find the angle whose log sin is 7.33740, we refer to page 99, and find that the angle is between 0.12° and 0.13° and hence

$$S = 1.75812$$

$$\log \sin = \frac{7.33740 - 10}{9.09552 - 10} = \overline{1}.09552.$$
(page 76) log 0.1246° = $9.09552 - 10 = \overline{1}.09552$.

TABLE XXVI. — LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS FOR EACH 0.02° OF THE QUADRANT

The use of this table will be evident except the interpolation for small angles and for external secants for angles near 90°.

For small angles use the quantity V for versed sines and E for external secants as follows:

Log vers
$$\alpha = 2 \log \alpha^{\circ} + V$$
.
Log exsec $\alpha = 2 \log \alpha^{\circ} + E$.

Interpolate for V and E when necessary. Example. — Required log vers 1.354°.

Log I.354 = 0.13162

$$V \text{ for I.36}^\circ = \frac{2}{0.26324}$$

 $V \text{ for I.36}^\circ = \frac{6.18270}{6.44594}$
Log $\alpha^\circ = \frac{\log \text{vers } \alpha - V}{2} = \frac{\log \text{exsec } \alpha - E}{2}$.

For external secants near 90° the interpolation is as follows: $Log \operatorname{exsec} A = \log \operatorname{vers} A - \log \sin (90 - A).$

_0°							179°	
	Sin	d.	Tan	d. c.	Cot	Cos		
00							100	S
or	6.24188	20702	6.24188	20702	3.75812	0.00000	99	
02	6.54291	30103 17609	6.54291	30103 17609	3.45709	0.00000	98	° 1.758
03	6.71900	12494	6.71900	12494	3.28100	0.00000	97	.0 123
04	6.84394	9691	6.84394	9691	3.15606	0.00000	96	.1 123
05	6.94085	7918	6.94085	7918	3.05915	0.00000	95	.2 I24 .3 I25
06	7.02003	6695	7.02003	6695	2.97997	0.00000	94	.3 125 .4 126
07	7.08698	5799	7.08698	5799	2.91302	0.00000	93	.5 128
08	7.14497	5115	7.14497	5115	2.85503	0.00000	92	.0
09	7.19612	4576	7.19612	4576	2.80388	0.00000	91	\
10	7.24188	4139	7.24188	4139	2.75812	0.00000	90	
11	7.28327	3779	7.28327	3779	2.71673	0.00000	89	
12	7.32106	3476	7.32106	3476	2.67894	0.00000	88 87	
13	7.35582	3218	7.35582	3219	2.64418	0.00000		
14	7.38800	2997	7.38801	2996	2.61199	0.00000	86	ائد
15	7.41797	2803	7.41797	2803	2.58203	0.00000	85 84	$T_{ m ;}$
16	7.44600	2633	7.44600	2633	2.55400			To interpolate when angles are small: $\log \sin \alpha = \log \alpha^\circ - S; \ \log \tan \alpha = \log \alpha^\circ - T;$ $\log \alpha^\circ = \log \sin \alpha + S = \log \tan \alpha + T.$ For \cos and \cot near 90° use \sin and \tan of $\operatorname{complement}$
17	7.47233	2482	7.47233	2482	2.52767	0.00000	83 82	o interpolation
18	7.49715	2348	7.49715	2348	2.50285	0.00000	81	$\frac{g}{T}\alpha^{o}$
19	7.52063	2228	7.52063 7.54291	2228	2.47937	0.00000		10, x + f cc f cc
20	7.54291	2119		2119	2.45709	0.00000	80	are small: S; log tan $\alpha = \log + S = \log \tan \alpha + c$ e sin and tan of cop
21	7.56410	2020	7.56410	2020	2.43590	0.00000	79	: s ta tan
22	7.58430	1930	7.58430	1931	2.41570	0.00000	78	tall tar log log
23	7.60360	1849	7.60361	1848	2.39639	0.00000	77	sm logo
24	7.62209	1773	7.62209	1773	2.37791	0.00000	76	re 5; 1 5; 1 sin
25	7.63982	1703	7.63982	1703	2.36018	0.00000	75	8 1 8 8
26	7.65685	1639	7.65685	1639	2.34315	0.00000	74	gle f in e
27	7.67324	1579	7.67324	1580	2.32676	0.00000	73	g s s
28	7.68903	1524	7.68904	1524	2.31096	9.99999	72	24 c c c c c c c c c c c c c c c c c c c
29	7.70427	1473	7.70428	1472	2.29572	9.99999	71	d k
30	7.71900	1424	7.71900	1424	2.28100	9.99999	70	To interpolate when angles are small: $\log \sin \alpha = \log \alpha^{\circ} - S$; log tan $\alpha = \log \alpha$ of $\log \sin \alpha + S = \log \tan \alpha + T$. For \cos and \cot near 90° use \sin and \tan of compi
31	7.73324	1379	7.73324	1379	2.26676	9.99999	69	s si g si log log
32	7.74703	1336	7.74703	1337	2.25297	9.99999	68	log log
33	7.76039	1296	7.76040	1296	2.23960	9.99999	67	os sos
34	7.77335	1259	7.77336	1259	2.22664	9.99999	66	o ir
35	7.78594	1224	7.78595	1224	2.21405	9.99999	65	Ť ŭ
36	7.79818	1190	7.79819	1190	2.20181	9.99999	64	
37	7.81008	1158	7.81009	1158	2.18991	9.99999	63	
38	7.82166	1128	7.82167	1128	2.17833	9.99999	62 61	
39	7.83294	1099	7.83295	1099		9.99999		
40	7.84393	1073	7.84394	1073	2.15606	9.99999	60	
41	7.85466	1046	7.85467	1046	2.14533	9.99999	59	
42	7.86512	1022	7.86513	1022	2.13487	9.99999	58	T
43	7.87534	999	7.87535	999	2.12465	9.99999	57	° 1.758
44	7.88533	976	7.88534	976	2.11466	9.99999	56	_ 1.756
45	7.89509	954	7.89510	954	2.10490	9.99999	55	.0 123
46	7.90463	934	7.90464	934	2.09536	9.99999	54	.I 122 .2 121
47	7.91397	914	7.91398	915	2.08602	9.99999	53	.3 119
48	7.92311	896	7.92313	895	2.07687	9.99998	52	:4 116
49	7.93207	877	7.93208	878		9.99998	51	.5 112
50	7.94084		7.94086		2.05914	9.99998	50	
	Cos	_d.	Cot	d. c.	Tan	Sin	l	

			T (7)	1				
	Sin	d.	Tan	d.c.	Cot	Cos	 	
50	7.94084	860	7.94086	860	2.05914	9.99998	50	S
51	7.94944	843	7.94946	843	2.05054	9.99998	49	_
52	7.95787	828	7.95789	828	2.04211	9.99998	48	_ 1.730
53	7.96615	811	7.96617	811	2.03383	9.99998	47	.5 128
54	7.97426	797	7.97428	797	2.02572	9.99998	46	.6 131
55	7.98223	783	7.98225	783	2.01775	9.99998	45	.7 133
56	7.99006	769	7.99008	769	2.00992	9.99998	44	.8 137
57	7.99775	755	7 99777	755	2.00223	9.99998	43	.9 140 1.0 145
58	8.00530	742	8.00532	742	1.99468	9.99998	42	1.0 145
59	8.01272	730	8.01274	730	1.98726	9.99998	41	
60	8.02002	718	8.02004	718	1.97996	9.99998	40	
61	8.02720	706	8.02722	707	1.97278	9.99998	39	· ·
62	8.03426	695	8.03429	695	1.96571	9.99997	38	
63	8.04121	684	8.04124	684	1.95876	9.99997	37	
64	8.04805	673	8.04808	673	1.95192	9.99997	36	i,
65	8.05478	663	8.05481	663	1.94519	9.99997	35	Jen
66	8.06141	653	8.06144	653	1.93856	9.99997	34	T;
67	8.06794	644	8.06797	644	1.93203	9.99997	33	lg n
68	8.07438	634	8.07441	634	1.92559	9.99997	32	α_o^{α}
69	8.08072	624	8.08075	625	1.91925	9.99997	31	s are small: S; log tan $\alpha = \log \alpha^{\circ} -$ $+ S = \log \tan \alpha + T$. use sin and tan of compl
70	8.08696	616	8.08700	616	1.91300	9.99997	30	π α μ α μ α μ α μ α μ α μ α μ α μ α μ α
71	8.09312	608	8.09316	607	1.90684	9.99997	29	tar ta
72	8.09920	599	8.09923	599	1.90077	9.99997	28	an all
73	8.10519	591	8.10522	591	1.89478	9.99996	27	sn gt l
74	8.11110	583	8.11113	583	1.88887	9.99996	26	are lo S = siis
75	8.11693	575	8.11696	576	1.88304	9.99996	25	SS (S + S);
76	8.12268	568	8.12272	567	1.87728	9.99996	24	when angle $= \log \alpha^{\circ} -$ $= \log \sin \alpha$ of near 90° u
77	8.12836	560	8.12839	561	1.87161	9.99996	23	ang sin 190
78	8.13396	553	8.13400	553	1.86600	9.99996	22	log og ean
79	8.13949	546	8.13953	547	1.86047	9.99996	21	1
80	8.14495		8.14500		1.85500	9.99996	20	To interpolate when angles are small: $\log \sin \alpha = \log \alpha^* - S; \ \log \tan \alpha = \log \alpha^* - T; \\ \log \alpha^* = \log \sin \alpha + S = \log \tan \alpha + T.$ For \cos and \cot near 90° use \sin and \tan of complement.
81	8.15035	540 533	8.15039	539 533	1.84961	9.99996	19	ola sin sin og c
82	8.15568	526	8.15572	527	1.84428	9.99996	18	og Se
83	8.16094	- 1	8.16099		1.83901	9.99995	17	nte Je
84	8.16614	520 514	8.16619	520 514	1.83381	9.99995	16	o i
85	8.17128	508	8.17133	508	1.82867	9.99995	15	T Æ
86	8.17636	502	8.17641	502	1.82359	9.99995	14	
87	8.18138	496	8.18143	496	1.81857	9.99995	13	
88	8.18634	491	8.18639	491	1.81361	9.99995	12	Ω.
89	8.19125	485	8.19130	486	1.80870	9.99995	11	
90	8.19610	480	8.19616	480	1.80384	9.99995	10	
91	8.20090	475	8.20096	474	1.79904	9.99995	09	
92	8.20565	469	8.20570	474	1.79430	9.99994	08	T
93	8.21034	465	8.21040	464	1.78960	9.99994	07	_
94	8.21499	459	8.21504	460	1.78496	9.99994	06	<u>°</u> 1.758
95	8.21958	455	8.21964	455	1.78036	9.99994	05	.5 112
96	8.22413	450	8.22419	450	1.77581	9.99994	04	.6 107
97	8.22863	445	8.22869	446	1.77131	9.99994	03	.7 101
98	8.23308	443 44I	8.23315	441	1.76685	9.99994	02	8 094
99	8.23749	- 1	8.23756	436	1.76244	9.99994	01	9 087
100	8.24186	437	8.24192	430	1.75808	9.99993	00	1.0 079
	Cos	d.	Cot	d. c.	Tan	Sin		
						~		

1°							178	
	Sin	d.	Tan	d. c.	Cot	Cos		
00	8.24186		8.24192		1.75808	9.99993	100	
01	8.24618	432	8.24624	432	1.75376	9.99993	99	S
02	8.25045	427	8.25052	428	1.74948	9.99993	98	° 1.758
43	8.25469	424	8.25476	424	1.74524	9.99993	97	
04	8.25889	420	8,25896	420	1.74104	9.99993	96	1.0 145
05	8.26304	415	8.26312	416	1.73688	9.99993	95	.1 149 .2 154
oŝ	8.26716	412	8.26723	411	1.73277	9.99993	94	.3 160
07	8.27124	408	8.27131	408	1.72869	9.99992	93	.4 166
08	8.27528	404	8.27535	404	1.72465	9.99992	92	.5 172
09	8.27928	400	8.27936	401	1.72064	9.99992	91	
10	8.28324	396	8.28332	396	1.71668	9.99992	90	
•	8.28717	393	8.28725	393	1.71275	9.99992	89	
II I2	8.29107	390	8.29115	390	1.70885	9.99992	88	
13	8.29493	386	8.29501	386	1.70499	9.99992	87	
		382	8.29884	383	l .		86	jt.
14	8.29875	380	8.30263	379	1.70116	9.99991	85	ne.
15 16	8.30255 8.30631	376	8.30639	376	1.69737	9.99991	84	ler
		372		373	1	9.99991		n du
17	8.31003	370	8.31012	370	1.68988	9.99991	83	T;
18	8.31373	366	8.31382	367	1.68618	9.99991	82	1 💃
19	8.31739	364	8.31749	363	1.68251	9.99991	81	α° – T.
20	8.32103	360	8.32112	361	1.67888	9.99990	80	e small: S; log tan α = log $+S$ = log tan α + 9 ° use sin and ta
21	8.32463	_	8.32473	-	1.67527	9.99990	79	l = 1 nd
22	8.32820	357	8.32830	357	1.67170	9.99990	78	and a
23	8.33175	355 352	8.33185	355 352	1.66815	9.99990	77	un og t
24	8.33527		8.33537		1.66463	9.99990	76	2 tz 2 tz 3 tz 3 tz 3 tz 3 tz 3 tz 3 tz
25	8.33875	348	8.33886	349	1.66114	9.99990	75	log log
26	8.34221	346	8.34232	346	1.65768	9.99989	74	S: S1
27	8.34565	344	8.34575	343	1.65425	9.99989	73	βα', απ' μτ' μτ' μτ' μτ' μτ' μτ' μτ' μτ' μτ' μτ
28	8.34905	340	8.34916	341	1.65084	9.99989	72	ne ii. 🕻 s
29	8.35243	338	8.35254	338	1.64746	9.99989	71	rgi g g s g s s s
30	8.35578	335	8.35590	336	1.64410	9.99989	70	olate when angles are small: $\log \sin \alpha = \log \alpha^{o} - T;$ $\log \sin \alpha = \log \sin \alpha + S = \log \tan \alpha + T.$ $\det \cot \sin \alpha = \cot \alpha + T.$ $\det \cot \alpha = \cot \alpha $
	8.35911	333	8.35922	332	1.64078	9.99989	69	8 B
31	8.36241	330	8.36253	331	1.63747	9.99988	68	ute wheginα sinα cot of a
32	8.36569	328	8.36581	328	1.63419	9.99988	67	te og si
33		325	ľ	325	1			ola log ld
34	8.36894	323	8.36906	323	1.63094	9.99988 9.99988	66 65	ar ar
35 36	8.37217	321	8.37229 8.37550	321	1.62450	9.99988	64	nte os
	8.37538	318		318	1			To interpolate when angles are small: $\log \sin \alpha = \log \alpha' - S$; $\log \tan \alpha = \log \sin \alpha + S = \log \cos \sin \alpha + S = \log \cos \cos \alpha$ For $\cos \sin \alpha \cos \alpha$ or of angles near $\cos \alpha$ use
37	8.37856	315	8.37868	316	1.62132	9.99988	63 62	T Y
38	8.38171	314	8.38184 8.38498	314	1.61502	9.99987	61	
39	8.38485	311		311		9.99987		
40	8.38796	309	8.38809	309	1.61191	9.99987	60	
4 I	8.39105	307	8.39118	307	1.60882	9.99987	59	
42	8.39412	305	8.39425	305	1.60575	9.99987	58	
43	8.39717	302	8.39730	303	1.60270	9.99986	57	T
44	8.40019	301	8.40033	301	1.59967	9.99986	56	° 1.758
45	8.40320	298	8.40334	298	1.59666	9.99986	55	1.0 079
46	8.40618	293	8.40532	298	1.59368	9.99986	54	.1 069
47	8.40915		8.40929		1.59071	9.99986	53	.2 059
48	8.41209	294	8.41224	295	1.58776	9.99986	52	.3 048
49	8.41501	292	8.41516	292	1.58484	9.99985	51	.4 036
50	8.41792	291	8.41807	291	1.58193	9.99985	50	.5 023
	Cos	d.	Cot	d. c.	Tan	Sin	_	
	CUS	u,	COL	u, c.	1 Lan	DIII	·	

	· C.	. 3	. T	1	C :			
<u> </u>	Sin	d.	Tan	d.c.	Cot	Cos	 	
50	8.41792	288	8.41807	288	1.58193	9.99985	50	
51	8.42080	287	8.42095	287	1.57905	9.99985	49 48	S
52	8.42367	285	8.42382	285	1.57618	9.99985		° 1.758
53	8.42652	283	8.42667	283	1.57333	9.99985	47	I.5 172
54	8.42935	281	8.42950	282	1.57050	9.99984	46	.6 179
55	8.43216	279	8.43232	279	1.56768	9.99984	45	.7 186
56	8.43495	277	8.43511	278	1.56489	9.99984	44	.8 194
57	8.43772	276	8.43789	275	1.56211	9.99984	43	.9 202
58	8.44048	274	8.44064	275	1.55936	9.99983	42	2.0 211
59	8.44322	272	8.44339	272	1.55661	9.99983	41	
60	8.44594	271	8.44611	271	1.55389	9.99983	40	
61	8.44865	268	8.44882	269	1.55118	9.99983	39	
62	8.45133	268	8.45151	267	1.54849	9.99983	38	
63	8.45401	265	8.45418	266	1.54582	9.99982	37	<u>;</u>
64	8.45666	264	8.45684	264	1.54316	9.99982	36	Je II
65	8.45930	262	8.45948	263	I.54052	9.99982	35	en
66	8.46192	261	8.46211	261	1.53789	9.99982	34	,. Idu
67	8.46453		8.46472		1.53528	9.99982	33	roz
68	8.46712	259 258	8.46731	259 258	I.53269	9.99981	32	, . Je
69	8.46970	256	8.46989	256	1.53011	9.99981	31	r T.
70	8.47226		8.47245		I.52755	9.99981	30	10g + 21
71	8.47481	255	8.47500	255	1.52500	9.99981	29	nd n
72	8.47734	253	8.47754	254	1.52246	9.99980	28	tan n
73	8.47986	252	8.48006	252	1.51994	9.99980	27	Sin sin
74	8.48236	250	8.48256	250	1.51744	9.99980	26	2g 1 = 1 1se
75	8.48485	249	8.48505	249	1.51495	9.99980	25	. 1c. S
76	8.48732	247	8.48753	248	1.51247	9.99980	24	s s + g
77	8.48978	246	8.48999	246	1.51001	9.99979	23	η α στ σ – σ στ σ – σ στ
78	8.49223	245	8.49244	245	1.50756	9.99979	22	Sir a sir
79	8.49466	243	8.49487	243	1.50513	9.99979	21	log log
80	8.49708	242	8.49729	242	1.50271	9.99979	20	To interpolate when angles are small: $\log \sin \alpha = \log \alpha' - T;$ $\log \sin \alpha = \log \alpha' - S; \log \tan \alpha = \log \alpha' - T;$ $\log \alpha' = \log \sin \alpha + S = \log \tan \alpha + T.$ For \cos and \cot of angles near 90° use \sin and \tan of complement.
81	8.49948	240	8.49970	241	1.50030	9.99978	19	a, α of ε
82	8.50188	240	8.50209	239	1.49791	9.99978	18	sin og o
83	8.50425	237	8.50448	239	1.49552	9.99978	17	ate og s lc l cc
84	8.50662	237	8.50684	236	1.49316	9.99978	16	Pod F H
85	8.50897	235	8.50920	236	1.49080	9.99977	15	er!
86	8.51131	234	8.51154	234	1.48846	9.99977	14	Tii 55
87	8.51364	233	8.51387	233	1.48613	9.99977	13	For
88	8.51596	232	8.51619	232	1.48381	9.99977	12	
89	8.51826	230	8.51850	231	1.48150	9.99976	11	
90	8.52055	229	8.52079	229	1.47921	9.99976	10	
91	8.52283	228	8.52307	228	1.47693	9.99976	09	
92	8.52510	227	8.52534	227	1.47466	9.99976	08	T
93	8.52735	225	8.52760	226	1.47240	9.99975	07	
94	8.52960	225	8.52985	225	1.47015	9.99975	06	1./3
95	8.53183	223	8.53208	223	1.46792	9.99975	05	1.5 8023
96	8.53405	222	8.53430	222	1.46570	9.99975	04	.6 8010
97	8.53626	221	8.53651	221	1.46349	9.99974	03	.7 7995
98	8.53846	220	8.53872	221	1.46128	9.99974	02	.8 7980 .9 7963
99	8.54064	218	8.54091	219	1.45909	9.99974	OI	.9 7963 2.0 7946
100	8.54282	218	8.54308	217	1.45692	9.99974	00	2.0 . /940
	Cos	d.	Cot	d. c.	Tan	Sin	اتت	
	COS	u.	COL	u. c.	Tan	• 5111	I	

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	Sin	d.	Tan	d. c.	Cot	Cos	I	
00	8.54282	216	8.54308	217	1.45692	9.99974	100	
01	8.54498		8.54525		1.45475	9.99973	99	S
02	8.54714	216	8.54741	216	I.45259	9.99973	98	° 1.758
03	8.54928	214 214	8.54956	215 213	1.45044	9.99973	97	2.0 211
04	8.55142		8.55169		1.44831	9.99972	96	.I 220
05	8.55354	212	8.55382	213	1.44618	9.99972	95	.2 229
06	8.55565	2II 2I0	8.55593	211 211	I.44407	9.99972	94	.3 239
07	8.55775		8.55804	1 !	1.44196	9.99972	93	.4 250
08	8.55985	210	8.56013	209	1.43987	9.99971	92	.5 260
09	8.56193	208 207	8.56222	209	1.43778	9.99971	91	
10	8.56400		8.56429	207	1.43571	9.99971	90	
11	8.56606	206	8.56636	207	1.43364	9.99971	89	
12	8.56811	205	8.56841	205	1.43159	9.99970	88	í
13	8.57016	205	8.57046	205	I.42954	9.99970	87	نيا
14	8.57219	203	8.57249	203	1.42751	9.99970	86	l E
15	8.57421	202	8.57452	203	1.42548	9.99969	85	en
16	8.57623	202	8.57654	202	1.42346	9.99969	84	lqr
		200		200	1.42146	9.99969	83	T_i
17 18	8.57823	200	8.57854 8.58054	200	1.42140	9.99969	82	1 , 4
19	8.58023 8.58222	199	8.58253	199	1.41747	9.99968	81	^{-}T .
		197		198			80	80 + tg
20	8.58419	197	8.58451	198	1.41549	9.99968	1	e small: S; log $\tan \alpha = \log \alpha^{\circ} - T$; $+ S = \log \tan \alpha + T$. 90° use sin and \tan of complement.
21	8.58616	196	8.58649	196	1.41351	9.99968	79	ta:
22	8.58812	195	8.58845	195	1.41155	9.99967	78	og og
23	8.59007	194	8.59040	195	1.40960	9.99967	77	
24	8.59201	194	8.59235	193	1.40765	9.99967	76	lo lo u
25	8.59395	192	8.59428	193	1.40572	9.99967	75	S + S
26	8.59587	192	8.59621	192	1.40379	9.99966	74	# 8 F
27	8.59779	191	8.59813	191	1.40187	9.99966	73	es a sin
28	8.59970	190	8.60004	190	1.39996	9.99966	72	181 28 28 29 29 29 29 29 29 29 29 29 29 29 29 29
29	8.60160	189	8.60194	190	1.39806	9.99965	71	F 1 2 12 12 12 12 12 12 12 12 12 12 12 12
30	8.60349	188	8.60384	188	1.39616	9.99965	70	To interpolate when angles are small: $\log\sin\alpha = \log\alpha' - S$; $\log\tan\alpha = \log\sin\alpha + S = \log\sin\alpha + S = 1$ For \cos and \cot of angles near 90° use
31	8.60537		8.60572	188	1.39428	9.99965	69	wh in g
32	8.60725	188 186	8.60760		1.39240	9.99964	68	te lo lo col
33	8.60911	186	8.60947	187 186	1.39053	9.99964	67	log pr
34	8.61097		8.61133	1	1.38867	9.99964	66	E E
35	8.61282	185	8.61319	186	1.38681	9.99963	65	l t 8
36	8.61467	185 183	8.61504	185 183	1.38496	9.99963	64	, in 19
37	8.61650		8.61687	1	1.38313	9.99963	63	ř ř
38	8.61833	183	8.61870	183	1.38130	9.99963	62	I
39	8.62015	182	8.62053	183	1.37947	9.99962	61	1
40	8.62196	181	8.62234		1.37766	9.99962	60	
41	8.62377	181	8.62415	181	1.37585	9.99962	59	Ì
42	8.62556	179	8.62595	180	1.37405	9.99961	58	T
43	8.62735	179	8.62774	179	1.37226	9.99961	57	
1 '	8.62914	179	8.62953	179	1.37047	9.99961	56	1.757
44 45	8.63091	177	8.63131	178	1.36869	9.99960	55	2.0 946
46	8.63268	177	8.63308	177	1.36692	9.99960	54	.1 928
		176	8.63484	176	1.36516	9.99960	53	.2 909
47 48	8.63444 8.63619	175	8.63660	176	1.36340	9.99959	52	.3 889
49	8.63794	175	8.63835	175	1.36165	9.99959	51	.4 869
50		174		174		9.99959	50	.5 847
-00	8.63968		8.64009		1.35991	Sin	——	
	Cos	d.	Cot	d.c.	Tan	• 51n		

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	Sin	d.	Tan	d. c.	Cot	Cos		
50	8.63968	173	8.64009	174	1.35991	9.99959	50	
51	8.64141		8.64183		1.35817	9.99958	49	S
52	8.64314	173	8.64356	173	1.35644	9.99958	48	° 1.758
53	8.64486	172 171	8.64528	172 172	1.35472	9.99958	47	2.5 260
54	8.64657		8.64700		1.35300	9.99957	46	.6 272
55	8.64827	170	8.64870	170	1.35130	9.99957	45	.7 283
56	8.64997	170 169	8.65041	171 169	1.34959	9.99957	44	.8 296
57	8.65166		8.65210	-	1.34790	9.99956	43	.9 308
58	8.65335	169	8.65379	169	1.34621	9.99956	42	3.0 32 I
59	8.65503	168 167	8.65547	168 168	I.34453	9.99956	41	
60	8.65670	167	8.65715	167	1.34285	9.99955	40	
61	8.65837		8.65882		1.34118	9.99955	39	
62	8.66003	166	8.66048	166	1.33952	9.99955	38	
63	8.66168	165	8.66214	166	1.33786	9.99954	37	44
64	8.66333	165	8.66379	165	1.33621	9.99954	36	en
65	8.66497	164	8.66543	164	1.33457	9.99954	35	E
66	8.66660	163	8.66707	164	I.33293	9.99953	34	la
67	8.66823	163	8.66870	163	1.33130	9.99953	33	-T;
68	8.66985	162	8.67033	163	1.32967	9.99952	32	ا پي
69	8.67147	162	8.67195	162	1.32805	9.99952	31	$g \alpha^{\circ}$. + T.
70	8.67308	161	8.67356	161	1.32644	9.99952	30	e small: S; log tan $\alpha = \log x$ $+S = \log \tan \alpha + \cos \alpha$ 90° use sin and tan
	8.67468	160		161	1.32483			nd a
71 72	8.67628	160	8.67517 8.67677	160	1.32403	9.99951 9.99951	29 28	tar a
73	8.67788	160	8.67837	160	1.32323	9.99951	27	an Sir
		158		159			26	
74	8.67946	158	8.67996	158	1.32004	9.99950		S = S
75 76	8.68104 8.68262	158	8.68154 8.68312	158	1.31846	9.99950	25	8 + 8
		157	1	158	1.31688	9.99950	24	n angles are si = $\log \alpha^{\alpha} - S$; = $\log \sin \alpha +$ angles near 90
77	8.68419	156	8.68470	156	1.31530	9.99949	23	es sin ne
78	8.68575	156	8.68626	157	1.31374	9.99949	22	12g1
79	8.68731	155	8.68783	155	1.31217	9.99948	21	ng = F
80	8.68886	155	8.68938	155	1.31062	9.99948	20	late when angles: $\log \sin \alpha = \log \alpha^{\circ}$ $\log \alpha^{\circ} = \log \sin \alpha$ d cot of angles ne
81	8.69041	154	8.69093	155	1.30907	9.99948	19	t o ii w
82	8.69195	154	8.69248	154	1.30752	9.99947	18	8 5 g te
83	8.69349	153	8.69402	153	1.30598	9.99947	17	를 의 함
84	8.69502	152	8.69555	153	1.30445	9.99947	16	G e
85	8.69654	152	8.69708	152	1.30292	9.99946	15	l i š
86	8.69806	152	8.69860	152	1.30140	9.99946	14	To interpolate when angles are small: $\log \sin \alpha = \log \alpha' - S; \log \tan \alpha = \log \alpha' - T; \\ \log \sin \alpha = \log \sin \alpha + S = \log \tan \alpha + T.$ For cos and cot of angles near 90° use sin and tan of complement.
87	8.69958	151	8.70012	152	1.29988	9.99945	13	F &
88	8.70109	150	8.70164	150	1.29836	9.99945	12	
89	8.70259	150	8.70314	151	1.29686	9.99945	11	
90	8.70409	149	8.70465	149	1.29535	9.99944	10	
91	8.70558		8.70614	1	1.29386	9.99944	09	
92	8.70707	149 149	8.70764	150 148	1.29236	9.99944	.08	T
93	8.70856	149	8.70912	149	1.29088	9.99943	07	° 1.757
94	8.71003	148	8.71061		1.28939	9.99943	06	
95	8.71151	148	8.71208	147	1.28792	9.99942	05	2.5 847 .6 824
96	8.71298	147	8.71356	146	1.28644	9.99942	04	.7 801
97	8.71444		8.71502		1.28498	9.99942	03	.8 777
98	8.71590	146	8.71649	147	1.28351	9.99941	02	.9 752
99	8.71735	145 145	8.71794	145	1.28206	9.99941	OI	3.0 725
100	8.71880	143	8.71940	140	1.28060	9.99940	00	' '
	Cos	d.	Cot	d.c.	Tan	Sin	J——	
	. 003	u.	- 000	u.c.	. 1911	. 0111	-	•

3°							176°			
	Sin	d.	Tan	d.c.	Cot	Cos			P. P.	
00	8.71880		8.71940		1.28060	9.99940	100	ı	145	143
01	8.72024	144	8.72084	144	1.27916	9.99940	99	2	14.5 29.0	14.3 28.6
02	8.72168	144	8.72229	145	1.27771	9.99940	98	3	43.5	42.9
03	8.72312	144 143	8.72373	I44 I43	1.27627	9.99939	97	5	58.0 72.5	57.2 71.5
04	8.72455		8.72516		1.27484	9.99939	96	5 6	87.0	85.8
05	8.72597	142 142	8.72659	143 142	1.27341	9.99938	95	7 8	101.5	100.1 114.4
06	8.72739	142	8.72801	142	1.27199	9.99938	94	9	130.5	128.7
07	8.72881	141	8.72943		1.27057	9.99938	93		141	139
08	8.73022	141	8.73085	142 141	1.26915	9.99937	92	1 2	14.1 28.2	13.9 27.8
09	8.73163	140	8.73226	140	1.26774	9.99937	91	3	42.3	41.7
10	8.73303	139	8.73366	140	1.26634	9.99936	90	4	56.4 70.5	55.6
11	8.73442		8.73506	1	1.26494	9.99936	89	5 6	84.6	69.5 83.4
12	8.73582	140 139	8.73646	140	1.26354	9.99936	88	7	98.7	97.3
13	8.73721	138	8.73785	139	1.26215	9.99935	87	8 9	112.8	111.2
14	8.73859	138	8.73924	1	1.26076	9.99935	86	"	120.9	125.1 137
15	8.73997	137	8.74063	139	1.25937	9.99934	85	1	13.8	13.7
16	8.74134	138	8.74201	137	1.25799	9.99934	84	3	27.6 41.4	27.4 41.1
17	8.74272	136	8.74338	137	1.25662	9.99933	83	4	55.2	54.8
18	8.74408	136	8.74475	137	I.25525	9.99933	82	5	69.0	68.5
19	8.74544	136	8.74612	136	1.25388	9.99933	81		82.8 96.6	82.2
20	8.74680	136	8.74748	136	I.25252	9.99932	80	7 8	110.4	95.9 109.6
21	8.74816	_	8.74884	_	1.25116	9.99932	79	9	124.2	123.3
22	8.74950	134 135	8.75019	135	1.24981	9.99931	78	1	135 13.5	138
23	8.75085	134	8.75154	135	1.24846	9.99931	77	2	27.0	13.3 26.6
24	8.75219	134	8.75289	134	1.24711	9.99931	76	3	40.5	39.9
25	8.75353	133	8.75423	133	1.24577	9.99930	75	4 5	54.0 67.5	53.2 66.5
26	8.75486	133	8.75556	134	I.24444	9.99930	74	5 6	81.0	79.8
27	8.75619	132	8.75690	133	1.24310	9.99929	73	7 8	94.5	93.1 106.4
28 29	8.75751 8.75883	132	8.75823	132	1.24177	9.99929	72	9	121.5	119.7
		132	8.75955	132	1.24045	9.99928	71		131	129
30	8.76015	131	8.76087	132	1.23913	9.99928	70	1 2	13.1 26.2	12.9 25.8
31	8.76146	131	8.76219	131	1.23781	9.99927	69	3	39.3	38.7
32	8.76277 8.76408	131	8.76350	131	1.23650	9.99927	68	4	52.4	51.6
33		130	8.76481	131	1.23519	9.99927	67	5 6	65.5 78.6	64.5 77.4
34	8.76538 8.76667	129	8.76612	130	1.23388	9.99926	66	7 8	91.7	90.3
35 36	8.76797	130	8.76742 8.76871	129	1.23258	9.99926	65 64	9	104.8	103.2 116.1
		129		130		9.99925		"	128	127
37 38	8.76926 8.77054	128	8.77001 8.77130	129	1.22999	9.99925 9.99924	63 62	1	12.8	12.7
39	8.77182	128	8.77258	128	1.22742	9.99924	61	3	25.6 38.4	25.4 38.1
40	8.77310	128	8.77387	129			60	4	51.2	50.8
		128		127	1.22613	9.99923		5 6	64.0 76.8	63.5 76.2
41 42	8.77438 8.77565	127	8.77514 8.77642	128	1.22486	9.99923	59 58		89.6	88.9
43	8.77691	126	8.77769	127	I.22358 I.2223I	9.99923 9.99922	58 57	7 8	102.4	101.6
44	8.77817	126		127				9	115.2 125	114.3 124
45	8.77943	126	8.77896 8.78022	126	1.22104	9.99922 9.99921	56 55	1	12.5	12.4
46	8.78069	126	8.78148	126	1.21852	9.99921	54	2	25.0	24.8
47	8.78194	125	8.78274	126	1.21726	9.99920	53	3 4	37.5 50.0	37.2 49.6
48	8.78319	125	8.78399	125	1.21/20	9.99920	53 52	5 6	62.5	02.0
49	8.78443	124 125	8.78524	125 125	1.21476	9.99919	51		75.0 87.5	74.4 86.8
50	8.78568	123	8.78649	125	1.21351	9.99919	50	7 8	100.0	99.2
								9	112.5	111.6
	Cos	d.	Cot	d. c.	Tan	Sin			P. P.	

3°							176°	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	8.78568		8.78649		1.21351	9.99919	50	123 122 1 12.3 12.2
51	8.78691	123	8.78773	124	1.21227	9.99918	49	2 24.6 24.4
52	8.78815	124	8.78897	124	1.21103	9.99918	48	3 36.9 36.6 4 49.2 48.8
53	8.78938	123 122	8.79020	123 123	1.20980	9.99918	47	5 61.5 61.0
54	8.79060		8.79143		1.20857	9.99917	46	
55	8.79183	123	8.79266	I23 I23	1.20734	9.99917	45	7 86.1 85.4 8 98.4 97.6
56	8.79305	121	8.79389	122	1.20611	9.99916	44	9 110.7 109.8
57	8.79426	122	8.79511	122	1.20489	9.99916	43	121 119 I I2.I II.9
58 59	8.79548 8.79669	121	8.79633	121	1.20367	9.99915	42	2 24.2 23.8
		120	8.79754	121	1.20246	9.99915	41	3 36.3 35.7 4 48.4 47.6
60	8.79789	121	8.79875	121	1.20125	9.99914	40	5 60.5 59.5
61	8.79910	120	8.79996	120	1.20004	9.99914	39	
62 63	8.80030 8.80149	119	8.80116 8.80237	121	1.19884	9.99913	38	7 84.7 83.3 8 96.8 95.2
55.		120		119	1.19763	9.99913	37	9 108.9 107.1
64 65	8.80269 8.80388	119	8.80356 8.80476	120	1.19644	9.99912	36	118 117 1 11.8 11.7
66	8.80506	118	8.80470	119	I.19524 I.19405	9.99912	35 34	2 23.6 23.4
	8.80625	119		119				3 35 4 35 I
67 68	8.80743	118	8.80714 8.80832	118	1.19286	9.99911	33 32	4 47.2 46.8 5 59.0 58.5
69	8.80860	117	8.80950	118	1.19050	9.99910	31	6 70.8 70.2
70	8.80978	118	8.81068	118	1.18932	9.99909	30	7 82.6 81.9 8 94.4 93.6
71	8.81095	117	8.81186	118	1.18814	9.99909	29	9 106.2 105.3
72	8.81212	117	8.81303	117	1.18697	9.99909	28	116 115
73	8.81328	116	8.81420	117	1.18580	9.99908	27	1 II.6 II.5 2 23.2 23.0
74	8.81444	116	8.81537	117	1.18463	9.99907	26	3 34.8 34.5
75	8.81560	116	8.81653	116	1.18347	9.99907	25	4 46.4 46.0 5 58.0 57.5
76	8.81675	115 116	8.81769	116	1.18231	9.99906	24	6 69.6 69. 0
77	8.81791		8.81885		1.18115	9.99906	23	7 81.2 80.5 8 92.8 92.0
78	8.81905	114 115	8.82000	115	1.18000	0.99905	22	9 104.4 103.5
79	8.82020	114	8.82115	115	1.17885	9.99905	21	114 113
80	8.82134	114	8.82230	114	1.17770	9.99904	20	I II.4 II.3 2 22.8 22.6
81	8.82248	114	8.82344	114	1.17656	9.99904	19	3 34.2 33.9
82	8.82362 8.82475	113	8.82458 8.82572	114	1.17542	9.99903	18	4 45.6 45.2 5 57.0 56.5
83		113		114	1.17428	9.99903	17	6 68.4 67.8
84 85	8.82588 8.82701	113	8.82686 8.82799	113	I.17314 I.17201	9.99902	16 15	7 79.8 79.1 8 91.2 90.4
86	8.82814	113	8.82912	113	1.17281	9.99902	14	9 102.6 101.7
87	8.82926	112	8.83025	113	1.16975	9.99901	13	112 111
88	8.83038	112	8.83137	112	1.16863	9.99900	13	I II.2 II.I 2 22.4 22.2
89	8.83149	111 112	8.83249	II2 II2	1.16751	9.99900	11	3 33.6 33.3
90	8.83261	III	8.83361	112	1.16639	9.99899	10	4 44.8 44.4 5 56.0 55.5 6 67.2 66.6
91	8.83372		8.83473		1.16527	9.99899	09	
92	8.83482	111	8.83584	III	1.16416	9.99898	08	8 89.6 88.8
93	8.83593	110	8.83695	III	1.16305	9.99898	07	9 100.8 99.9
94	8.83703	110	8.83806	110	1.16194	9.99897	06	1 109 108 1 10.9 10.8
95	8.83813	110	8.83916	110	1.16084	9.99897	05	2 21.8 21.6
96	8.83923	109	8.84026	110	1.15974	9.99896	04	3 32.7 32.4 4 43.6 43.2
97 98	8.84032 8.84141	109	8.84136 8.84246	110	1.15864	9.99896	03	5 54.5 54.0
99	8.84250	109	8.84355	109	1.15/54	9.99895	01	6 65.4 64.8
100	8.84358	108	8.84464	109	1.15536	9.99894	00	8 87.2 86.4
		d.	Cot	4 .		Sin		9 98.1 97.2 P. P.
	Cos	a.	COt	d. c.	Tan	Sin		P. P.

_							110			
	Sin	d.	Tan	d. c.	Cot	Cos	<u> </u>		P. P.	
00	8.84358		8.84464		1.15536	9.99894	100	1	109 10.9	108 10.8
01	8.84467	109	8.84573	109	I.15427	9.99894	99	2	21.8	21.6
02	8.84575	108	8.84682	109	1.15318	9.99893	98	3	32.7	32.4
03	8.84682	107	8.84790	108	1.15210	9.99892	97	4	43.6 54.5	43.2
		108		108				5 6	65.4	54.0 64.8
04	8.84790 8.84897	107	8.84898 8.85006	108	1.15102	9.99892 9.99891	96	7 8	76.3	75.6 86.4
o5 o6	8.85004	107	8.85113	107	1.14994	9.99891	95 94		87.2	
		107		107				9	98.1 107	97.2 106
07	8.85111	106	8.85220	107	1.14780	9.99890	93	1	10.7	10.6
08	8.85217	106	8.85327	107	1.14673	9.99890	92	2	21.4	21.2
09	8.85323	106	8.85434	106	1.14566	9.99889	91	3	32.I	31.8
10	8.85429	106	8.85540	106	1.14460	9.99889	90	4	42.8 53.5	42.4
11	8.85535		8.85646		I.14354	9.99888	89	5 6	64.2	53.0 63.6
12	8.85640	105	8.85752	106	1.14248	9.99888	88	7 8	74.9 85.6	74.2
13	8.85745	105	8.85858	106	1.14142	9.99887	87			84.8
14	8.85850	105	8.85963	105	1.14037	9.99887	86	9	96.3 105	95.4 104
15	8.85955	105	8.86069	106	1.13931	9.99886	85	I	10.5	10.4
16	8.86059	104	8.86173	104	1.13931	9.99885	84	2	21.0	20.8
1		104		105			· ·	3	31.5	31.2
17	8.86163	104	8.86278	105	1.13722	9.99885	83	4	42.0	41.6
18	8.86267 8.86370	103	8.86383 8.86487	104	1.13617	9.99884	82 81	5 6	52.5 63.0	52.0 62.4
19		101		104	1.13513	9.99884			73.5	72.8
20	8.86474	103	8.86591	103	1.13409	9.99883	80	7 8	84.0	83.2
21	8.86577	_	8.86694		1.13306	9.99883	79	9	94.5	93.6
22	8.8668o	103	8.86798	104	1.13202	9.99882	78	1	103	102 10.2
23	8.86782	102	8.86901	103	1.13099	9.99882	77	2	10.3 20.6	20.4
24	8.86885	103	8.87004	103	1.12996	9.99881	76	3	30.9	30.6
25	8.86987	102	8.87106	102	1.12894	9.99880	75	4	41.2	40.8
26	8.87089	102	8.87209	103	1.12791	9.99880	74	5 6	51.5 61.8	51.0 61.2
		IOI		102					72.I	71.4
27 28	8.87190 8.87292	102	8.87311	102	1.12689	9.99879	73	7 8	82.4	81.0
20 29	8.87393	IOI	8.87515	102	1.12507	9.99879 9.99878	72 71	9	92.7	91.8
		IOI		IOI					101	100
30	8.87494	100	8.87616	IOI	1.12384	9.99878	70	I 2	10.I 20.2	10.0 20.0
31	8.87594		8.87717	ì	1.12283	9.99877	69	3	30.3	30.0
32	8.87695	101	8.87819	102	1.12181	9.99876	68	4	40.4	40.0
33	8.87795	100	8.87919	100	1.12081	9.99876	67	5 6	50.5 60.6	50.0 60.0
34	8.87895		8.88020		1.11980	9.99875	66	7	70.7	70.0
35	8.87995	100	8.88120	100	1.11880	9.99875	65	7 8	80.8	80.0
36	8.88094	99	8.88220	100	1.11780	9.99874	64	9	90.9	90.0
37	8.88194	100	8.88320	100	1.11680	9.99874	63		99	98
38	8.88293	99	8.88420	100	1.11580	9.99873	62	I 2	9.9	9.8 19.6
39	8.88392	99	8.88519	99	1.11481	9.99872	61	3	29.7	29.4
40	8.88490	98	8.88618	99			60	4	39.6	39.2
		99		99	1.11382	9.99872		4 5 6	49.5 59.4	49.0 58.8
41	8.88589	98	8.88717	99	1.11283	9.99871	59	7	69.3	68.6
42	8.88687	98	8.88816	99	1.11184	9.99871	58	7 8	79.2	78.4
43	8.88785	98	8.88915	98	1.11085	9.99870	57	9	89.1	88.2
44	8.88883	97	8.89013	98	1.10987	9.99869	56	1	97	96 9.6
45	8.88980	97	8.89111	98 98	1.10889	9.99869	55	2	9.7 19.4	19.2
46	8.89077	97	8.89209	98	1.10791	9.99868	54	3	29.I	28.8
47	8.89174		8.89307		1.10693	9.99868	53	4	38.8	38.4
48	8.89271	97	8.89404	97	1.10596	9.99867	52	4 5 6	48.5 58.2	48.0
49	8.89368	97 96	8.89501	97	1.10499	9.99867	51	7	67.9	57.6 67.2
50	8.89464	90	8.89598	97	1.10402	9.99866	50	7 8 9	77.6 87.3	76.8 86.4
	Cos	d.	Cot	d. c.	Tan	Sin			P. P	
			200		2 411	~				

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	8.89464	0.77	8.89598	07	1.10402	9.99866	50	
51	8.89561	97	8.89695	97	1.10305	9.99865	49	97 96
52	8.89657	° 96	8.89792	97 96	1.10208	9.99865	48	I 9.7 9.6 2 19.4 19.2
53	8.89752	95 96	8.89888	96 96	1.10112	9.99864	47	3 29.1 28.8
54	8.89848		8.89984		1.10016	9.99864	46	4 38.8 38.4
55	8.89943	95	8.90080	96 96	1.09920	9.99863	45	5 48.5 48.0 6 58.2 57.6
56	8.90038	95 95	8.90176	96	1.09824	9.99862	44	7 67.9 67.2
57	8.90133		8.90272		1.09728	9.99862	43	8 77.6 76.8
58	8.90228	95	8.90367	95	1.09633	9.99861	42	9 87.3 86.4
59	8.90323	95 94	8.90462	95 95	1.09538	9.99860	41	95 94
60	8.90417	94	8.90557	95	1.09443	9.99860	40	I 9.5 9.4 2 19.0 18.8
61	8.90511		8.90652		1.09348	9.99859	39	3 28.5 28.2
62	8.90605	94	8.90746	94 95	1.09254	9.99859	38	4 38.0 37.6
63	8.90699	94	8.90841	93 94	1.09159	9.99858	37	5 47.5 47.0 6 57.0 56.4
64	8.90792	93	8.90935	94	1.09065	9.99857	36	6 57.0 56.4 7 66.5 65.8
65	8.90885	93	8.91029	93	1.08971	9.99857	35	7 66.5 65.8 8 76.0 75.2
66	8.90978	93 93	8.91122	93	1.08878	9.99856	34	9 85.5 84.6
67	8.91071		8.91216		1.08784	9.99856	33	93 92
68	8.91164	93	8.91309	93 93	1.08691	9.99855	32	1 9.3 9.2
69	8.91257	93 92	8.91402	93	1.08598	9.99854	31	2 18.6 18.4
70	8.91349	92	8.91495	93	1.08505	9.99854	30	3 27.9 27.6 4 37.2 36.8
71	8.91441		8.91588	93	1.08412	9.99853	29	
72	8.91533	92	8.91680	93	1.08320	9.99852	28	6 55.8 55.2
73	8.91625	92 91	8.91773	93	1.08227	9.99852	27	7 65.1 64.4 8 74.4 73.6
74	8.91716		8.91865		1.08135	9.99851	26	8 74.4 73.6 9 83.7 82.8
75	8.91807	91	8.91957	92 92	1.08043	9.99851	25	
76	8.91898	91	8.92049	91	1.07951	9.99850	24	1 91 90 9.1 9.0
77	8.91989	91	8.92140	91	1.07860	9.99849	23	2 18.2 18.0
78	8.92080	91	8.92231	92	1.07769	9.99849	22	3 27.3 27.0
79	8.92171	91 90	8.92323	91	1.07677	9.99848	21	4 36.4 36.0
80	8.92261		8.92414	90	1.07586	9.99847	20	5 45.5 45.0 6 54.6 54.0
81	8.92351	90	8.92504	91	1.07496	9.99847	19	7 63.7 63.0
82	8.92441	90	8.92595	90	1.07405	9.99846	18	8 72.8 72.0
83	8.92531	90	8.92685	91	1.07315	9.99846	17	9 81.9 81.0
84	8.92621	90	8.92776	90	1.07224	9.99845	16	89
85	8.92710	89	8.92866	90	1.07134	9.99844	15	I 8.9 2 17.8
86	8.92799	89 89	8.92956	89	1.07044	9.99844	14	2 17.8 3 26.7
87	8.92888	89	8.93045	90	1.06955	9.99843	13	4 35.6
88	8.92977	89	8.93135	89	1.06865	9.99842	12	5 44.5
89	8.93066	88	8.93224	89	1.06776	9.99842	11	
90	8.93154	89	8.93313	89	1.06687	9.99841	10	8 71.2
91	8.93243	88	8.93402	89	1.06598	9.99840	09	9 80.1
92	8.93331	88	8.93491	89	1.06509	9.99840	08	88 87
93	8.93419	88	8.93580	88	1.06420	9.99839	07	I 8.8 8.7
94	8.93507	87	8.93668	88	1.06332	9.99838	06	2 17.6 17.4 3 26.4 26.1
95	8.93594	88	8.93756	89	1.06244	9.99838	05	3 26.4 26.1 4 35.2 34.8
96	8.93682	87	8.93845	87	1.06155	9.99837	04	5 44.0 43.5
97	8.93769	87	8.93932	88	1.06068	9.99836	03	6 52.8 52.2 7 61.6 60.9
98	8.93856	87	8.94020	88	1.05980	9.99836	02	7 61.6 60.9 8 70.4 69.6
99	8.93943	87	8.94108	87	1.05892	9.99835	01	9 79.2 78.3
100	8.94030		8.94195		1.05805	9.99834	00	
	Cos	d.	Cot	d. c.	Tan	Sin	l	P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	1	P. P.
00	8.94030	86	8.94195	0.0	1.05805	9.99834	100	
01	8.94116		8.94282	87	1.05718	9.99834	99	1 87 86 1 8.7 8.6
02	8.94203	87 86	8.94369	87	1.05631	9.99833	98	2 17.4 17.2
03	8.94289	86	8.94456	87 87	1.05544	9.99832	97	3 26.1 25.8
04	8.94375	86	8.94543		1.05457	9.99832	96	4 34.8 34.4
05	8.94461	85	8.94630	87 86	1.05370	9.99831	95	5 43.5 43.0 6 52.2 51.6
06	8.94546	86	8.94716	86	1.05284	9.99830	94	7 60.9 60.2
07	8.94632	85	8.94802	86	1.05198	9.99830	93	8 69.6 68.8 9 78.3 77.4
08	8.94717	85	8.94888	86	1.05112	9.99829	92	
09	8.94802	85	8.94974	86	1.05026	9.99828	91	I 85 84 I 8.5 8.4
10	8.94887	85	8.95060	85	1.04940	9.99828	90	2 17.0 16.8
11	8.94972	85	8.95145	86	1.04855	9.99827	89	3 25.5 25.2
12	8.95057	84	8.95231	85	1.04769	9.99826	88	4 34.0 33.6 5 42.5 42.0
13	8.95141	85	8.95316	85	1.04684	9.99826	87	6 51.0 50.4
14	8.95226	84	8.95401	85	1.04599	9.99825	86	7 59.5 58.8 8 68.0 67.2
15 16	8.95310	84	8.95486	84	1.04514	9.99824	85 84	8 68.0 67.2 9 76.5 75.6
	8.95394	84	8.95570	85	1.04430	9.99824		
17	8.954 7 8 8.95562	84	8.95655	84	1.04345	9.99823 9.99822	83 82	83
19	8.95645	83	8.95739 8.95823	84	I.04261 I.04177	9.99822	81	I 8.3 2 16.6
20	8.95728	83	8.95908	85	1.04177	9.99821	80	3 24.9
		84		83				4 33.2
2I 22	8.95812 8.95895	83	8.95991 8.96075	84	I.04009 I.03925	9.99820 9.99820	79 78	5 41.5 6 49.8
23	8.95978	83	8.96159	84	1.03925	9.99819	77	7 58.1
-	8.96060	82	8.96242	83	1.03758	9.99819	76	
24 25	8.96143	83	8.96325	83	1.03758	9.99818	76 75	9 74.7
26	8.96225	82	8.96409	84	1.03573	9.99817	74	82 81
27	8,96308	83	8.96492	83	1.03508	9.99816	73	1 8.2 8.1 2 16.4 16.2
28	8.96390	82	8.96574	82	1.03426	9.99815	72	3 24.6 24.3
29	8.96472	82	8.96657	83	1.03343	9.99815	71	4 32.8 32.4
30	8.96553	81	8.96739	82	1.03261	9.99814	70	5 41.0 40.5 6 49.2 48.6
31	8.96635	82	8.96822	83	1.03178	9.99813	69	7 57.4 56.7 8 65.6 64.8
32	8.96716	81	8.96904	82	1.03096	9.99813	68	8 65.6 64.8
33	8.96798	82 81	8.96986	82 82	1.03014	9.99812	67	9 73.8 72.9
34	8.96879		8.97068		1.02932	9.99811	66	80
35	8.96960	81 81	8.97150	82 81	1.02850	9.99810	65	I 8.0
36	8.97041	81	8.97231	82	1.02769	9.99810	64	2 16.0 3 24.0
37	8.97122	80	8.97313	81	1.02687	9.99809	63	4 32.0
38	8.97202	81	8.97394	81	1.02606	9.99808	62	5 40.0 6 48.0
39	8.97283	80	8.97475	81	1.02525	9.99808	61	6 48.0 7 56.0
40	8.97363	80	8.97556	81	1.02444	9.99807	6 0	8 64.0
41	8.97443	80	8.97637	80	1.02363	9.99806	59	9 72.0
42	8.97523	80	8.97717	81	1.02283	9.99805	58	79 78
43	8.97603	79	8.97798	80	1.02202	9.99805	57	1 7.9 7.8
44	8.97682	80	8.97878	81	1.02122	9.99804	56	2 15.8 15.6 3 23.7 23.4
45	8.97762	79	8.97959	80	1.02041	9.99803	55	4 31.6 31.2
46	8.97841	79	8.98039	80	1.01961	9.99803	54	5 39.5 39.0
47	8.97920	80	8.98119	80	1.01881	9.99802	53	6 47.4 46.8 7 55.3 54.6
48 49	8.98000 8.98078	78	8.98199 8.98278	79	1.01801	9.99801 9.99800	52 51	8 63.2 62.4
50		79		80	1.01/22		50	9 71.1 70.2
-00	8.98157		8.98358	-		9.99800		P. P.
<u> </u>	Cos	d.	Cot	d. c.	Tan	Sin	049	

	Sın	d.	Tan	d.c.	Cot	Cos		P. P.
50	8.98157	79	8.98358	79	1.01642	9.99800	50	79 78
51	8.98236	78	8.98437		1.01563	9.99799	49	I 79 78
52	8.98314	79	8.98516	79 79	1.01484	9.99798	48	2 15.8 15.6
53	8.98393	78	8.98595	79	1.01405	9.99797	47	3 23.7 23.4
54	8.98471	78	8.98674	79	1.01326	9.99797	46	4 31.6 31.2 5 39.5 39.0
55	8.98549	78	8.98753	79	1.01247	9.99796	45	6 47.4 46.8
56	8.98627	78	8.98832	78	1.01168	9.99795	44	7 55.3 54.6
57	8.98705	77	8.98910	79	1.01090	9.99794	43	
58	8.98782	78	8.98989	78	I.OIOII	9.99794	42	9 71.1 70.2
59	8.98860	77	8.99067	78	1.00933	9.99793	41	77
60	8.98937	78	8.99145	78	1.00855	9.99792	40	I 7.7
61	8.99015		8.99223	78	1.00777	9.99791	39	2 I5.4 3 23.1
62	8.99092	77	8.99301	78	1.00699	9.99791	38	4 30.8
63	8.99169	77 76	8.99379	77	1.00621	9.99790	37	5 38.5
64	8.99245		8.99456	78	1.00544	9.99789	36	
65	8.99322	77 77	8.99534	70	1.00466	9.99788	35	7 53.9 8 61.6
66	8.99399	76	8.99611	77	1.00389	9.99788	34	9 69.3
67	8.99475	76	8.99688		1.00312	9.99787	33	76
68	8.99551	77	8.99765	77 77	1.00235	9.99786	32	1 7.6
69	8.99628	76	8.99842	77	1.00158	9.99785	31	2 15.2
70	8.99704		8.99919	76	1.00081	9.99785	30	3 22.8
71	8.99779	75	8.99995		1.00005	9.99784	29	4 30.4 5 38.0
72	8.99855	76	9.00072	77	0.99928	9.99783	28	5 38.0 6 45.6
73	8.99931	76	9.00148	76	0.99852	9.99782	27	7 53.2
74	9.00006	75	9.00225	77	0.99775	9.99782	26	
75	9.00082	76	9.00301	76 -6	0.99699	9.99781	25	9 68.4
76	9.00157	75	9.00377	76	0.99623	9.99780	24	75 74
77	9.00232	75	9.00452	75	0.99548	9.99779	23	1 7.5 7.4 2 15.0 14.8
78	9.00307	75	9.00528	76	0.99472	9.99779	22	3 22.5 22.2
79	9.00382	75 74	9.00604	76 75	0.99396	9.99778	21	4 30.0 29.6
80	9.00456		9.00679	76	0.99321	9.99777	20	5 37.5 37.0 6 45.0 44.4
8r	9.00531	75	9.00755		0.99245	9.99776	19	
82	9.00605	74	9.00830	75	0.99170	9.99776	18	8 60.0 59.2
83	9.00680	75	9.00905	75	0.99095	9.99775	17	9 67.5 66.6
84	9.00754	74	9.00980	75	0.99020	9.99774	16	73
85	9.00828	74	9.01055	75	0.98945	9.99773	15	I 7.3
86	9.00902	74 74	9.01129	74 75	0.98871	9.99772	14	2 14.6 3 21.9
87	9.00976		9.01204		0.98796	9.99772	13	3 21.9 4 29.2
88	9.01049	73	9.01278	74	0.98722	9.99771	12	5 36.5
89	9.01123	74 73	9.01353	75 74	0.98647	9.99770	11	
90	9.01196		9.01427		0.98573	9.99769	10	7 51.1 8 58.4
91	9.01269	73	9.01501	74	0.98499	9.99769	09	9 65.7
92	9.01343	74	9.01575	74	0.98425	9.99768	08	72
93	9.01416	73	9.01649	74	0.98351	9.99767	07	I 7.2
94	9.01489	73	9.01722	73	0.98278	9.99766	о6	2 14.4
95	9.01561	72	9.01796	74	0.98204	9.99765	05	3 21.6 4 28.8
96	9.01634	73	9.01869	73	0.98131	9.99765	04	
97	9.01707	73	9.01943	74	0.98057	9.99764	03	6 43.2
98	9.01779	72	9.02016	73	0.97984	9.99763	02	7 50.4
99	9.01851	72	9.02089	73	0.97911	9.99762	01	8 57.6 9 64.8
100	9.01923	72	9.02162	73	0.97838	9.99761	00	9 04.0
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
		ч.	- 000	4. 0.	1411	OIII		****

6.							1/3	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.01923	72	9.02162	77.2	0.97838	9.99761	100	50
01	9.01996	73	9.02235	73	0.97765	9.99761	99	73
02	9.02067	71	9.02308	73	0.97692	9.99760	98	1 7.3 2 14.6
03	9.02139	72 72	9.02380	72 73	0.97620	9.99759	97	3 21.9
04	9.02211		9.02453		0.97547	9.99758	96	4 29.2
05	9.02283	72 71	9.02525	72 72	0.97475	9.99757	95	5 36.5 6 43.8
06	9.02354	71	9.02597	73	0.97403	9.99757	94	6 43.8 7 51.1
07	9.02425		9.02670	ſ	0.97330	9.99756	93	7 51.1 8 58.4
08	9.02497	72 71	9.02742	72 71	0.97258	9.99755	92	9 65.7
09	9.02568	71	9.02813	72	0.97187	9.99754	91	72 71
10	9.02639	71	9.02885	72	0.97115	9.99753	90	I 7.2 7.1
11	9.02710		9.02957		0.97043	9.99753	89	2 14.4 14.2 3 21.6 21.3
12	9.02780	70	9.03028	71	0.96972	9.99752	88	4 28.8 28.4
13	9.02851	71 70	9.03100	72 71	0.96900	9.99751	87	5 36.0 35.5
14	9.02921		9.03171		0.96829	9.99750	86	6 43.2 42.6 7 50.4 49.7
15	9.02992	7I 70	9.03242	71 72	0.96758	9.99749	85	7 50.4 49.7 8 57.6 56.8
16	9.03062	70	9.03314	71	0.96686	9.99749	84	9 64.8 63.9
17	9.03132	70	9.03385	70	0.96615	9.99748	83	70
18	9.03202	70	9.03455	70	0.96545	9.99747	82	I 7.0
19	9.03272	70	9.03526	71	0.96474	9.99746	81	2 14.0
20	9.03342	70	9.03597	70	0.96403	9.99745	80	3 2I.0 4 28.0
21	9.03412	69	9.03667	71	0.96333	9.99744	79	
22	9.03481	70	9.03738	70	0.96262	9.99744	78	6 42.0
23	9.03551	69	9.03808	70	0.96192	9.99743	77	7 40.0 8 56.0
24	9.03620	70	9.03878	70	0.96122	9.99742	76	9 63.0
25	9.03690	69	9.03948	70	0.96052	9.99741	75	69 68
26	9.03759	69	9.04018	70	0.95982	9.99740	74	I 6.9 6.8
27	9.03828	69	9.04088	70	0.95912	9.99739	73	2 13.8 13.6
28	9.03897	69	9.04158	70	0.95842	9.99739	72	3 20.7 20.4 4 27.6 27.2
29	9.03966	68	9.04228	69	0.95772	9.99738	71	
30	9.04034	69	9.04297	70	0.95703	9.99737	70	6 41.4 40.8
31	9.04103	68	9.04367	69	0.95633	9.99736	69	7 48.3 47.6 8 55.2 54.4
32	9.04171	69	9.04436	69	0.95564	9.99735	68	9 62.1 61.2
33	9.04240	68	9.04505	69	0.95495	9.99734	67	67
34	9.04308	68	9.04574	69	0.95426	9.99734	66	1 6.7
35	9.04376	68	9.04643	69	0.95357 0.95288	9.99733	65 64	2 13.4
36	9.04444	68	9.04712	69		9.99732		3 20.1
37	9.04512	68	9.04781	69	0.95219	9.99731 9.99730	63 62	4 26.8 5 33.5
38 39	9.04580 9.04648	68	9.04050	68	0.95130	9.99730	61	6 40.2
40	9.04048	67	9.04987	69	0.95013	9.99728	60	7 46.9 8 53.6
		68		68			ļ	8 53.6 9 60.3
4I 42	9.04783	67	9.05055 9.05124	69	0.94945	9.99728 9.99727	59 58	66
43	9.04030	68	9.05124	68	0.94808	9.99727	57	1 6.6
	9.04985	67	9.05260	68	0.94740	9.99725	56	2 13.2
44 45	9.04905	67	9.05200	68	0.94740	9.99723	55	3 19.8
46	9.05119	67	9.05396	68	0.94604	9.99723	54	4 26.4 5 33.0
47	9.05186	67	9.05463	67	0.94537	9.99723	53	5 33.0 6 39.6
48	9.05253	67	9.05531	68	0.94469	9.99723	52	7 46.2
49	9.05319	66	9.05599	68	0.94401	9.99721	51	8 52.8 9 59.4
50	9.05386	67	9.05666	67	0.94334	9.99720	50	9 39.4
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
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	Sın	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.05386	66	9.05666	67	0.94334	9.99720	50	
51	9.05452	67	9.05733	68	0.94267	9.99719	49	68
52	9.05519	66	9.05801	67	0.94199	9.99718	48	1 6.8 2 13.6
53	9.05585	66	9.05868	67	0.94132	9.99717	47	3 20.4
54	9.05651	66	9.05935	67	0.94065	9.99716	46	4 27.2
55	9.05717	66	9.06002	66	0.93998	9.99716	45	5 34.0 6 40.8
56	9.05783	66	9.06068	67	0.93932	9.99715	44	7 47.6
57 58	9.05849	66	9.06135 9.06202	67	0.93865	9.99714	43	
59	9.05915 9.05980	65	9.00202	66	0.93798	9.99713	42 41	
60	9.06046	66	9.06335	67			40	I 67 66 1 6.7 6.6
61		66		66	0.93665	9.99711		2 13.4 13.2
62	9.06112	65	9.06401	66	0.93599	9.99710	39	3 20.1 19.8
63	9.06242	65	9.06534	67	0.93533	9.99709	38	4 26.8 26.4
64	9.06307	65	9.06600	66		9.99709	37	5 33.5 33.0 6 40.2 39.6
65	9.00307	65	9.06666	66	0.93400	9.99708	36 35	7 46.9 46.2
66	9.06437	65	9.06731	65	0.93334	9.99707	34	
67	9.06502	65	9.06797	66	0.93203	9.99705	1	
68	9.06567	65	9.06863	66	0.93137	9.99703	33 32	65
69	9.06632	65	9.06928	65	0.93072	9.99703	31	I 6.5 2 13.0
70	9.06696	64	9.06994	66	0.93006	9.99702	30	2 13.0 3 19.5
71	9.06761	65	9.07059	65	0.92941	9.99701	29	4 26.0
72	9.06825	64	9.07124	65	0.92941	9.99701	28	5 32.5 6 39.0
73	9.06889	64	9.07190	66	0.92810	9.99700	27	
74	9.06954	65	9.07255	65	0.92745	9.99699	26	8 52.0
75	9.07018	64	9.07320	65	0.92680	9.99698	25	9 58.5
76	9.07082	64	9.07385	65	0.92615	9.99697	24	64 63
77	9.07145	63	9.07449	64	0.92551	9.99696	23	I 6.4 6.3 2 12.8 12.6
78	9.07209	6 4 64	9.07514	65 65	0.92486	9.99695	22	3 19.2 18.9
79	9.07273	64	9.07579	64	0.92421	9.99694	31	4 25.6 25.2 5 32.0 31.5
80	9.07337	63	9.07643	65	0.92357	9.99693	20	5 32.0 31.5 6 38.4 37.8
81	9.07400	64	9.07708	64	0.92292	9.99693	19	7 44.8 44.1
82	9.07464	63	9.07772	64	0.92228	9.99692	18	8 51.2 50.4 9 57.6 56.7
83	9.07527	63	9.07836	64	0.92164	9.99691	17	62
84	9.07590	63	9.07900	64	0.92100	9.99690	16	
85	9.07653	63	9.07964	64	0.92036	9.99689	15	I 6.2 2 12.4
86	9.07716	63	9.08028	64	0.91972	9.99688	14	3 18.6
87 88	9.07779	63	9.08092 9.08156	64	0.91908	9.99687	13	4 24.8 5 31.0
89	9.07842	63	9.08150	64	0.91844	9.99686 9.99685	12	6 37.2
90	9.07968	63	9.08283	63	0.91717	9.99684	10	7 43.4
	9.07908	62		64				8 49.6 9 55.8
91 92	9.08030	63	9.08347 9.08410	63	0.91653 0.91590	9.99683 9.99682	o9 o8	9 55.0 61
93	9.08093	62	9.08474	64	0.91596	9.99682	07	1 6.1
94	9.08217	62	9.08537	63	0.91463	9.99681	06	2 12.2
95	9.08280	63	9.08600	63	0.91403	9.99680	. 05	3 18.3
96	9.08342	62	9.08663	63	0.91337	9.99679	04	4 24.4 5 30.5 6 36.6
97	9.08404	62	9.08726	63	0.91274	9.99678	03	5 30.5 6 36.6
98	9.08466	62	9.08789	63	0.91211	9.99677	02	7 42.7
99	9.08528	62 61	9.08852	63 62	0.91148	9.99676	01	8 48.8 9 54.9
100	9.08589	01	9.08914	02	0.91086	9.99675	00	9 54.9
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

Sin d. Tan d. c. Cot Cos	99 98 97 96 95 94	P. P. 63 I 6.3 2 12.6 3 18.9 4 25.2
o1 9.08651 62 9.08977 63 0.91023 9.99674 o2 9.08713 62 9.09040 63 0.90960 9.99673 o3 9.08774 61 9.09102 62 0.90898 9.99672 o4 9.08836 61 9.09164 63 0.90836 9.99672 o4 9.08807 61 9.09164 63 0.90836 9.99672	99 98 97 96 95 94	I 6.3 2 12.6 3 18.9
o1 9.08651 62 9.08977 63 0.91023 9.99674 o2 9.08713 61 9.09040 63 0.90960 9.99673 o3 9.08774 62 9.09102 62 0.90898 9.99671 o4 9.08836 61 9.09164 63 0.90836 9.99671 o5 0.08877 63 0.00773 0.00670	98 97 96 95 94	I 6.3 2 12.6 3 18.9
03 9.08714 61 9.09040 62 0.90898 9.99672 04 9.08836 61 9.09164 63 0.90836 9.99671 05 0.08807 61 0.00323 63 0.00373 0.00670	97 96 95 94	2 12.6 3 18.9
04 9.08836 61 9.09164 63 0.00838 9.99671	96 95 94	3 18.9
04 9.08836 61 9.09164 63 0.90836 9.99671 0.00670	95 94	
	94	
		5 31.5 6 37.8
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0.2	
07 9.09019 61 9.09351 62 0.90649 9.99669	93	8 50.4
08 9.09080 61 9.09413 62 0.90587 9.99008	92	9 56.7
o9 9.09141 61 9.09475 62 0.90525 9.99667	91	62
10 9.09202 61 9.09537 61 0.90463 9.99666	90	I 6.2
11 9.09263 61 9.09598 62 0.90402 9.99665	89	2 12.4 3 18.6
12 9.09324 61 9.09660 62 0.90340 9.99664	88	4 24.8
13 9.09385 60 9.09722 61 0.90278 9.99663	87	5 31.0 6 37.2
14 9.09445 61 9.09783 62 0.90217 9.99662	86	
15 9.09506 61 9.09845 62 0.90155 9.99661	85	7 43.4 8 49.6
16 9.09566 60 9.09906 61 0.90094 9.99660	84	9 55.8
17 9.09626 6 9.09967 6 0.90033 9.99659	83	61
18 9.09686 61 9.10028 61 0.89972 9.99658	82	1 6.1
19 9.09747 60 9.10089 61 0.89911 9.99657	81	2 12.2
20 9.09807 60 9.10150 61 0.89850 9.99656	80	3 18.3
27 0 00867 0 10211 0 80780 0 00655	79	4 24.4 5 30.5
22 9.09926 59 9.10272 61 0.89728 9.99654	78	6 36.6
23 9.09986 60 9.10333 61 0.89667 9.99653	77	7 42.7
0 20046 0 20204 0 80606 0 00652	76	8 48.8 9 54.9
25 0 10106 00 0 10454 00 0 80546 0 00651	75	60
26 9.10165 59 9.10515 61 0.89485 9.99650	74	
27 0 10225 0 10575 0 80425 0 00640	73	I 6.0 2 12.0
28 9.10284 59 9.10635 00 0.89365 9.99648	72	3 18.0
29 9.10343 59 9.10696 60 0.89304 9.99648	71	4 24.0
30 9.10402 60 9.10756 60 0.89244 9.99647	70	5 30.0 6 36.0
0 10462 00 0 10816 00 0 80184 0 00646	69	
32 0 10521 59 0 10876 60 0 80124 0 00645	68	8 48.0
33 0 10580 59 0 10026 00 0 80064 0 00644	67	9 54.0
24 0 70638 58 0 10006 00 0 80004 0 00643	66	59
35 0 10607 59 0 11056 60 0 88044 0 00642	65	1 5.9 2 11.8
36 0 10756 59 0 11115 59 0 88885 0 90641	64	
37 9.10815 59 9.11175 60 0.88825 9.99640	63	3 17.7 4 23.6
38 0 70872 58 0 77224 59 0 88766 0 00620	62	5 29.5 6 35.4
30 0 10032 59 0 11204 ⁰⁰ 0 88706 0 00638	61	6 35.4
40 0 70000	60	7 41.3 8 47.2
47 0 17048 58 0 17413 00 0 88587 0 00636	59	9 53.1
42 0 11107 59 0 11472 59 0 88528 0 00625	58	58
43 0 11165 58 0 11531 59 0 88460 0 90634	57	I 5.8
44 0 11223 58 0 11500 59 0 88410 0 00633	56	2 11.6
45 9.11281 58 9.11649 59 0.88351 9.99632	55	3 17.4 4 23.2
46 0.11330 58 0.11708 59 0.88292 0.99631	54	5 29.0
47 9.11397 58 9.11767 59 0.88233 9.99630	53	6 34.8
48 9.11454 57 9.11826 59 0.88174 9.99629	52	7 40.6 8 46.4
40 0 TIST2 58 0 TISS4 58 0 88TI6 0 00628	51	8 46.4 9 52.2
50 9.11570 58 9.11943 59 0.88057 9.99627	50	9 3
Cos d. Cot d. c. Tan Sin		P. P.

	Sin	d.	Tan	d.c.	Cot	Cos	1	P. P.
50	9.11570		9.11943		0.88057	9.99627	50	
	9.11627	57	9.11943	58				59
51 52	9.11685	58	9.12060	59	0.87999	9.99626 9.99625	49 48	I 5.9 2 II.8
53	9.11742	57	9.12118	58	0.87882	9.99624	47	2 II.8 3 I7.7
54	9.11799	57	9.12177	59	0.87823	9.99623	46	4 23.6
55	9.11/99	58	9.12177	58	0.87765	9.99622	45	5 29.5 6 35.4
56	9.11914	57	9.12293	58	0.87707	9.99621	44	6 35.4 7 41.3
57	9.11971	57	9.12351	58	0.87649	9.99620	43	8 47.2
58	9.12028	57	9.12409	58	0.87591	9.99619	42	9 53.1
59	9.12085	57 57	9.12467	58 58	0.87533	9.99618	41	58
60	9.12142	56	9.12525	58	0.87475	9.99617	40	1 5.8
61	9.12198		9.12583		0.87417	9.99616	39	2 11.6
62	9.12255	57	9.12640	57 58	0.87360	9.99615	38	3 17.4 4 23.2
63	9.12312	57 56	9.12698	58	0.87302	9.99614	37	5 29.0
64	9.12368	-	9.12756	-	0.87244	9.99613	36	6 34.8
65	9.12425	57 56	9.12813	57 57	0.87187	9.99612	35	7 40.6 8 46.4
66	9.12481	56	9.12870	58	0.87130	9.99611	34	9 52.2
67	9.12537	57	9.12928	57	0.87072	9.99610	33	57
68	9.12594	56	9.12985	57	0.87015	9.99609	32	1 5.7
69	9.12650	56	9.13042	57	0.86958	9.99608	31	2 11.4
70	9.12706	56	9.13099	57	0.86901	9.99607	30	3 17.1 4 22.8
71	9.12762	56	9.13156	57	0.86844	9.99606	29	
72	9.12818	56	9.13213	57	0.86787	9.99605	28	6 34.2
73	9.12874	56	9.13270	57	0.86730	9.99604	27	7 39.9 8 45. 6
74	9.12930	55	9.13327	57	0.86673	9.99603	26	8 45.6 9 51.3
75	9.12985	56	9.13384	57	0.86616	9.99601	25	56
76	9.13041	56	9.13441	56	0.86559	9.99600	24	
77	9.13097	55	9.13497	57	0.86503	9.99599	23	I 5.6 2 II.2
78	9.13152	56	9.13554	56	0.86446	9.99598	22	3 16.8
79	9.13208	55	9.13610	57	0.86390	9.99597	21	4 22.4
80	9.13263	55	9.13667	56	0.86333	9.99596	20	5 28.0 6 33.6
81	9.13318	55	9.13723	56	0.86277	9.99595	19	7 39.2 8 44.8
82	9.13373	56	9.13779	56	0.86221	9.99594	18	
83	9.13429	55	9.13835	57	0.86165	9.99593	17	9 50.4
84	9.13484	55	9.13892	56	0.86108	9.99592	16	55
85 86	9.13539	55	9.13948	56	0.86052	9.99591	15	I 5.5
	9.13594	55	9.14004	56	0.85996	9.99590	14	2 II.0 3 I6.5
87 88	9.13649	54	9.14060	55	0.85940	9.99589	13	4 22.0
89	9.13703 9.13758	55	9.14115	56	0.85885 0.85829	9.99588 9.99587	12	5 27.5
90		55		56			10	6 33.0 7 38.5
	9.13813	54	9.14227	56	0.85773	9.99586		8 44.0
91 92	9.13867	55	9.14283	55	0.85717	9.99585	09 08	9 49.5
92	9.13922 9.13976	54	9.14338 9.14394	56	0.85662 0.85606	9.99584 9.99583	08	54
		55		55				1 5.4
94 95	9.14031 9.14085	54	9.14449 9.14504	55	0.85551	9.99582 9.99581	o6 o5	2 10.8
95 96	9.14139	54	9.14560	56	0.85490	9.99580	05	3 16.2 4 21.6
97	9.14193	54	9.14615	55	0.85385	9.99578		5 27.0
98	9.14193	55	9.14670	55	0.85330	9.99578	03	
99	9.14240	54	9.14725	55	0.85275	9.99576	01	7 37.8 8 43.2
100	9.14356	54	9.14780	55	0.85220	9.99575	00	9 48.6
	Cos	d.	Cot	d. c.	Tan	Sin	-	P. P.
	COS	u,	COL	u.c.	ran	9111		r.r.

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	Sin	d.	Tan	d.c.	Cot	Cos		P. P.
00	9.14356	53	9.14780	55	0.85220	9.99575	100	
10	9.14409	54	9.14835	55	0.85165	9.99574	99	55
02	9.14463	54	9.14890	55	0.85110	9.99573	98	I 5.5
03	9.14517	54	9.14945	55	0.85055	9.99572	97	2 II.0
04	9.14571	53	9.15000	54	0.85000	9.99571	96	3 16.5
05	9.14624	54	9.15054	55	0.84946	9.99570	95	4 22.0 5 27.5
06	9.14678	53	9.15109	55	0.84891	9.99569	94	6 33.0
07	9.14731	54	9.15164	54	0.84836	9.99568	93	7 38.5 8 44.0
08	9.14785	53	9.15218	55	0.84782	9.99567	92	8 44.0 9 49.5
09	9.14838	53	9.15273	54	0.84727	9.99566	91	3 . 45.3
10	9.14891	54	9.15327	54	0.84673	9.99565	90	
11	9.14945	53	9.15381	54	0.84619	9.99563	89	54
12	9.14998	53	9.15435	55	0.84565	9.99562	88	1 5.4
13	9.15051	53	9.15490	54	0.84510	9.99561	87	2 10.8
14	9.15104	53	9.15544	54	0.84456	9.99560	86	3 16.2 4 21.6
15	9.15157	53	9.15598	54	0.84402	9.99559	8 ₅	
16	9.15210	53	9.15652	54	0.84348	9.99558		6 32.4
17	9.15263	52	9.15706	54	0.84294	9.99557	8 ₃ 8 ₂	7 37.8 8 43.2
18	9.15315	53	9.15760	53	0.84240	9.99556	81	9 48.6
19	9.15368	53	9.15813	54		9.99555	80	
20	9.15421	52	9.15867	54	0.84133	9.99554		
21	9.15473	53	9.15921	53	0.84079	9.99553	79	53
22	9.15526	52	9.15974	54	0.84026	9.99552	78	I 5.3 2 10.6
23	9.15578	53	9.16028	53	0.83972	9.99550	77	
24	9.15631	52	9.16081	54	0.83919	9.99549	76	3 I5.9 4 21.2
25	9.15683	52	9.16135	53	0.83865	9.99548	75	5 26.5 6 31.8
26	9.15735	52	9.16188	53		9.99547	74	
27	9.15787	53	9.16241	54	0.83759	9.99546	73	7 37.1 8 42.4
28 29	9.15840 9.15892	52	9.16295 9.16348	53	0.83705	9.99545 9.99544	72 71	9 47.7
- 1		52		53			70	
30	9.15944	51	9.16401	53	0.83599	9.99543		
31	9.15995	52	9.16454	53	0.83546	9.99542	69 68	52
32	9.16047	52	9.16507	53	0.83493	9.99540	67	I 5.2
33	9.16099	52	9.16560	53	0.83440	9.99539	66	2 10.4 3 15.6
34	9.16151 9.16203	52	9.16613	52	0.83387	9.99538	65	4 20.8
35 36	9.16254	51	9.16718	53	0.83335	9.99537 9.99536	64	5 26.0
. 1		52		53	0.83229		63	6 31.2 7 36.4
37 38	9.16306 9.16357	51	9.16771	52	0.83229	9.99535 9.99534	62	8 41.6
39	9.16357	52	9.16876	53	0.83177	9.99534	61	9 46.8
40	9.16460	51	9.16928	52	0.83072	9.99532	60	
	9.16511	51		53	0.83019		59	
4I 42	9.16511	52	9.16981 9.17033	52	0.83019	9.99530 9.99529	59 58	51
42	9.10503	51	9.17033	52	0.82915	9.99529	57	I 5.I 2 10.2
	9.16665	51	9.17138	53	0.82862	9.99527	56	3 15.3
44 45	9.16716	51	9.17130	52	0.82810	9.99527	55	4 20.4
45	9.16767	51	9.17190	52	0.82758	9.99525	54	5 25.5
47	9.16818	51	9.17294	52	0.82706	9.99524	53	
47	9.16869	51	9.17294	52	0.82654	9.99524	53 52	8 40.8
49	9.16919	50	9.17348	52	0.82602	9.99521	51	9 45.9
50	9.16970	51	9.17450	52	0.82550	9.99520	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
080	003			а. с.	1411	17111	81°	1.1.

	C:-	-1	Ton	d 0	Cot	Cos		. 00
<u> </u>	Sin	<u>d.</u>	Tan	d. c.				P. P.
50	9.16970	51	9.17450	52	0.82550	9.99520	50	
51	9.17021	51	9.17502	51	0.82498	9.99519	49	52
52	9.17072 9.17122	5 <u>0</u>	9.17553 9.17605	52	0 82447	9.99518	48	I 5.2
53		51 -		52		9.99517	47	2 10.4
54	9.17173	50	9.17657	51	0.82343	9.99516	46	3 15.6 4 20.8
55 56	9.17223 9.17273	50	9.17760	52	0.82240	9.99515 9.99514	45 44	5 26.0 6 31.2
-		51		51	0.82189			6 31.2
57 58	9.17324 9.17374	50	9.17811	52	0.82137	9.99512	43 42	7 36.4 8 41.6
59	9.17424	50	9.17003	51	0.82086	9.99510	41	9 46.8
60	9.17474	50	9.17965	51	0.82035	9.99509	40	
61		50		52				
62	9.17524 9.17575	51	9.18017	51	0.81983	9.99508 9.99507	39 38	51
63	9.17575	49	9.18119	51	0.81881	9.99505	37	I 5.I
64		50	9.18170	51	0.81830	9.99504	36	2 IO.2 3 I5.3
65	9.17674 9.17724	50	9.18170	51	0.81779	9.99504	35	4 20.4
66	9.17774	50	9.18272	51	0.81728	9.99502	34	5 25.5
67	9.17824	50	9.18323	51	0.81677	9.99501	33	
68	9.17873	49	9.18374	51	0.81626	9.99500	33	7 35.7 8 40.8
69	9.17923	50	9.18425	51	0.81575	9.99499	31	9 45.9
70	9.17973	50	9.18475	50	0.81525	9.99497	30	
71	9.18022	49	9.18526	51	0.81474	9.99496	29	
72	9.18022	50	9.18577	51	0.81474	9.99490	28	50
73	9.18121	49	9.18627	50	0.81373	9.99493	27	I 5.0
74	9.18170	49	9.18678	51	0.81322	9.99494	26	2 IO.O 3 I5.O
74 75	9.18170	50	9.18728	50	0.81322	9.99493	25	4 20.0
76	9.18269	49	9.18778	50	0.81272	9.99492	24	5 25.0
77	9.18318	49	9.18829	51	0.81171	9.99489	23	6 30.0 7 35.0
78	9.18367	49	9.18879	50	0.81171	9.99488	22	7 35.0 8 40.0
79	9.18416	49	9.18929	50	0.81071	9.99487	21	9 45.0
80	9.18465	49	9.18979	50	0.81021	9.99486	20	
81	9.18514	49	9.10079	50	0.80971	9.99485	19	
82	9.18563	49	9.19029	51	0.80971	9.99483	18	49
83	9.18612	49	9.19000	50	0.80870	9.99482	17	I 4.9 2 9.8
84	9.18661	49	9.19179	49	0.80821	9.99481	16	3 14.7
85	9.18709	48	9.19179	50	0.80771	9.99480	15	4 19.6
86	9.18758	49	9.19279	50	0.80721	9.99479	14	5 24.5 6 29.4
87	9.18806	48	9.19329	50	0.80671	9.99477	13	
88	9.18855	49	9.19379	50	0.80621	9.99476	12	8 39.2
89	9.18904	49 48	9.19428	49 50	0.80572	9.99475	11	9 44.1
90	9.18952		9.19478		0.80522	9.99474	10	
91	9.19000	48	9.19528	50	0.80472	9.99473	09	48
92	9.19049	49	9.19577	49	0.80423	9.99472	08	I 4.8
93	9.19097	48 48	9.19627	50	0.80373	9.99470	07	2 9.6
94	9.19145		9.19676	49	0.80324	9.99469	06	3 14.4
95	9.19193	48 48	9.19725	49	0.80275	9.99468	05	4 19.2 5 24.0
96	9.19241	48 48	9.19775	50 49	0.80225	9.99467	04	6 28.8
97	9.19289	48	9.19824	1	0.80176	9.99466	03	7 33.6 8 38.4
98	9.19337	48 48	9.19873	49 49	0.80127	9.99464	02	8 38.4 9 43.2
99	9.19385	48	9.19922	49	0.80078	9.99463	01	9 43.2
100	9.19433	40	9.19971	45	0.80029	9.99462	00_	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos		D D
<u> </u>		<u>a.</u>		d. c.			122	P. P.
00	9.19433	48	9.19971	49	0.80029	9.99462	100	
OI	9.19481	48	9.20020	49	0.79980	9.99461	99	
02	9.19529	48	9.20069	49	0.79931	9.99460	98	49
03	9.19577	47	1 "	49	0.79882	9.99458	97	1 4.9 2 9.8
04	9.19624	48	9.20167	49	0.79833	9.99457	96	3 14.7
05	9.19672	47	9.20216	49	0.79784	9.99456	95	4 19.6
06	9.19719	48	9.20265	48	0.79735	9.99455	94	5 24.5 6 29.4
07	9.19767	47	9.20313	49	0.79687	9.99454	93	6 29.4 7 34.3
08	9.19814	48	9.20362	49	0.79638	9.99452	92	7 34.3 8 39.2
09	9.19862	47	9.20411	48	0.79589	9.99451	91	9 44.1
10	9.19909	47	9.20459	49	0.79541	9.99450	90	
11	9.19956	48	9.20508	48	0.79492	9.99449	89	48
12	9.20004	47	9.20556	49	0.79444	9.99447	88	I 4.8
13	9.20051	47	9.20605	48	0.79395	9.99446	87	2 9.6
14	9.20098	47	9.20653	48	0.79347	9.99445	86	3 14.4
15	9.20145	47	9.20701	49	0.79299	9.99444	85	4 19.2
16	9.20192	47	9.20750	48	0.79250	9.99443	84	5 24.0 6 28.8
17	9.20239	47	9.20798	48	0.79202	9.99441	83	7 33.6 8 38.4
18	9.20286	47	9.20846	48	0.79154	9.99440	82	
19	9.20333	47	9.20894	48	0.79106	9.99439	81	9 43.2
20	9.20380	47	9.20942	48	0.79058	9.99438	80	ł
21	9,20427	46	9.20990	48	0.79010	9.99436	79	47
22	9.20473	47	9.21038	48	0.78962	9.99435	78	I 4.7
23	9.20520	47	9.21086	48	0.78914	9.99434	77	2 9.4
24	9.20567	46	9.21134	48	0.78866	9.99433	76	3 14.1
25	9.20613	47	9.21182	47	0.78818	9.99432	75	4 18.8 5 23.5
26	9.20660	46	9.21229	48	0.78771	9.99430	74	6 28.2
27	9.20706	46	9.21277	48	0.78723	9.99429	73	7 32.9 8 37.6
28	9.20752	47	9.21325	47	0.78675	9.99428	72	8 37.6 9 42.3
29	9.20799	46	9.21372	48	0.78628	9.99427	71	7 1 4=-3
30	9.20845	46	9.21420	47	0.78580	9.99425	70	
31	9.20891	47	9.21467	48	0.78533	9.99424	69	46
32	9.20938	46	9.21515	47	0.78485	9.99423	68	I 4.6
33	9.20984	46	9.21562	48	0.78438	9.99422	67	2 9.2 3 13.8
34	9.21030	46	9.21610	47	0.78390	9.99420	66	4 18.4
35 36	9.21076 9.21122	46	9.21657	47	0.78343 0.78296	9.99419	65	5 23.0
-		46	9.21704	47		9.99418	64	6 27.6 7 32.2
37 38	9.21168 9.21214	46	9.21751	47	0.78249	9.99417	63 62	8 36.8
39	9.21214	46	9.21798	48	0.78202	9.99415 9.99414	61	9 41.4
40		46	<u> </u>	47			60	
	9.21306	45	9.21893	47	0.78107	9.99413		45
41	9.21351	46	9.21940	47	0.78060	9.99412	59	I 4.5
42 43	9.21397 9.21443	46	9.21987 9.22034	47	0.78013 0.77966	9.99410	58 57	2 9.0
		45		46				3 13.5
44 45	9.21488	46	9.22080	47	0.77920	9.99408	56	4 18.0 5 22.5
45 46	9.21534 9.21579	45	9.22127	47	0.77826	9.99407	55 54	5 22.5 6 27.0
		46		47				7 31.5
47 48	9.21625 9.21670	45	9.22221 9.22267	46	0.77779	9.99404	53 52	
49	9.21070	46	9.22314	47	o.77733 o.77686	9.99403	52 51	9 40.5
50		45		47			50	
- " -	9.21761		9.22361		0.77639	9.99400	- 50	- D D
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

		1	Т.	4 .	C-+ 1	Car		P. P.
<u> </u>	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.21761	45	9.22361	46	0.77639	9.99400	50	
51	9.21806	45	9.22407	47	0.77593	9.99399	49	47
52	9.21851	45	9.22454	46	0.77546	9.99398	48	I 4.7
53	9.21897	45	9.22500	47	0.77500	9.99396	47	2 9.4
54	9.21942	45	9.22547	46	0.77453	9.99395 9.99394	46	3 I4.I
55 56	9.21987 9.22032	45	9.22593 9.22639	46	0.77407 0.77361	9.99394	45 44	4 18.8 5 23.5
		45	9.22685	46	1	9.99393	43	6 28.2
57 58	9.22077	45	9.22085	47	0.77315	9.99391	43	7 32.9 8 37.6
59	9.22122	45	9.22778	46	0.77222	9.99390	41	8 37.6 9 42.3
60	9.22211	44	9 22824	46	0.77176	9.99388	40	9 1 42.3
61	9.22256	45	9.22870	46	0.77130	9.99386	39	
62	9.22250 9.2230I	45	9.22916	46	0.77130	9.99385	38	46
63	9.22346	45	9.22910	46	0.77038	9.99384	37	1 4 6
64	9.22390	44	9.23008	46	0.76992	9.99382	36	2 9.2 3 13.8
65	9.22390	45	9.23054	46	0.76946	9.99381	35	4 18.4
66	9.22480	45	9.23100	46 46	0.76900	9.99380	34	5 23.0
67	9.22524	44	9.23146		0.76854	9.99379	33	6 27.6
68	9.22568	44	9.23191	45 46	0.76809	9.99377	32	8 36.8
69	9.22613	45 44	9.23237	46	0.76763	9.99376	31	9 41.4
70	9.22657		9.23283	45	0.76717	9.99375	30	
71	9.22702	45	9.23328	45	0.76672	9.99373	29	45
72	9.22746	44	9.23374	45	0.76626	9.99372	28	1 4.5
73	9 22790	44 44	9.23419	46	0.76581	9.99371	27	2 9.0
74	9.22834	44	9.23465	45	0.76535	9.99369	26	3 13.5
75	9.22878	44	9.23510	45	0.76490	9.99368	25	4 18.0 5 22.5
76	9.22922	45	9.23556	45	0.76444	9.99367	24	6 27.0
77	9.22967	44	9.23601	45	0.76399	9.99366	23	7 31.5 8 36.0
78	9.23011	43	9.23646	45	0.76354	9.99364	22	8 36.0 9 40.5
79	9.23054	44	9.23692	45	0.76308	9.99363	21	3 40.3
80	9.23098	44	9.23737	45	0.76263	9.99362	20	
81	9.23142	44	9.23782	45	0.76218	9.99360	19	44
82	9.23186	44	9.23827	45	0.76173	9.99359	18	I 4.4
83	9.23230	44	9.23872	45	0.76128	9.99358	17	2 8.8 3 I3.2
84	9.23274	43	9.23917	45	0.76083	9.99356	16	4 17.6
85	9.23317	44	9.23962	45	0.76038	9 99355	15	5 22.0 6 26.4
86	9.23361	43	9.24007	45	0.75993	9.99354	14	6 26.4 7 30.8
87	9 . 23404	44	9.24052	45	0.75948	9.99352	13	8 35.2
88	9.23448	43	9.24097	45	0.75903	9.99351	12	9 39.6
89	9.23491	44	9.24142	44	0.75858	9.99350	11	1
90	9.23535	43	9.24186	45	0.75814	9.99348	10	43
91	9.23578	44	9.24231	45	0.75769	9 99347	09	I 4.3
92	9.23622	43	9.24276	45	0.75724	9.99346	08	2 8.6
93	9.23665	43	9.24321	4-1	0.75679	9.99344	07	3 12.9
94	9.23708	44	9.24365	45	0.75635	9.99343	06	4 17.2 5 21.5
95 06	9.23752	43	9.24410	44	0.75590	9.99342	05 04	6 25.8
96	9.23795	43	9.24454	45	0.75546	9.99340	1 .	7 30.1
97	9.23838	43	9.24499	44	0.75501	9.99339	03	8 34.4 9 38.7
98	9.23881 9.23924	43	9.24543 9.24588	45	0.75457 0.75412	9.99338 9.99336	02	9 7 30.1
99		43		44			00	A /
100	9.23967		9.24632	-	0.75368	9.99335		P. P.
l	Cos	đ.	Cot	d. c.	Tan	Sin		P. P.

10°							169°	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.23967	43	9.24632	44	0.75368	9.99335	100	
10	9.24010	43	9.24676	44	0.75324	9.99334	99	
02	9.24053	43	9.24720	44	0.75280	9.99332	98	
03	9.24096	43	9.24765	44	0.75235	9.99331	97	44
04	9.24139	42	9.24809	44	0.75191	9.99330	96	I 4.4
05	9.24181	43	9.24853	44	0.75147	9.99328	95	2 8.8
06	9.24224	43	9.24897	44	0.75103	9.99327	94	3 13.2
o7 o8	9.24267	43	9.24941	44	0.75059	9.99326	93	4 17.6 5 22.0
09	9.24310 9.24352	42	9.24985 9.25029	44	0.75015 0.74971	9.99324 9.99323	92 91	6 26.4
10		43		44			90	7 30.8
	9.24395	42	9.25073	44	0.74927	9.99322	1 1	8 35.2
II I2	9.24437	43	9.25117	44	0.74883	9.99320	89	9 39.6
13	9.24480	42	9.25161	44	0.74839	9.99319	88 87	
14	9.24522	43	9.25205	43	0.74795	9.99318	86	
15	9.24565 9.24607	42	9.25248 9.25292	44	0.74752 0.74708	9.99316 9.99315	85	43
16	9.24649	42	9.25292	44	0.74708	9.99315	84	
17	9.24692	43	9.25379	43	0.74621	9.99312	83	1 4.3 2 8.6
18	9.24734	42	9.25423	44	0.74577	9.99312	82	3 12.9
19	9.24776	42	9.25466	43	0.74534	9.99310	81	4 17.2
20	9.24818	42	9.25510	44	0.74490	9.99308	80	5 21.5
21	9.24860	42	9.25553	43	0.74447	9.99307	79	6 25.8 +
22	9.24902	42	9.25597	44	0.74403	9.99307	78	7 30.1
23	9.24944	42 42	9.25640	43	0.74360	9.99304	77	8 34.4 9 38.7
24	9.24986		9.25684	44	0.74316	9.99303	76	9 38.7
25	9.25028	42 42	9.25727	43	0.74273	9.99301	75	
26	9.25070	42	9.25770	43 43	0.74230	9.99300	74	
27	9.25112	42	9.25813	44	0.74187	9.99299	73	42
28	9.25154	42	9.25857	44	0.74143	9.99297	72	1 4.2
29	9.25196	41	9.25900	43	0.74100	9.99296	71	2 8.4
30	9.25237	42	9.25943	43	0.74057	9.99294	70	3 12.6
31	9.25279	42	9.25986	43	0.74014	9.99293	69	4 16.8 5 21.0
32	9.25321	41	9.26029	43	0.73971	9.99292	68	5 21.0 6 25.2
33	9.25362	42	9.26072	43	0.73928	9.99290	67	7 29.4
34	9.25404	41	9.26115	43	0.73885	9.99289	66	8 33.6
35	9.25445	42	9.26158	43	0.73842	9.99288	65	9 37.8
36	9.25487	41	9.26201	42	0.73799	9.99286	64	
37 38	9.25528	42	9.26243	43	0.73757	9.99285	63 62	
39	9.25570	41	9.26286	43	0.73714	9.99283 9.99282	61	41
40	9.25652	41	9.26372	43	0.73628	9.99281	60	1 4.1
41	9.25694	42	9.26414	42	0.73586	9.99279	59	2 8.2
42	9.25094	41	9.26414	43	0.73543	9.99279	58	3 12.3
43	9.25776	4I 4I	9.26500	43	0.73500	9.99276	57	4 16.4
44	9.25817		9.26542	42	0.73458	9.99275	56	5 20.5
45	9.25858	4I 4I	9.26585	43	0.73415	9.99274	55	6 24.6
46	9.25899	41	9.26627	42	0.73373	9.99272	54	7 28.7 8 32.8
47	9.25940	41	9.26670	43	0.73330	9.99271	53	9 36.9
48	9.25981	41	9.26712	42 42	0.73288	9.99269	52	9100.9
49	9.26022	41	9.26754	43	0.73246	9.99268	51	
50	9.26063		9.26797		0.73203	9.99267	50	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.
							700	

	Sin	d.	Tan	d. c.	l Cot	Cos		P. P.
50	9.26063		9.26797		0.73203	9.99267	50	1.1.
1	9.26104	41	9.26839	42	0.73161	9.99265		
51 52	9.26145	41	9.26881	42	0.73101	9.99264	49 48	
53	9.26186	41 °	9.26923	42	0.73077	9.99262	47	43
54	9.26227	41	9.26966	43	0.73034	9.99261	46	I 4.3
55	9.26267	40	9.27008	42	0.72992	9.99260	45	2 8.6
56	9.26308	4I 4I	9.27050	42 42	0.72950	9.99258	44	3 12.9
57	9.26349		9.27092		0.72908	9.99257	43	4 17.2
58	9.26389	40	9.27134	42 42	0.72866	9.99255	42	5 21.5
59	9.26430	4I 40	9.27176	42	0.72824	9.99254	41	6 25.8 7 30.1
60	9.26470	41	9.27218	42	0.72782	9.99252	40	8 34.4
61	9.26511	40	9.27260	42	0.72740	9.99251	39	9 38.7
62	9.26551	41	9.27302	41	0.72698	9.99250	38	
63	9.26592	40	9.27343	42	0.72657	9.99248	37	
64	9.26632	40	9.27385	42	0.72615	9.99247	36	42
65	9.26672	41	9.27427	42	0.72573	9.99245	35	
66	9.26713	40	9.27469	41	0.72531	9.99244	34	I 4.2 2 8.2
67	9.26753	40	9.27510	42	0.72490	9.99243	33	3 12.6
68 69	9.26793	40	9.27552	42	0.72448	9.99241	32	4 16.8
70	9.26833	40	9.27594	41	0.72406	9.99240	31	5 21.0
	9.26873	40	9.27635	42	0.72365	9.99238	30	6 25.2
71,	9.26913	41	9.27677	41	0.72323	9.99237	29 28	7 29.4
72 73	9.26954	40	9.27718 9.27760	42	0.72282	9.99236 9.99234	27	8 33.6
	9.26994	40		41			26	9 37.8
74	9.27034	39	9.27801	41	0.72199	9.99233	25	
75 76	9.27073 9.27113	40	9.27842 9.27884	42	0.72158	9.99231 9.99230	24	
77	9.27153	40	9.27925	41	0.72110	9.99238	23	41
77	9.27153	40	9.27925	41	0.72075	9.99227	22	I 4.I
79	9.27233	40	9.27900	42	0.71992	9.99227	21	2 8.2
80	9.27273	40	9.28049	41	0.71951	9.99224	20	3 12.3
81	9.27312	39	9.28090	41	0.71910	9.99222	19	4 16.4 5 20.5
82	9.27352	40	9.28131	41	0.71869	9.99221	18	5 20.5 6 24.6
83	9.27392	40	9.28172	4I 4I	0.71828	9.99220	17	7 28.7
84	9.27431	39	9.28213		0.71787	9.99218	16	8 32.8
85	9.27471	40 39	9.28254	41 41	0.71746	9.99217	15	9 36.9
86	9.27510	39 40	9.28295	41 4I	0.71705	9.99215	14	
87	9.27550	39	9.28336	41	0.71664	9.99214	13	
88	9.27589	40	9.28377	41	0.71623	9.99212	12	40
89	9.27629	39	9.28418	41	0.71582	9.99211	11	
90	9.27668	39	9.28459	41	0.71541	9.99209	10	1 4.0 2 8.0
91	9.27707	40	9.28500	40	0.71500	9.99208	09 08	3 12.0
92	9.27747	39	9.28540	41	0.71460	9.99206 9.99205	08	4 16.0
93	9.27786	39	9.28581	41	0.71419		06	5 20.0
94	9.27825 9.27864	39	9.28622	40	0.71378	9.99203 9.99202	05	6 24.0
95 96	9.27804	40	9.28703	41	0.71336	9.99202	04	7 28.0 8 32.0
97	9.27904	39	9.28744	41	0.71256	9.99201	03	9 36.0
98	9.27943	39	9.28744	40	0.71230	9.99199	02	9 001-
99	9.27902	39	9.28825	41	0.71175	9.99196	OI	
100	9.28060	39	9.28865	40	0.71135	9.99195	00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
		· · ·		· u. c.	. 1911	. 5111	<u> </u>	

11,							168	
	Sin	d.	Tan	d.c.	Cot	Cos		P. P.
00	9.28060	39	9.28865	41	0.71135	9.99195	100	
OI	9.28099	39	9.28906	40	0.71094	9.99193	99	
02	9.28138	39	9.28946	40	0.71054	9.99192	98	
03	9.28177	39	9.28986	41	0.71014	9.99190	97	41
04	9.28216	38	9.29027	40	0.70973	9.99189	96	1 4.1
05	9.28254	39	9.29067	40	0.70933	9.99187	95	2 8.2
06	9.28293	39	9.29107	41	0.70893	9.99186	94	3 12.3
07	9.28332	39	9.29148	40	0.70852	9.99184	93	4 16.4
08	9.28371	38	9.29188	40	0.70812	9.99183	92	5 20.5 6 24.6
09	9.28409	39	9.29228	40	0.70772	9.99181	91	7 28.7
10	9.28448	39	9.29268	40	0.70732	9.99180	90	8 32.8
11	9.28487	38	9.29308	40	0.70692	9.99178	89	9 36.9
12	9.28525	39	9.29348	40	0.70652	9.99177	88	
13	9.28564	38	9.29388	40	0.70612	9.99175	87	
14	9.28602	39	9.29428	40	0.70572	9.99174	86	40
15	9.28641	38	9.29468	40	0.70532	9.99172	85	40
16	9.28679	39	9.29508	40	0.70492	9.99171	84	I 4.0
17	9.28718	38	9.29548	40	0.70452	9.99169	83	2 8.0
18	9.28756	38	9.29588	40	0.70412	9.99168	82	3 12.0 4 16.0
19	9.28794	39	9.29628	40	0.70372	9.99166	81	5 20.0
20	9.28833	38	9.29668	39	0.70332	9.99165	80	6 24.0
21	9.28871	38	9.29707	40	0.70293	9.99163	79	7 28.0
22	9.28909	38	9.29747	40	0.70253	9.99162	78	8 32.0
23	9.28947	38	9.29787	40	0.70213	9.99160	77	9 36.0
24	9.28985	39	9.29827	39	0.70173	9.99159	76	
25 26	9.29024	38	9.29866	40	0.70134	9.99157	75	
		38	9.29906	39	0.70094	9.99156	74	39
27 28	9.29100	38	9.29945 9.29985	40	0.70055	9.99154 9.99153	73 72	1 3.9
29	9.29136	38	9.29903	39	0.69976	9.99151	71	2 7.8
30	9.29214	38	9.30064	40	0.69936		70	3 11.7
		38		39		9.99150	69	4 15.6
31 32	9.29252 9.29289	37	9.30103 9.30143	40	o.69897 o.69857	9.99148 9.99147	68	5 19.5
33	9.29209	38	9.30143	39	0.69818	9.99147	67	6 23.4
34	9.29365	38	9.30221	39	0.69779	9.99144	66	7 27.3 8 31.2
35	9.29303	38	9.30221	40	0.69779	9.99144	65	8 31.2 9 35.1
36	9.29441	38	9.30300	39	0.69700	9.99141	64	A . 22'T
37	9.29478	37	9.30339	39	0.69661	9.99139	63	
38	9.29516	38	9.30378	39	0.69622	9.99138	62	
39	9.29554	38 37	9.30418	40	0.69582	9.99136	61	38
40	9.29591	38	9.30457	39	0.69543	9.99135	60	I 3.8
41	9.29629	1 -	9.30496	39	0.69504	9.99133	59	2 7.6
42	9.29666	37 38	9.30535	39	0.69465	9.99132	58	3 11.4
43	9.29704	37	9.30574	39 39	0.69426	9.99130	57	4 I5.2 5 I9.0
44	9.29741	38	9.30613	39	0.69387	9.99128	56	5 19.0 6 22.8
45	9.29779	37	9.30652	39	0.69348	9.99127	55	7 26.6
46	9.29816	38	9.30691	39	0.69309	9.99125	54	8 30.4
47	9.29854	37	9.30730	39	0.69270	9.99124	53	9 34.2
48	9.29891	37	9.30769	38	0.69231	9.99122	52	
49	9.29928	38	9.30807	39	0.69193	9.99121	51	1
50	9.29966		9.30846		0.69154	9.99119	50	
	Cos	d.	Cot	d. c.	Tan	Sin	ı	P. P.

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	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.29966	37	9.30846	39	0.69154	9.99119	50	
51	9.30003	37	9.30885	39	0.69115	9.99118	49	
52	9.30040	37	9.30924	39	0.69076	9.99116	48	
53	9.30077	37	9.30963	38	0.69037	9.99115	47	38
54	9.30114	37	9.31001	39	0.68999	9.99113	46	1 3.8
55	9.30151	37	9.31040	38	0.68960	9.99112	45	2 7.6
56	9.30188	38	9.31078	39	0.68922	9.99110	44	3 11.4
57	9.30226	37	9.31117	39	0.68883	9.99108	43	4 15.2 5 19.0
58	9.30263	36	9.31156	38	0.68844	9.99107	42	5 19.0 6 22.8
59	9.30299	37	9.31194	39	0.68806	9.99105	41	7 26.6
60	9.30336	37	9.31233	38	0.68767	9.99104	40	8 30.4
61	9.30373	37	9.31271	39	0.68729	9.99102	39	9 34.2
62	9.30410	37	9.31310	38	0.68690	9.99101	38	
63	9.30447	37	9.31348	38	0.68652	9.99099	37	
64	9.30484	37	9.31386	39	0.68614	9.99098	з6	37
65	9.30521	36	9.31425	38	0.68575	9.99096	35	
66	9.30557	37	9.31463	38	0.68537	9.99094	34	I 3.7
67	9.30594	37	9.31501	39	0.68499	9.99093	33	2 7.4
68	9.30631	36	9.31540	38	0.68460	9.99091	32	3 II.1 4 I4.8
69	9.30667	37	9.31578	38	0.68422	9.99090	31	
70	9.30704	37	9.31616	38	0.68384	9.99088	30	5 18.5 6 22.2
71	9.30741	36	9.31654	38	0.68346	9.99087	29	7 25.9
72	9.30777	37	9.31692	38	0.68308	9.99085	28	8 29.6
73	9.30814	36	9.31730	38	0.68270	9.99083	27	9 33.3
74	9.30850	37	9.31768	38	0.68232	9.99082	26	
75	9.30887	36	9.31806	38	0.68194	9.99080	25	
76	9.30923	37	9.31844	38	0.68156	9.99079	24	36
77	9.30960	36	9.31882	38	0.68118	9.99077	23	
78	9.30996	36	9.31920	38	0.68080	9.99076	22	1 3.6
79	9.31032	36	9.31958	38	0.68042	9.99074	31	2 7.2 3 10.8
80	9.31068	37	9.31996	38	0.68004	9.99072	20	3 IO.8 4 I4.4
81	9.31105	36	9.32034	38	0.67966	9.99071	19	5 18.0
82	9.31141	36	9.32072	38	0.67928	9.99069	18	6 21.6
83	9.31177	36	9.32110	37	0.67890	9.99068	17	7 25.2
84	9.31213	37	9.32147	38	0.67853	9.99066	16	8 28.8
85	9.31250	36	9.32185	38	0.67815	9.99064	15	9 32.4
86	9.31286	36	9.32223	37	0.67777	9.99063	14	
87	9.31322	36	9.32260	38	0.67740	9.99061	13	
88	9.31358	36	9.32298	38	0.67702	9.99060	12	35
89	9.31394	36	9.32336	37	0.67664	9.99058	11	
90	9.31430	36	9.32373	38	0.67627	9.99056	10	1 3.5
91	9.31466	36	9.32411	37	0.67589	9.99055	09	3 10.5
92	9.31502	36	9.32448	38	0.67552	9.99053	08	4 14.0
93	9.31538	35	9.32486	37	0.67514	9.99052	07	5 17.5
94	9.31573	36	9.32523	38	0.67477	9.99050	06	6 21.0
95	9.31609	36	9.32561	37	0.67439	9.99048	05	7 24.5
96	9.31645	36	9.32598	38	0.67402	9.99047	04	8 28.0
97	9.31681	36	9.32636	37	0.67364	9.99045	03	9 31.5
98	9.31717	35	9.32673	37	0.67327	9.99044	02	
99	9.31752	36	9.32710	37	0.67290	9.99042	10	
100	9.31788		9.32747		0.67253	9.99040	00	
	Cos	d.	l Cot	d. c.	Tan	Sin	1	P. P.

12							101	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.31788	36	9.32747	38	0.67253	9.99040	100	
01	9.31824	35	9.32785		0.67215	9.99039	99	
02	9.31859	35 36	9.32822	37 37	0.67178	9.99037	98	
03	9.31895	35	9.32859	37	0.67141	9.99036	97	38
04	9.31930	36	9.32896	37	0.67104	9.99034	96	r 3.8
05	9.31966	35	9.32933	38	0.67067	9.99032	95	2 7.6
06	9.32001	36	9.32971	37	0.67029	9.99031	94	3 11.4
07	9.32037	35	9.33008	37	0.66992	9.99029	93	4 15.2
о8	9.32072	36	9.33045	37	0.66955	9.99028	92	5 19.0
09	9.32108	35	9.33082	37	0.66918	9.99026	91	6 22.8 7 26.6
10	9.32143	35	9.33119	37	0.66881	9.99024	90	8 30.4
11	9.32178	36	9.33156	37	0.66844	9.99023	89	9 34.2
12	9.32214	35	9.33193	37	0.66807	9.99021	88	, , , ,
13	9.32249	35	9.33230	36	0.66770	9.99019	87	V
14	9.32284	35	9.33266	37	0.66734	9.99018	86	
15	9.32319	36	9 33303	37	0.66697	9.99016	85	37
16	9.32355	35	9.33340	37	0.66660	9.99014	84	I 3.7
17	9.32390	35	9.33377	37	0.66623	9.99013	83	2 7.4
18	9.32425	35	9.33414	36	0.66586	9.99011	82	3 11.1
19	9.32460	35	9.33450	37	0.66550	9.99010	81	4 14.8 5 18.5
20	9.32495	35	9.33487	37	0.66513	9.99008	80	5 18.5 6 22.2
21	9.32530	35	9.33524	36	0.66476	9.99006	79	7 25.9
22	9.32565	35	9.33560	37	0.66440	9.99005	78	8 29.6
23	9.32600	35	9.33597	37	0.66403	9.99003	77	9 33.3
24	9.32635	35	9.33634	36	0.66366	9.99001	76	
25	9.32670	35	9.33670	37	0.66330	9.99000	75	
26	9.32705	35	9.33707	36	0.66293	9.98998	74	0.0
27	9.32740	35	9 33743	37	0.66257	9.98996	73	36
28	9.32775	34	9.33780	36	0.66220	9.98995	72	I 3.6
29	9.32809	35	9.33816	37	0.66184	9.98993	71	2 7. 2 3 10.8
30	9.32844	35	9.33853	36	0.66147	9.98991	70	4 14.4
31	9.32879	35	9.33889	36	0.66111	9.98990	69	5 18.0
32	9.32914	34	9.33925	37	0.66075	9.98988	68	6 21.6
33	9.32948	35	9.33962	36	0.66038	9.98987	67	7 25.2
34	9.32983	35	9.33998	36	0.66002	9.98985	66	8 28.8
35	9.33018	34	9.34034	37	0.65966	9.98983	65 64	9 32.4
36	9.33052	35	9.34071	36	0.65929	9.98982		
37	9.33087	34	9.34107	36	0.65893	9.98980	63 62	
38 39	9.33121 9.33156	35	9.34143 9.34179	36	0.65857	9.98978 9.98977	61	35
40		34		36			60	1 3.5
	9.33190	35	9.34215	37	0.65785	9.98975		2 7.0
41	9.33225	34	9.34252	36	0.65748	9.98973 9.98972	59 58	3 10.5
42 43	9.33259 9.33294	35	9.34288 9.34324	36	0.65712	9.98972	50	4 14.0
		34	1	36		9.98978	56	5 17.5
44	9.33328 9.33362	34	9.34360	36	0.65640	9.98967	55	6 21.0
45 46	9.33302	35	9.34396 9.34432	36	0.65568	9.98965	55	7 24.5 8 28.0
		34		36	0.65532	9.98963	53	8 28.0 9 31.5
47 48	9.33431 9.33465	34	9.34468 9.34504	36	0.65496	9.98962	53	9 ' 31.3
49	9.33499	34	9.34540	36	0.65460	9.98960	51	
50	9.33534	35	9.34576	36	0.65424	9.98958	50	
├ ──	Cos	d.	Cot	d. c.	Tan	9.98938 Sin		P. P.
	Cos	ı a.	I COT	1 a. c.	ıan	ı sın		r.r.

12,							167	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9 - 33534	34	9.34576	35	0.65424	9.98958	50	
51	9.33568	34	9.34611	36	0.65389	9.98956	49	1
52	9.33602	34	9.34647	36	0.65353	9.98955	48	
53	9.33636	34	9.34683	36	0.65317	9.98953	47	36
54	9.33670	34	9.34719	36	0.65281	9.98951	46	1 3.6
55	9.33704	34	9.34755	35	0.65245	9.98950	45	2 7.2
56	9.33738	34	9.34790	36	0.65210	9.98948	44	3 10.8
57	9.33772	34	9.34826	36	0.65174	9.98946	43	4 14.4 5 18.0
58	9.33806	34	9.34862	35	0.65138	9.98945	43	5 18.0 6 21.6
59	9.33840	34	9.34897	36	0.65103	9.98943	41	7 25.2
60	9.33874	34	9.34933	35	0.65067	9.98941	40	8 28.8
61	9.33908	34	9.34968	36	0.65032	9.98940	39	9 32.4
621	9.33942	34	9.35004	36	0.64996	9.98938	38	
63	9.33976	34	9.35040	35	0.64960	9.98936	37	
64	9.34010	33	9.35075	36	0.64925	9.98934	36	95
65 66	9.34043	34	9.35111	35	0.64889	9.98933	35	35
	9.34077	34	9.35146	35	0.64854	9.98931	34	1 3.5
67	9.34111	34	9.35181	36	0.64819	9.98929	33	2 7.0
68 69	9.34145 9.34178	33	9.35217 9.35252	35	0.64783 0.64748	9.98928 9.98926	32	3 10.5 4 14.0
70		34		36			31	
	9.34212	34	9.35288	35	0.64712	9.98924	30	5 17.5 6 21.0
71	9.34246	33	9.35323	35	0.64677	9.98923	29	7 24.5
73	9.34279	34	9.35358	36	0.64642	9.98921 9.98919	28	8 28.0
73	9.34313	33	9.35394	35			37	9 31.5
74	9.34346 9.34380	34	9.35429	35	0.6457I 0.64536	9.98917 9.98916	26	
75 76	9.34413	33	9.35464 9.35499	35	0.64501	9.98910	25 24	
77	9.34447	34	9.35534	35	0.64466	9.98914		34
77 78	9.34447	33	9.35534	36	0.64430	9.98912	23 22	I 3.4
79	9.34514	34	9.35605	35	0.64395	9.98909	21	2 6.8
80	9.34547	33	9.35640	35	0.64360	9.98907	20	3 10.2
81		33		35				4 13.6
82	9.34580 9.34614	34	9.35675 9.35710	35	0.64325	9.98905 9.98904	19 18	5 17.0
83	9.34647	33	9.35745	35	0.64255	9.98904	17	6 20.4
84	9.34680	33	9.35780	35	0.64233	9.98900	16	7 23.8 8 27.2
85	9.34000	33	9.35760	35	0.64185	9.98898	15	8 27.2 9 30.6
86	9.34747	34	9.35850	35	0.64150	9.98897	14	9 30.0
87	9.34780	33	9.35885	35	0.64115	9.98895	13	
88	9.34813	33	9.35920	35	0.64080	9.98893	12	
89	9.34846	33	9.35955	35	0.64045	9.98892	11	33
90	9.34879	33	9.35989	34	0.64011	9.98890	10	I 3.3
91	9.34912	33	9.36024	35	0.63976	9.98888	09	2 6.6
92	9.34945	33 33	9.36059	35	0.63941	9.98886	08	3 9.9
93	9.34978	33	9.36094	35 34	0.63906	9.98885	07	4 13.2
94	9.35011	1	9.36128		0.63872	9.98883	06	5 16.5 6 19.8
95	9.35044	33 33	9.36163	35 35	0.63837	9.98881	05	7 23.1
96	9.35077	33	9.36198	35	0.63802	9.98879	04	8 26.4
97	9.35110	33	9.36233	34	0.63767	9.98878	03	9 29.7
98	9.35143	33	9.36267	35	0.63733	9.98876	02	
99	9.35176	33	9.36302	34	0.63698	9.98874	01	
100	9.35209		9.36336		0.63664	9.98872	00	
	Cos	đ.	Cot	d.c.	Tan	Sin		P. P.

13°							100	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.35209	33	9.36336	35	0.63664	9.98872	100	
01	9.35242	32	9.36371	35	0.63629	9.98871	99	
02	9.35274	33	9.36406	34	0.63594	9.98869	98	
03	9.35307	33	9.36440	35	0.63560	9.98867	97	35
04	9.35340		9.36475	34	0.63525	9.98865	96	1 3.5
05	9.35373	33 32	9.36509	34	0.63491	9.98864	95	2 7.0
06	9.35405	33	9.36543	35	0.63457	9.98862	94	3 10.5
07	9.35438	33	9.36578	34	0.63422	9.98860	93	4 14.0
о8	9.35471	32	9.36612	35	0.63388	9.98858	92	5 17.5
09	9.35503	33	9.36647	34	0.63353	9.98857	91	6 21.0 7 24.5
10	9.35536	32	9.36681	34	0.63319	9.98855	90	8 28.0
11	9.35568		9.36715		0.63285	9.98853	89	9 31.5
12	9.35601	33 32	9.36750	35 34	0.63250	9.98851	88	3 . 35
13	9.35633	33	9.36784	34	0.63216	9.98850	87	
14	9.35666		9.36818		0.63182	9.98848	86	
15	9.35698	32 33	9.36852	34 35	0.63148	9.98846	85	34
16	9.35731	33	9.36887	34	0.63113	9.98844	84	I 3.4
17	9.35763	33	9.36921	34	0.63079	9.98842	83	2 6.8
18	9.35796	33	9.36955	34	0.63045	9.98841	82	3 10.2
19	9.35828	32	9.36989	34	0.63011	9.98839	81	4 13.6
20	9.35860		9.37023		0.62977	9.98837	80	5 17.0
21	9.35893	33	9.37057	34	0.62943	9.98835	79	6 20.4 7 23.8
22	9.35925	32	9.37091	34	0.62909	9.98834	78	7 23.8 8 27.2
23	9.35957	32	9.37125	34	0.62875	9.98832	77	9 30.6
24	9.35989	32	9.37159	34	0.62841	9.98830	76	9 30.0
25	9.36022	33	9.37193	34	0.62807	9.98828	75	ļ
26	9.36054	32 32	9.37227	34 34	0.62773	9.98826	74	
27	9.36086	l	9.37261	1	0.62739	9.98825	73	33
28	9.36118	32	9.37295	34	0.62705	9.98823	72	I 3.3
29	9.36150	32 32	9.37329	34 34	0.62671	9.98821	71	2 6.6
30	9.36182	_	9.37363	1	0.62637	9.98819	70	3 9.9
31	9.36214	32	9.37397	34	0.62603	9.98817	69	4 13.2
32	9.36246	32	9.37431	34	0.62569	9.98816	68	5 16.5 6 19.8
33	9.36278	32	9.37464	33	0.62536	9.98814	67	6 19.8 7 23.1
34	9.36310	32	9.37498	34	0.62502	9.98812	66	8 26.4
35	9.36342	32	9.37532	34	0.62468	9.98810	65	9 29.7
36	9.36374	32 32	9.37566	34 33	0.62434	9.98808	64	
37	9.36406	1	9.37599	1	0.62401	9.98807	63	1
38	9.36438	32 32	9.37633	34 34	0.62367	9.98805	62	
39	9.36470	32	9.37667	33	0.62333	9.98803	61	32
40	9.36502	31	9.37700		0.62300	9.98801	60	I 3.2
41	9.36533		9.37734	34	0.62266	9.98799	59	2 6.4
42	9.36565	32	9.37768	34	0.62232	9.98798	58	3 9.6
43	9.36597	32 32	9.37801	33 34	0.62199	9.98796	57	4 12.8 5 16.0
44	9.36629	_	9.37835	1	0.62165	9.98794	56	5 16.0 6 19.2
45	9.36660	31 32	9.37868	33 34	0.62132	9.98792	55	7 22.4
46	9.36692	32	9.37902	33	0.62098	9.98790	54	8 25.6
47	9.36724	31	9.37935		0.62065	9.98789	53	9 28.8
48	9.36755	31	9.37969	34 33	0.62031	9.98787	52	1
49	9.36787	32	9.38002	33	0.61998	9.98785	51	
50	9.36819	J.	9.38035	33	0.61965	9.98783	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
		u.		, u. c.	· Ian	UIII		A + A +

13°							100	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.36819	31	9.38035	34	0.61965	9.98783	50	
51	9.36850	32	9.38069	33	0.61931	9.98781	49	
52	9.36882	31	9.38102	33	0.61898	9,98780	48	
53	9.36913	32	9.38135	34	0.61865	9.98778	47	33
54	9.36945	31	9.38169	33	0.61831	9.98776	46	I 3.3
55	9.36976	32	9.38202	33	0.61798	9.98774	45	2 6.6
56	9.37008	31	9.38235	34	0.61765	9.98772	44	3 9.9 4 13.2
57	9.37039	31	9.38269	33	0.61731	9.98770 9.98769	43	5 16.5
58 59	9.37070 9.37102	32	9.38302 9.38335	33	0.61665	9.98767	41	6 19.8
60		31	9.38368	33	0.61632	9.98765	40	7 23.I
61	9.37133	31		33		9.98763	39	8 26.4
62	9.37164 9.37196	32	9.3840I 9.38434	33	0.61599	9.98761	39	9 29.7
63	9.37190	31	9.38468	34	0.61532	9.98759	37	
64	9.37258	31	9.38501	33	0.61499	9.98758	36	
65	9.37289	31	9.38534	33	0.61466	9.98756	35	32
66	9.37321	32	9.38567	33	0.61433	9.98754	34	I 3.2
67	9.37352	31	9.38600	33	0.61400	9.98752	33	2 6.4
68	9.37383	31	9.38633	33	0.61367	9.98750	32	3 9.6
69	9.37414	3I 3I	9.38666	33 33	0.61334	9.98748	31	4 12.8
70	9.37445	31	9.38699	33	0.61301	9.98746	30	5 16.0 6 19.2
71	9.37476	-	9.38732		0.61268	9.98745	29	6 19.2 7 22.4
72	9.37507	31 31	9.38765	33 32	0.61235	9.98743	28	8 25.6
73	9.37538	31	9.38797	33	0.61203	9.98741	27	9 28.8
74	9.37569	31	9.38830	33	0.61170	9.98739	26	
75	9.37600	31	9.38863	33	0.61137	9.98737	25	
76	9.37631	31	9.38896	33	0.61104	9.98735	24	
77	9.37662	31	9.38929	33	0.61071	9.98734	23	31
78	9.37693	31	9.38962	32	0.61038	9.98732	22	I 3.I
79	9.37724	31	9.38994	33	0.61006	9.98730	31	2 6.2
80	9.37755	31	9.39027	. 33	0.60973	9.98728	20	3 9.3
81	9.37786	31	9.39060	32	0.60940	9.98726	19	5 15.5
82	9.37817	30	9.39092	33	0.60908	9.98724	18	6 18.6
83	9.37847	31	9.39125	33	0.60875	9.98722	17	7 21.7
84 85	9.37878	31	9.39158	32	0.60810	9.98720	15	8 24.8
86	9.37909	31	9.39190	33	0.60777	9.98719	14	9 27.9
87	9.37940	30	9.39223	33	0.60711	9.98715	13	
88	9.37970 9.38001	31	9.39288	32	0.60712	9.98713	12	1
89	9.38032	31 30	9.39200	33	0.60679	9.98711	11	30
90	9.38062		9.39353	1 -	0.60647	9.98709	10	1 3.0
91	9.38093	31	9.39386	. 33	0.60614	9.98707	- 09	2 6.0
92	9.38124	31 30	9.39300	32 33	0.60582	9.98705	08	3 9.0
93	9.38154	31	9.39451	33	0.60549	9.98704	07	4 12.0 5 15.0
94	9.38185	30	9.39483	32	0.60517	9.98702	06	5 15.0 6 18.0
95	9.38215	31	9.39515	33	0.60485	9.98700	05	7 21.0
96	9.38246	30	9.39548	32	0.60452	9.98698	04	8 24.0
97	9.38276	31	9.39580	32	0.60420	9.98696	03	9 27.0
98	9.38307	30	9.39612	33	0.60388	9.98694	02	
99	9.38337	31	9.39645	32	0.60355	9.98692	01	
100	9.38368		9.39677		0.60323	9.98690	00	
	Cos	d.	Cot	d.c.	Tan	Sin	1	P. P.

14°							165°	
	Sin	d.	Tan	d.c.	Cot	Cos	1.	P. P.
00	9.38368	30	9.39677	32	0.60323	9.98690	100	
01	9.38398	30	9.39709	33	0.60291	9.98689	99	Į.
02	9.38428	31	9.39742	33	0.60258	9.98687	98	
03	9.38459	30	9.39744	32	0.60226	9.98685	97	33
04	9.38489	30	9.39806	32	0.60194	9.98683	96	I 3.3
05	9.38519	31	9.39838	32	0.60162	9.98681	95	2 6.6
06	9.38550	30	9.39870	33	0.60130	9.98679	94	3 9.9
07	9.38580	30	9.39903	32	0.60097	9.98677	93	4 13.2 5 16.5
08 09	9.38610 9.38640	30	9.39935	32	0.60065	9.98675 9.98673	92 91	6 19.8
-		30	9.39967	32			90	7 23.1
10	9.38670	31	9.39999	32	0.60001	9.98671	1	8 26.4
11	9.38701	30	9.40031	32	0.59969	9.98670 9.98668	89 88	9 29.7
12	9.38731 9.38761	30	9.40063	32	0.59937	9.98666	87	
14	9.38791	30		32	0.59873	9.98664	86	
15	9.38791	30	9.40127	32	0.59841	9.98662	85	32
16	9.38851	30	9.40191	32	0.59809	9.98660	84	I 3.2
17	9.38881	30	9.40223	32	0.59777	9.98658	83	2 6.4
18	9.38911	30	9.40223	32	0.59717	9.98656	82	3 9.6
19	9.38941	30 30	9.40287	32 32	0.59713	9.98654	81	4 12.8
20	9.38971	-	9.40319		0.59681	9.98652	80	5 16.0
21	9.39001	30	9.40351	32	0.59649	9_98650	79	6 19.2
22	9.39031	30	9.40382	31	0.59618	9.98648	78	7 22.4 8 25.6
23	9.39061	30 30	9.40414	32 32	0.59586	9.98647	77	9 28.8
24	9.39091		9.40446	1 -	0.59554	9.98645	76	,
25	9.39121	30 29	9.40478	32 32	0.59522	9.98643	75	
26	9.39150	30	9.40510	31	0.59490	9.98641	74	
27	9.39180	30	9.40541	32	0.59459	9.98639	73	31
28	9.39210	30	9.40573	32	0.59427	9.98637	72	I 3.I
29	9.39240	30	9.40605	31	0.59395	9.98635	71	2 6.2
30	9.39270	29	9.40636	32	0.59364	9.98633	70	3 9.3
31	9.39299	30	9.40668	32	0.59332	9.98631	69	4 12.4 5 15.5
32	9.39329	30	9.40700	31	0.59300	9.98629	68	6 18.6
33	9.39359	29	9.40731	32	0.59269	9.98627	67	7 21.7
34	9.39388	30	9.40763	32	0.59237	9.98625	66	8 24.8
35	9.39418	30	9.40795	31	0.59205	9.98623	65	9 27.9
36	9.39448	29	9.40826	32	0.59174	9.98621	64	I
37	9.39477	30	9.40858	31	0.59142	9.98620	63	l
38	9.39507 9.39536	29	9.40889 9.40921	32	0.59111	9.98618 9.98616	62 61	30
39 40		30		31		9.98614	60	I 3.0
	9.39566	29	9.40952	32	0.59048		1	2 6.0
41	9.39595 9.39625	30	9.40984	31	0.59016 0.58985	9.98612 9.98610	59 58	3 9.0
42 43	9.39654	29	9.41015 9.41046	31	0.58954	9.98608	57	4 12.0
43	9.39684	30	9.41048	32	0.58922	9.98606	56	5 15.0
45	9.39084	29	9.41078	31	0.58891	9.98604	55	6 18.0
46	9.39743	30 29	9.41141	32 31	0.58859	9.98602	54	7 21.0 8 24.0
47	9.39772		9.41172		0.58828	9.98600	53	9 27.0
48	9.39801	29 30	9.41203	31 32	0.58797	9.98598	52	J
49	9.39831	29	9.41235	31	0.58765	9.98596	51	
50	9.39860	-9	9.41266	J-	0.58734	9.98594	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
		٠.						

14							165°	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.39860	29	9.41266	31	0.58734	9.98594	50	
51	9.39889	30	9.41297	31	0.58703	9.98592	49	
52	9.39919	29	9.41328	32	0.58672	9.98590	48	
53	9.39948	29	9.41360	31	0.58640	9.98588	47	31
54	9 39977	29	9.41391	31	0.58609	9.98586	46	I 3.I
55 56	9.40006	29	9.41422	31	0.58578	9.98584	45	2 6.2
	9.40035	30	9.41453	31	0.58547	9.98582	44	3 9.3
57 58	9.40065	29	9.41484	31	0.58516	9.98580	43	4 12.4 5 15.5
59	9.40094 9.40123	29	9.41515 9.41546	31	0.58485	9.98578 9.98576	42 41	6 18.6
60	9.40152	29	9.41578	32	0.58422	9.98574	40	7 21.7
61		29		31				8 24.8
62	9.40181	29	9.41609 9.41640	31	0.58391 0.58360	9.98573 9.98571	39 38	9 27.9
63	9.40239	29	9.41641	31	0.58329	9.98569	37	
64	9.40268	29	9.41702	31	0.58298	9.98567	36	
65	9.40208	29	9.41702	31	0.58298	9.98565	35	30
66	9.40326	29 29	9.41764	31 31	0.58236	9.98563	34	I 3.0
67	9.40355	-	9.41795		0.58205	9.98561	33	2 6.0
68	9.40384	29 29	9.41825	30 31	0.58175	9.98559	32	3 9.0
69	9.40413	29	9.41856	31	0.58144	9.98557	31	4 12.0
70	9.40442	29	9.41887	31	0.58113	9.98555	30	5 15.0
71	9.40471	29	9.41918	31	0.58082	9.98553	29	6 18.0 7 21.0
72	9.40500	29	9.41949	31	0.58051	9.98551	28	8 21.0
73	9.40529	28	9.41980	31	0.58020	9.98549	27	9 27.0
74	9.40557	29	9.42011	30	0.57989	9.98547	26	
75	9.40586	29	9.42041	31	0.57959	9.98545	25	
76	9.40615	29	9.42072	31	0.57928	9.98543	24	20
77	9.40644	28	9.42103	31	0.57897	9.98541	23	29
78 79	9.40672	29	9.42134	30	0.57866	9.98539	22	1 2.9
80	9.40701	29	9.42164	31	0.57836	9.98537	21	2 5.8 3 8.7
	9.40730	29	9.42195	31	0.57805	9.98535	20	4 11.6
81 82	9.40759	28	9.42226	30	0.57774	9.98533	19	5 14.5
83	9.40787	29	9.42256	31	0.57744	9.98531	18 17	6 17.4
84	9.40816	28	9.42287	31	0.57713	9.98529	16	7 20.3
85	9.40844	29	9.42318	30	0.57682 0.57652	9.98527	15	8 23.2
86	9.40902	29	9.42348 9.42379	31	0.57621	9.9852 5 9.9852 3	14	9 26.1
87	9.40930	28	9.42410	31	0.57590	9.98521	13	
88	9.40959	29 28	9.42410	30	0.57560	9.98519	12	
89	9.40987	28 29	9.42471	31 30	0.57529	9.98517	11	28
90	9.41016	28	9.42501	31	0.57499	9.98515	10	I 2.8
91	9.41044		9.42532	1	0.57468	9.98513	09	2 5.6
92	9.41073	29 28	9.42562	30 31	0.57438	9.98511	08	3 8.4
93	9.41101	29	9.42593	30	0.57407	9.98509	07	4 II.2 5 I4.0
94	9.41130	28	9.42623	30	0.57377	9.98507	06	5 14.0 6 16.8
95	9.41158	28	9.42653	31	0.57347	9.98505	05	7 19.6
96	9.41186	29	9.42684	30	0.57316	9.98502	04	8 22.4
97	9.41215	28	9.42714	31	0.57286	9.98500	03	9 25.2
98	9.41243	28	9.42745	30	0.57255	9.98498	02	
99	9.41271	29	9.42775	30	0.57225	9.98496	01	
100	9.41300		9.42805		0.57195	9.98494	00	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

10							104	
	Sin	d.	Tan	d. c.	Cot	Cos	I	P. P.
00	9.41300	28	9.42805	31	0.57195	9.98494	100	
01	9.41328	28	9.42836	30	0.57164	9.98492	99	
02	9.41356	28	9.42866	30	0.57134	9.98490	98	
03	9.41384	29	9.42896	30	0.57104	9.98488	97	31
04	9.41413	28	9.42926	31	0.57074	9.98486	96	I 3.I
05	9.41441	28	9.42957	30	0.57043	9.98484	95	2 6.2
о6	9.41469	28	9.42987	30	0.57013	9.98482	94	3 9.3
07	9.41497	28	9.43017	30	0.56983	9.98480	93	4 I2.4 5 I5.5
o8 o9	9.41525	28	9.43047	30	0.56953	9.98478	92	6 18.6
10	9.41553	29	9.43077	31	0.56923	9.98476	91	7 21 7
	9.41582	28	9.43108	30	0.56892	9.98474	90	8 24.8
11	9.41610	28	9.43138	30	0.56862	9.98472	89	9 27.9
12 13	9.41638 9.41666	28	9.43168 9.43198	30	0.56832	9.98470 9.98468	88 87	
-	9.41604	28		30	1	1	86	
14 15	9.41094	28	9.43228 9.43258	30	0.56772	9.98466 9.98464	85	30
16	9.41750	28	9.43288	30	0.56712	9.98462	84	I 3.0
17	9.41778	28	9.43318	30	0.56682	9.98460	83	2 6.0
18	9.41776	28	9.43348	30	0.56652	9.98458	82	3 9.0
19	9.41834	28 27	9.43378	30	0.56622	9.98456	81	4 12.0
20	9.41861		9.43408	30	0.56592	9.98453	80	5 15.0
21	9.41889	28	9 43438	30	0.56562	9.98451	79	6 18.0
22	9.41917	28 28	9.43468	30	0.56532	9.98449	78	7 21.0 8 24.0
23	9.41945	28	9.43498	30 30	0.56502	9.98447	77	9 27.0
24	9.41973	28	9.43528	_	0.56472	9.98445	76	3 1 =7.0
25	9.42001	28	9.43558	30 29	0.56442	9.98443	75	
26	9.42029	27	9.43587	30	0.56413	9.98441	74	
27	9.42056	28	9.43617	30	0.56383	9.98439	73	29
28	9.42084	28	9.43647	30	0.56353	9.98437	72	I 2.9
29	9.42112	28	9.43677	30	0.56323	9.98435	71	2 5.8
30	9.42140	27	9.43707	29	0.56293	9.98433	70	3 8.7 4 11.6
31	9.42167	28	9.43736	30	0.56264	9.98431	69	5 14.5
32	9.42195	28	9.43766	30	0.56234	9.98429	68	6 17.4
33	9.42223	27	9.43796	30	0.56204	9.98427	67	7 20.3
34	9.42250	28	9.43826	29	0.56174	9.98425	66	8 23.2
35 36	9.42278 9.42305	27	9.43855 9.43885	30	0.56145	9.98422	65	9 26.1
37	9.42333	28	9.43005	30		9.98420	64	
37 38	9.42333	28	9.43915	29	0.56085 0.56056	9.98418	63 62	
39	9.42388	27	9.43944	30	0.56026	9.98414	61	28
40	9.42416	28	9.44004	30	0.55996	9.98412	60	1 2.8
41	9.42443	27	9.44033	29	0.55967	9.98410	59	2 5.6
42	9.42443	28	9.44063	30	0.55907	9.98408	59 58	3 8.4
43	9.42498	27 28	9.44092	29 30	0.55908	9.98406	57	4 11.2
44	9.42526	27	9.44122		0.55878	9.98404	56	5 14.0 6 16.8
45	9.42553	27 27	9.44151	29 30	0.55849	9.98402	55	7 19.6
46	9.42580	28	9.44181	29	0.55819	9.98399	54	8 22.4
47	9.42608	27	9.44210	30	0.55790	9.98397	53	9 25.2
48	9.42635	28	9.44240	29	0.55760	9.98395	52	
49	9.42663	27	9.44269	30	0.55731	9.98393	51	
50	9.42690		9.44299		0.55701	9.98391	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.42690	27	9.44299	29	0.55701	9.98391	50	
51	9.42717	28	9.44328	-	0.55672	9.98389	49	
52	9.42745	20	9.44358	न्द् 29	0.55642	9.98387	48	
53	9.42772	27	9.44387	29	0.55613	9.98385	47	29
54	9.42799	27	9.44416	30	0.55584	9.98383	46	I 2.9
55	9.42826	28	9.44446	29	0.55554	9.98381	45	2 5.8
56	9.42854	27	9 44475	29	0.55525	9.98378	44	3 8.7 4 11.6
57	9.42881	27	9.44504	30	0.55496	9.98376	43	5 14.5
58 59	9.42908 9.42935	27	9 · 44534 9 · 44563	29	0.55466 0.55437	9.98374 9.98372	42 41	6 17.4
60	9.42933	27		29	0.55408	9.98370	40	7 20.3
61		27	9.44592	30		9.98368		8 23.2
62	9.42989	28	9.44622 9.44651	29	0.55378 0.55349	9.98366	39 38	9 26.1
63	9.43017	27	9.44680	29	0.55320	9.98364	37	
64	9.43071	27	9.44709	29	0.55291	9.98361	36	
65	9.43071	27	9.44738	29	0.55262	9.98359	35	28
66	9.43125	27 27	9.44768	30 29	0.55232	9.98357	34	1 2.8
67	9.43152	27	9.44797	29	0.55203	9.98355	33	2 5.6
68	9.43179	27	9.44826	29	0.55174	9.98353	32	3 8.4
69	9.43206	27	9.44855	29	0.55145	9.98351	31	4 II.2 5 I4.0
70	9.43233	27	9.44884	29	0.55116	9.98349	30	5 14.0 6 16.8
71	9.43260	27	9.44913	29	0.55087	9.98347	29	7 19.6
72	9.43287	27	9.44942	29	0.55058	9.98344	28	8 22.4
73	9.43314	27	9.44971	29	0.55029	9.98342	27	9 25.2
74	9.43341	26	9.45000	29	0.55000	9.98340	26	
75 76	9.43367	27	9.45029 9.45058	29	0.5497I 0.54942	9.98338 9.98336	25 24	
	9.43394	27		29		9.98334		27
77 78	9.4342I 9.43448	27	9.45087 9.45116	29	0.54913	9.98334	23 22	I 2.7
79	9.43446	27	9.45145	29	0.54855	9.98329	21	2 5.4
80	9.43502	27	9.45174	29	0.54826	9.98327	20	3 8.1
81	9.43528	26	9.45203	29	0.54797	9.98325	19	4 10.8
82	9.43555	27	9.45232	29	0.54768	9.98323	18	5 13.5 6 16.2
83	9.43582	27 27	9.45261	29 29	0.54739	9.98321	17	7 18.9
84	9.43609	26	9.45290	29	0.54710	9.98319	16	8 21.6
85	9.43635	20 27	9.45319	29	0.54681	9.98317	15	9 24.3
86	9.43662	27	9.45348	28	0.54652	9.98314	14	
87	9.43689	26	9.45376	29	0.54624	9.98312	13	
88	9.43715	27	9.45405	29	0.54595	9.98310	12	26
89	9.43742	27	9 45434	29	0.54566	9.98308	11	1 2.6
90	9.43769	26	9.45463	29	0.54537	9.98306	10	2 5.2
91	9 43795	27	9.45492	28	0.54508	9.98304	o9 o8	3 7.8
92 93	9.43822 9.43848	26	9.45520 9.45549	29	0.54480 0.5445I	9.98302	08	4 10.4
		27		29		9.98299	06	5 13.0
94 95	9.43875 9.43901	26	9.45578 9.45606	28	0.54422 0.54394	9.98297	05	6 15.6
95 96	9.43901	27	9.45635	29	0.54365	9.98293	04	7 18.2 8 20.8
97	9.43954	26	9.45664	29	0.54336	9.98291	03	9 23.4
98	9.43981	27	9.45692	28	0.54308	9.98289	02	,
99	9.44007	26 27	9.45721	29 29	0.54279	9.98286	01	
100	9.44034	41	9.45750	29	0.54250	9.98284	00	
_	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

		400
l6°		163

16°							163°	
	Sin	d.	Tan	d. c.	Cot	Cos	1	P. P.
00	9.44034	26	9.45750	28	0.54250	9.98284	100	
OI	9.44060	27	9.45778	29	0.54222	9.98282	99	
02	9.44087	26	9.45807	28	0.54193	9.98280	98	29
03	9.44113	26	9.45835	29	0.54165	9.98278	97	
04	9.44139 9.44166	27	9.45864	28	0.54136	9.98275 9.98273	96	1 2.9 2 5.8
05 06	9.44192	26	9.45892 9.45921	29	0.54108	9.98271	95 94	3 8.7
07	9.44218	26	9.45950	29	0.54050	9.98269	93	4 11.6
۰8 80	9.44245	27	9.45978	28 28	0.54022	9.98267	93	5 14.5 6 17.4
09	9.44271	26 26	9.46006	28 29	0.53994	9.98265	91	6 17.4 7 20.3
10	9.44297	27	9.46035	28	0.53965	9.98262	90	8 23.2
11	9.44324	26	9.46063	29	0.53937	9.98260	89	9 26.1
12	9.44350	26	9.46092	28	0.53908	9.98258	88	
13	9.44376	26	9.46120	29	0.53880	9.98256	87	28
14	9.44402	26	9.46149	28	0.53851	9.98254	86	
15 16	9.44428	27	9.46177	28	0.53823	9.98251	85	1 2.8 2 5.6
	9.44455	26	9.46205	29	0.53795	9.98249	84	3 8.4
17 18	9.44481 9.44507	26	9.46234	28	0.53766	9.98247 9.98245	83 82	4 11.2
19	9.44533	26	9.46290	28	0.53710	9.98243	81	5 14.0
20	9.44559	26	9.46319	29	0.53681	9.98240	80	6 16.8
21	9.44585	26	9.46347	28	0.53653	9.98238	79	7 19.6 8 22.4
22	9.44611	26 26	9.46375	28 28	0.53625	9.98236	78	9 25.2
23	9.44637	26	9.46403	29	0.53597	9.98234	77	
24	9.44663	26	9.46432	28	0.53568	9.98232	76	
25	9.44689	26	9.46460	28	0.53540	9.98229	75	
26	9.44715	26	9.46488	28	0.53512	9.98227	74	
27	9.44741	26	9.46516	28	0.53484	9.98225	73	
28 29	9.44767 9.44793	26	9.46544 9.46573	29	0.53456	9.98223 9.98221	72 71	27
30	9.44793	26	9.46601	28		9.98218	70	I 2.7
31	9.44845	26	9.46629	28	0.53399	9.98216	69	2 5.4 3 8.1
32	9.44845	26	9.46657	28	0.53371	9.98210	68	4 10.8
33	9.44897	26 26	9.46685	28 28	0.53315	9.98212	67	5 13.5
34	9.44923		9.46713		0.53287	9.98209	1 66	6 16.2
35	9.44948	25 26	9.46741	28 28	0.53259	9.98207	65	7 18.9 8 21.6
36	9.44974	26	9.46769	28	0.53231	9.98205	64	9 24.3
37	9.45000	26	9.46797	28	0.53203	9.98203	63	y 1 = T.0
38	9.45026	26	9.46825	28	0.53175	9.98201	62	
39	9.45052	25	9.46853	28	0.53147	9.98198	61	26
40	9.45077	26	9.46881	28	0.53119	9.98196	60	1 2.6
41	9.45103	26	9.46909	28	0.53091	9.98194	59	2 5.2 3 7.8
42 43	9.45129 9.45155	26	9.46937 9.46965	28	0.53063	9.98192 9.98189	58 57	3 7.8
43	9.45180	25	9.46993	28	0.53007	9.98187	56	5 13.0
44 45	9.45206	26	9.40993	28	0.53007	9.98185	55	6 15.6
46	9.45232	26 25	9.47049	28 28	0.52951	9.98183	54	7 18.2
47	9.45257	25 26	9.47077	28	0.52923	9.98180	53	8 20.8 9 23.4
48	9.45283	26	9.47105	28 28	0.52895	9.98178	52	9 23.4
49	9.45309	25	9.47133	27	0.52867	9.98176	51	
50	9 · 45334		9.47160		0.52840	9.98174	50	
	Cos	d.	Cot	d. c.	Tan	Sin	ı	P. P.

e de la composição de l		1	T.	-	C .			D D
	Sin	_d.	Tan	d. c.	Cot	Cos		P. P.
50	9 - 45334	26	9.47160	28	0.52840	9.98174	50	
51	9.45360	25	9.47188	28-	0.52812	9.98171	49	
52	9.45385	26	9.47216	28	0.52784	9.98169	48	28
53	9.45411	25	9.47244	28	0.52756	9.98167	47	
54	9.45436	26	9.47272	27	0.52728	9.98165	46	1 2.8 2 5.6
55	9.45462	25	9.47299	28	0.52701	9.98162	45	3 8.4
56	9.45487	26	9.47327	28	0.52673	9.98160	44	4 11.2
57	9.45513	25	9.47355	28	0.52645	9.98158	43	5 14.0
58 59	9.45538	26	9.47383	27	0.52617	9.98156	42	6 16.8
60	9.45564	25	9.47410	28	0.52590	9.98153	41	7 19.6
	9.45589	26	9.47438	28	0.52562	9.98151	40	8 22.4
61	9.45615	25	9.47466	27	0.52534	9.98149	39	9 25.2
62	9.45640	25	9 - 47493	28	0.52507	9.98147	38	
63	9.45665	26	9.47521	28	0.52479	9.98144	37	
64	9.45691	25	9.47549	27	0.52451	9.98142	36	27
65 66	9.45716	26	9.47576	28	0.52424	9.98140	35	I 2.7
	9.45742	25	9.47604	28	0.52396	9.98138	34	2 5.4
67 68	9.45767	25	9.47632	27	0.52368	9.98135	33	3 8.1 4 10.8
69	9.45792 9.45817	25	9.47659	28	0.52341	9.98133	32	4 10.8 5 13.5
70		26	9.47687	27	0.52313	9.98131	31	6 16.2
	9.45843	25	9.47714	28	0.52286	9.98129	30	7 18.9
71	9.45868	25	9.47742	27	0.52258	9.98126	29	8 21.6
72	9.45893	25	9.47769	28	0.52231	9.98124	28	9 24.3
73	9.45918	26	9-47797	27	0.52203	9.98122	27	
74	9.45944	25	9.47824	28	0.52176	9.98119	26	
75 76	9.45969	25	9.47852	27	0.52148	9.98117	25	
1 .	9 45994	25	9.47879	28	0.52121	9.98115	24	
77 78	9.46019	25	9.47907	27	0.52093	9.98113	23	25
78 79	9.46044	25	9.47934 9.47961	27	o.52066 o.52039	9.98110	22 21	I 2.5
80		26		28				2 5.0
	9.46095	25	9.47989	27	0.52011	9.98106	20	3 7.5
81	9.46120	25	9.48016	28	0.51984	9.98103	19	4 10.0
82 83	9.46145	25	9.48044	27	0.51956	9.98101	18	5 12.5
		25	9.48071	27	0.51929	9.98099	17	6 15.0
84	9.46195	25	9.48098	28	0.51902	9.98097	16	7 17.5
85 86	9.46220 9.46245	25	9.48126	27	0.51874	9.98094	15 14	8 20.0
87		25	9.48153	27	0.51847	9.98092		9 22.5
88 88	9.46270 9.46295	25	9.48180 9.48208	28	0.51820	9.98090 9.98087	13 12	
89	9.46320	25	9.48235	27	0.51792	9.98087	12	24
90	9.46345	25	9.48262	27		9.98083	10	
		25		27	0.51738			2 4.8
91	9.46370	25	9.48289	28	0.51711	9.98080	o9 o8	3 7.2
92 93	9.46395	25	9.48317 9.48344	27	0.51683	9.98078 9.98076	07	4 9.6
		24		27			06	5 12.0
94 95	9.46444 9.46469	25	9.48371	27	0.51629	9.98074 9.98071	05	6 14.4
95 96	9.46494	25	9.48398 9.48425	27	0.51575	9.98071	05	7 16.8
97	9.46519	25		28		9.98009		8 19.2
97	9.46544	25	9.48453 9.48480	27	0.51547	9.98007	03	9 21.6
99	9.46569	25	9.48507	27	0.51520	9.98004	01	
100	9.46594	25	9.48534	27	0.51466	9.98060	00	
1	Cos	d.		d a		Sin		P. P.
1000	COS	u.	Cot	d. c.	Tan	SIII		1.1.

							102	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.46594	24	9.48534	27	0.51466	9.98060	100	
OI	9.46618	25	9.48561	27	0.51439	9.98057	99	
02	9.46643	25	9.48588	27	0.51412	9.98055	98	0.7
03	9.46668	25	9.48615	27	0.51385	9.98053	97	27
04	9.46693	24	9.48642	27	0.51358	9.98050	96	I 2.7
05	9.46717	25	9.48669	27	0.51331	9.98048	95	2 5.4
06	9.46742	25	9.48696	27	0.51304	9.98046	94	3 8.1
07	9.46767	24	9.48723	27	0.51277	9.98043	93	4 10.8
о8	9.46791	25	9.48750	27	0.51250	9.98041	92	5 13.5 6 16.2
09	9.46816	25	9.48777	27	0.51223	9.98039	91	7 18.9
10	9.46841	24	9.48804	27	0.51196	9.98036	90	8 21.6
11	9.46865		9.48831		0.51169	9.98034	89	9 24.3
12	9.46890	25	9.48858	27	0.51142	9.98032	88	, ,
13	9.46915	25	9.48885	27	0.51115	9.98029	87	
14	9.46939	24	9.48912	27	0.51088	9.98027	86	26
15	9.46964	25	9.48939	27	0.51061	9.98027	85	1 2.6
16	9.46988	24	9.48966	27	0.51034	9.98022	84	2 5.2
17	9.47013	25	9.48993	27	0.51007	9.98020	83	3 7.8
18	9.47013	24	9.40993	27	0.50980	9.98020	82	4 10.4
19	9.47062	25	9.49046	26	0.50954	9.98015	81	5 13.0
20	9.47086	24		27	0.50927		80	6 15.6
		25	9.49073	27		9.98013	1	7 18.2
21	9.47111	24	9.49100	27	0.50900	9.98011	79	8 20.8
22	9.47135	25	9.49127	27	0.50873	9.98008	78	9 23.4
23	9.47160	24	9.49154	27	0.50846	9.98006	77	!
24	9.47184	25	9.49181	26	0.50819	9.98004	76	
25	9.47209	24	9.49207	27	0.50793	9.98001	75	
26	9.47233	24	9.49234	27	0.50766	9.97999	74	ļ
27	9.47257	25	9.49261	27	0.50739	9.97997	73	م م
28	9.47282	24	9.49288	26	0.50712	9 97994	72	25
29	9.47306	24	9.49314	27	0.50686	9.97992	71	I 2.5
30	9.47330	25	9.49341	27	0.50659	9.97989	70	2 5.0
31	9.47355	24	9.49368	26	0.50632	9.97987	69	3 7.5
32	9.47379	24	9.49394	27	0.50606	9.97985	68	4 10.0
33	9.47403	25	9.49421	27	0.50579	9.97982	67	5 12.5 6 15.0
34	9.47428		9.49448		0.50552	9.97980	66	7 17.5
35	9.47452	24	9 49474	26	0.50526	9.97978	65	8 20.0
36	9.47476	24	9.49501	27 27	0.50499	9.97975	64	9 22.5
37	9.47500	24	9.49528		0.50472	9.97973	63] ,
38	9.47525	25	9.49554	26	0.50446	9.97971	62	
39	9.47549	24	9.49581	27 26	0.50419	9.97968	61	24
40	9.47573	24	9.49607		0.50393	9.97966	60	
41	9.47597	24	9.49634	27	0.50366			2 2.4
41	9.47597	24	9.49660	26	0.50340	9.97963 9.97961	59 58	3 7.2
43	9.47646	25	9.49687	27	0.50313	9.97959	50	4 9.6
		24		26				5 12.0
44	9.47670	24	9.49713	27	0.50287	9.97956	56	6 14.4
45 46	9.47094	24	9.49740 9.49766	26	0.50260	9.97954	55	7 16.8
		24	ł .	27		9.97951	54	8 19.2
47 48	9.47742	24	9.49793	26	0.50207	9.97949	53	9 21.6
40 49	9.47766	24	9.49819	27	0.50181	9.97947	52	
	9.47790	24	9.49846	26	0.50154	9.97944	51	
50	9.47814		9.49872		0.50128	9.97942	50	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

_	- 0:	-						NAME OF TAXABLE PARTY.
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.47814	24	9.49872	27	0.50128	9.97942	50	
51	9.47838	24	9.49899	26	0.50101	9.97940	49	
52	9.47862	24	9.49925	26	0.50075	9.97937	48	
53	9.47886	24	9.49951	27	0.50049	9.97935	47	27
54	9.47910	24	9.49978	26	0.50022	9.97932	46	1 2.7
55	9.47934	24	9.50004	27	0.49996	9.97930	45	2 5.4
56	9.47958	24	9.50031	26	0.49969	9.97928	44	3 8.1
57	9.47982	2.1	9.50057	26	0.49943	9.97925	43	4 10.8 5 13.5
58	9.48006	24	9.50083	27	0.49917	9.97923	42	6 16.2
59	9.48030	24	9.50110	26	0.49890	9.97920	41	7 18.9
60	9.48054	24	9.50136	26	0.49864	9.97918	40	8 21.6
61	9.48078	24	9.50162	26	0.49838	9.97916	39	9 24.3
62	9.48102	23	9.50188	27	0.49812	9.97913	38	ł
63	9.48125	24	9.50215	26	0.49785	9.97911	37	
64	9.48149	24	9.50241	26	0.49759	9.97908	36	26
65	9.48173	2.4	9.50267	26	0.49733	9.97906	35	1 2.6
66	9.48197	2.4	9.50293	27	0.49707	9.97904	34	2 5.2
67	9.48221	24	9.50320	26	0.49680	9.97901	33	3 7.8
68	9.48245	23	9.50346	26	0.49654	9.97899	32	4 10.4
69	9.48268	24	9.50372	26	0.49628	9.97896	31	5 13.0
70	9.48292	24	9.50398	26	0.49602	9.97894	30	6 15.6 7 18.2
71	9.48316	24	9.50424	27	0.49576	9.97891	29	7 18.2 8 20.8
72	9.48340	23	9.50451	26	0.49549	9.97889	28	9 23.4
73	9.48363	24	9.50477	26	0.49523	9.97887	27	3 1 23.4
74	9.48387	24	9.50503	26	0.49497	9.97884	26	
75	9.48411	23	9.50529	26	0.49471	9.97882	25	
76	9.48434	24	9.50555	26	0.49445	9.97879	24	
77	9.48458	24	9.50581	26	0.49419	9.97877	23	
78	9.48482	23	9.50607	26	0.49393	9.97874	22	24
79	9.48505	24	9.50633	26	0.49367	9.97872	21	I 2.4
80	9.48529	23	9.50659	26	0.49341	9.97870	20	2 4.8
81	9.48552	24	9.50685	26	0.49315	9.97867	19	3 7.2
82	9.48576	24	9.50711	26	0.49289	9.97865	18	4 9.6 5 12.0
83	9.48600	23	9.50737	26	0.49263	9.97862	17	5 12.0 6 14.4
84	9.48623	24	9.50763	26	0.49237	9.97860	16	7 16.8
85	9.48647	23	9.50789	26	0.49211	9.97857	15	8 19.2
86	9.48670	24	9.50815	26	0.49185	9.97855	14	9 21.6
87	9.48694	23	9.50841	26	0.49159	9.97853	13	
88	9.48717	24	9.50867	26	0.49133	9.97850	12	
89	9.48741	23	9.50893	26	0.49107	9.97848	11	23
90	9.48764	24	9.50919	26	0.49081	9.97845	10	1 2.3
91	9.48788	23	9.50945	26	0.49055	9.97843	09	2 4.6
92	9.48811	23	9.50971	26	0.49029	9.97840	о8	3 6.9
93	9.48835	23	9.50997	26	0.49003	9.97838	07	4 9.2
94	9.48858	23	9.51023	25	0.48977	9.97835	06	5 11.5
95	9.48881	23 24	9.51048	25 26	0.48952	9.97833	05	- -51.
96	9.48905	23	9.51074	26	0.48926	9.97830	04	7 16.1 8 18.4
97	9.48928	24	9.51100	26	0.48900	9.97828	03	9 20.7
98	9.48952	23	9.51126	26 26	0.48874	9.97826	02	9 . 20.1
99	9.48975	23	9.51152	26	0.48848	9.97823	01	
100	9.48998	-5	9.51178		0.48822	9.97821	00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.
	000			4. 0.	T 0411	. 5111		1.1.

18							161	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.48998	24	9.51178	25	0.48822	9.97821	100	
01	9.49022	23	9.51203	26	0.48797	9.97818	99	
02	9.49045	23	9.51229	26	0.48771	9.97816	98	0.0
03	9.49068	23	9.51255	26	0.48745	9.97813	97	26
04	9.49091	24	9.51281	25	0.48719	9.97811	96	1 2.6
05	9.49115	23	9.51306	26	0.48694	9.97808	95	2 5.2
06	9.49138	23	9.51332	26	0.48668	9.97806	94	3 7.8 4 10.4
07	9.49161	23	9.51358	26	0.48642	9.97803	93	5 13.0
08	9.49184	24	9.51384	25	0.48616	9.97801	92	6 15.6
09	9.49208	23	9.51409	26	0.48591	9.97798	91	7 18.2
10	9.49231	23	9.51435	26	0.48565	9.97796	90	8 20.8
11	9.49254	23	9.51461	25	0.48539	9.97793	89	9 23.4
12	9.49277	23	9.51486	26	0.48514	9.97791	88	
13	9.49300	23	9.51512	25	0.48488	9.97788	87	25
14	9.49323	24	9.51537	26	0.48463	9.97786	86	
15	9.49347	23	9.51563	26	0.48437	9.97784	85	I 2.5 2 5.0
16	9.49370	23	9.51589	25	0.48411	9.97781	84	2 5.0 3 7.5
17	9.49393	23	9.51614	26	0.48386	9.97779	83	4 10.0
18	9.49416	23	9.51640	25	0.48360	9.97776	82	5 12.5
19	9.49439	23	9.51665	26	0.48335	9.97774	81	6 15.0
20	9.49462	23	9.51691	26	0.48309	9.97771	80	7 17.5
21	9.49485	23	9.51717	25	0.48283	9.97769	79	8 20.0
22	9.49508	23	9.51742	26	0.48258	9.97766	78	9 22.5
23	9.49531	23	9.51768	25	0.48232	9.97764	77	
24	9 - 49554	23	9.51793	26	0.48207	9.97761	76	
25	9 49577	23	9.51819	25	0.48181	9.97759	75	i
26	9.49600	23	9.51844	26	0.48156	9.97756	74	İ
27 28	9.49623	23	9.51870	25	0.48130	9.97754	73	24
20	9.49646	23	9.51895	25	0.48105	9.97751	72 71	I 2.4
30		23		26		9.97749	70	2 4.8
	9.49692	23	9.51946	25	0.48054	9.97746	1	3 7.2
31	9.49715	23	9.51971	26	0.48029	9.97744	69 68	4 9.6
32 33	9.49738 9.49761	23	9.51997 9.52022	25	0.48003	9.97741 9.97739	67	5 12.0 6 14.4
	9.49783	22		25		9.97736	66	6 14.4 7 16.8
34 35	9.49783	23	9.52047 9.52073	26	0.47953	9.97730	65	8 19.2
36	9.49829	23	9.52073	25	0.47927	9.97731 9.97731	64	9 21.6
37	9.49852	23	9.52124	26	0.47876	9.97729	63	
38	9.49875	23	9.52124	25	0.47851	9.97726	62	1
39	9.49898	23	9.52174	25 26	0.47826	9.97723	61	23
40	9.49920	22	9.52200	}	0.47800	9.97721	60	I 2.3
41	9.49943	23	9.52225	25	0.47775	9.97718	59	2 4.6
42	9.49966	23	9.52250	25	0.47750	9.97716	58	3 6.9
43	9.49989	23 22	9.52275	25 26	0.47725	9.97713	57	4 9.2
44	9.50011		9.52301		0.47699	9.97711	56	5 II.5 6 I3.8
45	9.50034	23	9.52326	25 25	0.47674	9.97708	55	7 16.1
46	9.50057	23	9.52351	25	0.47649	9.97706	54	8 18.4
47	9.50080	23	9.52376	26	0.47624	9.97703	53	9 20.7
48	9.50102	23	9.52402	25	0.47598	9.97701	52	
49	9.50125	23	9.52427	25	0.47573	9.97698	51	
50	9.50148		9.52452		0.47548	9.97696	50	
	Cos	d.	Cot	d. c.	Tan	Sin	1	P. P.

	0:	,	· /	-	0 .			
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.50148	22	9.52452	25	0.47548	9.97696	50	
51	9.50170	23	9.52477	25	0.47523	9.97693	49	
52	9.50193	23	9.52502	26	0.47498	9.97691	48	
53	9.50216	22	9.52528	25	0.47472	9.97688	47	25
54	9.50238	23	9.52553	25	0.47447	9.97686	46	1 2.5
55	9.50261	22	9.52578	25	0.47422	9.97683	45	2 5.0
56	9.50283	23	9.52603	25	0.47397	9.97680	44	3 7.5
57	9.50306	22	9.52628	25	0.47372	9.97678	43	4 10.0
58	9.50328	23	9.52653	25	0.47347	9.97675	42	5 12.5 6 15.0
59	9.50351	23	9.52678	25	0.47322	9.97673	41	7 17.5
60	9.50374	22	9.52703	25	0.47297	9.97670	40	8 20.0
61	9.50396	23	9.52728	25	0.47272	9.97668	39	9 22.5
62	9.50419	22	9.52753	25	0.47247	9.97665	38	
63	9.50441	23	9.52778	26	0.47222	9.97663	37	10
64	9.50464	22	9.52804	25	0.47196	9.97660	36	
65	9.50486	22	9.52829	25	0.47171	9.97657	35	24
66	9.50508	23	9.52854	25	0.47146	9.97655	34	I 2.4
67	9.50531	22	9.52879	25	0.47121	9.97652	33	2 4.8
68	9.50553	23	9.52904	25	0.47096	9.97650	32	3 7.2
69	9.50576	22	9.52929	24	0.47071	9.97647	31	4 9.6
70	9.50598	22	9.52953	25	0.47047	9.97645	30	5 12.0 6 14.4
71	9.50620	23	9.52978	25	0.47022	9.97642	29	7 16.8
72	9.50643	23	9.53003	25	0.46997	9.97640	28	8 19.2
73	9.50665	23	9.53028	25	0.46972	9.97637	27	9 21.6
74	9.50688	22	9.53053	25	0.46947	9.97634	26	
75	9.50710	22	9.53078	25	0.46922	9.97632	25	
76	9.50732	23	9.53103	25	0.46897	9.97629	24	
77	9.50755	22	9.53128	25	0.46872	9.97627	23	23
78	9.50777	22	9.53153	25	0.46847	9.97624	22	I 2.3
79	9.50799	22	9.53178	24	0.46822	9.97621	21	2 4.6
80	9.50821	23	9.53202	25	0.46798	9.97619	20	3 6.9
81	9.50844	22	9.53227	-	0.46773	9.97616	19	4 9.2
82	9.50866	22	9.53252	25 25	0.46748	9.97614	18	5 II.5 6 I3.8
83	9.50888	22	9.53277	25	0.46723	9.97611	17	7 16.1
84	9.50910		9.53302	25	0.46698	9.97609	16	8 18.4
85	9.50933	23 22	9.53327	24	0.46673	9.97606	15	9 20.7
86	9.50955	22	9.53351	25	0.46649	9.97603	14	
87	9.50977	22	9.53376	25	0.46624	9.97601	13	
88	9.50999	22	9.53401	25	0.46599	9.97598	12	
89	9.51021	22	9.53426	24	0.46574	9.97596	11	22
90	9.51043	23	9.53450	25	0.46550	9.97593	10	I 2.2
91	9.51066	23	9.53475	-	0.46525	9.97590	09	2 4.4
92	9.51088	22	9.53500	25 25	0.46500	9.97588	08	3 6.6
93	9.51110	22	9.53525	24	0.46475	9.97585	07	4 8.8 5 11.0
94	9.51132	22	9.53549	25	0.46451	9.97583	06	6 13.2
95	9.51154	22	9.53574	25	0.46426	9.97580	05	7 15.4
96	9.51176	22	9.53599	24	0.46401	9.97577	04	8 17.6
97	9.51198	22	9.53623	25	0.46377	9.97575	03	9 19.8
98	9.51220	22	9.53648	25	0.46352	9.97572	02	
99	9.51242	22	9.53673	24	0.46327	9.97570	OI	
100	9.51264		9.53697		0.46303	9.97567	00	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

19,							100	
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
00	9.51264	22	9.53697	25	0.46303	9.97567	100	
01	9.51286	22	9.53722	24	0.46278	9.97564	99	
02	9.51308	22	9.53746	25	0.46254	9.97562	98	25
03	9.51330	22	9.53771	25	0.46229	9-97559	97	
04	9.51352	22	9.53796	24	0.46204	9.97557	96	1 2.5
05	9.51374	22	9.53820	25	0.46180	9.97554	95	2 5.0 3 7.5
06	9.51396	22	9.53845	24	0.46155	9.97551	94	3 7.5 4 10.0
07	9.51418	22	9. 5 3869	25	0.46131	9.97549	93	5 12.5
о8	9.51440	22	9.53894	24	0.46106	9.97546	92	6 15.0
09	9.51462	22	9.53918	25	0.46082	9.97543	91	7 17.5
10	9.51484	22	9.53943	24	0.46057	9.97541	90	8 20.0
11	9.51506	21	9.53967	25	0.46033	9.97538	89	9 22.5
12	9.51527	22	9 53992	2.1	0.46008	9.97536	88	
13	9.51549	22	9.54016	25	0.45984	9.97533	87	24
14	9.51571	22	9.54041	24	0.45959	9.97530	86	
15	9.51593	22	9.54065	25	0.45935	9.97528	85	I 2.4 2 4.8
16	9.51615	22	9.54090	24	0.45910	9.97525	84	3 7.2
17	9.51637	21	9.54114	25	0.45886	9.97522	83	4 9.6
18	9.51658	22	9.54139	24	0.45861	9.97520	82	5 12.0
19	9.51680	22	9.54163	24	0.45837	9.97517	81	6 14.4
20	9.51702	22	9.54187	25	0.45813	9.97515	80	7 16.8
21	9.51724	21	9.54212	24	0.45788	9.97512	79	8 19.2
22	9.51745	22	9.54236	25	0.45764	9.97509	78	9 21.6
23	9.51767	22	9.54261	24	0.45739	9.97507	77	
24	9.51789	22	9.54285	24	0.45715	9.97504	76	
25	9.51811	21	9.54309	25	0.45691	9.97501	75	
26	9.51832	22	9.54334	24	0.45666	9.97499	74	
27	9.51854	22	9.54358	24	0.45642	9.97496	73	22
28	9.51876	21	9.54382	25	0.45618	9.97493	72	I 2.2
29	9.51897	22	9.54407	24	0.45593	9.97491	71	2 4.4
30	9.51919	22	9.54431	24	0.45569	9.97488	70	3 6.6
31	9.51941	21	9.54455	25	0.45545	9.97485	69	4 8.8
32	9.51962	22	9.54480	24	0.45520	9.97483	68	5 11.0
33	9.51984	22	9.54504	24	0.45496	9.97480	67	6 13.2
34	9.52006	21	9.54528	24	0.45472	9.97477	66	7 15.4 8 17.6
35	9.52027	22	9.54552	25	0.45448	9.97475	65	9 19.8
36	9.52049	21	9 54577	24	0.45423	9.97472	64	31-3
37	9.52070	22	9.54601	24	0.45399	9.97469	63	
38	9.52092	21	9.54625	24	0.45375	9.97467	62 61	21
39	9.52113	22	9.54649	24	0.45351	9.97464	60	I 2.I
40	9.52135	21	9.54673	25	0.45327	9.97461		2 4.2
41	9.52156	22	9.54698	24	0.45302	9.97459	59	3 6.3
42	9.52178	21	9.54722	24	0.45278	9.97456	58	4 8.4
43	9.52199	22	9.54746	24	0.45254	9.97453	57	5 10.5
44	9.52221	21	9.54770	24	0.45230	9.97451	56	6 12.6
45	9.52242	22	9.54794	24	0.45206	9.97448	55 54	7 14.7
46	9.52264	21	9.54818	25	0.45182	9.97445		8 16.8
47	9.52285	22	9.54843	24	0.45157	9.97443	53	9 18.9
48	9.52307 9.52328	21	9.54867	24	0.45133	9.97440	52 51	
49		22	9.54891	2.1		9.97437	50	
50	9.52350		9.54915		0.45085	9.97435	- 50	
	Cos	d.	Cot	d. c.	Tan	Sin	<u>. </u>	P. P.

19							100	3.0
	Sin	d.	Tan	d. c.	Cot	Cos		P. P.
50	9.52350	21	9.54915	24	0.45085	9.97435	50	
51	9.52371	21	9.54939	24	0.45061	9.97432	49	
52	9.52392	22	9.54963	24	0.45037	9.97429	48	24
53	9.52414	21	9.54987	24	0.45013	9.97427	47	===
54	9.52435	21	9.55011	24	0.44989	9.97424	46	I 2.4
55	9.52456	22	9.55035	24	0.44965	9.97421	45	2 4.8 3 7.2
56	9.52478	21	9.55059	24	0.44941	9.97419	44	4 9.6
57	9.52499	21	9.55083	2.1	0.44917	9.97416	43	5 12.0
58	9.52520	22	9.55107	24	0.44893	9.97413	42	6 14.4
59	9.52542	21	9.55131	24	0.44869	9.97410	41	7 16.8
60	9.52563	21	9.55155	24	0.44845	9.97408	40	8 19.2
61	9.52584	22	9.55179	24	0.44821	9.97405	39	9 21.6
62	9.52606	21	9.55203	24	0.44797	9.97402	38	
63	9.52627	21	9.55227	24	0.44773	9.97400	37	23
64	9.52648	21	9.55251	2.1	0.44749	9.97397	36	
65	9.52669	21	9.55275	24	0.44725	9.97394	35	I 2.3 2 4.6
66	9.52690	22	9.55299	24	0.44701	9.97392	34	3 6.9
67	9.52712	21	9.55323	24	0.44677	9.97389	33	4 9.2
68	9.52733	21	9.55347	24	0.44653	9.97386	32	5 11.5
69	9.52754	21	9.55371	24	0.44629	9.97383	31	6 13.8
70	9.52775	21	9.55395	23	0.44605	9.97381	30	7 16.1
71	9.52796	22	9.55418	24	0.44582	9.97378	29	8 18.4
72	9.52818	21	9.55442	2.4	0.44558	9.97375	28	9 20.7
73	9.52839	21	9.55466	2.1	0.44534	9.97373	27	
74	9.52860	21	9.55490	2.1	0.44510	9.97370	26	
75	9.52881	21	9.55514	24	0.44486	9.97367	25	
76	9.52902	21	9.55538	24	0.44462	9.97364	24	
77	9.52923	21	9.55562	23	0.44438	9.97362	23	21
78	9.52944	21	9.55585	24	0.44415	9.97359	22	I 2.I
79	9.52965	21	9.55609	24	0.44391	9.97356	21	2 4.2
80	9.52986	21	9.55633	24	0.44367	9.97353	20	3 6.3
18	9.53007	21	9.55657	23	0.44343	9.97351	19	4 8.4
82	9.53028	21	9.55680	24	0.44320	9.97348	18	5 10.5
83	9.53049	22	9.55704	24	0.44296	9.97345	17	6 12.6
84	9.53071	21	9.55728	2.1	0.44272	9.97343	16	7 14.7 8 16.8
85	9.53092	20	9.55752	23	0.44248	9.97340	15	9 18.9
86	9.53112	21	9.55775	24	0.44225	9.97337	14	9 1 10.9
87	9.53133	21	9.55799	24	0.44201	9.97334	13	
88	9.53154	21	9.55823	24	0.44177	9.97332	12 11	20
89	9.53175	21	9.55847	23		9.97329	10	I , 2.0
90	9.53196	21	9.55870	24	0.44130	9.97326		2 4.0
91	9.53217	21	9.55894	24	0.44106	9.97323	09 08	3 6.0
92	9.53238	21	9.55918	23	0.44082	9.97321	08	4 8.0
93	9.53259	21	9.55941	24	0.44059	9.97318		5 10.0
94	9.53280	21	9.55965	24	0.44035	9.97315	06 05	6 12.0
95 96	9.5330I 9.53322	21	9.55989 9.56012	23	0.44011	9.97312 9.97310	05	7 14.0
		21		24				8 16.0 9 18.0
9 7 9 8	9·53343 9·53363	20	9.56036 9.56059	23	0.43964	9.97307	03 02	9 18.0
99	9.53303	21	9.56083	24	0.43941	9.97304 9.97301	01	
100	9.53405	21		24	0.43893		00	
100			9.56107	4 -		9.97299		P. P.
1000	Cos	d.	Cot	d. c.	Tan	Sin	700	r.r.

20°							109	
	Sin	d	Tan	d. c.	Cot	Cos		Р. Р.
00	9.53405	21	9.56107	23	0.43893	9.97299	100	
01	9.53426	21	9.56130	24	0.43870	9.97296	99	
02	9.53447	21	9.56154	23	0.43846	9.97293	98	24
03	9.53468	20	9.56177	24	0.43823	9.97290	97	
04	9.53488	21	9.56201	23	0.43799	9.97288	96	I 2.4
05	9.53509	21	9.56224	24	0.43776	9.97285	95	2 4.8 3 7.2
06	9.53530	21	9.56248	23	0.43752	9.97282	94	3 7.2 4 9.6
07	9.53551	20	9.56271	24	0.43729	9.97279	93	5 12.0
о8	9.53571	21	9.56295	23	0.43705	9.97276	92	6 14.4
09	9.53592	21	9.56318	24	0.43682	9.97274	91	7 16.8
10	9.53613	21	9.56342	23	0.43658	9.97271	90	8 19.2
11	9.53634	20	9.56365	24	0.43635	9.97268	89	9 21.6
12	9.53654	21	9.56389	23	0.43611	9.97265	88	
13	9.53675	21	9.56412	24	0.43588	9.97263	87	23
14	9.53696	20	9.56436	23	0.43564	9.97260	86	
15	9.53716	21	9.56459	24	0.43541	9.97257	85	1 2.3
16	9.53737	21	9.56483	23	0.43517	9.97254	84	2 4.6 3 6.9
17	9.53758	20	9.56506	24	0.43494	9.97251	83	4 9.2
18	9.53778	21	9.56530	23	0.43470	9.97249	82 81	5 11.5
19	9.53799	20	9.56553	23	0.43447	9.97246		6 13.8
20	9.53819	21	9.56576	24	0.43424	9.97243	80	7 16.1
21	9.53840	21	9.56600	23	0.43400	9.97240	79	8 18.4
22	9.53861	20	9.56623	23	0.43377	9.97238	78	9 20.7
23	9.53881	21	9.56646	24	0.43354	9.97235	77	
24	9.53902	20	9.56670	23	0.43330	9.97232	76	
25 26	9.53922	21	9.56693 9.56716	23	0.43307	9.97229	75 74	
	9 53943	20		24	0.43284	9.97226		
27 28	9.53963 9.53984	21	9.56740 9.56763	23	0.43260	9.97224 9.97221	73 72	21
26 29	9.53964	20	9.56786	23	0.43237	9.97221	71	I 2.I
30	9.54025	21	9.56810	24	0.43190	9.97215	70	2 4.2
		20		23			69	3 6.3
31	9.54045 9.54066	21	9.56833 9.56856	23	0.43167	9.97212 9.97210	68	4 8.4
32 33	9.54086	20	9.56880	24	0.43144	9.97210	67	5 10.5 6 12.6
	9.54107	21	9.56903	23	0.43097	9.97204	66	7 14.7
34 35	9.54107	20	9.56926	23	0.43097	9.97201	65	8 16.8
36	9.54148	21	9.56949	23	0.43051	9.97198	64	9 18.9
37	9.54168	20	9.56973	24	0.43027	9.97195	63	
38	9.54188	20	9.56996	23	0.43004	9.97193	62	
39	9.54209	2I 20	9.57019	23 23	0.42981	9.97190	61	20
40	9.54229	20	9.57042	23	0.42958	9.97187	60	I 2.0
41	9.54250		9.57065		0.42935	9.97184	59	2 4.0
42	9.54270	20 20	9.57089	24 23	0.42911	9.97181	58	3 6.0
43	9.54290	20	9.57112	23	0.42888	9.97179	57	4 8.0 5 10.0
44	9.54311	20	9.57135	23	0.42865	9.97176	56	6 12.0
45	9.54331	20	9.57158	23	0.42842	9.97173	55	7 14.0
46	9.54351	21	9.57181	23	0.42819	9.97170	54	8 16.0
47	9.54372	20	9.57204	24	0.42796	9.97167	53	9 18.0
48	9.54392	20	9.57228	23	0.42772	9.97164	52	
49	9.54412	21	9.57251	23	0.42749	9.97162	51	
50	9 - 54433		9.57274		0.42726	9.97159	50	
	Cos	d.	Cot	d. c.	Tan	Sin		P. P.

20							103	
	Sin	d.	Tan	d.c.	Cot	Cos		P. P.
50	9.54433	20	9.57274	23	0.42726	9.97159	50	
51	9.54453	20	9.57297	23	0.42703	9.97156	49	
52	9.54473	20	9.57320	23	0.42680	9.97153	48	
53	9.54493	21	9 - 57343	23	0.42657	9.97150	47	23
54	9.54514	20	9.57366	23	0.42634	9.97147	46	I 2.3
55	9.54534	20	9.57389	23	0.42611	9.97145	45	2 4.6
56	9 - 54554	20	9.57412	23	0.42588	9.97142	44	3 6.9
57	9.54574		9.57435		0.42565	9.97139	43	4 9.2
58	9.54594	20 2I	9.57458	23	0.42542	9.97136	42	5 II.5 6 I3.8
59	9.54615	20	9.57481	23 23	0.42519	9.97133	41	6 13.8 7 16.1
60	9.54635		9.57504		0.42496	9.97130	40	8 18.4
61	9.54655	20	9.57527	23	0.42473	9.97127	39	9 20.7
62	9.54675	20	9.57550	23	0.42473	9.97127	38	3 1 = 5.7
63	9.54695	20	9.57573	23	0.42427	9.97122	37	
64	9.54715	20	9.57596	23	0.42404	9.97119	36	22
65	9.54715	20		23	0.42381	9.97119	-	I 2.2
66		21	9.57619	23			35	2 4.4
	9.54756	20	9.57612	23	0.42358	9.97113	34	3 6.6
67	9.54776	20	9.57665	23	0.42335	9.97110	33	4 8.8
68	9.54796	20	9.57688	23	0.42312	9.97108	32	5 11.0
69	9.54816	20	9.57711	23	0.42289	9.97105	31	6 13.2
70	9.54836	20	9 57734	23	0.42266	9.97102	30	7 15.4
71	9.54856	20	9.57757	23	0.42243	9.97099	29	8 17.6
72	9.54876	20	9.57780	23	0.42220	9.97096	28	9 19.8
73	9.54896	20	9.57803	23	0.42197	9.97093	27	
74	9.54916	20	9.57826	23	0.42174	9.97090	26	
75	9.54936	20	9.57849	23	0.42151	9.97087	25	
76	9.54956	20	9.57871	23	0.42129	9.97085	24	
77	9.54976	20	9.57894	- 1	0.42106	9.97082	23	20
78	9.54996	20	9.57917	23	0.42083	9.97079	22	
79	9.55016	20	9.57940	23	0.42060	9.97076	21	I 2.0
80	9.55036	20	9.57963	23	0.42037	9.97073	20	2 4.0 3 6.0
81	9.55056		9.57986	23	0.42014	9.97070	19	3 6.0 4 8.0
82	9.55076	20	9.58009	23	0.41991	9.97067	18	5 10.0
83	9.55096	20	9.58031	22	0.41969	9.97064	17	6 12.0
84	9.55116	}	9.58054	23	0.41946	9.97062	16	7 14.0
85	9.55136	20	9.58077	23	0.41940	9.97059	15	8 16.0
86	9.55155	19	9.58100	23	0.41923	9.97056	14	9 18.0
87	9.55175	20	9.58122	22	0.41878	9.97053	13	
88	9.551/5	20	9.58122	23	0.41878	9.97050	13	
89	9.55215	20	9.58168	23	0.41832	9.97047	11	19
90	9.55235	20	9.58191	23	0.41809	9.97044	10	1 1.9
91	9.55255	20	9.58213	22	0.41787	9.97041	09	2 3.8
92		20	9.58236	23	0.41764	9.97038	08	3 5.7
93	9.55275 9.55294	19	9.58259	23	0.41704	9.97036	07	4 7.6
	1	20	9.58282	23		•	06	5 9.5
94	9.55314	20		22	0.41718	9.97033	1	6 11.4
95 96	9.55334	20	9.58304 9.58327	23	0.41673	9.97030	05 04	7 13.3
	9.55354	20		23				8 15.2
97	9.55374	19	9.58350	22	0.41650	9.97024	03	9 17.1
98	9.55393	20	9.58372	23	0.41628	9.97021	02 01	
99	9.55413	20	9.58395	23		9.97018	4	
100	9 . 55433		9.58418		0.41582	9.97015	00	
	Cos	d.	Cot	d.c.	Tan	Sin	<u> </u>	P. P.

21								100	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
00	9.55433	20	9.58418	22	0.41582	9.97015	3	100	
10	9.55453		9.58440	- 1	0.41560	9.97012		99	23
02	9.55472	19 20	9.58463	23 23	0.41537	9.97009	3	98	I 2.3
03	9.55492	20	9.58486	23	0.41514	9.97006	2	97	2 4.6
04	9.55512		9.58508	23	0.41492	9.97004		96	3 6.9
05	9.55532	20	9.58531	23	0.41469	9.97001	3	95	4 9.2
06	9.55551	19 20	9.58554	23	0.41446	9.96998	3	94	5 11.5 6 13.8
07	9.55571		9.58576		0.41424	9.96995		93	7 16.1
o8	9.55591	20 19	9.58599	23 22	0.41401	9.96992	3 3	92	
09	9.55610	20	9.58621	23	0.41379	9.96989	3	91	9 20.7
10	9.55630	20	9.58644	22	0.41356	9.96986	3	90	
11	9.55650		9.58666		0.41334	9.96983		89	22
12	9.55669	19 20	9.58689	23	0.41311	9.96980	3	88	I 2.2
13	9.55689	19	9.58712	23 22	0.41288	9.96977	3	87	2 4.4 3 6.6
14	9.55708		9.58734		0.41266	9.96974		86	4 8.8
15	9.55728	20 20	9.58757	23 22	0.41243	9.96971	3	85	5 11.0
16	9.55748	19	9.58779	23	0.41221	9.96968	3	84	
17	9.55767	1 -	9.58802		0.41198	9.96965	2	83	7 15.4 8 17.6
18	9.55787	20 19	9.58824	22 23	0.41176	.9.96963	3	82	9 19.8
19	9.55806	20	9.58847	23	0.41153	9.96960	3	81	
20	9.55826	19	9.58869	23	0.41131	9.96957	3	80	
21	9.55845	1	9.58892	1	0.41108	9.96954	1	79	20
22	9.55865	20	9.58914	22	0.41086	9.96951	3	78	1 2.0
23	9.55884	19	9.58937	23 22	0.41063	9.96948	3	77	2 4.0
24	9.55904		9.58959	1	0.41041	9.96945	1	76	3 6.0
25	9 55923	19	9.58981	22	0.41019	9.96942	3	75	4 8.0 5 10.0
26	9.55943	20 19	9.59004	23 22	0.40996	9.96939	3	74	5 10.0 6 12.0
27	9.55962	1 -	9.59026		0.40974	9.96936	3	73	7 14.0 8 16.0
28	9.55982	20 19	9.59049	23 22	0.40951	9.96933	3	72	8 16.0 9 18.0
29	9.56001	20	9.59071	23	0.40929	9.96930	3	71	9 10.0
30	9.56021	19	9.59094	22	0.40906	9.96927	3	70	40
31	9.56040		9.59116	1	0.40884	9.96924	1	69	19
32	9.56060	20	9.59138	22	0.40862	9.96921	3	68	1 1.9 2 3.8
33	9.56079	19	9.59161	23 22	0.40839	9.96918	3	67	3 5.7
34	9.56098	19	9.59183	1	0.40817	9.96915	1	66	4 7.6
35	9.56118	20	9.59205	22	0.40795	9.96912	3	65	5 9.5 6 11.4
36	9.56137	19	9.59228	23	0.40772	9.96909	3	64	6 11.4
37	9.56157	1	9.59250	22	0.40750	9.96906	2	63	8 15.2
38	9.56176	19	9.59272	23	0.40728	9.96904	3	62	9 17.1
39	9.56195	20	9.59295	23	0.40705	9.96901	3	61	
40	9.56215	19	9.59317	22	0.40683	9.96898	3	60	
41	9.56234	1	9.59339	1	0.40661	9.96895	1	59	3
42	9.56253	19	9.59362	23	0.40638	9.96892	3	58	1 0.3
43	9.56273	19	9.59384	22	0.40616	9.96889	3	57	2 0.6
44	9.56292	1 -	9.59406	1	0.40594	9.96886	3	56	3 0.9 4 1.2
45	9.56311	19	9.59429	23	0.40571	9.96883	3	55	
46	9.56330	20	9.59451	22	0.40549	9.96880	3	54	
47	9.56350	19	9.59473	22	0.40527	9.96877	3	53	7 2.I 8 2.4
48	9.56369	19	9.59495	23	0.40505	9.96874	3	52	9 2.4
49	9.56388	- 20	9.59518	- 22	0.40482	9.96871	3	51	1 ' '
50	9.56408		9 - 59540		0.40460	9.96868		50	
	Cos	d.	Cot	d.c.	Tan	Sin	d.		P. P.

21°								158°	•
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.56408	19	9.59540	22	0.40460	9.96868		50	
51	9.56427		9.59562	22	0.40438	9.96865	3	49	22
52	9.56446	19	9.59584	22	0.40416	9.96862	3	48	I 2.2
53	9.56465	19	9.59606	23	0.40394	9.96859	3	47	2 4.4
54	9.56484	20	9.59629	22	0.40371	9.96856	3	46	3 6.6 4 8.8
55	9.56504	19	9.59651	22	0.40349	9.96853	3	45	
56	9.56523	19	9.59673	22	0.40327	9.96850	3	44	6 13.2
57 58	9.56542 9.56561	19	9.59695 9.59717	22	0.40305	9.96847 9.96844	3	43 42	7 I5.4 8 I7.6
59	9.56580	19	9.59717	22	0.40261	9.96841	3	41	9 19.8
60	9.56599	19	9.59762	23	0.40238	9.96838	3	40	
61	9.56619	20	9.59784	22	0.40216	9.96835	3	39	21
62	9.56638	19	9.59806	22	0.40194	9.96832	3	38	I 2.I
63	9.56657	19	9.59828	22	0.40172	9.96829	3	37	2 4.2
64	9.56676	19	9.59850	22	0.40150	9.96826	3	36	3 6.3 4 8.4
65	9.56695	19	9.59872	22 22	0.40128	9.96823	3	35	5 10.5
66	9.56714	19 19	9.59894	22	0.40106	9.96820	3	34	6 12.6
67	9.56733	19	9.59916	23	0.40084	9.96817	3	33	7 14.7 8 16.8
68	9.56752	19	9.59939	22	0.40061	9.96814	3	32	9 18.9
69	9.56771	19	9.59961	22	0.40039	9.96811	3	31	
70	9.56790	19	9.59983	22	0.40017	9.96808	3	30	
71	9.56809	20	9.60005	22	0.39995	9.96805	3	29	19
72	9.56829 9.56848	19	9.60027	22	0.39973	9.96802	3	28 27	1 1.9 2 3.8
73		19	9.60049	22	0.39951	9.96799	3		2 3.8 3 5.7
74 75	9.56867 9.56886	19	9.60071	22	0.39929	9.96796 9.96793	3	26 25	4 7.6
76	9.56905	19	9.60115	22	0.39885	9.96790	3	24	5 9.5
77	9.56924	19	9.60137	22	0.39863	9.96787	3	23	6 II.4 7 I3.3
78	9.56943	19	9.60159	22	0.39841	9.96784	3	22	8 15.2
79	9.56961	18	9.60181	22 22	0.39819	9.96781	3	21	9 17.1
80	9.56980	19	9.60203	22	0.39797	9.96778	3	20	
81	9.56999		9.60225	22	0.39775	9.96774		19	18
82	9.57018	19 19	9.60247	22	0.39753	9.96771	3	18	I 1.8 2 3.6
83	9.57037	19	9.60269	22	0.39731	9.96768	3	17	3 5.4
84	9.57056	19	9.60291	22	0.39709	9.96765	3	16	4 7.2
85 86	9.57075	19	9.60313	22	0.39687	9.96762 9.96759	3	15 14	5 9.0 6 10.8
87	9.57094	19	9.60335	22	1	9.90759	3		7 12.6
88	9.57113 9.57132	19	9.60357 9.60379	22	0.39643	9.96750	3	13	8 t4.4 9 16.2
89	9.57151	19	9.60400	21	0.39600	9.96750	3	11	9, 10.4
90	9.57169	18	9.60422	22	0.39578	9.96747	3	10	
91	9.57188	19	9.60444	22	0.39556	9.96744	3	09	4
92	9.57207	19	9.60466	22	0.39534	9.96741	3	08	1 0.4
93	9.57226	19	9.60488	22 22	0.39512	9.96738	3	07	2 0.8
94	9.57245	- 1	9.60510	22	0.39490	9.96735		06	3 I.2 4 I.6
95	9.57264	19 18	9.60532	22	0.39468	9.96732	3	05	5 2.0
96	9.57282	19	9.60554	21	0.39446	9.96729	3	04	6 2.4
97	9.57301	19	9.60575	22	0.39425	9.96726	3	03	4 I.6 5 2.0 6 2.4 7 2.8 8 3.2
98	9.57320	19	9.60597	22	0.39403	9.96723 9.96720	3	02 01	9 3.6
99 100	9.57339	19	9.60619	22			3	00	
100	9.57358		9.60641		0.39359 T	9.96717	d.		P. P.
	Cos	d.	Cot	d. c.	Tan	Sin	a.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
-00	9.57358		9.60641		0.39359	9.96717		100	
OI	9.57376	18	9.60663	22	0.39337	9.96714	3	99	22
02	9.57395	19	9.60685	22	0.39315	9.96710	4	98	1 2.2
03	9.57414	19	9.60706	21	0.39294	9.96707	3	97	
04	9.57433	19	9.60728	22	0.39272	9.96704	3	96	3 6.6
05	9.57451	18	9.60750	22	0.39250	9.96701	3	95	4 8.8
06	9.57470	19 19	9.60772	22 22	0.39228	9.96698	3	94	5 II.0 6 I3.2
07	9.57489	18	9.60794	i /	0.39206	9.96695		93	7 15.4
о8	9.57507	18	9.60815	2I 22	0.39185	9.96692	3	92	8 17.6
09	9.57526	19	9.60837	22	0.39163	9.96689	3	91	9 19.8
10	9.57545	18	9.60859	22	0.39141	9.96686	3	90	
11	9.57563	19	9.60881		0.39119	9.96683		89	21
12	9.57582	19	9.60902	2I 22	0.39098	9.96680	3	88	I 2.I
13	9.57601	18	9.60924	22	0.39076	9.96677	3	87	2 4.2 3 6.3
14	9.57619	19	9.60946	21	0.39054	9.96674		86	4 8.4
15	9.57638	19	9.60967	21	0.39033	9.96670	4	85	5 10.5
16	9.57657	18	9.60989	22	0.39011	9.96667	3	84	6 12.6
17	9.57675	19	9.61011	22	0.38989	9.96664	3	83	7 14.7 8 16.8
18	9.57694	18	9.61033	21	0.38967	9.96661	3	82	9 18.9
19	9.57712	19	9.61054	22	0.38946	9.96658	3	81	
20	9.57731	18	9.61076	22	0.38924	9.96655	3	80	
2 I	9.57749	19	9.61098	21	0.38902	9.96652	3	79	19
22	9.57768	19	9.61119	22	0.38881	9.96649	3	78	I I.9 2 3.8
23	9.57787	18	9.61141	21	0.38859	9.96646	3	77	2 3.8
24	9.57805	19	9.61162	22	0.38838	9.96643	3	76	3 5.7 4 7.6
25	9.57824	18	9.61184	22	0.38816	9.96640	4	75	5 9.5
26	9.57842	19	9.61206	21	0.38794	9.96636	3	74	5 9.5 6 II.4
27	9.57861	18	9.61227	22	0.38773	9.96633	3	73	7 13.3 8 15.2
28	9.57879	19	9.61249	22	0.38751	9.96630	3	72	9 17.1
29	9.57898	18	9.61271	21	0.38729	9.96627	3	7 ¹	
30	9.57916	19	9.61292	22	0.38708	9.96624	3		18
31	9.57935	18	9.61314	21	0.38686	9.96621	3	69 68	1 1.8
32	9.57953	19	9.61335	22	0.38665	9.96618	3	67	2 3.6
33	9.57972	18	9.61357	21			3	66	3 5.4
34	9.57990	18	9.61378	22	0.38622	9.96612 9.96608	4	65	4 7.2 5 9.0
35 36	9.58008 9.58027	19	9.61400	22	0.38578	9.96605	3	64	6 10.8
	9.58027	18	-	21	0.38557	9.96602	3	63	7 12.6
37 38	9.58045	19	9.61443 9.61465	22	0.38557	9.96599	3	62	8 14.4 9 16.2
39	9.58082	18	9.61486	21	0.38514	9.96596	3	61	9 10.2
40	9.58101	19	9.61508	22	0.38492	9.96593	3	60	I
41	9.58119	18	9.61529	21	0.38471	9.96590	3	59	3
42	9.58137	18	9.61551	22	0.38449	9.96587	3	58	1 0.3
43	9.58156	19	9.61572	21	0.38428	9.96583	4	57	2 0.6
44	9.58174	18	9.61594	22	0.38406	9.96580	3	56	3 0.9
45	9.58192	18	9.61615	21	0.38385	9.96577	3	55	4 I.2 5 I.5
46	9.58211	19	9.61637	22	0.38363	9.96574	3	54	5 I.5 6 I.8
47	9.58229	18	9.61658	21	0.38342	9.96571	3	53	7 2.1
48	9.58247	18	9.61680	22	0.38320	9.96568	3	52	8 2.4 9 2.7
49	9.58266	19	9.61701	2I 2I	0.38299	9.96565	3	51	9 2.7
50	9.58284	10	9.61722	21	0.38278	9.96562	3	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.

								101	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.58284	18	9.61722		0.38278	9.96562		50	
51	9.58302		9.61744	22	0.38256	9.96558	4	49	22
52	9.58321	19 18	9.61765	21	0.38235	9.96555	3	48	I 2.2
53	9.58339	18	9.61787	22 21	0.38213	9.96552	3	47	2 4.4
54	9.58357		9.61808		0.38192	9.96549		46	3 6.6
55	9.58375	18	9.61830	22 2I	0.38170	9.96546	3	45	4 8.8
56	9.58394	19 18	9.61851	21	0.38149	9.96543	3	44	5 II.0 6 I3.2
57	9.58412	18	9.61872	22	0.38128	9.96540		43	7 15.4
58	9.58430	18	9.61894	22 2I	0.38106	9.96536	4 3	42	
59	9.58448	19	9.61915	21	0.38085	9.96533	3	41	9 19.8
60	9.58467	18	9.61936	22	0.38064	9.96530	3	40	
61	9.58485		9.61958		0.38042	9.96527		39	21
62	9.58503	18 18	9.61979	21	0.38021	9.96524	3	38	I ' 2.I
63	9.58521	18	9.62001	22 21	0.37999	9.96521	3 4	37	2 4.2 3 6.3
64	9.58539	18	9.62022	21	0.37978	9.96517		36	4 8.4
65	9.58557	18	9.62043	21	0.37957	9.96514	3	35	5 10.5
66	9.58576	18	9.62065	21	0.37935	9.96511	3	34	
67	9.58594	18	9.62086	21	0.37914	9.96508	3	33	7 14.7 8 16.8
68	9 58612	18	9.62107	21	0.37893	9.96505		32	9 18.9
69	9.58630	18	9.62128	22	0.37872	9.96502	3	31	
70	9.58648	18	9.62150	21	0.37850	9.96498	3	30	
71	9.58666	18	9.62171		0.37829	9.96495		29	18
72	9.58684	18	9.62192	2I 22	0.37808	9.96492	3	28	1 1.8
73	9.58702	19	9.62214	21	0.37786	9.96489	3	27	2 3.6
74	9.58721	18	9.62235	21	0.37765	9.96486	3	26	3 5.4 4 7.2
75	9.58739	18	9.62256	21	0.37744	9.96483	4	25	
76	9.58757	18	9.62277	22	0.37723	9.96479	3	24	6 10.8
77	9.58775	18	9.62299	21	0.37701	9.96476	3	23	7 12.6 8 14.4
78	9.58793	18	9.62320	21	0.37680	9.96473	3	22	9 16.2
79	9.58811	18	9.62341	21	0.37659	9.96470	3	21	
80	9.58829	18	9.62362	21	0.37638	9.96467	4	20	17
81	9.58847	18	9.62383	22	0.37617	9.96463	3	19	1 1.7
82	9.58865	18	9.62405	21	0.37595	9.96460	3	18	2 3.4
83	9.58883	18	9.62426	21	0.37574	9.96457	3	17	3 5.1
84	9.58901	18	9.62447	21	0.37553	9.96454	3	16	4 6.3 5 8.5
85	9.58919	18	9.62468	21	0.37532	9.96451	4	15	5 8.5 6 10.2
86	9 58937	18	9.62489	22	0.37511	9.96447	3	14	7 11.9
87	9.58955	18	9.62511	21	0.37489	9.96444	3	13	
88	9.58973	18	9.62532	21	0.37468	9.96441	3	12	9 15.3
89	9.58991	18	9.62553	21	0.37447	9.96438	3	II	
90	9.59009	18	9.62574	21	0.37426	9.96435	3	10	4
91	9.59027	18	9.62595	21	0.37405	9.96432	4	09	
92	9.59045	18	9.62616	21	0.37384	9.96428	3	08	I 0.4 2 0.8
93	9.59063	18	9.62637	22	0.37363	9.96425	3	07	3 1.2
94	9.59081	17	9.62659	21	0.37341	9.96422	3	06	4 1.6
95	9.59098	18	9.62680	21	0.37320	9.96419	4	05	5 2.0 6 2.4
96	9.59116	18	9.62701	21	0.37299	9.96415	3	04	7 2.8 8 3.2
97	9.59134	18	9.62722	21	0.37278	9.96412	3	03	
98	9.59152	18	9.62743	21	0.37257	9.96409	3	02	9 3.6
99	9.59170	18	9.62764	21	0.37236	9.96406	3	10	i .
100	9.59188		9.62785		0.37215	9.96403		00	
	Cos	d.	Cot	đ. c.	Tan	Sin	d.	1	P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.59188		9.62785		0.37215	9.96403		100	
00	9.59206	18	9.62806	21	0.37194	9.96399	4	99	
02	9.59223	17	9.62827	21	0.37173	9.96396	3	98	21
03	9.59241	18	9.62848	21	0.37152	9.96393	3	97	I 2.1 2 4.2
04	9.59259	18	9.62869	21	0.37131	9.96390	3	96	3 6.3
05	9.59239	18	9.62890	21	0.37110	9.96387	3	95	4 8.4
06	9.59295	18	9.62912	22	0.37088	9.96383	4	94	5 10.5 6 12.6
07	9.59313	18	9.62933	21	0.37067	9.96380	3	93	4 8.4 5 10.5 6 12.6 7 14.7 8 16.8
08	9.59330	17	9.62954	21	0.37046	9.96377	3	92	8 16.8
09	9.59348	18	9.62975	21	0.37025	9.96374	3	91	9 18.9
10	9.59366	18	9.62996	21	0.37004	9.96370	4	90	
11	9.59384	18	9.63017	21	0.36983	9.96367	3	89	20
12	9.59401	17	9.63038	21	0.36962	9.96364	3	88	I 2.0
13	9.59419	18 18	9.63059	2I 2I	0.36941	9.96361	3	87	2 4.0 3 6.0
14	9.59437		9.63080		0.36920	9.96357	4	86	4 8.0
15	9.59455	18	9.63101	21	0.36899	9.96354	3	85	5 10.0
16	9.59472	17 18	9.63121	20 21	0.36879	9.96351	3	84	
17	9.59490		9.63142	l	0.36858	9.96348		83	7 14.0 8 16.0
18	9.59508	18 18	9.63163	2I 2I	0.36837	9.96344	4	82	9 18.0
19	9.59526	17	9.63184	21	0.36816	9.96341	3	81	
20	9.59543	18	9.63205	21	0.36795	9.96338	3	80	1
21	9.59561	18	9.63226	l	0.36774	9.96335		79	18
22	9.59579		9.63247	21	0.36753	9.96331	4	78	1 1.8
23	9.59596	17 18	9.63268	2I 2I	0.36732	9.96328	3	77	2 3.6
24	9.59614		9.63289	1 .	0.36711	9.96325	3	76	3 5.4
25	9.59632	18	9.63310	2I 2I	0.36690	9.96322	3	75	4 7.2 5 9.0
26	9.59649	17 18	9.63331	21	0.36669	9.96318	4 3	74	6 10.8
27	9.59667		9.63352	1	0.36648	9.96315)	73	7 12.6 8 14.4
28	9.59684	17 18	9.63373	2I 20	0.36627	9.96312	3	72	8 14.4 9 16.2
29	9.59702	18	9.63393	21	0.36607	9.96309	4	7I	9 10.2
30	9.59720	17	9.63414	21	0.36586	9.96305	3	70	17
31	9.59737	18	9.63435	21	0.36565	9.96302		69	1
32	9.59755	17	9.63456	2I 2I	0.36544	9.96299	3	68	I 1.7 2 3.4
33	9.59772	18	9.63477	21	0.36523	9.96296	4	67	3 5.1
34	9.59790	18	9.63498	21	0.36502	9.96292	3	66	4 6.8
35	9.59808	17	9.63519	20	0.36481	9.96289	3	65	5 8.5 6 10.2
36	9.59825	18	9.63539	21	0.36461	9.96286	4	64	7 11.9
37	9.59843	17	9.63560	21	0.36440	9.96282	3	63	
38	9.59860	18	9.63581	21	0.36419	9.96279	3	62	9 15.3
39	9.59878	17	9.63602	21	0.36398	9.96276	3	61	
40	9.59895	18	9.63623	20	0.36377	9.96273	4	60	3
41	9.59913	17	9.63643	21	0.36357	9.96269	3	59	
42	9.59930	18	9.63664	21	0.36336	9.96266	3	58	I 0.3 2 0.6
43	9.59948	17	9.63685	21	0.36315	9.96263	3	57	3 0.9
44	9.59965	18	9.63706	20	0.36294	9.96260	4	56	4 1.2
45	9.59983	17	9.63726	21	0.36274	9.96256	3	55	5 I.5 6 I.8
46	9.60000	18	9.63747	21	0.36253	9.96253	3	54	7 2.1
47	9.60018	17	9.63768	21	0.36232	9.96250	4	53	8 2.4
48 49	9.60035 9.60053	18	9.63789 9.63809	20	0.36211	9.96246 9.96243	3	52	9 2.7
49 50		17		21			3	51 50	1
-00-	9.60070 Cos	d.	9.63830 Cot	d. c.	0.36170 Tan	9.96240 Sin	d.	100	P. P.
	Cos	a.	COT	a. c.	ı ıan	Sin	a.	1	P. P.

	Sin	1 1	Т- ::	4 -	Cit	Corr	.1		D D
		<u>d.</u>	Tan	d. c.	Cot	Cos	<u>d.</u>		P. P.
50	9.60070	17	9.63830	21	0.36170	9.96240	4	50	
51	9.60087	18	9.63851	21	0.36149	9.96236	3	49	21
52	9.60105	17	9.63872	20	0.36128	℃9.96233	3	48	I 2.I
53	9.60122	18	9.63892	21	0.36108	9.96230	3	47	2 4.2
54	9.60140	17	9.63913	21	0.36087	9.96227	4	46	3 6.3
55	9.60157	17	9.63934	20	0.36066	9.96223	3	45	4 8.4 5 10.5 6 12.6
56	9.60174	18	9.63954	21	0.36046	9.96220	3	44	5 10.5 6 12.6
57	9.60192	17	9.63975	21	0.36025	9.96217	4	43	7 14.7 8 16.8
58	9.60209	18	9.63996	20	0.36004	9.96213	3	42	8 16.8 9 18.9
59	9.60227	17	9.64016	21	0.35984	9.96210	3	41	9 10.9
60	9.60244	17	9.64037	21	0.35963	9.96207	4	40	
61	9.60261	18	9.64058	20	0.35942	9.96203		39	20
62	9.60279	17	9.64078	21	0.35922	9.96200	3	38	I 2.0
63	9.60296	17	9.64099	21	0.35901	9.96197	4	37	2 4.0 3 6.0
64	9.60313	18	9.64120	20	0.35880	9.96193		36	4 8.0
65	9.60331	17	9.64140	21	0.35860	9.96190	3	35	5 10.0
66	9.60348	17	9.64161	21	0.35839	9.96187	3	34	6 12.0
67	9.60365		9.64182	20	0.35818	9.96184	1	33	7 14.0 8 16.0
68	9.60382	17 18	9.64202	21	0.35798	9.96180	4	32	9 18.0
69	9.60400	17	9.64223	20	0.35777	9.96177	3	31	'
70	9.60417	1	9.64243	21	0.35757	9.96174	1	30	1
71	9.60434	17	9.64264	l	0.35736	9.96170	4	29	18
72	9.60451	17	9.64285	21	0.35715	9.96167	3	28	1 1.8
73	9.60469	18	9.64305	20	0.35695	9.96164	3	27	2 3.6
74	9.60486	17	9.64326	21	0.35674	9.96160	4	26	3 5.4
75	9.60503	17	9.64346	20	0.35654	9.96157	3	25	4 7.2 5 9.0
76	9.60520	17	9.64367	21	0.35633	9.96154	3	24	5 9.0 6 10.8
77	9.60538	18	9.64387	20	0.35613	9.96150	4	23	7 12.6
78	9.60555	17	9.64408	21	0.35592	9.96147	3	22	8 14.4
79	9.60572	17	9.64429	21	0.35571	9.96144	3	21	9 16.2
80	9.60589	17	9.64449	20	0.35551	9.96140	4	20	
81	9.60606	17	9.64470	21	0.35530	9.96137	3	19	17
82	9.60624	18	9.64490	20	0.35510	9.96134	3	18	I I.7
83	9.60641	17	9.64511	21	0.35489	9.96130	4	17	2 3.4
84	9.60658	17	9.64531	20	0.35469	9.96127	3	16	3 5.I 4 6.8
85	9.60675	17	9.64552	21	0.35448	9.96127	4	15	5 8.5
86	9.60692	17	9.64572	20	0.35428	9.96120	3	14	6 10.2
87	9.60709	17	9.64593	21	0.35407	9.96117	3	13	7 II.9 8 I3.6
88	9.60726	17	9.64613	20	0.35407	9.96117	4	13	9 15.3
89	9.60744	18	9.64634	21	0.35366	9.96110	3	111	
90	9.60761	17	9.64654	20	0.35346	9.96107	3	10	1
91		17		20			4		4
91 92	9.60778 9.60795	17	9.64674	21	0.35326	9.96103 9.96100	3	o9 o8	1 0.4
93	9.60795	17	9.64695 9.64715	20	0.35305	9.96097	3	07	2 0.8
		17		21			4	06	3 1.2
94 95	9.60829 9.60846	17	9.64736	20	0.35264	9.96093 9.96090	3		4 1.6 5 2.0 6 2.4
95 96	9.60863	17	9.64756	21	0.35244	9.96090	3	05 04	6 2.4
-		17	9.64777	20	1		4		7 2.8
97 98	9.60880	17	9.64797	21	0.35203	9 96083 9.96080	3	03	8 3.2
98 99	9.60897 9.60914	17	9.64818 9.64838	20	0.35182	9.96076	4	02 01	9 3.6
		17		20			3	1	
100	9.60931		9.64858		0.35142	9.96073		00	
	Cos	d.	Cot	d.c.	Tan	Sin	d.	i	P. P.

24								100	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.60931	17	9.64858	21	0.35142	9.96073	3	100	
01	9.60948		9.64879	20	0.35121	9.96070	-	99	21
02	9.60965	17 17	9.64899	20	0.35101	9.96066	4	98	I 2.I
03	9.60982	17	9.64919	21	0.35081	9.96063	3	97	
04	9.60999		9.64940		0.35060	9.96060		96	2 4.2 3 6.3
05	9.61016	17 17	9.64960	20 2I	0.35040	9.96056	4	95	4 8.4
о6	9.61033	17	9.64981	20	0.35019	9.96053	3	94	5 10.5 6 12.6
07	9.61050		9.65001		0.34999	9.96049		93	7 14.7 8 16.8
08	9.61067	17	9.65021	20 2I	0.34979	9.96046	3	92	
09	9.61084	17 17	9.65042	20	0.34958	9.96043	3	9r	9 18.9
10	9.61101		9.65062	20	0.34938	9.96039		90	
11	9.61118	17	9.65082		0.34918	9.96036	3	89	20
12	9.61135	17	9.65103	21	0.34897	9.96032	4	88	I 2.0
13	9.61152	17	9.65123	20	0.34877	9.96029	3	87	2 4.0 3 6.0
14	9.61169	17	9.65143	20	0.34857	9.96026	3	86	3 6.0 4 8.0
15	9.61186	17	9.65164	21	0.34836	9.96022	4	85	
16	9.61203	17	9.65184	20	0.34816	9.96019	3	84	6 12.0
17	9.61220	17	9.65204	20	0.34796	9.96015	4	83	7 14.0 8 16.0
18	9.61236	16	9.65224	20	0.34776	9.96012	3	82	9 18.0
19	9.61253	17	9.65245	21	0.34755	9.96009	3	81	9 10.0
20	9.61270	17	9.65265	20	0.34735	9.96005	4	80	1
	9.61287	17	9.65285	20	0.34715	9.96002	3	79	4
2I 22	9.61287	17	9.65306	21	0.34715	9.95998	4	78	17
23	9.61304	17	9.65326	20	0.34674	9.95995	3	77	1 I.7 2 3.4
•		17		20	0.34654	9.95992	3	76	
24	9.61338	16	9.65346	20	0.34634	9.95992	4	75	4 6.8
25 26	9.61354 9.61371	17	9.65366 9.65387	21	0.34613	9.95985	3	74	5 8.5
		17	-	20	1	4	4	1	
27 28	9.61388	17	9.65407	20	0.34593	9.95981	3	73 72	7 II.9 8 13.6
28 29	9.61405 9.61422	17	9.65427 9.65447	20	0.34573	9.95978 9.95974	4	71	9 15.3
		16		20			3	70	ļ
30	9.61438	17	9.65467	21	0.34533	9.95971	3		16
31	9.61455	17	9.65488	20	0.34512	9.95968	4	69	1 1.6
32	9.61472	17	9.65508	20	0.34492	9.95964	3	68	2 3.2
33	9.61489	17	9.65528	20	0.34472	9.95961	4	67	3 4.8
34	9.61506	16	9.65548	20	0.34452	9.95957	3	66	4 6.4 5 8.0
35	9.61522	17	9.65568	21	0.34432	9.95954	4	65 64	5 8.0 6 9.6
36	9.61539	17	9.65589	20	0.34411	9.95950	3		7 11.2
37	9.61556	17	9.65609	20	0.34391	9.95947	3	63	
38	9.61573	16	9.65629	20	0.34371	9.95944	4	62 61	9 14.4
39	9.61589	17	9.65649	20	0.34351	9.95940	3		1
40	9.61606	17	9.65669	20	0.34331	9.95937	4	60	
41	9.61623	16	9.65689	21	0.34311	9.95933	3	59	3
42	9.61639	17	9.65710	20	0.34290	9.95930	4	58	1 0.3
43	9.61656	17	9.65730	20	0.34270	9.95926	3	57	2 0.6
44	9.61673	16	9 65750	20	0.34250	9.95923	3	56	3 0.9 4 1.2
45	9.61689	17	9.65770	20	0.34230	9.95920	4	55	
46	9.61706	17	9.65790	20	0.34210	9 .95916	3	54	6 1.8
47	9.61723	16	9.65810	20	0.34190	9.95913	4	53	7 2.1 8 2.4
48	9.61739	17	9.65830	20	0.34170	9.95909	3	52	8 2.4 9 2.7
49	9.61756	17	9.65850	20	0.34150	9.95906	4	51] ,
50	9.61773		9.65870		0.34130	9.95902		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.

114° 65°

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.61773	16	9.65870	20	0.34130	9.95902	_	50	
51	9.61789	1	9.65890	1	0.34110	9.95899	3	49	20
52	9.61806	17	9.65911	2I 20	0.34089	9,95895	4	48	1 2.0
53	9.61823	16	9.65931	20	0.34069	9.95892	3	47	2 4.0
54	9.61839		9.65951	i	0.34049	9.95888	4	46	3 6.0
55	9.61856	17 16	9.65971	20	0.34029	9.95885	3	45	4 8.0
56	9.61872	17	9.65991	20	0.34009	9.95882	3	44	5 10.0 6 12.0
57	9.61889		9.66011	4	0.33989	9.95878	4	43	7 14.0
58	9.61906	17	9.66031	20	0.33969	9.95875	3	42	8 16.0
59	9.61922	16 17	9.66051	20 20	0.33949	9.95871	4	41	9 18.0
60	9.61939	16	9.66071	20	0.33929	9.95868	3	40	
61	9.61955		9.66091		0.33909	9.95864	4	39	19
62	9.61972	17 16	9.66111	20	0.33889	9.95861	3	38	I I.9
63	9.61988	17	9.66131	20 20	0.33869	9.95857	4	37	2 3.8
64	9.62005		9.66151	}	0.33849	9.95854	3	36	3 5·7 4 7.6
65	9.62021	16	9.66171	20	0.33829	9.95850	4	35	5 9.5
66	9.62038	17 16	9.66191	20 20	0.33809	9.95847	3	34	6 11.4
67	9.62054		9.66211		0.33789	9.95843	4	33	7 13.3 8 15.2
68	9.62071	17	9.66231	20	0.33769	9.95840	3	32	9 17.1
69	9.62087	16	9.66251	20	0.33749	9.95836	4	31	1 31-7
70	9.62104	17	9.66271	20	0.33729	9.95833	3	30	
71	9.62120	16	9.66291	, 20	0.33709	9.95829	4	29	17
72	9.62137	17	9.66311	20	0.33689	9.95826	3	28	L .
73	9.62153	16	9.66331	20	0.33669	9.95822	4	27	I I.7 2 3.4
74	9.62170	17	9.66351	20	0.33649	9.95819	3	26	
75	9.62186	16	9.66371	20	0.33629	9.95815	4	25	4 6.8
76	9.62203	17	9.66391	20	0.33609	9.95812	3	24	5 8.5 6 10.2
77	9.62219	16	9.66411	20	0.33589	9.95808	4	23	
78	9.62235	16	9.66430	19	0.33570	9.95805	3	22	8 13.6
79	9.62252	17	9.66450	20	0.33550	9.95801	4	21	9 15.3
80	9.62268	16	9.66470	20	0.33530	9.95798	3	20	
8r	9.62285	17	9.66490	20	0.33510	9.95794	4	19	16
82	9.62301	16	9.66510	20	0.33490	9.95791	3	18	1 1.6
83	9.62317	16	9.66530	20	0.33470	9.95787	4	17	2 3.2
84	9.62334	17	9.66550	20	0.33450	9.95784	3	16	3 4.8 4 6.4
85	9.62350	16	9.66570	20	0.33430	9.95780	4	15	5 8.0
86	9.62367	17	9.66590	20	0.33410	9.95777	3	14	6 9.6
87	9.62383	16	9.66609	19	0.33391	9.95773	4	13	7 II.2 8 I2.8
88	9.62399	16	9.66629	20	0.33371	9.95770	3	12	9 14.4
89	9.62416	17	9.66649	20	0.33351	9.95766	4	11	, ,
90	9.62432	16	9.66669	20	0.33331	9.95763	3	10	
91	9.62448	16	9.66689	20	0.33311	9.95759	4	09	4
92	9.62465	17	9.66709	20	0.33291	9.95756	3	08	1 0.4
93	9.62481	16	9.66729	20	0.33271	9.95752	4	07	2 0.8
94	9.62497	16	9.66748	19	0.33252	9.95749	3	06	3 1.2
95	9.62513	16	9.66768	20	0.33232	9.95745	4	05	4 1.6
96	9.62530	17	9.66788	20	0.33212	9.95742	3	04	5 2.0 6 2.4
97	9.62546	16	9.66808	20	0.33192	9.95738	4	03	
98	9.62562	16	9.66828	20	0.33192	9.95735	3	02	8 3.2
99	9.62579	17	9.66847	19	0.33153	9.95731	4	01	9 3.6
100	9.62595	16	9.66867	20	0.33133	9.95728	3	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

25								104	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
00	9.62595	16	9.66867	20	0.33133	9.95728	4	100	
OI	9.62611		9.66887		0.33113	9.95724	4	99	20
02	9.62627	16	9.66907	20 20	0.33093	9.95720	4	98	1 2.0
03	9.62644	17 16	9.66927	19	0.33073	9.95717	3	97	2 4.0
04	9.62660		9.66946		0.33054	9.95713		96	3 6.0
05	9.62676	16 16	9.66966	20 20	0.33034	9.95710	3	95	4 8.0
06	9.62692	16	9.66986	20	0.33014	9.95706	4	94	5 10.0 6 12.0
07	9.62708		9.67006		0.32994	9.95703	3	93	7 14.0
о8	9.62725	17 16	9.67025	19 20	0.32975	9.95699	4	92	8 16.0
09	9.62741	16	9.67045	20	0.32955	9.95696	3	91	9 18.0
10	9.62757	16	9.67065	20	0.32935	9.95692	1	90	
11	9.62773		9.67085		0.32915	9.95689	3	89	19
12	9.62789	16	9.67104	19	0.32896	9.95685	4	88	1 1.9
13	9.62806	17 16	9.67124	20 20	0.32876	9.95681	4	87	2 3.8
14	9.62822		9.67144		0.32856	9.95678	3	86	3 5.7 4 7.6
15	9.62838	16	9.67163	19	0.32837	9.95674	4	85	5 9.5
16	9.62854	16 16	9.67183	20 20	0.32817	9.95671	3	84	
17	9.62870		9.67203		0.32797	9.95667	4	83	7 13.3 8 15.2
18	9.62886	16	9.67223	20	0.32777	9.95664	3	82	9 17.1
19	9.62902	16 16	9.67242	19 20	0.32758	9.95660	4	81	
20	9.62918		9.67262		0.32738	9.95657	3	80	
21	9.62935	17	9.67282	20	0.32718	9.95653	4	79	17
22	9.62951	16	9.67301	19	0.32699	9.95649	4	78	1 1.7
23	9.62967	16	9.67321	20 20	0.32679	9.95646	3	77	2 3.4
24	9.62983	16	9.67341		0.32659	9.95642	4	76	3 5.1
25	9.62999	16	9.67360	19	0.32640	9.95639	3	75	4 6.8 5 8.5
26	9.63015	16 16	9.67380	20 19	0.32620	9.95635	4	74	5 8.5 6 10.2
27	9.63031		9.67399		0.32601	9.95632	3	73	7 11.9
28	9.63047	16	9.67419	20 20	0.32581	9.95628	4	72	8 13.6
29	9.63063	16 16	9.67439	19	0.32561	9.95624	4	71	9 15.3
30	9.63079	16	9.67458	20	0.32542	9.95621	3	70	
31	9.63095		9.67478	1	0.32522	9.95617	4	69	16
32	9.63111	16	9.67498	20	0.32502	9.95614	3	68	1 1.6
33	9.63127	16 16	9.67517	19 20	0.32483	9.95610	4	67	2 3.2
34	9.63143		9.67537	1	0.32463	9.95606	4	66	3 4.8 4 6.4 5 8.0 6 9.6
35	9.63159	16 16	9.67556	19 20	0.32444	9.95603	3	65	5 8.0
36	9.63175	16	9.67576	20	0.32424	9.95599	4	64	
37	9.63191		9.67596	ļ.	0.32404	9.95596	3	63	8 12.8
38	9.63207	16 16	9.67615	19	0.32385	9.95592	4	62	9 14.4
39	9.63223	16	9.67635	19	0.32365	9.95588	3	61	
40	9.63239	16	9.67654	20	0.32346	9.95585	l .	60	
41	9.63255		9.67674	!	0.32326	9.95581	4	59	3
42	9.63271	16 16	9.67693	19	0.32307	9.95578	3	58	1 0.3
43	9.63287	16	9.67713	19	0.32287	9.95574	4	57	2 0.6
44	9.63303	16	9.67732	20	0.32268	9.95570	ì	56	3 0.9 4 1.2
45	9.63319	16	9.67752	20	0.32248	9.95567	3 4	55	4 1.2 5 1.5
46	9.63335	16	9.67772	19	0.32228	9.95563	3	54	6 1.8
47	9.63351	16	9.67791	20	0.32209	9.95560	1	53	7 2.I 8 2.4
48	9.63367	16	9.67811	19	0.32189	9.95556	4	52	8 2.4 9 2.7
49	9.63383	15	9.67830	20	0.32170	9.95552	3	51	912.1
50	9.63398		9.67850		0.32150	9.95549		50	
	Cos	d.	Cot	d.c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.63398		9.67850	_	0.32150	9.95549		50	
51	9.63414	16	9.67869	19	0.32131	9.95545	4	49	
52	9.63430	16	9.67889	20	0.32111	9.95542	3	48	20
53	9.63446	16 16	9.67908	19	0.32092	9.95538	4	47	I 2.0 2 4.0
54	9.63462		9.67928	20	0.32072	9.95534	4	46	3 6.0
55	9.63478	16 16	9.67947	19	0.32053	9.95531	3	45	4 8.0
56	9.63494	16	9.67967	20 19	0.32033	9.95527	4	44	5 IO.0 6 I2.0
57	9.63510		9.67986	1 -	0.32014	9.95523	4	43	7 14.0
58	9.63525	15 16	9.68005	19 20	0.31995	9.95520	3	42	
59	9.63541	16	9.68025	19	0.31975	9.95516	4 3	41	9 18.0
60	9.63557	16	9.68044	20	0.31956	9.95513	4	40	
61	9.63573	16	9.68064	19	0.31936	9.95509		39	19
62	9.63589	15	9.68083	20	0.31917	9.95505	4	38	I I.9 2 3.8
63	9.63604	16	9.68103	19	0.31897	9.95502	4	37	3 5.7
64	9.63620	16	9.68122	20	0.31878	9.95498	4	36	4 7.6
65 66	9.63636	16	9.68142	19	0.31858	9.95494	3	35	4 7.6 5 9.5 6 11.4
	9.63652	16	9.68161	19	0.31839	9.95491	4	34	
67 68	9.63668 9.63683	15	9.68180 9.68200	20	0.31820	9.95487	4	33	8 15.2
69	9.63683	16	9.68219	19	0.31800	9.95483 9.95480	3	32 31	9 17.1
70	9.63715	16	9.68239	20	0.31761	9.95476	4	30	
		16		19			3		
71 72	9.63731 9.63746	15	9.68258 9.68277	19	0.31742	9.9 5 473 9.95469	4	29 28	16
73	9.63740	16	9.68277	20	0.31723	9.95465	4	27	1 1.6
74	9.63778	16	9.68316	19	0.31684	9.95462	3	26	2 3.2 3 4.8
75	9.63778	16	9.68336	20	0.31664	9.95458	4	25	4 6.4
76	9.63809	15	9.68355	19	0.31645	9.95454	4	24	5 8.0 6 9.6
77	9.63825	16	9.68374	19	0.31626	9.95451	3	23	6 9.6 7 11.2
78	9.63841	16	9.68394	20	0.31606	9.95447	4	22	7 II.2 8 I2.8
79	9.63856	15 16	9.68413	19	0.31587	9.95443	4	21	9 14.4
80	9.63872		9.68432	19	0.31568	9.95440	3	20	
81	9.63888	16	9.68452	20	0.31548	9.95436	4	19	15
82	9.63903	15	9.68471	19	0.31529	9.95432	4	18	1 1.5
83	9.63919	16 16	9.68490	19 20	0.31510	9.95429	3	17	2 3.0
84	9.63935		9.68510	1	0.31490	9.95425	4	16	3 4.5 4 6.0
85	9.63950	15 16	9.68529	19	0.31471	9.95421	4	15	5 7.5
86	9.63966	16	9.68548	19 20	0.31452	9.95418	3	14	6 9.0 7 10.5
87	9.63982	15	9.68568	19	0.31432	9.95414	4	13	7 IO.5 8 I2.0
88	9.63997	16	9.68587	19	0.31413	9.95410	3	12	9 13.5
89	9.64013	15	9.68606	20	0.31394	9.95407	4	II	
90	9.64028	16	9.68626	19	0.31374	9.95403	4	10	
91	9.64044	16	9.68645	19	0.31355	9.95399	3	09	4
92	9.64060	15.	9.68664 9.68683	19	0.31336	9.95396	4	08	I 0.4
93	9.64075	16		20	0.31317	9.95392	4	07	2 0.8 3 1.2
94	9.64091	15	9.68703 9.68722	19	0.31297	9.95388	4	06	3 I.2 4 I.6
95 96	9.64106 9.64122	16	9.68722	19	0.31278	9.95384 9.95381	3	05 04	5 2.0
	9.64122	16	9.68760	19	0.31239		4		
97 98	9.64138	15	9.68780	20	0.31240	9.95377 9.95373	4	03 02	7 2.8 8 3.2
99	9.64169	16	9.68799	19	0.31220	9.95369	4	01	9 3.6
100	9.64184	15	9.68818	19	0.31182	9.95366	3	00	
<u> </u>	Cos	d.	Cot	d. c.	Tan	Sin	d.	 	P. P.
		· u.	,	4. 0.	LGII	. 0111	u.		- 4.1.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.64184		9.68818		0.31182	9.95366	_	100	
oI.	9.64200	16	9.68837	19	0.31163	9.95362	4	99	
02	9.64215	15	9.68857	20	0.31143	9.95359	3	98	20
03	9.64231	16	9.68876	19	0.31124	9.95355	4	97	I 2.0 2 4.0
04	9.64246	15	9.68895	19	0.31105	9.95351	4	96	3 6.0
05	9.64262	16	9.68914	19	0.31086	9.95348	3	95	4 8.0
о6	9.64277	15 16	9.68934	20 19	0.31066	9.95344	4	94	4 8.0 5 10.0 6 12.0
07	9.64293	1	9.68953	1 -	0.31047	9.95340	1	93	7 14.0
о8	9.64308	15 16	9.68972	19	0.31028	9.95336	3	92	8 16.0
09	9.64324	15	9.68991	19	0.31009	9.95333	4	91	9 18.0
10	9.64339	16	9.69010	19	0.30990	9.95329	4	90	
11	9.64355	15	9.69029	20	0.30971	9.95325		89	19
12	9.64370	16	9.69049	19	0.30951	9.95322	3	88	1 1.9 3.8
13	9.64386	15	9.69068	19	0.30932	9.95318	4	87	3 5.7
14	9.64401	16	9.69087	19	0.30913	9.95314	4	86	4 7.6
15	9.64417	15	9.69106	19	0.30894	9.95310	3	85	5 9.5 6 11.4
16	9.64432	15	9.69125	19	0.30875	9.95307	4	84	7 13.3
17	9.64447	16	9.69144	20	0.30856	9.95303	4	83	8 15.2
18 19	9.64463 9.64478	15	9.69164 9.69183	19	0.30836	9.95299	4	82 81	9 17.1
20		16		19		9.95295	3	80	I
	9.64494	15	9.69202	19	0.30798	9.95292	4	1	i
21	9.64509	15	9.69221	19	0.30779	9.95288	4	79 78	16
22 23	9.64524 9.64540	16	9.69240 9.69259	19	0.30760	9.95284 9.95281	3	70	1 1.6
		15		19			4		2 3.2 3 4.8
24	9.64555 9.64571	16	9.69278 9.69298	20	0.30722	9.95277	4	76	4 6.4
25 26	9.64586	15	9.69298	19	0.30702	9.95273 9.95269	4	75 74	5 8.0
27	9.64601	15	9.69336	19	0.30664	9.95266	3	73	
28	9.64617	16	9.69355	19	0.30645	9.95262	4	72	7 II.2 8 I2.8
29	9.64632	15	9.69374	19	0.30626	9.95258	4	71	9 14.4
30	9.64647	15	9.69393	19	0.30607	9.95254	4	70	
31	9.64663	16	9.69412	19	0.30588	9.95251	3	69	15
32	9.64678	15	9.69431	19	0.30569	9.95247	4	68	1 1.5
33	9.64693	15	9.69450	19	0.30550	9.95243	4	67	2 3.0
34	9.64709	16	9.69469	19	0.30531	9.95239	4	66	3 4.5 4 6.0
35	9.64724	15	9.69488	19	0.30512	9.95236	3	65	5 7.5
36	9.64739	15 16	9.69507	19 19	0.30493	9.95232	4	64	6 9.0 7 10.5
37	9.64755	15	9.69526		0.30474	9.95228	4	63	7 10.5 8 12.0
38	9.64770	15	9.69545	19 20	0.30455	9.95224	3	62	9 13.5
39	9.64785	15	9.69565	19	0.30435	9.95221	4	61	ľ
40	9.64800	16	9.69584	19	0.30416	9.95217	4	60	1
41	9.64816	15	9.69603	19	0.30397	9.95213		59	3
42	9.64831	15	9.69622	19	0.30378	9.95209	4 3	58	и 0.3
43	9.64846	15	9.69641	19	0.30359	9.95206	4	57	2 0.6
44	9.64861	16	9.69660	19	0.30340	9.95202	4	56	3 0.9 4 1.2
45	9.64877	15	9.69679	19	0.30321	9.95198	4	55	
46	9.64892	15	9.69698	19	0.30302	9.95194	4	54	6 1.8
47	9.64907	15	9.69717	19	0.30283	9.95190	3	53	7 2.I 8 2.4
48 49	9.64922 9.64938	16	9.69736 9.69755	19	0.30264	9.95187	4	52	9 2.7
50		15		19		9.95183	4	51 50	
	9.64953		9.69774		0.30226	9.95179		90	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	l	P. P.

20			_						
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.64953	15	9.69774	19	0.30226	9.95179	4	50	
51	9.64968		9.69793		0.30207	9.95175		49	19
52	9.64983	15 15	9.69812	19 19	0.30188	9-95172	3 4	48	1 1.9
53	9.64998	16	9.69831	19	0.30169	9.95168	4	47	2 3.8
54	9.65014		9.69850	18	0.30150	9.95164	- 1	46	3 5.7
55	9.65029	15 15	9.69868	19	0.30132	9.95160	4	45	4 7.6 5 9.5
56	9.65044	15	9.69887	19	0.30113	9.95156	3	44	5 9.5 6 11.4
57	9.65059	-	9.69906	-	0.30094	9.95153		43	7 13.3
58	9.65074	15 15	9.69925	19 19	0.30075	9.95149	4	42	
59	9.65089	15	9.69944	19	0.30056	9.95145	4	41	9 17.1
60	9.65104	16	9.69963	19	0.30037	9.95141	4	40	
61	9.65120		9.69982		0.30018	9.95137		39	18
62	9.65135	15	9.70001	19	0.29999	9.95134	3	38	1 1.8
63	9.65150	15 15	9.70020	19	0.29980	9.95130	4 4	37	2 3.6 3 5.4
64	9.65165		9.70039	19	0.29961	9.95126		36	4 7.2
65	9.65180	15	9.70058	19	0.29942	9.95122	4	35	5 9.0
66	9.65195	15	9.70077	19 19	0.29923	9.95118	4 3	34	
67	9.65210		9.70096		0.29904	9.95115		33	7 12.6 8 14.4
68	9.65225	15	9.70114	18	0.29886	9.95111	4	32	9 16.2
69	9.65240	15 15	9.70133	19 19	0.29867	9.95107	4	31	* *
70	9.65255	16	9.70152		0.29848	9.95103		30	\ \
71	9.65271		9.70171	19	0.29829	9.95099	4	29	15
72	9.65286	15	9.70190	19	0.29810	9.95096	3	28	1 1.5
73	9.65301	15	9.70209	19	0.29791	9.95092	4	27	2 3.0
74	9.65316	15	9.70228	19	0.29772	9.95088	4	26	3 4.5
75	9.65331	15	9.70247	19	0.29753	9.95084	4	25	
76	9.65346	15	9.70265	18	0.29735	9.95080	4	24	5 7.5 6 9.0
77	9.65361	15	9.70284	19	0.29716	9.95076	4	23	7 10.5
78	9.65376	15	9.70303	19	0.29697	9.95073	3	22	
79	9.65391	15	9.70322	19 19	0.29678	9.95069	4	21	9 13.5
80	9.65406	1	9.70341	19	0.29659	9.95065	4	20	
8r	9.65421	15	9.70360	-	0.29640	9.95061		19	14
82	9.65436	15	9.70379	19	0.29621	9.95057	4	18	I 1.4
83	9.65451	15	9.70397	18	0.29603	9.95054	3	17	2 2.8 3 4.2
84	9.65466	15	9.70416	19	0.29584	9.95050	4	16	4 5.6
85	9.65481	15	9.70435	19	0.29565	9.95046	4	15	5 7.0
86	9.65496	15	9.70454	19	0.29546	9.95042	4	14	6 8.4
87	9.65511	15	9.70473	1 .	0.29527	9.95038		13	7 9.8 8 11.2
88	9.65526	15	9.70491	18	0.29509	9.95034	4	12	9 12.6
89	9.65541	15	9.70510	19	0.29490	9.95030	4 3	11	
90	9.65556	15	9.70529	19	0.29471	9.95027	4	10	
91	9.65571	1	9.70548	1	0.29452	9.95023	1	09	4
92	9.65585	14	9.70567	19	0.29433	9.95019	4 4	08	1 0.4 2 0.8
93	9.65600	15	9.70585	19	0.29415	9.95015	4	07	
94	9.65615	1	9.70604	19	0.29396	9.95011	4	06	3 1.2
95	9.65630	15 15	9.70623	19	0.29377	9.95007	3	٥5	
96	9.65645	15	9.70642	18	0.29358	9.95004	4	04	6 2.4
97	9.65660	1	9.70660	19	0.29340	9.95000	4	03	7 2.8 3.2
98	9.65675	15	9.70679	19	0.29321	9.94996	4	02	8 3.2 9 3.6
99	9.65690	15	9.70698	19	0.29302	9.94992	4	10	1
100	9.65705		9.70717		0.29283	9.94988		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.65705	15	9.70717	18	0.29283	9.94988		100	
OI	9.65720	1 -	9.70735		0.29265	9.94984	4	99	19
02	9.65734	14	9.70754	19	0.29246	9.94980	4	98	
03	9.65749	15 15	9.70773	19 19	0.29227	9.94976	4	97	1 1.9 2 3.8
04	9.65764		9.70792		0.29208	9.94973	3	96	
05	9.65779	15	9.70810	18	0.29190	9.94969	4	95	4 7.6
06	9.65794	15	9.70829	19	0.29171	9.94965	4	94	5 9.5
07	9.65809	15	9.70848	19	0.29152	9.94961	4	93	6 II.4 7 I3.3
о8	9.65823	14	9.70866	18	0.29134	9.94957	4	92	8 15.2
09	9.65838	15 15	9.70885	19	0.29115	9.94953	4	91	9 17.1
10	9.65853	15	9.70904	18	0.29096	9.94949	4	90	
11	9.65868	1 -	9.70922	1	0.29078	9.94946	3	89	18
12	9.65883	15	9.70941	19	0.29059	9.94942	4	88	1 1.8
13	9.65898	15 14	9.70960	19	0.29040	9.94938	4	87	2 3.6
14	9.65912		9.70978	1	0.29022	9.94934	4	86	3 5.4 4 7.2
15	9.65927	15	9.70997	19	0.29003	9.94930	4	85	5 9.0
16	9.65942	15 15	9.71016	19	0.28984	9.94926	4	84	6 10.8
17	9.65957		9.71034	}	0.28966	9.94922	4	83	7 12.6 8 14.4
18	9.65971	14	9.71053	19	0.28947	9.94918	4	82	8 14.4 9 16.2
19	9.65986	15 15	9.71072	19	0.28928	9.94914	4	81	9 1 20.2
20	9.66001	15	9.71090	19	0.28910	9.94911	3	80	
21	9.66016		9.71109	1 .	0.28891	9.94907	4	79	15
22	9.66030	14	9.71128	19	0.28872	9.94903	4	78	1 1.5
23	9.66045	15 15	9.71146	18	0.28854	9.94899	4	77	2 3.0
24	9.66060	-	9.71165	1 -	0.28835	9.94895	4	76	3 4.5
25	9.66075	15	9.71184	19	0.28816	9.94891	4	75	4 6.0
26	9.66089	14 15	9.71202	18	0.28798	9.94887	4	74	5 7.5 6 9.0
27	9.66104		9.71221	19	0.28779	9.94883	4	73	7 10.5
28	9.66119	15 14	9.71239	18	0.28761	9.94879	4	72	
29	9.66133	15	9.71258	19	0.28742	9.94875	4	71	9 13.5
30	9.66148	15	9.71277	19	0.28723	9.94871	4	70	
31	9.66163		9.71295	1	0.28705	9.94868		69	14
32	9.66177	14	9.71314	19 18	0.28686	9.94864	4	68	I 1.4 2 2.8
33	9.66192	15 15	9.71332	19	0.28668	9.94860	4	67	2 2.8 3 4.2
34	9.66207		9.71351	, -	0.28649	9.94856	,	66	4 5.6
35	9.66221	14 15	9.71370	19 18	0.28630	9.94852	4	65	5 7.0 6 8.4
36	9.66236	15	9.71388	19	0.28612	9.94848	4	64	6 8.4
37	9.66251	- 1	9.71407	18	0.28593	9.94844		63	7 9.8 8 11.2
38	9.66265	14 15	9.71425	18	0.28575	9.94840	4	62	9 12.6
39	9.66280	15	9.71444	18	0.28556	9.94836	4	61	
40	9.66295	14	9.71462	19	0.28538	9.94832	4	60	
41	9.66309	15	9.71481	18	0.28519	9.94828	4	59	3
42	9.66324	14	9.71499	19	0.28501	9.94824	4	58	I 0.3 2 0.6
43	9.66338	15	9.71518	19	0.28482	9.94820	3	57	2 0.6
44	9.66353	15	9.71537	18	0.28463	9.94817	4	56	3 0.9 4 1.2
45	9.66368	14	9.71555	19	0.28445	9.94813	4	55	5 1.5
46	9.66382	15	9.71574	18	0.28426	9.94809	4	54	5 I.5 6 I.8
47	9.66397	14	9.71592	19	0.28408	9.94805	4	53	7 2.1 8 2.4
48	9.66411	15	9.71611	18	0.28389	9.94801	4	52	8 2.4
49	9.66426	15	9.71629	19	0.28371	9.94797	4	51	91-1
50	9.66441		9.71648		0.28352	9.94793		50	
L	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P .

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	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.66441	14	9.71648	18	0.28352	9.94793	4	50	
51	9.66455		9.71666	Í	0.28334	9.94789		49	19
52	9.66470	15 14	9.71685	19	0.28315	9.94785	4	48	
53	9.66484	15	9.71703	19	0.28297	9.94781	4	47	1 1.9 2 3.8
54	9.66499	-	9.71722		0.28278	9.94777		46	3 5.7
55	9.66513	14	9.71740	18	0.28260	9.94773	4	45	4 7.6
56	9.66528	15 14	9.71759	19	0.28241	9.94769	4	44	5 9.5 6 11.4
57	9.66542		9.71777		0.28223	9.94765	4	43	7 13.3 8 15.2
58	9.66557	15	9.71796	19	0.28204	9.94761	4	42	
59	9.66571	14 15	9.71814	18	0.28186	9.94757	4	41	9 17.1
60	9.66586	_	9.71833	18	0.28167	9.94753	4	40	
61	9.66600	14	9.71851	1	0.28149	9.94749	4	39	18
62	9.66615	15	9.71869	18	0.28131	9.94745	4	38	1 1.8
63	9.66629	14	9.71888	19	0.28112	9.94741	4	37	2 3.6
64	9.66644	15	9.71906		0.28094	9.94737	4	36	3 5.4 4 7.2
65	9.66658	14	9.71925	19	0.28075	9.94734	3	35	5 9.0
66	9.66673	15	9.71943	18	0.28057	9.94730	4	34	6 10.8
67	9.66687	14	9.71962	19	0.28038	9.94726	4	33	7 12.6 8 14.4
68	9.66702	15	9.71980	18	0.28020	9.94722	4	32	8 14.4 9 16.2
69	9.66716	14	9.71998	18	0.28002	9.94718	4	31	3 1 20.2
70	9.66731	15	9.72017	19	0.27983	9.94714	4	30	6_
71	9.66745	14	9.72035	1	0.27965	9.94710	4	29	15
72	9.66759	14	9.72054	19	0.27946	9.94706	4	28	
73	9.66774	15	9.72072	18	0.27928	9.94702	4	27	I 1.5 2 3.0
74	9.66788	14	9.72091	19	0.27909	9.94698	4	26	3 4.5
75	9.66803	15	9.72109	18	0.27891	9.94694	4	25	4 6.0
76	9.66817	14	9.72127	18	0.27873	9.94690	4	24	5 7.5 6 9.0
77	9.66831	14	9.72146	19	0.27854	9.94686	4	23	7 10.5
78	9.66846	15	9.72164	18	0.27836	9.94682	4	22	8 12.0
79	9.66860	14	9.72182	18	0.27818	9.94678	4	21	9 13.5
80	9.66875	15	9.72201	19	0.27799	9.94674	4	20	1 12-0
8r	9.66889	14	9.72219	18	0.27781	9.94670	4	19	14
82	9.66903	14	9.72238	19	0.27762	9.94666	4	18	I I.4 2 2.8
83	9.66918	15	9.72256	18	0.27744	9.94662	4	17	2 2.8
84	9.66932	14	9.72274	18	0.27726	9.94658	4	16	3 4.2 4 5.6
85	9.66946	14	9.72293	19	0.27707	9.94654	4	15	5 7.0 6 8.4
86	9.66961	15	9.72311	18	0.27689	9.94650	4	14	6 8.4
87	9.66975	14	9.72329	18	0.27671	9.94646	4	13	7 9.8 8 11.2
88	9.66989	14	9.72348	19	0.27652	9.94642	4	12	9 12.6
89	9.67004	15 14	9.72366	18 18	0.27634	9.94638	4	11	
90	9.67018		9.72384	i	0.27616	9.94634	4	10	1
91	9.67032	14	9.72403	19	0.27597	9.94630	4	09	4
92	9.67047	15	9.72421	18	0.27579	9.94626	4	08	1 0.4
93	9.67061	14	9.72439	18	0.27561	9.94622	4	07	2 0.8
94	9.67075	14	9.72458	19	0.27542	9.94618	4	06	3 1.2
9 5	9.67090	15	9.72476	18	0.27524	9.94614	4	05	4 I.6 5 2.0
96	9.67104	14	9.72494	18	0.27506	9.94610	4	04	5 2.0 6 2.4
97	9.67118	14	9.72513	19	0.27487	9.94606	4	03	7 2.8
98	9.67132	14	9.72531	18	0.27469	9.94602	4	02	8 3.2
99	9.67147	15 14	9.72549	18 18	0.27451	9.94598	4 5	10	9 3.6
100	9.67161	14	9.72567	10	0.27433	9.94593	5	00	
	Cos	d.	Cot	d. c.	Tan	Sin	đ.	l	P. P.
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<u></u>	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.67161	14	9.72567	19	0.27433	9.94593	4	100	
or	9.67175	14	9.72586	18	0.27414	9.94589		99	19
02	9.67189	15	9.72604	18	0.27396	9.94585	4	98	
03	9.67204	14	9.72622	19	0.27378	9.94581	4	97	1 1.9 2 3.8
04	9.67218		9.72641	18	0.27359	9.94577	1	96	3 5.7
05	9.67232	14	9.72659	18	0.27341	9.94573	4	95	4 7.6
06	9.67246	15	9.72677	18	0.27323	9.94569	4	94	5 9.5 6 II.4
07	9.67261	1 -	9.72695	1	0.27305	9.94565	4	93	6 II.4 7 I3.3
о8	9.67275	14	9.72714	19	0.27286	9.94561	4	92	7 13.3 8 15.2
09	9.67289	14	9.72732	18	0.27268	9.94557	4	91	9 17.1
10	9.67303	14	9.72750	18	0.27250	9.94553	4	90	
11	9.67317		9.72768		0.27232	9.94549	4	89	18
12	9.67332	15	9.72787	19	0.27213	9.94545	4	88	1 1.8
13	9.67346	14	9.72805	18	0.27195	9.94541	4	87	2 3.6
14	9.67360	14	9.72823	18	0.27177	9.94537	- 4	86	3 5.4
15	9.67374	14	9.72841	18	0.27159	9.94533	4	85	4 7.2 5 9.0
16	9.67388	14	9.72859	18	0.27141	9.94529	4	84	5 9.0 6 10.8
17	9.67402	14	9.72878	19	0.27122	9.94525	4	83	7 12.6
18	9.67417	15	9.72896	18	0.27104	9.94521	4	82	8 14.4
19	9.67431	14	9.72914	18	0.27104	9.94521	4	81	9 16.2
20	9.67445	14	9.72932	18	0.27068	9.94513	4	80	
21	9.67459	14	9.72950	18			5	1	
21	9.67459	14		19	0.27050	9.94508	4	79	15
23	9.67487	14	9.72969 9.72987	18	0.27031	9.94504	4	78	I I.5
		14		18	0.27013	9.94500	4	77	2 3.0
24	9.67501	14	9.73005	18	0.26995	9.94496	4	76	3 4.5 4 6.0
25	9.67515	15	9.73023	18	0.26977	9.94492	4	75	
26	9.67530	14	9.73041	19	0.26959	9.94488	4	74	5 7.5 6 9.0
27	9.67544	14	9.73060	18	0.26940	9.94484	4	73	7 10.5
28	9.67558	14	9.73078	18	0.26922	9.94480	4	72	8 12.0
29	9.67572	14	9.73096	18	0.26904	9.94476	4	71	9 13.5
30	9.67586	14	9.73114	18	0.26886	9.94472	4	70	
31	9.67600	14	9.73132	18	0.26868	9.94468		69	14
32	9.67614	14	9.73150	19	0.26850	9.94464	4	68	I I.4 2 2.8
33	9.67628	14	9.73169	18	0.26831	9.94460	4	67	
34	9.67642		9.73187	18	0.26813	9.94455	5	66	3 4.2 4 5.6
35	9.67656	14 14	9.73205	18	0.26795	9.94451	4	65	5 7.0
36	9.67670	14	9.73223	18	0.26777	9.94447	4	64	6 8.4
37	9.67684		9.73241	18	0.26759	9.94443	4	63	7 9.8 8 11.2
38	9.67698	14	9.73259	18	0.26741	9.94439	4	62	9 12.6
39	9.67712	14 14	9.73277	18	0.26723	9.94435	4	61	,
40	9.67726	14	9.73295	10	0.26705	9.94431	4	60	
4 T	9.67740		9.73314		0.26686	9.94427	4	59	4
42	9.67754	14	9.73332	18 18	0.26668	9.94423	4	58	1 0.4
43	9.67768	14 14	9.73350	18	0.26650	9.94419	4	57	2 0.8
44	9.67782		9.73368		0.26632	9.94415	4	56	3 1.2
45	9.67796	14	9.73386	18	0.26614	9.94410	5	55	4 1.6
46	9.67810	14 14	9.73404	18 18	0.26596	9.94406	4	54	4 1.6 5 2.0 6 2.4 7 2.8 8 3.2
47	9.67824		9.73422		0.26578	9.94402	4	53	7 2.8
48	9.67838	14	9.73440	18	0.26560	9.94398	4	52	
49	9.67852	14 14	9.73458	18 18	0.26542	9.94394	4	51	9 3.6
50	9.67866	14	9.73476	10	0.26524	9.94390	4	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
						OIII	ч.		

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	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.67866		9.73476	19	0.26524	9.94390		50	
51	9.67880	14	9.73495		0.26505	9.94386	4	49	18
52	9.67894	14	9.73513	18 18	0.26487	9.94382	4	48	1 1.8
53	9.67908	14	9.73531	18	0.26469	9.94377	5	47	2 3.6
54	9.67922	14	9.73549		0.26451	9.94373	4	46	3 5.4
55	9.67936	14	9.73567	18	0.26433	9.94369	4	45	4 7.2
56	9.67950	14	9.73585	18 18	0.26415	9.94365	4	44	5 9.0 6 10.8
57	9.67964	14	9.73603		0.26397	9.94361	4	43	
58	9.67978	14	9.73621	18 18	0.26379	9.94357	4	42	7 12.6 8 14.4
59	9.67992	14 14	9.73639	18	0.26361	9.94353	4	41	9 16.2
60	9.68006		9.73657		0.26343	9.94349	4	40	
61	9.68020	14	9.73675	18	0.26325	9.94344	5	39	17
62	9.68033	13	9.73693	18	0.26307	9.94340	4	38	1 1.7
63	9.68047	14	9.73711	18	0.26289	9.94336	4	37	2 3.4
64	9.68061	14	9.73729	18	0.26271	9.94332	4	36	3 5.1 4 6.8
65	9.68075	14	9.73747	18	0.26253	9.94332	4	35	4 6.8 5 8.5 6 10.2
66	9.68089	1.4	9.73765	18	0.26235	9.94324	4	34	6 10.2
67	9.68103	14	9.73783	18	0.26217	9.94320	4	33	7 II.9 8 I3.6
68	9.68117	14	9.73801	18	0.26199	9.94320	5	32	8 13.6 9 15.3
69	9.68130	13	9.73819	18	0.26181	9.94311	4	31	9 13.3
70	9.68144	14	9.73837	18	0.26163	9.94307	4	30	
71	9.68158	14		18	0.26145		4	29	14
71	9.68158	14	9.73855 9.73873	18	0.26127	9.94303	4	28	
73	9.68186	14	9.7389I	18	0.26109	9.94299 9.94295	4	27	I I.4 2 2.8
	9.68200	14		18			4	26	3 4.2
74 75	9.68213	13	9.73909	18	0.26091 0.26073	9.94291 9.94286	5	25	4 5.6
76	9.08213	14	9.73927 9.73945	18	0.26055	9.94282	4	24	5 7.0 6 8.4
		14		18			4		
77 78	9.68241	14	9.73963	18	0.26037	9.94278	4	23 22	7 9.8 8 II.2
79	9.68255	14	9.73981	18	0.26019	9.94274	4	21	9 12.6
		14	9.73999	18		9.94270	4	20	
80	9.68283	13	9.74017	18	0.25983	9.94266	5		13
81	9.68296	14	9.74035	18	0.25965	9.94261	4	19	1 1.3
82	9.68310	14	9.74053	18	0.25947	9.94257	4	18	I I.3 2 2.6
83	9.68324	14	9.74071	18	0.25929	9.94253	4	17	3 3.9
84	9.68338	13	9.74089	18	0.25911	9.94249	4	16	4 5.2 5 6.5
85 86	9.68351	14	9.74107	18	0.25893	9.94245	4	15	5 6.5 6 7.8
	9.68365	14	9.74125	17	0.25875	9.94241	5	14	7 9.1
87	9.68379	14	9.74142	18	0.25858	9.94236	4	13	
88	9.68393	13	9.74160	18	0.25840	9.94232	4	12	9 11.7
89	9.68406	14	9.74178	18	0.25822	9.94228	4	11	
90	9.68420	14	9.74196	18	0.25804	9.94224	4	10	
91	9.68434	14	9.74214	18	0.25786	9.94220	5	09	5
92	9.68448	13	9.74232	18	0.25768	9.94215	4	08	1 0.5
93	9.68461	14	9.74250	18	0.25750	9.94211	4	07	2 1.0
94	9.68475	14	9.74268	18	0.25732	9.94207	4	06	3 1.5 4 2.0
95	9.68489	13	9.74286	18	0.25714	9.94203	4	05	5 2.5
96	9.68502	14	9.74304	18	0.25696	9.94199	4	04	
97	9.68516	14	9.74322	17	0.25678	9.94195	5	03	7 3.5 8 4.0
98	9.68530	13	9 - 74339	18	0.25661	9.94190	4	02	9 4.5
99	9.68543	14	9 - 74357	18	0.25643	9.94186	4	01	3 , 4.0
100	9.68557		9.74375		0.25625	9.94182		00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
00	9.68557	_ u.			0.25625	9.94182	<u> </u>	100	1.1.
		14	9.74375	18			4		İ
01 02	9.68571 9.68584	13	9.74393	18	0.25607	9.94178	4	99 98	18
03	9.68598	14	9.74411 9. 7 4429	18	0.25589	9.94174 9.94169	5	98	1 1.8
		14		18	l		4		2 3.6
04	9.68612 9.68625	13	9.74447	18	0.25553	9.94165	4	96	3 5.4 4 7.2
o5 o6	9.68639	14	9.74465 9.74482	17	0.25535	9.94161 9.94157	4	95 94	5 9.0
		14	1	18		ı	5		6 10.8
07 08	9.68653 9.68666	13	9.74500 9.74518	18	0.25500	9.94152 9.94148	4	93 92	7 12.6 8 14.4
09	9.68680	14	9.74536	18	0.25462	9.94146	4	91	9 16.2
		14		18			4	90	, ,
10	9.68694	13	9.74554	18	0.25446	9.94140	4		17
11	9.68707	14	9.74572	17	0.25428	9.94136	5	89	, ,
12	9.68721	13	9.74589	18	0.25411	9.94131	4	88	I I.7 2 3.4
13	9.68734	14	9.74607	18	0.25393	9.94127	4	87	3 5.1
14	9.68748	14	9.74625	18	0.25375	9.94123	4	86	4 6.8
15	9.68762	13	9.74643	18	0.25357	9.94119	5	85	5 8.5 6 10.2
16	9.68775	14	9.74661	18	0.25339	9.94114	4	84	
17	9.68789	13	9.74679	17	0.25321	9.94110	4	83	7 II.9 8 I3.6
18	9.68802	14	9.74696	18	0.25304	9.94106	4	82 81	9 15.3
19	9.68816	13	9.74714	18	0.25286	9.94102	4	1	
20	9.68829	14	9.74732	18	0.25268	9.94098	5	80	
21	9.68843	14	9.74750	18	0.25250	9.94093	4	79	14
22	9.68857	13	9.74768	17	0.25232	9.94089	4	78	1 1.4
23	9.68870	14	9.74785	18	0.25215	9.94085	4	77	2 2.8 3 4.2
24	9.68884	13	9.74803	18	0.25197	9.94081	5	76	3 4.2 4 5.6
25	9.68897	14	9.74821	18	0.25179	9.94076	4	75	5 7.0 6 8.4
26	9.68911	13	9.74839	17	0.25161	9.94072	4	74	6 8.4
27	9.68924	14	9.74856	18	0.25144	9.94068	4	73	7 9.8 8 11.2
28	9.68938	13	9.74874	18	0.25126	9.94064	5	72	9 12.6
29	9.68951	14	9.74892	18	0.25108	9.94059	4	71	
30	9.68965	13	9.74910	17	0.25090	9.94055	4	70	13
31	9.68978	14	9.74927	18	0.25073	9.94051	4	69	
32	9.68992	13	9.74945	18	0.25055	9.94047	5	68	1 1.3 2 2.6
33	9.69005	14	9.74963	18	0.25037	9.94042	4	67	3 3.9
34	9.69019	13	9.74981	17	0.25019	9.94038	4	66	4 5.2
35	9.69032	14	9.74998	18	0.25002	9.94034	4	65	5 6.5 6 7.8
36	9.69046	13	9.75016	18	0.24984	9.94030	5	64	7 9.1
37	9.69059	14	9.75034	18	0.24966	9.94025	4	63	
38	9.69073	13	9.75052	17	0.24948	9.94021	4	62	9 11.7
39	9.69086	14	9.75069	18	0.24931	9.94017	5	61	
40	9.69100	13	9.75087	18	0.24913	9.94012	4	60	A.A.
41	9.69113	14	9.75105	18	0.24895	9.94008	4	59	4
42	9.69127	13	9.75123	17	0.24877	9.94004	4	58	I 0.4 2 0.8
43	9.69140	13	9.75140	18	0.24860	9.94000	5	57	
44	9.69153	14	9.75158	18	0.24842	9.93995	4	56	3 1.2 4 1.6
45	9.69167	13	9.75176	17	0.24824	9.93991	4	55	5 2.0
46	9.69180	14	9.75193	18	0.24807	9.93987	4	54	6 2.4
47	9.69194	13	9.75211	18	0.24789	9.93983	5	53	7 2.8 8 3.2
48	9.69207	13	9.75229	18	0.24771	9.93978	4	52	9 3.6
49	9.69220	14	9.75247	17	0.24753	9.93974	4	51	, , ,
50	9.69234		9.75264		0.24736	9.93970		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.69234		9.75264		0.24736	9.93970		50	
51	9.69247	13	9.75282	18	0.24718	9.93965	5	49	40
52	9.69261	14	9.75300	18	0.24700	9.93961	4	48	18
53	9.69274	13	9.75317	17	0.24683	9.93957	4	47	1 1.8 3.6
54	9.69287	13	9.75335	18	0.24665	9.93953	4	46	3 5.4
55	9.69301	14	9.75353	18	0.24647	9.93948	5	45	4 7.2
56	9.69314	13 14	9.75370	17	0.24630	9.93944	4	44	5 9.0 6 10.8
57	9.69328	1	9.75388	18	0.24612	9.93940	4	43	7 12.6 8 14.4
58	9.69341	13	9.75406	17	0.24594	9.93935	5 4	42	
59	9.69354	14	9.75423	18	0.24577	9.93931	4	41	9 16.2
60	9.69368	13	9.75441	18	0.24559	9.93927	5	40	
61	9.69381	13	9.75459	17	0.24541	9.93922	4	39	17
62	9.69394	14	9.75476	18	0.24524	9.93918	4	38	I I.7 2 3.4
63	9.69408	13	9 - 75494	17	0.24506	9.93914	5	37	3 5.1
64	9.69421	13	9.75511	18	0.24489	9.93909	4	36	4 6.8
65 66	9.69434 9.69448	14	9.75529	18	0.24471	9.93905	4	35	5 8.5 6 10.2
67		13	9.75547	17	0.24453	9.93901	4	34	7 11.9
68	9.69461 9.69474	13	9.75564	18	0.24436	9.93897 9.93892	5	33	8 13.6
69	9.69474	13	9.75582 9.75600	18	0.24416	9.93892	4	32 31	9 15.3
70	9.69501	14	9.75617	17	0.24383	9.93884	4	30	
71	9.69514	13		18	0.24365	9.93879	5		
72	9.69527	13	9.75635 9.75652	17	0.24348	9.93875	4	29 28	14
73	9.69541	14	9.75670	18	0.24330	9.93871	4	27	I 1.4 2 2.8
74	9.69554	13	9.75688	18	0.24312	9.93866	5	26	3 4.2
75	9.69567	13	9.75705	17	0.24295	9.93862	4	25	4 5.6
76	9.69580	13	9.75723	18 17	0.24277	9.93858	4	24	5 7.0 6 8.4
77	9.69594	14	9.75740	18	0.24260	9.93853	5	23	7 9.8
78	9.69607	13	9.75758	18	0.24242	9.93849	4	22	8 II.2 9 I2.6
79	9.69620	13	9.75776	17	0.24224	9.93845	4 5	21	9 12.0
80	9.69633	14	9.75793	18	0.24207	9.93840	4	20	13
81	9.69647	13	9.75811	17	0.24189	9.93836	4	19	
82	9.69660	13	9.75828	18	0.24172	9.93832	5	18	1 1.3 2.6
83	9.69673	13	9.75846	17	0.24154	9.93827	4	17	3 3.9
84	9.69686	13	9.75863	18	0.24137	9.93823	4	16	4 5.2
8 ₅ 86	9.69699	14	9.75881	18	0.24119	9.93819	5	15	5 6.5 6 7.8
	9.69713	13	9.75899	17	0.24101	9.93814	4	14	7 9.1
87 88	9.69726	13	9.75916	18	0.24084	9.93810	5	13	8 10.4 9 11.7
89	9.69739 9.69752	13	9.75934 9.75951	17	0.24000	9.93805 9.93801	4	12 11	9 11. /
90	9.69765	13	9.75969	18	0.24031	9.93797	4	10	
91		14		17			5		
91	9.69779 9.69792	13	9.75986 9.76004	18	0.24014	9.93792 9.93788	4	o9 o8	5
93	9.69805	13	9.76021	17	0.23990	9.93784	4	07	I 0.5 2 I.0
94	9.69818	13	9.76039	18	0.23961	9.93779	5	06	3 1.5
94 95	9.69831	13	9.76056	17	0.23944	9.93775	4	05	4 2.0
96	9.69844	13	9.76074	18	0.23926	9.93771	4	04	4 2.0 5 2.5 6 3.0
97	9.69858	14	9.76091	17	0.23909	9.93766	5	03	7 3.5
98	9.69871	13	9.76109	18 17	0.23891	9.93762	4	02	
99	9.69884	13 13	9.76126	18	0.23874	9.93757	5	01	9 4.5
100	9.69897	-5	9.76144		0.23856	9.93753	7	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.69897		9.76144		0.23856	9.93753		100	
OI	9.69910	13	9.76161	17	0.23839	9.93749	4	99	4.0
02	9.69923	13	9.76179	18	0.23821	9.93744	5	98	18
03	9.69936	13	9.76196	17	0.23804	9.93740	4	97	1 1.8 3.6
04	9.69949	13	9.76214		0.23786	9.93736	4	96	3 5.4
05	9.69963	14	9.76231	17 18	0.23769	9.93731	5	95	4 7.2
о6	9.69976	13	9.76249	17	0.23751	9.93727	4 5	94	4 7.2 5 9.0 6 10.8
07	9.69989	1 -	9.76266	18	0.23734	9.93722		93	7 12.6
о8	9.70002	13	9.76284	17	0.23716	9.93718	4	92	8 14.4
09	9.70015	13	9.76301	18	0.23699	9.93714	5	91	9 16.2
10	9.70028	13	9.76319	17	0.23681	9.93709	4	90	
11	9.70041		9.76336	18	0.23664	9.93705		89	17
12	9.70054	13 13	9.76354	17	0.23646	9.93700	5 4	88	I 1.7
13	9.70067	13	9.76371	18	0.23629	9.93696	4	87	2 3.4 3 5.1
14	9.70080	13	9.76389	17	0.23611	9.93692	5	86	4 6.8
15	9.70093	13	9.76406	18	0.23594	9.93687	5 4	85	5 8.5
16	9.70106	13	9.76424	17	0.23576	9.93683	5	84	6 10.2 7 11.9
17	9.70119	13	9.76441	17	0.23559	9.93678	4	83	8 13.6
18	9.70132	13	9.76458	18	0.23542	9.93674	4	82	9 15.3
19	9.70145	14	9.76476	17	0.23524	9.93670	5	81	
20	9.70159	13	9.76493	18	0.23507	9.93665	4	80	
21	9.70172	13	9.76511	17	0.23489	9.93661	5	79	14
22	9.70185	13	9.76528	18	0.23472	9.93656	4	78	1 1.4
23	9.70198	13	9.76546	17	0.23454	9.93652	4	77	2 2.8 3 4.2
24	9.70211	13	9.76563	17	0.23437	9.93648	5	76	
25 26	9.70224	13	9.76580	18	0.23420	9.93643	4	75	5 7.0
	9.70237	13	9.76598	17	0.23402	9.93639	5	74	
27 28	9.70250	13	9.76615	18	0.23385	9.93634	4	73	7 9.8 8 11.2
20	9.70263 9.70276	13	9.76633 9.76650	17	0.23367 0.23350	9.93630 9.93625	5	72 71	9 12.6
30	9.70278	12	9.76668	18	0.23332	9.93621	4	70	
		13		17			4	69	13
31	9.70301	13	9.76685 9.76702	17	0.23315	9.93617 9.93612	5	68	
32 33	9.70314 9.70327	13	9.76720	18	0.23280	9.93012 9.936c8	4	67	2 2.6
	9.70340	13	9.76737	17	0.23263	9.93603	5	66	3 3.9
34 35	9.70340	13	9.76754	17	0.23246	9.93599	4	65	4 5.2 5 6.5 6 7.8
36	9.70366	13	9.76772	18	0.23228	9.93594	5	64	5 6.5 6 7.8
37	9.70379	13	9.76789	17	0.23211	9.93590	4	63	7 9.1 8 10.4
38	9.70392	13	9.76807	18	0.23193	9.93585	5	62	9 11.7
39	9.70405	13	9.76824	17	0.23176	9.93581	4	61	, ,
40	9.70418	13	9.76841	17	0.23159	9.93577	4	60	
41	9.70431	13	9.76859	18	0.23141	9.93572	5	59	4
42	9.70444	13	9.76876	17	0.23124	9.93568	4	58	1 0.4
43	9.70457	13	9.76893	17 18	0.23107	9.93563	5	57	2 0.8
44	9.70470	13	9.76911		0.23089	9.93559	4	56	3 1.2
45	9.70482	12	9.76928	17	0.23072	9.93554	5	55	4 I.6 5 2.0
46	9.70495	13	9.76945	17 18	0.23055	9.93550	4 5	54	4 1.6 5 2.0 6 2.4
47	9.70508	-	9.76963		0.23037	9.93545	1	53	7 2.8
48	9.70521	13	9.76980	17 18	0.23020	9.93541	4	52	8 3.2 9 3.6
49	9.70534	13 13	9.76998	17	0.23002	9.93537	4 5	51	9 3.0
50	9.70547		9.77015		0.22985	9.93532	J	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

30 -								149	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.70547	13	9.77015	17	0.22985	9.93532	4	50	
51	9.70560	-	9.77032	18	0.22968	9.93528		49	18
52	9.70573	I3 I2	9.77050	17	0.22950	9.93523	5	48	-т т8
53	9.70585	13	9.77067	17	0.22933	9.93519	4 5	47	2 3.6
54	9.70598	13	9.77084	17	0.22916	9.93514		46	2 3.6 3 5.4 4 7.2
55	9.70611	13	9.77101	18	0.22899	9.93510	4 5	45	4 7.2 5 9.0
56	9.70624	13	9.77119	17	0.22881	9.93505	4	44	3 5.4 4 7.2 5 9.0 6 10.8
57	9.70637	13	9.77136	17	0.22864	9.93501	5	43	7 12.6
53	9.70050	12	9.77153	is	0.22847	9.93496	4	42	8 I4.4 9 I6.2
59	9.70662	13	9.77171	17	0.22829	9.93492	5	41	9 10.2
60	9.70075	13	9.77188	17	0.22812	9.93487	4	40	
61	9 70688		9.77205	18	0.22795	9.93483		39	17
62	9 70701	13	9.77223	17	0.22777	9.93478	5	38	I I.7
63	9.70714	13	9.77240	17	0.22760	9.93474	5	37	2 3.4 2 5 T
64	9 70727	12	9.77257	17	0.22743	9.93469	4	36	2 3.4 3 5.1 4 6.8
65	9.70739	13	9.77274	18	0.22726	9.93465	5	35	5 8.5
66	9.70752	13	9.77292	17	0.22708	9.93460	4	34	6 10.2
67	9.70765	13	9.77309	17	0.22691	9.93456	5	33	7 II.9 8 I3.6
68	9.70778	12	9.77326	18	0.22074	9.93451	4	32	9 15.3
69	9.70790	13	9.77344	17	0.22656	9.93447	5	31	
70	9.70803	13	9.77361	17	0.22639	9.93442	4	30	
71	9.70816	13	9.77378	17	0.22522	9.93438		29	13
72	9.70829	13	9.77395	18	0.22603	9.93433	5 4	28	I I.3 2 2.6
73	9.70842	12	9.77413	17	0.22587	9 93429	5	27	
74	9.70854	13	9.77430	17	0.22570	9.93424	4	26	3 3.9 4 5.2 5 6.5 6 7.8
75	9.70867	13	9.77447	17	0.22553	9.93420	5	25	5 6.5
76	9.70880	12	9.77464	18	0.22536	9.93415	4	24	3 3.9 4 5.2 5 6.5 6 7.8 7 9.1 8 10.4
77	9.70892	13	9.77482	17	0.22518	9.93411	5	23	7 9.I 8 10.4
78	9.70905	13	9.77499	17	0.22501	9.93406	4	22	9 11.7
79	9.70918	13	9.77516	17	0.22484	9.93402	5	21	
80	9.70931	12	9.77533	18	0.22467	9.93397	4	20	12
81	9.70943	13	9.77551	17	0.22449	9.93393	5	19	
82	9.70956	13	9.77568	17	0.22432	9.93388	4	18	I I.2 2 2.4
83	9 70969	12	9.77585	17	0.22413	9.93384	5	17	3 3.6
84	9.70981	13	9.77602	17	0.22398	9.93379	4	16	4 4.8
85 86	9 70994	13	9.77619	18	0.22381	9.93375	5	15	6 7.2
	9.71007	13	9.77637	17	0.22363	9.93370	4	14	5 6.0 6 7.2 7 8.4 8 9.6
87	9.71020	12	9.77654	17	0.22346	9.93366	5	13	
88 89	9-71032	13	9.77671	17	0.22329	9.93361	4	12	9 10.8
	9.71045	13	9.77688	18		9.93357	5	1	
90	9 71058	12	9.77706	17	0.22294	9.93352	5	10	Į.
91	9.71070	13	9.77723	17	0.22277	9.93347	4	09	5
92	9.71083	13	9.77740	17	0.22260	9.93343	5	08	1 0.5
93	9.71096	12	9.77757	17	0.22243	9.93338	4	07	2 I.0 3 I.5
94	9.71108	13	9.77774	17	0.22226	9.93334	5	06	4 2.0
95 96	9.71121	12	9.77791	18	0.22209	9.93329	4	05	5 2.5
	9.71133	13	9.77809	17		9.93325	5	04	6 3.0
97 98	9.71146	13	9.77826	17	0.22174	9.93320	4	03	7 3.5
99	9.71159	12	9.77843 9.77860	17	0.22157	9.93316	5	02	9 4.5
100	9.71171	13		17		9.93311	- 4	00	
100	9.71184		9.77877		0.22123	9.93307		-00	
	Cos	d.	Cot	d.c.	Tan	Sin	d.		P. P.

Sin d. Tan d.c. Cot Cos d. P.P.	31 °								148°	
13		Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
18	00	9.71184	7.2	9.77877	7.8	0.22123	9.93307	-	100	
0.2 0.7 1.20 0.3 0.7 1.20 1.3 0.7 0.7 0.2 0.	10	9.71197	-	9.77895		0.22105	9.93302			18
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10	о8	9.71285		9.78015		0.21985	9.93270		92	
10	09	9.71297		9.78032		0.21968	9.93265		91	9 16.2
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13	12									
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15	14	0.71360		0.78117		0.21883	0.03213		86	3 5.1
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Cos d. Cot d.c. Tan Sin d. P.P.	50							_	50	
		Cos	d.	Cot	d. c.	Tan	Sin	∣ d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	I A	_	D D
		α.		a. c.			<u>d.</u>		P. P.
50	9.71809	12	9.78732	17	0.21268	9.93077	5	50	
51	9.71821	12	9.78749	17	0.21251	9.93072	5	49	17
52	9.71833	13	9.78766	17	0.21234	9.93067	4	48	17 1.7
53	9.71846	12	9.78783	17	0.21217	9.93063	5	47	2 3.4
54	9.71858	12	9.78800	17	0.21200	9.93058	5	46	3 5.1 4 6.8
55	9.71870	13	9.78817	17	0.21183	9.93053	4	45	4 6.8 5 8.5
56	9.71883	12	9.78834	17	0.21166	9.93049	5	44	6 10.2
57	9.71895	12	9.78851	17	0.21149	9.93044	5	43	7 II.9 8 I3.6
58	9.71907	13	9.78868	17	0.21132	9.93039	4	42	8 13.6 9 15.3
59	9.71920	12	9.78885	17	0.21115	9.93035	5	41	9 13.3
60	9.71932	12	9.78902	17	0.21098	9.93030	5	40	
61	9.71944	13	9.78919	17	0.21081	9.93025	4	39	16
62	9.71957	12	9.78936	17	0.21064	9.93021	5	38	I I.6 2 3.2
63	9.71969	12	9.78953	17	0.21047	9.93016	5	37	2 3.2 3 4.8
64	9.71981	13	9.78970	17	0.21030	9.93011	4	36	4 0.4
65	9.71994	13	9.78987	17	0.21013	9.93007	5	35	5 8.0
66	9.72006	12	9.79004	17	0.20996	9.93002	5	34	6 9.6 7 II.2
67	9.72018	12	9.79021	17	0.20979	9.92997	4	33	7 II.2 8 I2.8
68	9.72030	13	9.79038	17	0.20962	9.92993	5	32	9 14.4
69	9.72043	12	9.79055	17	0.20945	9.92988	5	31	
70	9.72055	12	9.79072	17	0.20928	9.92983	4	30	
71	9.72067		9.79089		0.20911	9.92979		29	13
72	9.72079	12 13	9.79106	17 16	0.20894	9.92974	5 5	28	1 1.3
73	9.72092	13	9.79122	17	0.20878	9.92969	4	27	2 2.6
74	9.72104		9.79139		0.20861	9.92965	}	26	3 3.9
75	9.72116	12 12	9.79156	17	0.20844	9.92960	5	25	4 5.2
76	9.72128	13	9.79173	17	0.20827	9.92955	5 4	24	4 5.2 5 6.5 6 7.8
77	9.72141	-	9.79190		0.20810	9.92951		23	7 9.1
78	9.72153	12	9.79207	17	0.20793	9.92946	5	22	
79	9.72165	I2 I2	9.79224	17	0.20776	9.92941	5 5	21	9 11.7
80	9.72177		9.79241		0.20759	9.92936		20	
8ı	9.72190	13	9.79258	17	0.20742	9.92932	4	19	12
82	9.72202	12	9.79275	17	0.20725	9.92927	5	18	I I.2
83	9.72214	12	9.79292	17	0.20708	9.92922	5	17	2 2.4 3 3.6
84	9.72226	12	9.79309	17	0.20691	9.92918	4	16	4 4.8
85	9.72238	12	9.79326	17	0.20674	9.92913	5	15	5 6.0
86	9.72251	13	9.79343	17 16	0.20657	9.92908	5	14	0 7.2
87	9.72263	12	9.79359		0.20641	9.92903	5	13	6 7.2 7 8.4 8 9.6
88	9.72275	12	9.79376	17	0.20624	9.92899	4	12	9 10.8
89	9.72287	12 12	9.79393	17 17	0.20607	9.92894	5 5	11	
90	9.72299		9.79410		0.20590	9.92889		10	
91	9.72312	13	9.79427	17	0.20573	9.92885	4	09	5
92	9.72324	12	9.79444	17	0.20556	9.92880	5	08	1 0.5
93	9.72336	12	9.79461	17	0.20539	9.92875	5	07	2 1.0
94	9.72348	12	9.79478	17	0.20522	9.92870	5	06	3 1.5
95	9.72340	12	9.79475	17	0.20505	9.92866	4	05	4 2.0
96	9.72372	12	9.79511	16	0.20489	9.92861	5	04	5 2.5 6 3.0
97	9.72385	13	9.79528	17	0.20472	9.92856	5	03	7 3.5
98	9.72397	12	9.79545	17	0.20455	9.92852	4	02	
99	9.72409	12	9.79562	17	0.20438	9.92847	5	01	9 4.5
100	9.72421	12	9 - 79579	17	0.20421	9.92842	5	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
L'	Cos	α.	COL	d.c.	lan	OIII	u.		I.I.

34									
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.72421	12	9.79579	17	0.20421	9.92842	5	100	
01	9 72433	12	9.79596	17	0.20404	9.92837	4	99	17
02	9.72445	12	9.79613	17	0.20387	9.92833	5	98	1 1.7
03	9.72457	12	9.79630	16	0.20370	9.92828	5	97	2 3.4
04	9.72469	1	9.79646		0.20354	9.92823	5	96	3 5.1
05	9.72482	13 12	9.79663	17 17	0.20337	9.92818	4	95	4 6.8 5 8.5
06	9.72494	12	9.79680	17	0.20320	9.92814	5	94	5 8.5 6 10.2
07	9.72506		9.79697		0.20303	9.92809	5	93	7 11.9
08	9.72518	12 12	9.79714	17 17	0.20286	9.92804	5	92	
09	9.72530	12	9.79731	16	0.20269	9.92799	4	91	9 15.3
10	9.72542	12	9.79747	17	0.20253	9.92795	5	90	
11	9.72554		9.79764		0.20236	9.92790		8 9	16
12	9.72566	12 12	9.79781	17	0.20219	9.92785	5 5	88	1 1.6
13	9.72578	12	9.79798	17	0.20202	9.92780	4	87	2 3.2 3 4.8
14	9.72590	1	9.79815		0.20185	9.92776	1	86	4 6.4
15	9.72602	12	9.79832	17 16	0.20168	9.92771	5 5	85	5 8.0
16	9.72614		9.79848	17	0.20152	9.92766	5	84	6 9.6
17	9.72627	13	9.79865		0.20135	9.92761	1	83	7 11.2 8 12.8
18	9.72639	12	9.79882	17	0.20118	9.92756	5 4	82	9 14.4
19	9.72651	12 12	9.79899	17	0.20101	9.92752	5	81	
20	9.72663	12	9.79916	16	0.20084	9.92747	5	80	
21	9.72675	1	9.79932	1	0.20068	9.92742		79	13
22	9.72687	12	9.79949	17	0.20051	9.92737	5	78	1 1.3
23	9.72699	12	9.79966	17	0.20034	9.92733	4	77	2 2.6
24	9.72711	12	9.79983	17	0.20017	9.92728	5	76	3 3.9
25	9.72723	12	9.80000	17	0,20000	9.92723	5	75	4 5.2
26	9.72735	12	9.80016	16	0.19984	9.92718	5	74	4 5.2 5 6.5 6 7.8
27	9.72747	12	9.80033	17	0.19967	9.92713	5	73	7 9.1
28	9.72759	12	9.80050	17	0.19950	9.92709	4	72	
29	9.72771	12	9.80067	17	0.19933	9.92704	5	71	9 11.7
30	9.72783	1	9.80084	17	0.19916	9.92699	5	70	
31	9.72795	12	9.80100		0.19900	9.92694	1 -	69	12
32	9.72807	12	9.80117	17	0.19883	9.92690	4	68	1 1.2
33	9.72819	12	9.80134	17	0.19866	9.92685	5	67	2 2.4 3 3.6
34	9.72831		9.80151		0.19849	9.92680	1	66	4 4.8
35	9.72843	12	9.80168	17	0.19832	9.92675	5	65	5 6.0
36	9.72855	12	9.80184	16	0.19816	9.92670	5	64	6 7.2
37	9.72867	1	9.80201	1	0.19799	9.92666		63	7 8.4 8 9.6
38	9.72879	12	9.80218	17	0.19782	9.92661	5	62	9 10.8
39	9.72890	11	9.80235	17	0.19765	9.92656	5	61	l
40	9.72902	12	9.80251	17	0.19749	9.92651	5	60	i
41	9.72914	1	9.80268	1 '	0.19732	9.92646	1	59	4
42	9.72926	12	9.80285	17	0.19715	9.92641	5	58	1 0.4
43	9.72938	I 2 I 2	9.80302	17	0.19698	9.92637	5	57	2 0.8
44	9.72950	ł	9.80318	1	0.19682	9.92632	1 -	56	3 1.2
45	9.72962	12	9.80335	17	0.19665	9.92627	5	55	4 1.6 5 2.0
46	9.72974	12 12	9.80352	17	0.19648	9.92622	5	54	6 2.4
47	9.72986		9.80369	1 '	0.19631	9.92617	1	53	7 2.8
48	9.72998	I2 I2	9.80385	16	0.19615	9.92613	5	52	8 3.2 9 3.6
49	9.73010	- 12	9.80402	17	0.19598	9.92608	5	51	9 3.0
50	9.73022	12	9.80419	17	0.19581	9.92603		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	6:-	d.	Tan	4 .	C-+	C			D D
	Sin	а.		d. c.	Cot	Cos	d.		P. P.
50	9.73022	12	9.80419	16	0.19581	9.92603	5	50	
51	9.73034	11	9.80435	17	0.19565	9.92598	5	49	17
52	9.73045	12	9.80452	17	0.19548	9.92593	5	48	I 1.7
53	9.73057	12	9.80469	17	0.19531	9.92588	4	47	2 3.4
54	9.73069	12	9.80486	16	0.19514	9.92584	5	46	3 5.I 4 6.8
55	9.73081	12	9.80502	17	0.19498	9.92579	5	45	4 6.8 5 8.5
56	9.73093	12	9.80519	17	0.19481	9.92574	5	44	6 10.2
57	9.73105	12	9.80536	16	0.19464	9.92569	5	43	7 II.9 8 I3.6
58	9.73117	12	9.80552	17	0.19448	9.92564	5	42	
59	9.73129	11	9.80569	17	0.19431	9.92559	4	41	9 15.3
60	9.73140	12	9.80586	17	0.19414	9.92555	5	40	
61	9.73152	12	9.80603	16	0.19397	9.92550	5	39	16
62	9.73164	12	9.80619	17	0.19381	9.92545	5	38	1 1.6
63	9.73176	12	9.80636	17	0.19364	9.92540	5	37	2 3.2 3 4.8
64	9.73188	12	9.80653	16	0.19347	9.92535	5	36	4 6.4
65	9.73200	II	9.80669	17	0.19331	9.92530	5	35	5 8.0
66	9.73211	12	9.80686	17	0.19314	9.92525	4	34	6 9.6 7 II.2
67	9.73223	12	9.80703	16	0.19297	9.92521		33	7 II.2 8 I2.8
68	9.73235	12	9.80719	17	0.19281	9.92516	5 5	32	9 14.4
69	9.73247	12	9.80736	17	0.19264	9.92511	5	31	
70	9.73259	12	9.80753	16	0.19247	9.92506		30	
71	9.73271		9.80769		0.19231	9.92501	5	29	12
72	9.73282	II	9.80786	17	0.19214	9.92496	. 5	28	I I.2
73	9.73294	12 12	9.80803	17 16	0.19197	9.92491	5	27	
74	9.73306		9.80819	!	0.19181	9.92486	5	26	2 2.4 3 3.6
75	9.73318	12	9.80836	17	0.19164	9.92482	4	25	4 4.8 5 6.0
76	9.73329	II I2	9.80853	17 16	0.19147	9.92477	5	24	5 6.0 6 7.2
77	9.73341		9.80869		0.19131	9 92472	5	23	7 8.4
78	9.73353	12	9.80886	17	0.19114	9.92467	5	22	8 9.6
79	9.73365	12 12	9.80903	17 16	0.19097	9.92462	5	21	9 10.8
80	9.73377		9.80919		0.19081	9.92457	1	20	
81	9.73388	II	9.80936	17	0.19064	9.92452	5	19	11
82	9.73400	12	9.80953	17	0.19047	9.92447	5	18	I I.I
83	9.73412	12	9.80969	16	0.19031	9.92443	4	17	2 2.2
84	9.73424	12	9.80986	17	0.19014	9.92438	5	16	3 3.3 4 4.4
85	9.73424	II	9.81003	17	0.18997	9.92433	5	15	5 5.5 6 6.6
86	9.73447	12	9.81019	16	0.18981	9.92428	5	14	6 6.6
87	9.73459	12	9.81036	17	0.18964	9.92423	5	13	7 7.7
88	9.73470	II	9.81052	16	0.18948	9.92418	5	12	9 9.9
89	9.73482	12	9.81069	17	0.18931	9.92413	5	11	1
90	9.73494	12	9.81086	17	0.18914	9.92408	5	10	l
91	9.73506	12	9.81102	16	0.18898	9.92403	5	09	5
91	9.73517	11	9.81119	17	0.18881	9.92398	5	08	1 0.5
93	9.73529	12	9.81136	17	0.18864	9.92394	4	07	2 I.O
94	9.73541	12	9.81152	16	0.18848	9.92389	5	06	3 1.5
94 95	9.73552	II	9.81169	17	0.18831	9.92384	5	05	4 2.0
96	9.73564	12	9.81185	16	0.18815	9.92379	5	04	5 2.5 6 3.0
97	9.73576	12	9.81202	17	0.18798	9.92374	5	03	
98	9.73588	12	9.81219	17	0.18781	9.92369	5	02	8 4.0
99	9.73599	11	9.81235	16	0.18765	9.92364	5	01	9 4.5
100	9.73611	12	9.81252	17	0.18748	9.92359	5	l 00	
100		-	Cot	d. c.	Tan	Sin	d.	ات	P. P.
1	Cos	d.	· Cot	. a. c.	· Ian	· OIII	· u.	<u> </u>	F.F.

	C:		dr.		C-4	C-	1		T) T)
	Sin	_d.	Tan	d.c.	Cot	Cos	d.	400	P. P.
00	9.73611	12	9.81252	16	0.18748	9.92359	5	100	
10	9.73623	11	9.81268	17	0.18732	9.92354	5	99	17
02	9.73634	12	9.81285	17	0.18715	9.92349	5	98	I I.7
03	9.73646	12	9.81302	16	0.18698	9.92344	5	97	2 3.4
04	9.73658	11	9.81318	17	0.18682	9.92339	4	96	3 5.1 4 6.8
05 06	9.73669	12	9.81335	16	0.18665	9.92335	5	95 94	5 8.5
	9.73681	11	9.81351	17		9.92330	5		6 10.2
07	9.73692	12	9.81368 9.81384	16	0.18632 0.18616	9.92325	5	93 92	7 II.9 8 I3.6
o8 o9	9.73704	12	9.81384	17	0.18599	9.92320 9.92315	5	92 91	9 15.3
10	9.73716	11		17	0.18582		5	90	
	9.73727	12	9.81418	16		9.92310	5		16
II	9.73739	12	9.81434	17	0.18566 0.18549	9.92305	5	89 88	1 1.6
12 13	9.73751 9.73762	11	9.81451 9.81467	16	0.18533	9.92300 9.92295	5	87	2 3.2
		12		17			5	86	3 4.8
14	9.73774	11	9.81484 9.81500	16	0.18516 0.18500	9.92290 9.92285	5	85	4 6.4
15 16	9.73785	12	9.81500	17	0.18483	9.92280	5	8 ₄	5 8.0 6 9.6
	9.73797	12		16	0.18467		5	83	7 11.2
17 18	9.73809	11	9.81533 9.81550	17	0.18407	9.92275 9.92270	5	82	
18	9.73820 9.73832	12	9.81567	17	0.18433	9.92270	5	81	9 14.4
20	9.73843	11	9.81583	16	0.18417	9.92260	5	80	
		12		17			5	1	
21	9.73855	12	9.81600 9.81616	16	0.18400	9.92255	5	79 78	12
22 23	9.73867 9.73878	11	9.81633	17	0.18367	9.92250 9.92245	5	78 77	I I.2
		12		16			5		2 2.4 3 3.6
24	9.73890	11	9.81649 9.81666	17	0.18351	9.92240	5	76	4 4.8
25 26	9.73901 9. 7 3913	12	9.81682	16	0.18334	9.92235 9.92231	4	75 74	5 6.0
		11	9.81699	17	0.18301	9.92231	5		6 7.2
27 28	9.73924 9.73936	12	9.81715	16	0.18285	9.92221	5	73 72	7 8.4 8 9.6
29	9.73930	11	9.81713	17	0.18268	9.92221	5	71	9 10.8
30		12	9.81748	16	0.18252	9.92211	5	70	
	9.73959	12		17			5	69	11
31	9.73971 9.73982	11	9.81765 9.81781	16	0.18235	9.92206 9.92201	5	68	1 1.1
32 33	9.73982 9.73 994	12	9.81781	17	0.18219	9.92201	5	67	2 2.2
		11	9.81798	16	0.18186	9.92190	5	66	3 3.3
34 35	9. 7 4005 9.74017	12	9.81831	17	0.18180	9.92191	5	65	4 4.4
35 36	9.74017	11	9.81847	16	0.18153	9.92181	5	64	5 5.5 6 6.6
	9.74040	12	9.81864	17	0.18136	9.92176	5	63	7 7.7 8 8.8
37 38	9.74040	11	9.81880	16	0.18130	9.92170	5	62	8 8.8 9 9.9
39	9.74063	12	9.81897	17	0.18103	9.92171	5	61	9 (9.9
40	9.74074	11	9.81913	16	0.18087	9.92161	5	60	1
41	9.74074	12	9.81930	17	0.18070	9.92156	5	59	
41	9.74080	11	9.81930	16	0.18070	9.92150	5	59 58	5
43	9.74109	12	9.81963	17	0.18037	9.92146	5	57	1 0.5
44	9.74120	11	9.81979	16	0.18021	9.92141	5	56	3 1.5
44 45	9.74120	12	9.81979	17	0.18004	9.92141	5	55	4 2.0
46	9.74143	11	9.82012	16	0.17988	9.92131	5	54	5 2.5
47	9.74155	12	9.82029	17	0.17971	9.92126	5	53	6 3.0 7 3.5
48	9.74166	11	9.82045	16	0.17955	9.92121	5	52	8 4.0
49	9.74177	11	9.82062	17	0.17938	9.92116	5	51	9 4.5
50	9.74189	12	9.82078	16	0.17922	9.92111	5	50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.	ا ا	P. P.
<u> </u>		u.		u. c.	1 au	OIII	· · · ·	·	

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.74189	11	9.82078	17	0.17922	9.92111		50	
51	9.74200		9.82095		0.17905	9.92106	5	49	17_
52	9.74212	12 11	9.82111	16	0.17889	9.92101	5	48	
53	9.74223	11	9.82128	17 16	0.17872	9.92096	5 5	47	1 1.7
54	9.74235		9.82144		0.17856	9.92091		46	3 5.1 4 6.8
55	9.74246	II 12	9.82161	17 16	0.17839	9.92086	5	45	4 6.8
56	9.74258	II	9.82177	17	0.17823	9.92081	5 6	44	5 8.5 6 10.2
57	9.74269		9.82194		0.17806	9.92075		43	7 II.9 8 I3.6
58	9.74280	11 12	9.82210	16 16	0.17790	9.92070	5	42	
59	9.74292	II	9.82226	17	0.17774	9.92065	5 5	4 I	9 15.3
60	9.74303	12	9.82243	16	0.17757	9.92060	5	40	
61	9.74315	11	9.82259	17	0.17741	9.92055	5	39	16
62	9.74326	II	9.82276	16	0.17724	9.92050	5	38	1 1.6
63	9.74337	12	9.82292	17	0.17708	9.92045	5	37	2 3.2 3 4.8
64	9.74349	11	9.82309	16	0.17691	9.92040	5	36	4 6.4
65	9.74360	12	9.82325	16	0.17675	9.92035	5	35	5 8.0
66	9.74372	11	9.82341	17	0.17659	9.92030	5	34	6 9.6
67	9.74383	II	9.82358	16	0.17642	9.92025	5	33	7 II.2 8 I2.8
68	9.74394	12	9.82374	17	0.17626	9.92020	5	32	9 14.4
69	9.74406	II	9.82391	16	0.17609	9.92015	5	31	
70	9.74417	11	9.82407	17	0.17593	9.92010	5	30	
71	9.74428	12	9.82424	16	0.17576	9.92005	5	29	12
72	9.74440	II	9.82440	16	0.17560	9.92000	5	28	1 1.2
73	9.74451	12	9.82456	17	0.17544	9.91995	5	27	2 2.4
74	9.74463	11	9.82473	16	0.17527	9.91990	5	26	3 3.6 4 4.8
75	9.74474	II	9.82489	17	0.17511	9.91985	5	25	4 4.8 5 6.0
76	9.74485	12	9.82506	16	0.17494	9.91980	5	24	6 7.2
77	9 74497	11	9.82522	16	0.17478	9.91975	6	23	7 8.4 8 9.6
78 70	9.74508	II	9.82538	17	0.17462	9.91969	5	22 2I	9 10.8
79	9.74519	12	9.82555	16	0.17445		5		• 1
80	9.74531	11	9.82571	17	0.17429	9.91959	5	20	11
81	9.74542	11	9.82588	16	0.17412	9.91954	5	19	1 1.1
82	9.74553	12	9.82604 9.82620	16	0.17396	9.91949	5		2 2.2
83	9.74565	11	1 *	17	0.17380	9.91944	5	17 16	3 3.3
84	9.74576	11	9.82637 9.82653	16	0.17363	9.91939	5	15	4 4.4
85 86	9.74587 9.74598	11	9.82670	17	0.17347 0.17330	9.91934	5	15	5 5.5 6 6.6
87		12	9.82686	16			5		7 7.7
87 88	9.74610 9.74621	11	9.82080	16	0.17314	9.91924	5	13 12	8 8.8 9 9.9
89	9.74632	11	9.82702	17	0.17298	9.91919	5	II	9 1 9.9
90	9.74644	12	9.82735	16	0.17265	9.91908	6	10	
91	9.74655	11	9.82751	16	0.17249	9.91903	5	09	6
91	9.74666	11	9.82768	17	0.17232	9.91903	5	08	1 0.6
93	9.74677	11	9.82784	16	0.17216	9.91893	5	07	1 0.0 2 1.2
94	9.74689	12	9.82801	17	0.17199	9.91888	5	06	3 1.8
94	9.74700	11	9.82817	16	0.17163	9.91883	5	05	4 2.4
96	9.74711	11	9.82833	16	0.17167	9.91878	5	04	5 3.0 6 3.6
97	9.74722	11	9.82850	17	0.17150	9.91873	5	03	7 4.2
98	9.74734	12	9.82866	16	0.17134	9.91868	5	02	
99	9.74745	11	9.82882	16	0.17118	9.91863	5	10	9 5.4
100	9.74756	II	9.82899	17	0.17101	9.91857	0	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
								ECO	

34°								140	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.74756	11	9.82899	16	0.17101	9.91857	5	100	
01	9.74767		9.82915	16	0.17085	9.91852		99	17
02	9.74779	12 11	9.82931	17	0.17069	9.91847	5 5	98	1 1.7
03	9.74790	II	9.82948	16	0.17052	9.91842	5	97	2 3.4
04	9.74801		9.82964	16	0.17036	9.91837		96	3 5.1
05	9.74812	11 12	9.82980	17	0.17020	9.91832	5 5	95	
06	9.74824	11	9.82997	16	0.17003	9.91827	5	94	5 8.5 6 10.2
07	9.74835		9.83013		0.16987	9.91822	6	93	7 11.9 8 13.6
o8	9.74846	II II	9.83029	16	0.16971	9.91816		92	
09	9.74857	II	9.83046	17 16	0.16954	9.91811	5 5	91	9 15.3
10	9.74868	-	9.83062		0.16938	9.91806		90	
11	9.74880	12	9.83078	16	0.16922	9.91801	5	89	16
12	9.74891	11	9.83095	17	0.16905	9.91796	5	88	1 1.6
13	9.74902	11	9.83111	16	0.16889	9.91791	5	87	2 3.2
14	9.74913	11	9.83127	16	0.16873	9.91786	5	86	3 4.8 4 6.4
15	9.74924	11	9.83144	17	0.16856	9.91781	5	85	4 6.4 5 8.0
16	9.74935	II	9.83160	16	0.16840	9.91775	6	84	6 9.6
17	9.74947	12	9.83176	16	0.16824	9.91770	5	83	7 II.2 8 I2.8
18	9.74947	II	9.83170	17	0.16807	9.91765	5	82	
19	9.74969	11	9.83209	16	0.16791	9.91760	5	81	9 14.4
20		11	9.83225	16	0.16775	9.91755	5	80	l
	9.74980	11		17			5	1	
21	9.74991	11	9.83242	16	0.16758 0.16742	9.91750	6	79 78	12
22	9.75002	12	9.83258	16	0.16742	9.91744 9.91739	5	70	I I.2
23	9.75014	11	9.83274	16	1 1		5		2 2.4 3 3.6
24	9.75025	11	9.83290	17	0.16710	9.91734	5	76	3 3.6
25	9.75036	11	9.83307	16	0.16693	9.91729	5	75	5 6.0
26	9.75047	11	9.83323	16	0.16677	9.91724	5	74	6 7.2 7 8.4
27	9.75058	11	9.83339	17	0.16661	9.91719	5	73	7 8.4 8 9.6
28	9.75069	11	9.83356	16	0.16644	9.91714	6	72	9 10.8
29	9.75080	11	9.83372	16	0.16628	9.91708	5	71	* '
30	9.75091	12	9.83388	17	0.16612	9.91703	5	70	11
31	9.75103	II	9.83405	16	0.16595	9.91698	5	69	
32	9.75114	II	9.83421	16	0.16579	9.91693	5	68	I I.I 2 2.2
33	9.75125	11	9.83437	16	0.16563	9.91688	6	67	3 3.3
34	9.75136	11	9.83453	1	0.16547	9.91682	5	66	4 4.4
35	9.75147	11	9.83470	17	0.16530	9.91677	5	65	5 5.5 6 6.6
36	9.75158	11	9.83486	16	0.16514	9.91672	5	64	7 7.7
37	9.75169		9.83502	16	0.16498	9.91667	5	63	7 7.7 8 8.8
38	9.75180	II II	9.83518	17	0.16482	9.91662	5	62	9 9.9
39	9.75191	II	9.83535	16	0.16465	9.91657	5 6	61	Ì
40	9.75202		9.83551	16	0.16449	9.91651		60	1
41	9.75213	11	9.83567	1	0.16433	9.91646	5	59	5
42	9.75224	11	9.83583	16	0.16417	9.91641	5	58	1 0.5
43	9.75236	12	9.83600	17	0.16400	9.91636	5 5	57	2 I.O
44	9.75247	11	9.83616	16	0.16384	9.91631		56	3 1.5
45	9.75258	II	9.83632	16	0.16368	9.91625	6	55	4 2.0
46	9.75269	11	9.83648	16	0.16352	9.91620	5	54	5 2.5 6 3.0
47	9.75280	II	9.83665	17	0.16335	9.91615	5	53	7 3.5
48	9.75291	11	9.83681	16	0.16319	9.91610	5	52	
49	9.75302	11	9.83697	16	0.16303	9.91605	5	51	9 4.5
50	9.75313	11	9.83713	16	0.16287	9.91599	6	50	
<u> </u>	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
	Cos	· u.		u. c.	, Ian	- 5111	ı u.		1.1.

	Sin	d.	1 Tan	d. c.	Cot	Cos	d.	1	P. P.
50	9.75313		9.83713		0.16287	9.91599		50	
51	9.75324	II	9.83730	17	0.16270	9.91594	5	49	
52	9.75335	II	9.83746	16	0.16254	9.91589	5	48	17
53	9.75346	II	9.83762	16	0.16238	9.91584	5	47	I I 7\ 2 3.4
54	9.75357	11	9.83778	16	0.16222	9.91579	5	46	
55	9.75368	11	9.83795	17	0.16205	9.91573	6	45	4 6.8
56	9.75379	II	9.83811	16 16	0.16189	9.91568	5	44	5 8.5 6 IC.2
57	9.75390	l	9.83827	Į.	0.16173	9.91563	5	43	6 IC.2
58	9.75401	II	9.83843	16 16	0.16157	9.91558	5	42	7 II.9 8 I3.6
59	9.75412	11	9.83859	17	0.16141	9.91552	6 5	41	9 15.3
60	9.75423	II	9.83876	16	0.16124	9.91547	5	40	
61	9.75434	II	9.83892	16	0.16108	9.91542	l	39	16
62	9.75445	11	9.83908	16	0.16092	9.91537	5	38	1 1.6
63	9.75456	11	9.83924	17	0.16076	9.91531	5	37	2 3.2 3 4.8
64	9.75467	11	9.83941	16	0.16059	9.91526	5	36	4 6.4
65	9.75478	II	9.83957	16	0.16043	9.91521	5	35	5 8.0
66	9.75489	II	9.83973	16	0.16027	9.91516	5	34	6 9.6 7 II.2
67	9.75500	11	9.83989	16	0.16011	9.91511	6	33	7 II.2 8 I2.8
68 60	9.75511	II	9.84005	17	0.15995	9.91505	5	32	9 14.4
69	9.75522	11	9.84022	16	0.15978	9.91500	5	31	
70	9.75533	11	9.84038	16	0.15962	9.91495	5	30	
71	9.75544	10	9.84054	16	0.15946	9.91490	6	29	11
72	9.75554	II	9.84070	16	0.15930	9.91484	5	28	I I.I
73	9.75565	II	9.84086	17	0.15914	9.91479	5	27	2 2.2
74	9.75576	II	9.84103	16	0.15897	9.91474	5	26	3 3.3 4 4.4
75 76	9.75587	II	9.84119 9.84135	16	0.15881 0.15865	9.91469	6	25	5 5.5 6 6.6
	9.75598	II		16		9.91463	5	24	5 5.5 6 6.6
77 78	9.75609 9.75620	II	9.84151 9.84167	16	0.15849 0.15833	9.91458	5	23 22	7 7.7 8 8.8
79	9.75631	II	9.84183	16	0.15817	9.91453 9.91447	6	21	9 9.9
80	9.75642	11	9.84200	17	0.15800	9.91442	5	20	
81		II	9.84216	16			5		10
82	9.75653 9.75664	II	9.84232	16	0.15784 0.15768	9.91437 9.91432	5	19 18	I 1 I.O
83	9.75675	II	9.84248	16	0.15752	9.91432	6	17	2 2.0
84	9.75685	10	9.84264	16	0.15736	9.91421	5	16	3 3.0
85	9.75696	11	9.84280	16	0.15720	9.91421	5	15	4 4.0 5 5.0
86	9.75707	11	9.84297	17	0.15703	9.91411	5 6	14	6 6.0
87	9.75718	11	9.84313	16	0.15687	9.91405		13	7 7.0 8 8.0
88	9.75729	II	9.84329	16	0.15671	9.91400	5	12	8 8.0 9 9.0
89	9.75740	11	9.84345	16	0.15655	9.91395	5 6	11	5 3. ♥
90	9.75751	11	9.84361	16	0.15639	9.91389		10	
91	9.75762	11	9.84377	i	0.15623	9.91384	5	09	6
92	9.75772	10 11	9.84394	17 16	0.15606	9.91379	5	∘8	I 0.6
93	9.75783	II	9.84410	16	0.15590	9.91374	5	07	2 1.2
94	9.75794	11	9.84426	16	0.15574	9.91368	5	06	3 1.8
95	9.75805	II	9.84442	16	0.15558	9.91363	5	05	4 2.4 5 3.0
96	9.75816	II	9.84458	16	0.15542	9.91358	6	04	6 3.6
97	9.75827	10	9.84474	16	0.15526	9.91352	5	03	7 4.2 8 4.8
9 8 99	9.75837 9.75848	11	9.84490 9.84507	17	0.15510	9.91347	5	02 01	9 5.4
100		11		16	0.15493	9.91342	6	00	
100	9.75859 Cos	d.	9.84523 Cot	d. c.	0.15477 Tan	9.91336 Sin	d.		- D D
	Cos	α.	LOT	u.c.	ıan	Sin	a.		P. P.

_	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.75859	<u> </u>	9.84523		0.15477	9.91336		100	
		11		16	0.15461	9.91331	5	99	
0I 02	9.75870 9.75881	11	9.84539 9.84555	16	0.15445	9.91331	5	98	17
03	9.75892	11	9.84571	16	0.15429	9.91321	5	97	I I.7
		10	9.84587	16	0.15413	9.91315	6	96	2 3.4 3 5.1
04	9.75902	11	9.84603	16	0.15413	9.91315	5	95	3 5.I 4 6.8
05 06	9.75913 9.75924	11	9.84619	16	0.15381	9.91310	5	93	5 8.5
07		11	9.84636	17	0.15364	9.91299	6	93	6 10.2
07	9.75935 9.75946	11	9.84652	16	0.15348	9.91299	5	93	7 II.9 8 I3.6
09	9.75956	10	9.84668	16	0.15332	9.91294	5	91	9 15.3
10	9.75967	11	9.84684	16	0.15316	9.91283	6	90	
		11		16			5		16
II	9.75978	11	9.84700 9.84716	16	0.15300	9.91278 9.91273	5	89 88	1 1.6
12 13	9.75989 9.76000	11	9.84732	16	0.15268	9.91273	6	87	2 32
		10	-	16	1 - 1		5	86	3 4.8
14	9.76010 9.76021	11	9.84748 9.84764	16	0.15252 0.15236	9.91262 9.91257	5	85 85	4 0.4
15 16	9.76032	11	9.84781	17	0.15230	9.91257	6	8 ₄	5 8.0 6 9.6
		II	9.84797	16	0.15219		5	83	7 11.2
17 18	9.76043 9.76053	10	9.84813	16	0.15203	9.91246 9.91241	5	82	
19	9.76064	II	9.84829	16	0.15171	9.91241	6	81	9 14.4
20		11	9.84845	16			5	80	İ
	9.76075	II		16	0.15155	9.91230	5		
21	9.76086	10	9.84861	16	0.15139	9.91225	6	79	11
22	9.76096	11	9.84877 9.84893	16	0.15123	9.91219	5	78	I I.I
23	9.76107	11		16		9.91214	5	77	2 2.2
24	9.76118	11	9.84909	16	0.15091	9.91209	6	76	3 3.3 4 4.4
25 26	9.76129	10	9.84925	16	0.15075	9.91203	5	75	3 3.3 4 4.4 5 5.5 6 6.6
	9.76139	11	9.84941	17	0.15059	9.91198	6	74	6 6.6
27	9.76150	11	9.84958	16	0.15042	9.91192	5	73	7 7.7 8 8.8
28	9.76161	10	9.84974	16	0.15026	9.91187 9.91182	5	72	9 9.9
29	9.76171	11	9.84990	16			6	71	
30	9.76182	11	9.85006	16	0.14994	9.91176	5	70	10
31	9.76193	10	9.85022	16	0.14978	9.91171		69	1 1.0
32	9.76203	11	9.85038	16	0.14962	9.91166	5 6	68	2 2.0
33	9.76214	11	9.85054	16	0.14946	9.91160	5	67	3 3.0
34	9.76225	11	9.85070	16	0.14930	9.91155	6	66	4 4.0
35 36	9.76236 9.76246	10	9.85086 9.85102	16	0.14914	9.91149 9.91144	5	65 64	4 4.0 5 5.0 6 6.0
		II		16			5		7 7.0 8 8.0
37	9.76257	11	9.85118	16	0.14882 0.14866	9.91139	6	63 62	
38 39	9.76268 9.76278	10	9.85134	16	0.14850	9.91133 9.91128	5	61	9 9.0
40		II		16			5	60	
	9.76289	11	9.85166	16	0.14834	9.91123	6		
41	9.76300	10	9.85182	16	0.14818	9.91117	5	59	5
42	9.76310 9.76321	11	9.85198 9.85215	17	0.14802 0.14785	9.91112	6	58	I 0.5
43		11		16		9.91106	5	57	2 I.0 3 I.5
44	9.76332	10	9.85231	16	0.14769	9.91101	5	56	
45 46	9.76342 9.76353	II	9.85247 9.85263	16	0.14753 0.14737	9.91096 9.91090	6	55	5 2.5
	-	11		16			5	54	
47 48	9.76364 9.76374	10	9.85279 9.85295	16	0.14721	9.91085 9.91079	6	53 52	7 3.5 8 4.0
40 49	9.76374	11	9.85311	16	0.14705	9.91079	5	52 51	9 4.5
50		10	9.85327	16	0.14673		5	50	
- 50	9.76395	d.	Cot	-	Tan	9.91069			
	Cos	· a.	COT	d.c.	lan	Sin	đ.		P. P.

				d					
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.76395	11	9.85327	16	0.14673	9.91069	6	50	
51	9.76406		9.85343	16	0.14657	9.91063		49	16
52	9.76417	II IO	9.85359	16	0.14641	9.91058	5 6	48	1 1.6
53	9.76427	11	9.85375	16	0.14625	9.91052	5	47	2 3.2
54	9.76438		9.85391	16	0.14609	9.91047		46	3 4.8
55	9.76448	10	9.85407	16	0.14593	9.91042	5 6	45	4 6.4 5 8.0
56	9.76459	11	9.85423	16	0.14577	9.91036	5	44	5 8.0 6 9.6
57	9.76470	10	9.85439	16	0.14561	9.91031	6	43	7 11.2
58	9.76480	II	9.85455	16	0.14545	9.91025	5	42	
59	9.76491	10	9.85471	16	0.14529	9.91020	6	41	9 14.4
60	9.76501	II	9.85487	16	0.14513	9.91014	5	40	
61	9.76512		9.85503	16	0.14497	9.91009		39	15
62	9.76523	II	9.85519	16	0.14481	9.91004	5	38	I I.5
63	9.76533	II	9.85535	16	0.14465	9.90998	5	37	2 3.0 3 4.5
64	9.76544		9.85551	16	0.14449	9.90993	6	36	4 6.0
65	9.76554	IO II	9.85567	16	0.14433	9.90987	5	35	5 7.5
66	9.76565	10	9.85583	16	0.14417	9.90982	6	34	6 9.0
67	9.76575	11	9.85599	16	0.14401	9.90976	5	33	7 IO.5 8 I2.0
68	9.76586	11	9.85615	16	0.14385	9.90971	5	32	9 13.5
69	9.76597	10	9.85631	16	0.14369	9.90966	6	31	
70	9.76607	II	9.85647	16	0.14353	9.90960	5	30	
71	9.76618		9.85663		0.14337	9.90955	6	29	11
72	9.76628	IO	9.85679	16 16	0.14321	9.90949		28	1 1.1
73	9.76639	11 10	9.85695	16	0.14305	9.90944	5 6	27	2 2.2
74	9.76649		9.85711		0.14289	9.90938		26	3 3.3
75	9.76660	II	9.85727	16 16	0.14273	9.90933	5 6	25	4 4.4
76	9.76670	IO II	9.85743	16	0.14257	9.90927	5	24	5 5.5 6 6.6
77	9.76681		9.85759		0.14241	9.90922	6	23	7 7.7 8 8.8
78	9.76691	10	9.85775	16 16	0.14225	9.90916	1	22	8 8.8 9.9
79	9.76702	11	9.85791	16	0.14209	9.90911	5	21	9 9.9
80	9.76712	11	9.85807	16	0.14193	9.90906	6	20	
81	9.76723		9.85823		0.14177	9.90900		19	10
82	9.76733	10	9.85839	16	0.14161	9.90895	5	18	I I.0
83	9.76744	II	9.85855	16 16	0.14145	9.90889	6 5	17	2 2.0 3.0
84	9.76754		9.85871		0.14129	9.90884	6	16	4 4.0
85	9.76765	II	9.85887	16	0.14113	9.90878		15	5 5.0 6 6.0
86	9.76775	IO II	9.85903	16 16	0.14097	9.90873	5 6	14	0 0.0
87	9.76786		9.85919		0.14081	9.90867		13	7 7.0 8 8.0
88	9.76796	10	9.85935	16 16	0.14065	9.90862	5 6	12	9 9.0
89	9.76807	10	9.85951	16	0.14049	9.90856	5	11	
90	9.76817	11	9.85967	16	0.14033	9.90851	6	10	
91	9.76828		9.85983		0.14017	9.90845		09	6
92	9.76838	10	9.85999	16	0.14001	9.90840	5 6	08	1 0.6
93	9.76849	11	9.86014	15 16	0.13986	9.90834	5	07	2 1.2
94	9.76859		9.86030		0.13970	9.90829	6	06	3 1.8
95	9.76870	II	9.86046	16	0.13954	9.90823		05	4 2.4 5 3.0
96	9.76880	IO II	9.86062	16 16	0.13938	9.90818	5 6	04	5 3.0 6 3.6
97	9.76891		9.86078	}	0.13922	9.90812		03	7 4.2
98	9.76901	10	9.86094	16	0.13906	9.90807	5 6	02	
99	9.76911	10	9.86110	16 16	0.13890	9.90801	5	10	9 5.4
100	9.76922	11	9.86126	10	0.13874	9.90796	3	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
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	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.76922		9.86126	16	0.13874	9.90796	6	100	
OI	9.76932	10	9.86142	16	0.13858	9.90790		99	16
02	9.76943	11	9.86158	16	0.13842	9.90785	5	98	
03	9.76953	II	9.86174	16	0.13826	9.90779	5	97	1 1.6
04	9.76964	10	9.86190	16	0.13810	9.90774	6	96	3 4.8
05	9.76974	10	9.86206	16	0.13794	9.90768	5	95	4 6.4 5 8.0
06	9.76984	11	9.86222	16	0.13778	9.90763	6	94	5 8.0 6 9.6
07	9.76995	10	9.86238	16	0.13762	9.90757	5	93	7 11.2
08	9.77005	11	9.86254	15	0.13746	9.90752	6	92	8 12.8 9 14.4
09	9.77016	10	9.86269	16	0.13731	9.90746	5	91	9 14.4
10	9.77026	10	9.86285	16	0.13715	9.90741	6	90	4-
11	9.77036	11	9.86301	16	0.13699	9.90735	5	89	15
12	9.77047	10	9.86317	16	0.13683 0.13667	9.90730	6	88 87	I I.5 2 3.0
13	9.77057	11	9.86333	16		9.90724	6		3 4.5
14	9.77068	10	9.86349 9.86365	16	0.13651	9.90718 9.90713	5	86 85	4 6.0
15 16	9.77078 9.77088	10	9.86381	16	0.13035	9.90713	5 6	84	5 7.5 6 9.0
		11		16	1	9.90702	5	83	7 10.5
17 18	9.77099 9.77109	10	9.86397 9.86413	16	0.13603	9.90702	6	82	8 12.0
19	9.77119	10	9.86429	16	0.13571	9.90691	5	81	9 13.5
20	9.77130	11	9.86445	16	0.13555	9.90685	6	80	
		10	9.86460	15	0.13540	9.90680	5	79	
2I 22	9.77140	10	9.86476	16	0.13540	9.90674	6	78	11
23	9.77161	11	9.86492	16	0.13508	9.90669	5	77	I I.I 2 2.2
24	9.77171	10	9.86508	16	0.13492	9.90663	6	76	3 3.3
25	9.77181	10	9.86524	16	0.13476	9.90657	6	75	4 4.4
26	9.77192	11	9.86540	16	0.13460	9.90652	5	74	5 5.5 6 6.6
27	9.77202	10	9.86556	16	0.13444	9.90646	6	73	7 7.7 8 8.8
28	9.77212	10	9.86572	16	0.13428	9.90641	5	72	8 8.8
29	9.77223	11	9.86588	16 15	0.13412	9.90635	6	71	9 9.9
80	9.77233	l .	9.86603		0.13397	9.90630	5 6	70	
31	9.77243	10	9.86619	16	0.13381	9.90624		69	10
32	9.77254	II	9.86635	16	0.13365	9.90618	6	68	I I.O
33	9.77264	10	9.86651	16 16	0.13349	9.90613	5	67	2 2.0 3 3.0
34	9.77274	1	9.86667	16	0.13333	9.90607	ł	66	4 4.0
35	9.77285	11	9.86683	16	0.13317	9.90602	5	65	5 5.0 6 6.0
36	9.77295	10	9.86699	16	0.13301	9.90596	5	64	7 7.0
37	9.77305	11	9.86715	16	0.13285	9.90591	6	63	7 7.0 8 8.0
38	9.77316	10	9.86731	15	0.13269	9.90585	6	62	9 9.0
39	9.77326	10	9.86746	16	0.13254	9.90579	5	61	l
40	9.77336	10	9.86762	16	0.13238	9.90574	6	60	i -
41	9.77346	II	9.86778	16	0.13222	9.90568	5	59	5
42	9.77357	10	9.86794	16	0.13206	9.90563	6	58	1 0.5
43	9.77367	10	9.86810	16	0.13190	9.90557	6	57	3 1.5
44	9.77377	10	9.86826	16	0.13174	9.90551	5	56	4 2.0
45	9.77387	11	9.86842	15	0.13158	9.90546	6	55 54	5 2.5 6 3.0
46	9.77398	10		16	0.13143	9.90540	5		7 3.5
47	9.77408	10	9.86873 9.86889	16	0.13127	9.90535 9.90529	6	53 52	8 4.0
48 49	9.77418 9.77429	II	9.86905	16	0.13111	9.90529	6	51	9 4.5
50		10	9.86921	16	0.13079	9.90518	5	50	1
	9·77439 Cos	d.	Cot	d. c.	Tan	Sin	d.	التي	P. P.
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	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.77439	10	9.86921	16	0.13079	9.90518	6	50	
31	9.77449	10	9.86937	16	0.13063	9.90512	5	49	16
52	9.77459	10	9.86953	15	0.13047	9.90507	6	48	1 1.6
53	9.77469	II	9.86968	16	0.13032	9 90501	6	47	2 3.2
54	9.77480	10	9.86984	16	0.13016	9.90495	5	46	3 4.8
55	9.77490	10	9.87000	16	0.13000	9.90490		45	4 6.4 5 8.0
56	9.77500	10	9.87016	16	0.12984	9.90484	6	44	5 8.0 6 9.6
57	9.77510	11	9.87032	16	0.12968	9.90479	5 6	43	7 II.2 8 I2.8
58	9.77521	10	9.87048	15	0.12952	9.90473	6	42	
59	9.77531	10	9.87063	16	0.12937	9.90467		41	9 14.4
60'	9.77541	10	9 87079	16	0.12921	9.90462	5 6	40	
61	9.77551		9.87095		0.12905	9.90456		39	15
62	9.77561	10	9.87111	16 16	0.12889	9.90450	6	38	1 1.5
63	9.77572	10	9.87127	16	0.12873	9.90445	5 6	37	2 3.0
64	9.77582		9.87143		0.12857	9.90439	1	36	3 4.5 4 6.0
65	9.77592	10	9.87158	15 16	0.12842	9.90434	5 6	35	
66	9.77602	10	9.87174	16	0.12826	9.90428	6	34	6 9.0
67	9.77612		9.87190	1	0.12810	9.90422	l	33	7 10.5 8 12.0
68	9.77623	11	9.87206	16 16	0.12794	9.90417	5 6	32	8 12.0 9 13.5
69	9.77633	10	9.87222	16	0.12778	9.90411	6	31	9 20.0
70	9.77643	1	9.87238	}	0.12762	9.90405	ŀ	30	•
71	9.77653	10	9.87253	15	0.12747	9.90100	5	29	11
72	9.77663	10	9.87269	16	0.12731	9.90394	6	28	
73	9.77673	10	9.87285	16	0.12715	9.90388	6	27	I I.I 2 2.2
74	9.77684	11	9.87301	16	0.12699	9.90383	5	26	3 3.3
75	9.77694	10	9.87317	16	0.12683	9.90377	6	25	4 4.4
76	9.77704	10	9.87332	15	0.12668	9.90371	6	24	5 5.5 6 6.6
77	9.77714	10	9.87348	16	0.12652	9.90366	5	23	7 7.7
78	9.77724	10	9.87364	16	0.12636	9.90360	6	22	7 7.7 8 8.8
79	9.77734	10	9.87380	16	0.12620	9.90354	6	21	9 9.9
80	9.77744	10	9.87396	16	0.12604	9.90349	5	20	
81		11	9.87412	16	0.12588	9.90343	6	19	10
82	9.77755 9.77765	10	9.87427	15	0.12573	9.90343	6	18	1 1.0
83	9.77775	10	9.87443	16	0.12557	9.90332	5	17	2 2.0
84	•	10	9.87459	16	0.12541	9.90326	6	16	3 3.0 4 4.0
85	9.77785 9.77795	10	9.87475	16	0.12525	9.90320	6	15	4 4.0
86	9.77805	10	9.87490	15	0.12510	9.90320	5	14	5 5.0 6 6.0
87	9.77815	10	9.87506	16	0.12494	9.90309	6		7 7.0 8 8.0
88	9.77825	10	9.87522	16	0.12494	9.90309	6	13 12	9 9.0
89	9.77835	10	9.87538	16	0.12462	9.90303	5	111	9 9.0
90	1	11	9.87554	16	0.12446		6	10	
1	9.77846	10		15		9.90292	6		6
91	9.77856	10	9.87569	16	0.12431	9.90286	6	09 08	
92 93	9.77866 9.77876	10	9.87585 9.87601	16	0.12415	9.90280 9.90275	5	07	I 0.6 2 I.2
		10	-	16			6		3 1.8
94	9.77886	10	9.87617	16	0.12383	9.90269	6	06	4 2.4
95 96	9.77896 9.77906	10	9.87648	15	0.12367	9.90263 9.90258	5	05 04	5 3.0 6 3.6
		10		16			6	1 '	7 12
97	9.77916	10	9.87664	16	0.12336	9.90252	6	03	8 4.8
98 99	9.77926	10	9.87680 9.87696	16	0.12320 0.12304	9.90246	5	02 01	9 5.4
	9.77936	10		15			6	00	
100	9.77946		9.87711		0.12289	9.90235	_	<u> </u>	I———
	Cos	d.	Cot	d.c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.77946		9.87711		0.12289	9.90235		100	
		10	9.87727	16	0.12273	9.90229	6	99	
01 02	9.77956 9.77966	10	9.87743	16	0.12273	9.90229	6	98	16
03	9.77976	10	9.87759	16	0.12241	9.90218	5	97	1 1.6
-		11	9.87775	16	0.12225	9.90212	6	96	2 3.2
04 05	9.77987	10	9.87790	15	0.12225	9.90212	6	95	3 4.8 4 6.4
06	9.78007	10	9.87806	16	0.12194	9.90201	5	94	5 8.0
07	9.78017	10	9.87822	16	0.12178	9.90195	6	93	5 8.0 6 9.6
07	9.78017	10	9.87838	16	0.12170	9.90193	6	93	7 II.2 8 I2.8
09	9.78027	10	9.87853	15	0.12147	9.90183	6	91	9 14.4
		10	9.87869	16	0.12131	9.90178	5	90	9 (-4.4
10	9.78047	10		16			6		
11	9.78057	10	9.87885	16	0.12115	9.90172	6	89 88	15
12	9.78067	10	9.87901	15	0.12099	9.90166	6	87	I 1.5 2 3.0
13	9.78077	10	9.87916	16		1 1	5		2 3.0 3 4.5
14	9.78087	10	9.87932	16	0.12068 0.12052	9.90155	6	86 85	4 6.0
15 16	9.78097	10	9.87948	16	0.12032	9.90149	6	84	5 7.5
	9.78107	10	9.87964	15			6		6 9.0 7 10.5
17	9.78117	10	9.87979	16	0.12021	9.90137	5	83 82	7 10.5 8 12.0
18	9.78127	10	9.87995 9.88011	16	0.12005	9.90132 9.90126	6	81	9 13.5
19	9.78137	10		16			6		
20	9.78147	10	9.88027	15	0.11973	9.90120	6	80	
21	9.78157	10	9.88042	16	0.11958	9.90114	5	79	11
22	9.78167	10	9.88058	16	0.11942	9.90109	6	78	1 1.1
23	9.78177	10	9.88074	15	0.11926	9.90103	6	77	2 2.2
24	9.78187	10	9.88089	16	0.11911	9.90097	6	76	3 3.3
25	9.78197	10	9.88105	16	0.11895	9.90091	5	75	4 4.4
26	9.78207	10	9.88121	16	0.11879	9.90086	6	74	5 5.5 6 6.6
27	9.78217	10	9.88137	15	0.11863	9.90980	6	73	7 7.7 8 8.8
28	9.78227	9	9.88152	16	0.11848	9.90074	6	72	8 8.8
29	9.78236	10	9.88168	16	0.11832	9.90068	5	71	9 9.9
30	9.78246	10	9.88184	16	0.11816	9.90063	6	70	
31	9.78256	10	9.88200	15	0.11800	9.90057	6	69	9
32	9.78266	10	9.88215	16	0.11785	9.90051	6	68	I 0.9
33	9.78276	10	9.88231	16	0.11769	9.90045	6	67	2 I.8 3 2.7
34	9.78286	10	9.88247	1	0.11753	9.90039	1	66	4 3.6
35	9.78296	10	9.88262	15 16	0.11738	9.90034	5	65	5 4.5
36	9.78306	10	9.88278	16	0.11722	9.90028	6	64	6 5.4 7 6.3
37	9.78316	10	9.88294	16	0.11706	9.90022	6	63	7 6.3 8 7.2
38	9.78326	10	9.88310	15	0.11690	9.90016	5	62	8 7.2 9 8.1
39	9.78336	10	9.88325	16	0.11675	9.90011	6	61	
40	9.78346	10	9.88341	16	0.11659	9.90005	6	60	
41	9.78356	1	9.88357	1	0.11643	9.89999	1	59	5
42	9.78366	10	9.88372	15	0.11628	9.89993	6	58	1 0.5
43	9.78375	9	9.88388	16 16	0.11612	9.89987	5	57	2 I.O
44	9.78385		9.88404	1	0.11596	9.89982		56	3 1.5 4 2.0
45	9.78395	10	9.88420	16	0.11580	9.89976	6	55	
46	9.78405	10	9.88435	15	0.11565	9.89970	6	54	6 3.0
47	9.78415	}	9.88451	1	0.11549	9.89964	1	53	7 3.5
48	9.78425	10	9.88467	16	0.11533	9.89958	6	52	8 4.0 9 4.5
49	9.78435	10	9.88482	15	0.11518	9.89952	5	51	9 1 4.3
50	9.78445	10	9.88498	10	0.11502	9.89947	3	50	1
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
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	Sın	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.78445	10	9.88498	16	0.11502	9.89947	6	50	
51	9.78455	9	9.88514	15	0.11486	9.89941	6	49	16
52	9.78464	10	9.88529	16	0.11471	9.89935	6	48	1 1.6
53	9.78474	10	9.88545	16	0 11455	9.89929	6	47	2 3.2
54	9.78484	10	9.88561	16	0.11439	9.89923	5	46	3 4.8 4 6.4
55 56	9.78494 9.78504	10	9.88577 9.88592	15	0.11423	9.89918 9.89912	6	45 44	5 8.0
-	9.78514	10	9.88608	16	0.11392	9.89906	6	1	
57 58	9.78524	10	9.88624	16	0.11392	9.89900	6	43	7 11.2 8 12.8
59	9.78533	9	9.88639	15	0.11361	9.89894	6	41	9 14.4
60	9.78543	10	9.88655	16	0.11345	9 89888	6	40	
61	9.78553	10	9.88671	16	0.11329	9.89883	5	39	15
62	9.78563	10	9.88686	15	0.11314	9.89877	6	38	1 1.5
63	9.78573	10	9.88702	16 16	0.11298	9.89871	6	37	2 3.0
64	9.78583		9.88718	1	0.11282	9.89865	6	36	3 4.5 4 6.0
65	9.78592	9	9.88733	15	0.11267	9.89859	6	35	5 7.5
66	9.78602	10	9.88749	16	0.11251	9.89853	6	34	6 9.0
67	9.78612	10	9.88765	15	0.11235	9.89847	5	33	7 10.5 8 12.0
68	9.78622	10	9.88780	16	0.11220	9.89842	6	32	9 13.5
69	9.78632	10	9.88796	16	0.11204	9.89836	6	31	1
70	9.78642	9	9.88812	15	0.11188	9.89830	6	30	l
71	9.78651	10	9.88827	16	0.11173	9.89824	6	29	10
72 73	9.78661 9.78671	10	9.88843 9.88859	16	0.11157	9.89818 9.89812	6	28	I I.O
74	9.78681	10	9.88874	15	0.11126	9.89806	6	26	2 2.0 3.0
74 75	9.78691	10	9.88890	16	0.11110	9.89801	5	25	4 4.0
76	9.78700	9	9.88906	16	0.11094	9.89795	6	24	5 5.0 6 6.0
77	9.78710	10	9.88921	15	0.11079	9.89789	6	23	7 7.0 8 8.0
78	9.78720	10	9.88937	16	0.11063	9.89783	6	22	
79	9.78730	10 9	9.88953	16 15	0.11047	9.89777	6	21	9 9.0
80	9.78739	10	9.88968	16	0.11032	9.89771	6	20	A
81	9.78749		9.88984	16	0.11016	9.89765	6	19	9
82	9.78759	10	9.89000	15	0.11000	9.89759	5	18	I 0.9 2 1.8
83	9.78769	10	9.89015	16	0.10985	9.89754	6	17	3 2.7
84	9.78779	9	9.89031	15	0.10969	9.89748	6	16	4 3.6
85 86	9.78788	10	9.89046 9.89062	16	0.10954	9.89742	6	15	5 4.5 6 5.4
87	9.78798 9.78808	10		16	0.10938	9.89736	6	14	7 6.3
88	9.78818	10	9.89078	15	0.10922	9.89730 9.89724	6	13	8 7.2 9 8.1
89	9.78827	9	9.89109	16	0.10891	9.89718	6	11	9 0.1
90	9.78837	10	9.89125	16	0.10875	9.89712	6	10	
91	9.78847	10	9.89140	15	0.10860	9.89706	6	09	6
92	9.78856	9	9.89156	16	0.10844	9.89701	5	08	110.6
93	9.78866	10	9.89172	16	0.10828	9.89695	6	07	2 1.2
94	9.78876	10	9.89187	15	0.10813	9.89689	6	о6	3 1.8
95	9.78886	10 9	9.89203	16 15	0.10797	9.89683	6	05	4 2.4 5 3.0 6 3.6
96	9.78895	10	9.89218	16	0.10782	9.89677	6	04	6 3.6
97	9.78905	10	9.89234	16	0.10766	9.89671	6	03	7 4.2
98	9.78915	9	9.89250	15	0.10750	9.89665	6	02	8 4.8 9 5.4
99	9.78924	10	9.89265	16	0.10735	9.89659	6	10	3,0.7
100	9.78934		9.89281		0.10719	9.89653		_00_	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

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	Sin	d.	Tan	d.c.	Cot	Cos	d.	1	P. P.
00	9.78934	10	9.89281	16	0.10719	9.89653	6	100	
OI	9 78944	1	9.89297	1	0.10703	9.89647	1	99	16
02	9.78954	10	9.89312	15	0.10688	9.89641	6	98	1 1.6
03	9.78963	9	9.89328	15	0.10672	9.89635	5	97	2 3.2
04	9.78973	1	9.89343	16	0.10657	9.89630	6	96	3 4.8 4 6.4
05	9.78983	10	9.89359	16	0.10641	9.89624	6	95	4 6.4
06	9.78992	9	9.89375	15	0.10625	9.89618	6	94	5 8.0 6 9.6
07	9.79002	1	9.89390	16	0.10610	9.89612	1	93	7 11.2
о8	9.79012	10	9.89406	16	0.10594	9.89606	6	92	8 12.8
09	9.79021	9	9.89422	15	0.10578	9.89600	6	91	9 14.4
10	9.79031	10	9.89437	16	0.10563	9.89594	6	90	
11	9.79041	1	9.89453	1	0.10547	9.89588	1	89	15
12	9.79050	9	9.89468	15 16	0.10532	9.89582	6	88	I 1.5
13	9.79060	10	9.89484	16	0.10516	9.89576	6	87	2 3.0
14	9.79070	i .	9.89500		0.10500	9.89570		86	3 4.5 4 6.0
15	9.79079	9	9.89515	15 16	0.10485	9.89564	6	85	
16	9.79089	10 10	9.89531	15	0.10469	9.89558	6	84	6 9.0
17	9.79099	1	9.89546	l	0.10454	9.89552	l	83	7 10.5 8 12.0
18	9.79108	9	9.89562	16 16	0.10438	9.89546	6	82	8 12.0 9 13.5
19	9.79118	10 10	9.89578	15	0.10422	9.89540	6	81	9 13.3
20	9.79128	į.	9.89593	16	0.10407	9.89534	6	80	
21	9.79137	9	9.89609		0.10391	9.89528	1	79	10
22	9.79147	10	9.89624	15	0.10376	9.89522	6	78	
23	9.79156	9 10	9.89640	16 16	0.10360	9.89516	6	77	I I.0 2 2.0
24	9.79166		9.89656	1	0.10344	9.89510		76	3 3.0
25	9.79176	10	9.89671	15 16	0.10329	9.89504	6	75	4 4.0
26	9.79185	9	9.89687	15	0.10313	9.89499	5 6	74	5 5.0 6 6.0
27	9.79195		9.89702		0.10298	9.89493		73	7 7.0
28	9.79204	9 10	9.89718	16 16	0.10282	9.89487	6	72	8 8.0
29	9.79214	10	9.89734	15	0.10266	9.89481	6	71	9 9.0
30	9.79224		9.89749	16	0.10251	9.89475	6	70	
31	9.79233	9	9.89765		0.10235	9.89469		69	9
32	9.79243	10	9.89780	15	0.10220	9.89463	6	68	1 0.9
33	9.79252	9 10	9.89796	16 15	0.10204	9.89457	6	67	2 1.8
34	9.79262		9.89811	,	0.10189	9.89451		66	3 2.7 4 3.6
35	9.79272	10	9.89827	16 16	0.10173	9.89445	6	65	
36	9.79281	9 10	9.89843	15	0.10157	9.89439	6	64	6 5.4
37	9.79291		9.89858	16	0.10142	9.89433	6	63	7 6.3 8 7.2
38	9.79300	9	9.89874	15	0.10126	9.89427	6	62	9 8.1
3 9	9.79310	9	9.89889	16	0.10111	9.89421	6	61	•
40	9.79319	10	9.89905	15	0.10095	9.89415	6	60	
41	9.79329	10	9.89920	16	0.10080	9.89409	6	59	6
42	9.79339	9	9.89936	16	0.10064	9.89403	6	58	I 0.6
43	9.79348	10	9.89952	15	0.10048	9.89397	6	57	2 1.2
44	9.79358	9	9.89967	16	0.10033	9.89391	6	56	3 1.8
45	9.79367	10	9.89983	15	0.10017	9.89385	6	55	4 2.4 5 3.0 6 3.6
46	9.79377	9	9. 89998	16	0.10002	9.89379	6	54	6 3.6
47	9.79386	10	9 90014	15	0.09986	9.89373	7	53	7 4.2
48	9.79396	9	9.90029	16	0.09971	9.89366	6	52	8 4.8 9 5.4
49	9.79405	10	9.90045	16	0.09955	9.89360	6	51	9 1 3 4
50	9.79415		9.90061		0.09939	9.89354		50	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.79415		9.90061		0.09939	9.89354	6	50	
51	9.79424	9	9.90076	15	0.09924	9.89348		49	16
52	9.79434	10	9.90092	16 15	0.09908	9.89342	6	48	1 1.6
53	9.79444	9	9.90107	16	0.09893	9.89336	6	47	2 3.2
54	9.79453	10	9.90123	15	0.09877	9.89330	6	46	3 4.8
55	9.79463	9	9.90138	16	0.09862	9.89324	6	45	4 6.4 5 8.0
56	9.79472	10	9.90154	15	0.09846	9.89318	6	44	6 9.6
57	9.79482	9	9.90169	16	0.09831	9.89312	6	43	7 II.2 8 I2.8
58	9.79491	10	9.90185	15	0.09815	9.89306	6	42	8 12.8 9 14.4
59 60	9.79501	9	9.90200	16	0.09800	9.89300	6	41	3 24.4
	9.79510	10	9.90216	16	0.09784	9.89294	6	40	15
61 62	9.79520	9	9.90232	15	0.09768	9.89288 9.89282	6	39 38	1 1.5
63	9.79529 9.79539	10	9.90247	16	0.09753	9.89282	6	37	2 3.0
64		9	9.90203	15	0.09722	9.89270	6	36	3 4.5
65	9.79548 9.79558	10	9.90278	16	0.09722	9.89270	6	35	4 6.0 5 7.5 6 9.0
66	9.79567	9	9.90309	15	0.09691	9.89258	6	34	6 9.0
67	9.79576	9	9.90325	16	0.09675	9.89252	6	33	7 10.5
68	9.79586	10	9.90340	15	0.09660	9.89246	6	32	8 12.0 9 13.5
69	9.79595	9	9.90356	16	0.09644	9.89239	7 6	31	91 *3.3
70	9.79605		9 90371	15	0.09629	9.89233	6	30	
71	9.79614	9	9.90387	1	0.09613	9.89227		29	10
72	9.79624	10	9.90403	16	0.09597	9.89221	6	28	1 1.0
73	9.79633	9	9.90418	15 16	0.09582	9.89215	6	27	2 2.0
74	9.79643	9	9.90434	15	0.09566	9.89209	6	26	3 3.0
75	9.79652	10	9.90449	16	0.09551	9.89203	6	25	4 4.0
76	9.79662	9	9.90465	15	0.09535	9.89197	6	24	5 5.0 6 6.0
77	9.79671	9	9.90480	16	0.09520	9.89191	6	23	7 7.0 8 8.0
78	9.79680	10	9.90496	15	0.09504	9.89185 9.89179	6	22	9 9.0
79 80	9.79690	9	9.90511	16			6	20	
	9.79699	10	9.90527	15	0.09473	9.89173	7		9
81 82	9.79709	9	9.90542	16	0.09458	9.89166 9.89160	6	19 18	1 0.9
83	9.79718 9.79728	10	9.90558 9.90573	15	0.09442	9.89154	6	17	2 1.8
84		9	9.90589	16	0.09411	9.89148	6	16	3 2.7 4 3.6
85	9.79737 9.79746	9	9.90509	15	0.09396	9.89148	6	15	4 3.0 5 4.5
86	9.79756	10	9.90620	16	0.09380	9.89136	6	14	6 5.4
87	9.79765	9	9.90635	15	0.09365	9.89130	6	13	7 6.3 8 7.2
88	9.79775	10	9.90651	16	0.09349	9.89124	6	12	8 7.2 9 8.1
89	9.79784	9	9.90666	15	0.09334	9.89118	6	11	1
90	9.79793	10	9.90682		0.09318	9.89112	7	10	1
91	9.79803		9.90697	15	0.09303	9.89105	6	09	7
92	9.79812	9	9.90713	15	0.09287	9.89099	6	08	I 0.7
93	9.79822	9	9.90728	16	0.09272	9.89093	6	07	2 1.4
94	9.79831	9	9.90744	15	0.09256	9.89087	6	06	3 2.I 4 2.8
95	9.79840	10	9.90759	16	0.09241	9.89081	6	05	5 3.5
96	9.79850	9	9.90775	15	0.09225	9.89075	6	04	6 4.2
97	9.79859	9	9.90790	16	0.09210	9.89069	6	03	7 4.9 8 5.6 9 6.3
98 99	9.79868 9.79878	10	9.90806	15	0.09194	9.89063 9.89056	7	02 01	9 6.3
100		9	9.90837	16	0.09179	9.89050	6	00	1
100	9.79887			4 0	Tan	Sin	d.		P. P.
	Cos	l d.	Cot	d. c.	· Ian	1 9111	· u.		r.r.

	0:			-	Car	C 1	a 1		P. P.
	Sin	d.	Tan	d. c.	Cot	Cos	_d.	100	P. P.
00	9.79887	10	9.90837	15	0.09163	9.89050	6		
10	9.79897	9	9.90852	16	0.09148	9.89044	6	99	16
02	9.79906	9	9.90868	15	0.09132	9.89038	6	98	1 1.6
03	9.79915	10	9.90883	16	0.09117	9.89032	6	97	2 .3.2
04	9.79925	9	9.90899	15	0.09101	9.89026	6	96	3 4.8 4 6.4
05	9 79934	9	9.90914	16	0.09086	9.89020 9.89013	7	95 94	5 8.0
06	9.79943	10	9.90930	15	0.09070		6		6 9.6
07	9.79953	9	9.90945	16	0.09055	9.89007	6	93 92	7 II.2 8 I2.8
o8 o9	9.79962	9	9.90961 9.90976	15	0.09039	9.88995	6	91	9 14.4
	9.79971	10		16		9.88989	6	90	
10	9.79981	9	9.90992	15	0.09008		6	1	15
11	9.79990	9	9.91007	16	0.08993	9.88983	7	89 88	1 1.5
12	9.79999	10	9.91023	15	o.08977 o.08962	9.88976 9.88970	6	87	2 3.0
13	9.80009	9	9.91038	16			6	86	3 4.5
14	9.80018	9	9.91054	15	0.08946 0.08931	9.88964 9.88958	6	85	
15 16	9.80027	10	9.91069 9.91085	16	0.08931	9.88952	6	84	5 7.5 6 9.0
	9.80037	9		15	0.08900	9.88946	6	83	7 10.5
17	9.80046	9	9.91100	16	0.08900	9.88940	7	82	
18 19	9.80055 9.80064	9	9.91116	15	0.08869	9.88933	6	81	9 13.5
		10		16	0.08853	9.88927	6	80	
20	9.80074	9	9.91147	15			6		
21	9.80083	9	9.91162	16	0.08838	9.88921	6	79 78	10
22	9.80092	10	9.91178	15	0.08822	9.88909	6	77	I 1.0
23	9.80102	9	9.91193	16			7		2 2.0 3 3.0
24	9.80111	9	9.91209	15	0.08791	9.88902 9.88896	6	76	
25	9.80120	9	9.91224	15	o.08776 o.08761	9.88890	6	75 74	4 4.0 5 5.0 6 6.0
26	9.80129	10	9.91239	16			6		6 6.0
27	9.80139	9	9.91255	15	0.08745	9.88884 9.88878	6	73 72	7 7.0 8 8.0
28 29	9.80148 9.80157	9	9.91270 9.91286	16	0.08730	9.88871	7	71	9 9.0
		9		15	0.08699	9.88865	6	70	
30	9.80166	10	9.91301	16			6		9
31	9.80176	9	9.91317	15	0.08683	9.88859 9.88853	6	69 68	1 0.9
32	9.80185	9	9.91332	16	0.08652	9.88847	6	67	2 1.8
33		10		15	_		7	66	3 2.7 4 3.6
34	9.80204	9	9.91363	16	0.08637	9.88840	6	65	5 4.5
35 36	9.80213	9	9.91379 9.91394	15	0.08606	9.88828	6	64	6 5.4 7 6.3
	9.80222	9		16	0.08590	9.88822	6	63	3 2.7 4 3.6 5 4.5 6 5.4 7 6.3 8 7.2
37	9.80231	9	9.91410	15	0.08575	9.88815	7	62	8 7.2 9 8.1
38 39	9.80240	10	9.91425	16	0.08559	9.88809	6	61	9 0.1
40	9.80259	9	9.91456	15	0.08544	9.88803	6	60	i
3		9		15	0.08529	9.88797	6		
41	9.80268	9	9.91471	. 16	0.08513	9.88791	6	59 58	6
42	9.80277	10	9.91407	15	0.08498	9.88784	7	57	I 0.6 2 I.2
43	1 -	9		16	0.08482	9.88778	6	56	3 1.8
44	9.80296	9	9.91518	15	0.08467	9.88772	6	55	4 2.4
45 46	9.80305	9	9.91533	16	0.08451	9.88766	6	54	5 3.0
	9.80314	9	9.91564	15	0.08436	9.88759	7	53	6 3.6
47 48	9.80323	10	9.91580	16	0.08420	9.88753	6	52	8 4.8
49	9.80333	9	9.91595	15	0.08405	9.88747	6	51	9 5.4
50	9.80351	9	9.91610	- 15	0.08390	9.88741	- 6	50	
- 50	Cos	d.	Cot	d. c.	Tan	Sin	d.	1	P. P.
	Cos	ı u.		· u. c.	, ran	Din	, u.	EOO	<u> </u>

51 0.80360 9 9.91626 15 0.08374 9.88734 7 52 9.80369 9.91641 15 0.08359 9.88728 6 4 53 9.80379 9 9.91657 16 0.08343 9.88722 6 4 54 9.80388 9.91672 15 0.08328 9.88702 6 4 55 9.80496 9.91703 16 0.08297 9.88703 6 4 57 9.80415 10 9.91703 16 0.08297 9.88697 6 4 58 9.80434 9 9.91734 15 0.08261 9.88697 6 4 59 9.80434 9 9.91749 16 0.08251 9.8864 6 4 60 9.80432 9 9.91765 15 0.08235 9.88678 6 4 61 9.80452 9 9.9185 15 0.08235 9.88672 <	9 9 8 7 6 5 4 3 2	P. P. 16 1 1.6 2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 11.2 8 12.8
51 9.80360 9 9.91626 15 0.08374 9.88734 7 52 9.80369 9.91641 15 0.08339 9.88728 6 4 53 9.80379 9 9.91657 16 0.08343 9.88722 6 4 54 9.80388 9.91672 15 0.08328 9.88702 6 4 55 9.80496 9.91703 16 0.08297 9.88703 6 4 57 9.80415 10 9.91703 16 0.08297 9.88697 6 4 58 9.80425 10 9.91734 15 0.08261 9.88697 6 4 59 9.80434 9 9.91749 16 0.08251 9.88644 7 4 60 9.80432 9 9.91765 15 0.08220 9.88678 6 4 61 9.80452 9 9.91780 16 0.08220 9.88672	9 8 7 6 5 4 3 2	1 1.6 2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 II.2
51 9.80360 9 9.91626 15 0.08371 9.88734 6 4 52 9.80369 9.91641 15 0.08373 9.88728 6 4 53 9.80379 9 9.91657 15 0.08333 9.88726 6 4 54 9.80388 9.9.91672 15 0.08328 9.88716 6 4 55 9.80397 9 9.91688 16 0.08312 9.88709 7 4 56 9.80406 9 9.91703 16 0.08281 9.88697 6 4 57 9.80413 9 9.91734 15 0.08269 9.88697 6 4 59 9.80434 9 9.91749 16 0.08231 9.88664 7 4 60 9.80452 9 9.91785 16 0.08235 9.88678 6 4 61 9.80452 9 9.9182 15 0.08235	8 7 6 5 4 3 2	1 1.6 2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 II.2
53 9.80379 9.91657 16 0.08339 9.88728 6 4 54 9.80388 9.91657 15 0.08333 9.88726 6 4 55 9.80397 9 9.91688 16 0.08312 9.88709 7 4 56 9.80406 9 9.91703 15 0.08297 9.88697 6 4 57 9.80413 10 9.91734 15 0.08281 9.88697 6 4 59 9.80434 9 9.91734 16 0.08251 9.88691 6 4 60 9.80434 9 9.91734 16 0.08251 9.88664 7 4 61 9.80452 9 9.91785 16 0.08235 9.88678 6 4 62 9.80470 9 9.9181 15 0.08204 9.88657 7 3 64 9.80489 9 9.91827 15 0.08133<	7 6 5 4 3 2	1 1.6 2 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 II.2
53 9.80379 9 9.91672 15 0.08343 9.88722 6 4 55 9.80397 9 9.91672 16 0.08328 9.88703 6 56 9.80405 9 9.91703 15 0.08297 9.88703 6 4 57 9.80415 10 9.91719 16 0.08261 9.88697 6 4 58 9.80425 10 9.91734 15 0.08261 9.88697 6 4 59 9.80434 9 9.91749 16 0.08261 9.88664 7 4 60 9.80443 9 9.91785 15 0.08221 9.88672 6 4 61 9.80451 9 9.91785 15 0.08220 9.88672 6 4 62 9.80461 9 9.91851 15 0.08220 9.88665 6 3 63 9.80479 10 9.91827 15 <th>6 5 4 3 2</th> <th>3 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 11.2</th>	6 5 4 3 2	3 3.2 3 4.8 4 6.4 5 8.0 6 9.6 7 11.2
54 9.80388 9 9.91672 16 0.08328 9.88716 7 4 55 9.80397 9 9.91688 15 0.08329 9.88709 7 4 57 9.80415 10 9.91719 16 0.08297 9.88697 6 4 58 9.80423 9 9.91734 15 0.08266 9.88691 7 4 60 9.80434 9 9.91765 16 0.08235 9.88661 7 4 61 9.80452 9 9.91780 16 0.08230 9.88672 7 3 62 9.80470 9 9.91811 15 0.08123 9.88659 6 3 64 9.80479 9 9.91827 15 0.08173 9.88653 6 3 64 9.80498 9 9.91857 15 0.08173 9.88653 6 3 65 9.80498 9 9.91857	5 4 3 2 1	3 4.8 4 6.4 5 8.0 6 9.6 7 II.2
55 9.80406 9 9.91703 15 0.08231 9.88709 6 4 57 9.80415 10 9.91719 15 0.08281 9.88691 6 4 58 9.80425 9 9.91749 15 0.08266 9.88691 6 4 59 9.80434 9 9.91749 16 0.08251 9.88664 6 4 60 9.80432 9 9.91785 15 0.08235 9.88678 6 4 61 9.80452 9 9.91780 16 0.08220 9.88672 6 3 62 9.80470 9 9.91811 15 0.08123 9.88659 6 3 64 9.80479 10 9.91827 15 0.08173 9.88653 6 3 65 9.80489 9 9.91842 15 0.08133 9.88653 6 3 66 9.80498 9 9.91857	4 3 2 1	4 6.4 5 8.0 6 9.6 7 II.2
57 9.80415 10 9.91719 15 0.08297 9.88703 6 4 5 9.80425 9 9.91719 15 0.08266 9.88697 6 4 6 9.80434 9 9.91749 16 0.08261 9.88684 7 6 4 6 6 9.80452 9 9.91765 15 0.08220 9.88672 6 6 9.80461 9 9.91796 16 0.08220 9.88672 6 9.80461 9 9.91811 15 0.08249 9.88659 6 6 3 9.80470 9 9.91811 15 0.08139 9.88659 6 6 3 9.80470 9 9.91827 15 0.08139 9.88653 6 3 6 6 9.80498 9 9.91857 16 0.08123 9.88653 6 3 6 6 9.80498 9 9.91857 16 0.08123 9.88647 7 3 6 6 9.80498 9 9.91857 16 0.08123 9.88647 7 3 6 6 9.80498 9 9.91857 16 0.08123 9.88647 7 3 6 6 9.80498 9 9.91857 16 0.08123 9.88647 7 3 6 6 9.80498 9 9.91857 16 0.08123 9.88647 7 3 6 6 9.80498 9 9.91857 16 0.08123 9.88644 6 3 6 6 9.80498 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9.80484 9 9.91857 16 0.08124 9 9.80484 9 9.91857 16 0.08124 9 9.91857 16 0.08124 9 9.80	3 2 I	6 9.6 7 II.2
57 9.80415 10 9.91719 15 0.08281 9.88697 6 4 58 9.80425 10 9.91714 15 0.08261 9.88691 6 4 59 9.80434 9 9.91749 16 0.08251 9.88691 7 4 60 9.80443 9 9.91765 15 0.08220 9.88672 6 4 61 9.80451 9 9.91780 16 0.08220 9.88672 6 3 62 9.80470 9 9.91811 15 0.08189 9.88659 6 3 64 9.80479 10 9.91827 15 0.08139 9.8863 6 3 66 9.80498 9 9.91857 15 0.08138 9.88677 6 3 67 9.80507 9.80507 9.91873 15 0.08127 9.88634 6 3 67 9.80507 9.91873 1	2 I	7 11.2
58 9.80423 9 9.91734 15 0.08266 9.88691 0 4 60 9.80443 9 9.91749 15 0.08251 9.88684 7 4 61 9.80452 9 9.91785 15 0.08226 9.88672 7 3 62 9.80461 9 9.91796 16 0.08220 9.88672 7 3 63 9.80479 9 9.91811 15 0.08189 9.88659 6 3 64 9.80479 9 9.91827 15 0.08173 9.88653 6 3 65 9.80489 10 9.91827 15 0.08173 9.88647 7 3 66 9.80498 9 9.91857 16 0.08173 9.88647 7 3 67 9.80507 9.91873 7 0.08127 9.88634 6 3	2 I	
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64 9.80479 9 9.91827 15 0.08173 9.88653 6 3 6 6 9.80498 9 9.91857 15 0.08143 9.88640 7 6 3 6 7 9.80507 9.91873 7 0.08127 9.88634 6 3		2 3.0
65 9.80489 9 9.91842 15 0.08158 9.88647 6 3 6 6 9.80498 9 9.91857 15 0.08143 9.88640 7 6 3 6 7 9.80507 9 9.91873 7 0.08127 9.88634 6 3	- 1	3 4.5
66 9.80498 9 9.91857 16 0.08143 9.88640 7 3 6 9.80507 9 9.91873 7 0.08127 9.88634 6 3		4 6.0 5 7.5
67 9.80507 9 9.91873 10 0.08127 9.88634 6 3		5 7.5 6 9.0
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69 0.80525 9 0.01004 16 0.08006 0.88627 7		9 13.5
70 0 80521 9 0 07070 15 0 08087 0 88677 6		
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71 9.80543 9.91935 0.08065 9.88609 6 2		10
72 9.80553 9.91950 0.08050 9.88003 2		1 1.0
73 9.80302 0 9.91903 16 0.08033 9.88390 6 2		2 2.0
74 9.80571 0 9.91981 7 0.08019 9.88590 6 2		3 3.0
75 9.80580 - 9.91990 - 0.08004 9.88584 - 2		4 4.0 5 5.0
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77 9.80598 9.92027 0.07973 9.88571 6 2	3	7 7.0 8 8.0
76 9.80007 9.92042 6 0.07958 9.88505 2		
79 9.30010 0 9.92030 15 0.07942 9.88388 6 2	- 1	9 9.0
80 9.80625 9 9.92073 16 0.07927 9.88552 6 2	0	
81 0 80635 0 02080 0 07011 0 88546 1	9	9
82 9.80644 9 9.92T04 15 0.07806 9.88540 6 T	8	I 0.9 2 I.8
83 9.80653 9 9.92120 10 9.07880 9.88533 7 1	7	2 1.8
84 9 80662 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	6 I	3 2.7 4 3.6
85 0 80671 9 0 02150 15 0 07850 0 88521 0 1		5 4.5
86 9.80680 9 9.92166 16 9.07834 9.88514 7 T		6 5.4
87 0 80689 9 0 02181 15 0 07810 0 88508 0 I	₃	7 6.3 8 7.2
88 9.80698 9 9.92197 16 0.07803 9.88502 6 I		8 7.2 9 8.1
89 9.80707 9 9.92212 15 9.97788 9.88495 7 1		9 0.1
90 9 80716 9 0 02227 15 0 07773 9 88489 0 1	- 1	
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92 9.80734 9 9.92238 16 0.07742 9.88470 6 0		1 0.7
93 9.80743 9 9.92274 15 0.07720 9.80470 6		2 I.4 3 2.1
94 9.80752 9.92289 0.07711 9.88464 7 0		4 2.8
95 9.80702 9.92304 2 0.07090 9.88457 2 0		5 3.5
90 9.80771 0 9.92320 15 0.07080 9.88451 7 0		6 4.2
97 9.80790 9.92335 0.07665 9.88444 0		7 4.9 8 5.6
98 9.80789 9.92351 7 0.07049 9.88438 6 0		8 5.6 9 6.3
99 9.80798 9 9.92300 15 0.07034 9.88432 7		y 1 0.0
100 9.80807 9.92381 0.07619 9.88425 0	n I	
Cos d. Cot d.c. Tan Sin d.	.اب	P. P.

	Sin	d.	Tan	d. c.	Cot	Cos	d.	ı	P. P.
00	9.80807		9.92381	16	0.07619	9.88425	6	100	
OI	9.80816	9	9.92397		0.07603	9.88419		99	16
02	9.80825	9	9.92412	15	0.07588	9.88413	6	98	1 1.6
03	9.80834	9	9.92428	16 15	0.07572	9.88406	7	97	2 3.2
04	9.80843		9.92443	1	0.07557	9.88400	6	96	3 4.8
05	9.80852	9	9.92458	15 16	0.07542	9.88394	7	95	4 6.4 5 8.0
06	9.80861	9	9.92474	15	0.07526	9.88387	6	94	4 6.4 5 8.0 6 9.6
07	9.80870	9	9.92489	15	0.07511	9.88381	7	93	7 11.2
о8	9.80879	9	9.92504	16	0.07496	9.88374	6	92	8 12.8 9 14.4
09	9.80888	9	9.92520	15	0.07480	9.88368	6	91	9 14.4
10	9.80897	9	9.92535	16	0.07465	9.88362	7	90	۱
II	9.80906	9	9.92551	15	0.07449	9.88355	6	89	15
12	9.80915	9	9.92566	15	0.07434	9.88349	6	88	1 1.5
13	9.80924	9	9.92581	16	0.07419	9.88343	7	87	3 4.5
14	9.80933	9	9.92597	15	0.07403	9.88336	6	86 85	4 6.0
15 16	9.80942 9.80951	9	9.92612 9.92628	16	0.07388	9.88330 9.88323	7	84	5 7.5 6 9.0
		9		15			6	83	7 10.5
17	9.80960 9.80969	9	9.92643 9.92658	15	0.07357	9.88317 9.88311	6	82	
19	9.80909	9	9.92674	16	0.07342	9.88304	7	81	9 13.5
20	9.80987	9	9.92689	15	0.07311	9.88298	6	80	
	9.80987	9		15	0.07311	9.88291	7	79	
2 I 2 2	9.80990	9	9.92704	16	0.07290	0.88285	6	78	9
23	9.81014	9	9.92725	15	0.07265	9.88279	6	77	I 0.9 2 1.8
24	9.81023	9	9.92751	16	0.07249	9.88272	7	76	3 2.7
25	9.81023	9	9.92766	15	0.07234	9.88266	6	75	
26	9.81041	9 8	9.92781	15	0.07219	9.88259	7	74	5 4.5
27	9.81049	1	9.92797	16	0.07203	9.88253	6	73	
28	9.81058	9	9.92812	15	0.07188	9.88246	7	72	8 7.2
29	9.81067	9	9.92827	15	0.07173	9.88240	6	71	9 8.1
30	9.81076	9	9.92843	16	0.07157	9.88234	ł	70	
31	0.81085	9	9.92858	15	0.07142	9.88227	7	69	8
32	9.81094	9	9.92873	15	0.07127	9.88221	6	68	1 0.8
33	9.81103	9	9.92889	16 15	0.07111	9.88214	7 6	67	2 I.6 3 2.4
34	9.81112	9	9.92904	1 -	0.07096	9.88208		66	4 3.2
35	9.81121	9	9.92920	16	0.07080	9.88201	7 6	65	5 4.0
36	9.81130	9	9.92935	15 15	0.07065	9.88195	6	64	6 4.8
37	9.81139		9.92950	16	0.07050	9.88189	7	63	7 5.6 8 6.4
38	9.81148	9	9.92966	15	0.07034	9.88182	6	62	9 7.2
39	9.81157	9	9.92981	15	0.07019	9.88176	7	61	l
40	9.81166	8	9.92996	16	0.07004	9.88169	6	60	
41	9.81174	9	9.93012	15	0.06988	9.88163	7	59	7
42	9.81183	9	9.93027	15	0.06973	9.88156	6	58	1 0.7
43	9.81192	9	9.93042	16	0.06958	9.88150	7	57	2 I.4 3 2.1
44	9.81201	9	9.93058	15	0.06942	9.88143	6	56	
45	9.81210	9	9.93073	15	0.06927	9.88137	7	55	5 3.5
46	9.81219	9	9.93088	16	0.06912	9.88130	6	54	6 4.2
47	9.81228	9	9.93104	15	0.06896	9.88124	7	53	7 4.9 8 5.6
48	9.81237	9	9.93119	16	0.06881	9.88117 9.88111	6	52 51	7 4.9 8 5.6 9 6.3
49	9.81246	8	9.93135	15			6	50	
50	9.81254		9.93150	<u> </u>	0.06850	9.88105		-00-	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

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	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.81254	9	9.93150	15	0.06850	9.88105	7	50	4
51	9.81263	9	9.93165	16	0.06835	9.88098	6	49	16
52	9.81272	9	9.93181	15	0.06819	9.88092	7	48	1 1.6
53	9.81281	9	9.93196	15	0.06804	9.88085	6	47	
54	9.81290	9	9.93211	16	0.06789	9.88079		46	3 4.8
55	9.81299		9.93227	15	0.06773	9.88072	7 6	45	4 6.4
56	9.81308	9	9.93242	15	0.06758	9.88066	7	44	4 6.4 5 8.0 6 9.6
57	9.81316	9	9.93257	16	0.06743	9.88059	6	43	7 11.2
58	9.81325	9	9.93273	15	0.06727	9.88053		42	
59	9.81334	9	9.93288	15	0.06712	9.88046	7 6	41	9 14.4
60	9.81343	9	9.93303	16	0.06697	9.88040	7	40	
61	9.81352		9.93319		0.06681	9.88033		39	15
62	9.81361	9	9.93334	15	0.06666	9.88027	6	38	1 1.5
63	9.81370	8	9.93349	15 16	0.06651	9.88020	7 6	37	2 3.0
64	9.81378		9.93365		0.06635	9.88014		36	3 4.5 4 6.0
65	9.81387	9	9.93380	15 15	0.06620	9.88007	7 6	35	5 7.5
66	9.81396	9	9 - 93395	16	0.06605	9.88001	7	34	6 9.0
67	9.81405		9.93411	-	0.06589	9.87994		33	7 IO.5 8 I2.0
68	9.81414	9	9.93426	15	0.06574	9.87988	6	32	9 13.5
69	9.81422	9	9.93441	15 16	0.06559	9.87981	7 6	31	, -5.5
70	9.81431		9.93457	ì	0.06543	9.87975		30	i
71	9.81440	9	9.93472	15	0.06528	9.87968	7	29	8
72	9.81449	9	9.93487	15	0.06513	9.87962	6	28	1 0.8
73	9.81458	9	9.93503	16	0.06497	9.87955	7	27	2 1.6
74	9.81467	9	9.93518	15	0.06482	9.87949	6	26	3 2.4
75	9.81475	8	9.93533	15	0.06467	9.87942	7	25	1 3.2
76	9.81484	9	9.93549	16	0.06451	9.87935	7	24	4 3.2 5 4.0 6 4.8 7 5.6 8 6.4
77	9.81493	9	9.93564	15	0.06436	9.87929		23	7 5.6
78	9.81502	9	9.93579	15	0.06421	9.87922	7	22	7 5.6 8 6.4
79	9.81510	8	9.93595	16	0.06405	9.87916	6	21	9 7.2
80	9.81519	9	9 93610	15	0.06390	9.87909	7	20	
81	9.81528	9	9.93625	15	0.06375	9.87903	6	19	7
82	9.81537	9	9.93641	16	0.06359	9.87896	7	18	1 0.7
83	9.81546	9 8	9.93656	15	0.06344	9.87890	6	17	2 1.4
84	9.81554		9.93671	15	0.06329	9.87883	7	16	3 2.I 4 2.8
85	9.81563	9	9.93671	16	0.06313	9.87877	6	15	4 2.8 5 3.5 6 4.2
86	9.81572	9	9.93702	15	0.06298	9.87870	7	14	6 4.2
87	9.81581	9	9.93717	15	0.06283	9.87863	7	13	7 4.9 8 5.6 9 6.3
88	9.81589	8	9.93717	16	0.06267	9.87857	6	12	9 6.3
89	9.81598	9	9.93748	15	0.06252	9.87850	7	11	,
90	9.81607	9	9.93763	15	0.06237	9.87844	6	10	
91	9.81616	9	9.93778	15	0.06222	9.87837	7	09	6
92	9.81624	8	9.93776	16	0.06222	9.87831	6	08	
93	9.81633	9	9.93794	15	0.06191	9.87824	7	07	1 0.6
94	9.81642	9	9.93824	15	0.06176	9.87817	7	06	3 1.8
95	9.81651	9	9.93840	16	0.00170	9.87811	6	05	4 2.4
96	9.81659	8	9.93855	15	0.06145	9.87804	7	04	5 3.0 6 3.6
97	9.81668	9	9.93870	15	0.06130	9.87798	6	03	7 12
98	9.81677	9	9.93870	16	0.00130	9.87791	7	03	8 4.8
99	9.81686	9	9.93901	15	0.06099	9.87785	6	01	9 5.4
100	9.81694	8	9.93916	15	0.06084	9.87778	7	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
1000		ч.	COL	ч. С.	1 dil	OIII I	u.		1.1.

Sin d. Tan d. c. Cot Cos d.	P. P.
01 0.81703 9 9.93932 15 0.06068 9.87771 7 99 9.93947 7 7 98 9.93947 15 0.06068 9.87765 6 98 98 98 9.93947 15 0.06033 9.87758 6 97 98 9.939378 15 0.06038 9.87758 6 97 99 9.93978 15 0.06022 9.87752 7 95 96 99 9.93993 15 0.06022 9.87745 7 95 95 99 9.94023 15 0.05992 9.87733 6 94 94 99 99 99 99 99 9.87735 7 95 99	
o1 9.81703 9 9.93347 15 0.06068 9.87761 6 98 o3 9.81729 9 9.93947 15 0.06058 9.87765 7 98 o4 9.81729 9 9.93978 15 0.06053 9.87758 6 97 o5 9.81738 9 9.93993 15 0.0607 9.87745 7 95 o6 9.81747 8 9.94008 15 0.05992 9.87732 7 95 o7 9.81765 9 9.94031 16 0.05997 9.87732 7 93 o8 9.81764 9 9.94051 15 0.05996 9.87732 7 93 o9 9.81773 9 9.94051 15 0.05996 9.87719 7 92 o9 9.81799 9 9.94051 15 0.05946 9.87719 7 92 11 9.81896 9 9.94131	
03 9.81729 9 9.93962 15 0.06038 9.87758 7 97 04 9.81729 9 9.93978 15 0.06038 9.87758 6 96 05 9.81738 9 9.93993 15 0.06022 9.87752 6 96 06 9.81747 8 9.94008 15 0.05907 9.87738 6 94 07 9.81755 9.94023 16 0.05997 9.87732 7 93 08 9.81761 9 9.94031 15 0.05961 9.87725 6 92 09 9.81773 8 9.94051 15 0.05916 9.87712 7 90 10 9.81781 9 9.94051 15 0.05931 9.87712 7 90 11 9.81799 8 9.94100 15 0.05931 9.87702 7 80 12 9.81866 9 9.94113	16
04 9.81729 9.93978 16 0.06032 9.87758 6 96 05 9.81738 9.93998 15 0.06022 9.87732 7 95 06 9.81747 8 9.94028 15 0.05022 9.87732 7 95 07 9.81755 9.94023 16 0.05961 9.87732 7 92 08 9.81764 9.94039 16 0.05961 9.87719 7 91 10 9.81781 9.94054 15 0.05961 9.87719 7 91 11 9.81791 9.94059 16 0.05915 9.87712 7 90 12 9.81799 9.94051 15 0.05905 9.87699 6 88 13 9.81867 9.94106 15 0.05905 9.87699 7 87 14 9.81866 9.94115 16 0.05885 9.87692 7 85 15 9.94	
04 9.81729 9 9.93978 15 0.66022 9.87752 7 95 06 9.81738 9 9.93993 15 0.06007 9.87745 7 95 07 9.81755 9 9.94081 15 0.05992 9.87732 7 93 08 9.81764 9 9.94054 15 0.05961 9.87712 7 92 09 9.81773 8 9.94054 15 0.05961 9.87712 7 90 10 9.81799 9 9.94054 15 0.05961 9.87712 7 90 11 9.81790 9 9.94054 15 0.05961 9.87705 6 89 12 9.81799 9 9.9415 15 0.05969 9.87699 6 88 13 9.81826 9 9.94131 16 0.05869 9.87692 6 86 15 9.81825 9 9.94161	2 3.2
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o7 9.81755 9 9.94023 16 0.05977 9.87732 7 93 o8 9.81764 9 9.94039 16 0.05961 9.87715 6 91 10 9.81781 9 9.94054 15 0.05915 9.87712 7 90 11 9.81799 9 9.94085 15 0.05915 9.87705 6 89 12 9.81799 9 9.94105 15 0.05905 9.87692 6 88 13 9.81867 9 9.94115 16 0.05905 9.87692 6 88 14 9.81856 9 9.94161 15 0.05869 9.87692 6 86 15 9.81823 9 9.94161 15 0.05839 9.87672 6 86 16 9.81833 9 9.94161 15 0.05839 9.87672 6 84 17 9.81832 9 9.9417	5 8.0 6 9.6
o8 9.81764 9 9.94039 16 0.05961 9.87725 6 92 10 9.81781 9 9.94059 15 0.05961 9.87712 6 91 11 9.81790 9 9.94069 16 0.05931 9.87712 7 90 12 9.81790 9 9.94069 15 0.05931 9.87712 7 90 12 9.81790 9 9.94100 15 0.05900 9.87699 6 88 13 9.81866 9 9.94131 15 0.05865 9.87699 7 87 14 9.81835 9 9.94146 15 0.05864 9.87669 7 85 16 9.81832 9 9.94176 15 0.05864 9.87679 7 85 16 9.81842 9 9.94176 15 0.05824 9.87679 7 84 17 9.81842 9 9.9417	
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10 9.81781 9 9.94069 16 0.05931 9.87712 7 90 11 9.81799 9.94085 15 0.05931 9.87705 6 88 12 9.81799 8 9.94100 15 0.05905 9.87692 7 87 14 9.81816 9 9.94131 15 0.05869 9.87686 6 86 15 9.81825 9 9.94161 15 0.05839 9.87697 7 85 16 9.81831 9 9.94176 16 0.05839 9.87666 83 17 9.81832 9 9.94176 16 0.05808 9.87659 7 84 18 9.81859 9 9.94271 15 0.05793 9.87652 6 83 19 9.81868 9 9.94221 15 0.05793 9.87659 7 82 20 9.81868 9 9.94223 15 <td< th=""><th>9 14.4</th></td<>	9 14.4
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12 9.81799 9 9.94100 15 0.05900 9.87699 6 88 13 9.81807 9 9.94115 16 0.05885 9.87699 6 87 14 9.81816 9 9.94146 15 0.05869 9.87686 7 85 16 9.81833 9 9.94161 15 0.05834 9.87672 7 84 17 9.81842 9 9.94176 16 0.05834 9.87666 7 83 18 9.81859 9 9.94120 15 0.05808 9.87659 7 82 19 9.81859 9 9.94207 15 0.05808 9.87659 7 81 20 9.81868 9 9.94221 15 0.05703 9.87652 7 81 21 9.81887 9 9.94223 15 0.05762 9.87639 7 79 24 9.81993 9 9.9428	15
13	1 1.5
14	2 3.0
15	3 4.5
16 9.81833 8 9.94161 15 0.05839 9.87672 6 84 17 9.81831 9 9.94176 15 0.05824 9.87666 7 83 18 9.81851 9 9.94192 15 0.05824 9.87659 7 82 19 9.81859 9 9.94207 15 0.05793 9.87652 7 81 20 9.81868 9 9.94222 15 0.05703 9.87639 7 79 21 9.81887 8 9.94253 15 0.05762 9.87632 7 78 23 9.81894 9 9.94281 15 0.05732 9.87632 7 78 24 9.81993 8 9.94284 15 0.05732 9.87619 6 75 26 9.81920 9 9.94314 15 0.05606 9.87606 7 74 27 9.81929 8 9.9432	
17	6 9.0
18	7 IO.5 8 I2.0
19	8 12.0 9 13.5
20 9.81868 9 9.94222 16 0.05778 9.87639 7 79	9 13.3
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22 9.81885 8 9.9.94253 15 0.05747 9.87632 7 78 23 9.81894 9 9.94268 15 0.05732 9.87626 6 77 24 9.81903 8 9.94284 16 0.05701 9.87619 7 76 25 9.81911 8 9.94284 15 0.05701 9.87619 6 75 26 9.81920 9 9.94314 15 0.05686 9.87606 7 74 27 9.81929 8 9.94329 16 0.05671 9.87599 6 73 28 9.81937 9.94329 16 0.05651 9.87593 7 72 29 9.81946 9 0.04360 15 0.05655 9.87593 7 71	•
23 9.81894 9 9.94268 15 0.05732 9.87626 6 7 77 24 9.81993 9 9.94284 0.05716 9.87619 7 76 25 9.81911 8 9.94299 15 0.05716 9.87613 7 75 26 9.81920 9 9.94314 15 0.05686 9.87606 7 74 27 9.81929 8 9.94329 15 0.05671 9.87599 7 73 28 9.81937 8 9.94329 16 0.05655 9.87593 6 72 29 9.81946 9 0.04760 15 0.05630 9.87866 7 71	9
24 9.81903 9 9.94284 15 0.05716 9.87619 7 76 25 9.81911 8 9.94299 15 0.05701 9.87613 6 75 26 9.81920 9 9.94314 15 0.05686 9.87606 7 74 27 9.81929 8 9.94329 15 0.05671 9.87599 7 73 28 9.81937 8 9.94345 15 0.05655 9.87593 6 72 20 0.81946 9 0.04360 15 0.05650 9.87586 7 71	I 0.9 2 I.8
25 9.81911 0 9.94299 15 0.05701 9.87613 0 75 26 9.81920 9 9.94314 15 0.05686 9.87666 7 74 27 9.81929 9 9.94329 15 0.05671 9.87599 7 73 28 9.81937 8 9.94345 16 0.05655 9.87593 6 72 20 0.81946 9 0.04360 15 0.05655 9.87593 7 71	2 I.8 3 2.7
26 9.81920 9 9.94314 15 0.05686 9.87606 7 74 27 9.81929 9 9.94329 15 0.05671 9.87599 7 73 28 9.81937 9 9.94349 16 0.05651 9.87593 6 72 29 9.81046 9 9.04360 15 0.05630 9.87583 7 71	3 2.7 4 3.6
27 9.81929 8 9.94329 16 0.05671 9.87599 6 73 28 9.81937 9 9.94345 16 0.05655 9.87593 7 72 29 9.81946 9 9.94360 15 0.05635 9.87586 7 71	5 4.5
28 9.81937 8 9.94345 16 0.05655 9.87593 6 72 29 9.81946 9 9.94345 15 0.05640 9.87586 7 71	6 5.4
29 9.81946 9 9.94369 15 0.05640 9.87586 7 71	7 6.3 8 7.2
	9 8.1
30 9.81955 9 9.94375 15 0.05625 9.87579 7 70	
8 334015 16 341015 6	8
31 9.81963 9 9.94391 0.05609 9.87573 7 69 32 9.81972 9 9.94406 15 0.05594 9.87566 7 68	ı o.8
1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7	2 1.6
15 15 15 15 15 15 15 15 15 15 15 15 15 1	3 2.4
16 5 7 6	4 3.2
35 9.81998 9.94452 75 0.05546 9.87540 7 05	5 4.0 6 4.8
	7 5.6
37 9.82015 8 9.94482 16 0.05518 9.87533 7 62	8 6.4
30 9.82023 9 9.94498 I5 0.05502 9.87520 7 61	9 7.2
9 5 6	
8 15 7	
4I 9.82049 0 9.94543 16 0.05457 9.87506 7 59	7
42 9.82058 8 9.94559 5 0.05441 9.87499 7 58	1 0.7
43 9.82000 9 9.94574 5 0.05420 9.87492 6 57	2 I.4 3 2.1
44 9.82075 9.94589 0.05411 9.87486 7 56	3 2.1
45 9.82004 8 9.94004 76 0.03390 9.87479 7 53	5 3.5
40 9.82092 9.94020 15 0.05380 9.87472 6 54	6 4.2
47 9.82101 8 9.94635 TF 0.05365 9.87466 7 53	7 4.9 8 5.6
48 9.82109 0 9.94650 16 0.05350 9.87459 7 52	9 6.3
49 9.82118 8 9.94000 15 0.05334 9.87452 6 51	
50 9.82126 9.94681 0.05319 9.87446 50	
Cos d. Cot d. c. Tan Sin d.	P. P.

	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.82126	9	9.94681	15	0.05319	9.87446	-	50	
51	9.82135	9	9.94696		0.05304	9.87439	7	49	16
52	9.82144	8	9.94711	15 16	0.05289	9.87432	7	48	1 1.6
53	9.82152	9	9.94727	15	0.05273	9.87425	6	47	2 3.2
54	9.82161	8	9.94742	15	0.05258	9.87419	7	46	
55	9.82169	9	9.94757	15	0.05243	9.87412	7	45	4 6.4 5 8.0
56	9.82178	8	9.94772	16	0.05228	9.87405	6	44	3 4.8 4 6.4 5 8.0 6 9.6 7 II.2 8 12.8
57	9.82186	9	9.94788	15	0.05212	9.87399	7	43	7 II.2
58 59	9.82195	8	9.94803	15	0.05197	9.87392	7	42	8 12.8 9 14.4
60		9	9.94818	16	0.05182	9.87385	7	41	91144
	9.82212	9	9.94834	15	0.05166	9.87378	6	40	15
61 62	9.82221 9.82229	8	9.94849	15	0.05151	9.87372	7	39	15
63	9.82229	9	9.94864	15	0.05136	9.87365 9.87358	7	38	I I.5 2 3.0
64	9.82246	8		16			7	37	3 4.5
65	9.82255	9	9.94895 9.94910	15	0.05105	9.87351 9.87345	6	36 35	4 6.0
66	9.82263	8	9.94910	15	0.03090	9.87338	7	35	5 7.5 6 9.0
67	9.82272	9	9.94940	15	0.05060	9.87331	7	33	7 10.5
68	9.82280	8	9.94956	16	0.05044	9.87325	6	32	8 12.0 9 13.5
69	9.82289	9	9.94971	15	0.05029	9.87318	7	31	9 1 13.5
70	9.82297		9.94986	15	0.05014	9.87311	7	30	
71	9.82306	9	9.95001	15	0.04999	9.87304	7	29	
72	9.82314	8	9.95017	16	0.04983	9.87298	6	28	8 T 108
73	9.82323	9	9.95032	15	0.04968	9.87291	7	27	I 0.8 2 I.6
74	9.82331		9.95047	15	0.04953	9.87284	7	26	
75	9.82340	9	9.95062	15	0.04938	9.87277	7	25	1 32
76	9.82348	9	9.95078	16	0.04922	9.87270	7 6	24	3 2.4 4 3.2 5 4.0 6 4.8
77	9.82357	8	9.95093	15	0.04907	9.87264		23	5 4.0 6 4.8 7 5.6 8 6.4
78	9.82365	9	9.95108	15 16	0.04892	9.87257	7	22	8 6.4
79	9.82374	8	9.95124	15	0.04876	9.87250	7 7	21	9 7.2
80	9.82382	9	9.95139	15	0.04861	9.87243	6	20	
81	9.82391	8	9.95154		0.04846	9.87237		19	7
82	9.82399	9	9.95169	15 16	0.04831	9.87230	7	18	I 0.7
83	9.82408	8	9.95185	15	0.04815	9.87223	7	17	2 I.4 3 2.1
84	9.82416	8	9.95200	15	0.04800	9.87216	7	16	4 2.8
85	9.82424	9	9.95215	15	0.04785	9.87209	6	15	4 2.8 5 3.5 6 4.2
86	9.82433	8	9.95230	16	0.04770	9.87203	7	14	7 4.9
87	9.82441	9	9.95246	15	0.04754	9.87196	7	13	7 4.9 8 5.6 9 6.3
88 89	9.82450	8	9.95261	15	0.04739	9.87189	7	12	9 6.3
90	9.82458	9	9.95276	15	0.04724	9.87182	7	11	
	9.82467	8	9.95291	16	0.04709	9.87175	6	10	
91	9.82475	9	9.95307	15	0.04693	9.87169	7	09	6
92 93	9.82484 9.82492	8	9.95322	15	0.04678	9.87162	7	08 07	1 0.6
		9	9.95337	15		9.87155	7		2 I.2 3 I.8
94 95	9.82501 9.82509	8	9.95352 9.95368	16	0.04648	9.87148 9.87141	7	o6 o5	4 2.4
95 96	9.82517	8	9.95383	15	0.04617	9.87135	6	05	
97	9.82526	9	1	15	0.04602	9.87128	7	03	5 3 0 6 3.6 7 4.2 8 4.8 9 5.4
98	9.82520	8	9.95398 9.95413	15	0.04587	9.87125	7	03	8 4.8
99	9.82543	9 8	9.95429	16	0.04571	9.87114	7	01	9 5.4
100	9.82551	0	9.95444	15	0.04556	9.87107	7	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

42°								137°	
	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
00	9.82551	9	9.95444	15	0.04556	9.87107	6	100	
01	9.82560	8	9.95459	15	0.04541	9.87101	7	99	16
02	9.82568	8	9.95474	15	0.04526	9.87094	7	98	1 1.6
03	9.82576	9	9.95489	16	0.04511	9.87087	7	97	2 3.2
04	9.82585 9.82593	8	9.95505 9.95520	15	0.04495	9.87080 9.87073	7	96 95	3 4.8 4 6.4
o5 o6	9.82593	9	9.95535	15	0.04465	9.87066	7	95 94	5 8.0
07	9.82610	8	9.95550	15	0.04450	9.87060	6	93	
08	9.82618	8	9.95566	16	0.04434	9.87053	7	92	7 II.2 8 I2.8
09	9.82627	9	9.95581	15 15	0.04419	9.87046	7	91	9 14.4
10	9.82635	9	9.95596	15	0.04404	9.87039	7	90	
11	9.82644	8	9.95611	16	0.04389	9.87032		89	15
12	9.82652	8	9.95627	15	0.04373	9.87025	7	88	1 1.5
13	9.82660	9	9.95642	15	0.04358	9.87018	6	87	3 4.5
14	9.82669	8	9.95657	15	0.04343	9.87012	7	86	4 6.0
15 16	9.82677 9.82685	8	9.95672 9.95688	16	0.04328	9.87005 9.86998	7	85 84	5 7.5 6 9.0
17	9.82694	9	9.95703	15	0.04312	9.86991	7	83	7 10.5
18	9.82702	8	9.95718	15	0.04297	9.86984	7	82	8 12.0 9 13.5
19	9.82711	9 8	9.95733	15 15	0.04267	9.86977	7	8r	9 13.3
20	9.82719	8	9.95748	16	0.04252	9.86970	7	80	
21	9.82727		9.95764	1	0.04236	9.86963	7	79	9
22	9.82736	9 8	9.95779	15 15	0.04221	9.86957	6 7	78	1 0.9
23	9.82744	8	9.95794	15	0.04206	9.86950	7	77	1 0.9 2 1.8
24	9.82752	9	9.95809	16	0.04191	9.86943	7	76	3 2.7 4 3.6
25 26	9.82761	8	9.95825	15	0.04175	9.86936	7	75	5 4.5
	9.82769	8	9.95840	15		9.86929 9.86922	7	74	
27 28	9.82777 9.82786	9	9.95855 9.95870	15	0.04145	9.86915	7	73 72	8 7.2
29	9.82794	8	9.95886	16	0.04114	9.86908	7	71	9 8.1
30	9.82802	8	9.95901	15	0.04099	9.86902	6	70	
31	9.82811	9	9.95916	15	0.04084	9.86895	7	69	8
32	9.82819	8	9.95931	15	0.04069	9.86888	7	68	1 0.8 2 1.6
33	9.82827	9	9.95946	15 16	0.04054	9.86881	7	67	2 1.6 3 2.4
34	9.82836	8	9.95962	15	0.04038	9.86874	7	66	4 3.2
35	9.82844	8	9.95977	15	0.04023	9.86867	7	65	5 4.0 6 4.8
36	9.82852	9	9.95992	15	0.04008	9.86860	7	64	7 5.6 8 6.4
37 38	9.82861 9.82869	8	9.96007 9.96023	16	0.03993	9.86853 9.86846	7	63 62	8 6.4 9 7.2
39	9.82877	8	9.96038	15	0.03977	9.86839	7	61	9 1 1
40	9.82885	8	9.96053	15	0.03947	9.86832	7	60	
41	9.82894	9	9.96068	15	0.03932	9.86826	6	59	7
42	9.82902	8	9.96083	15 16	0.03932	9.86819	7	58	1 0.7
43	9.82910	9	9.96099	15	0.03901	9.86812	7	57	2 1.4
44	9.82919	8	9.96114	15	0.03886	9.86805	7	56	3 2.I 4 2.8
45	9.82927	8	9.96129	15	0.03871	9.86798	7	55	5 3.5
46	9.82935	9	9.96144	16	0.03856	9.86791	7	54	6 4.2
47	9.82944	8	9.96160	15	0.03840	9.86784	7	53	7 4.9 8 5.6 9 6.3
48 49	9.82952 9.82960	8	9.96175 9.96190	15	0.03825	9.86777 9.86770	7	52 51	9 6.3
50	9.82968	8	9.96205	15	0.03795	9.86763	7	50	
		d.	9.90205 Cot	d. c.	Tan	Sin	d.		P. P.
L	Cos	a.	· Cot	· a. c.	ran	om	· u.		1.1.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.82968		9.96205	15	0.03795	9.86763		50	
51	9.82977	9	9.96220		0.03780	9.86756	7	49	16
52	9.82985	8	9.96236	16 15	0.03764	9.86749	7	48	
53	9.82993	8	9.96251	15	0.03749	9.86742	7 7	47	I I.6 2 3.2
54	9.83001	l	9.96266	15	0.03734	9.86735		46	3 4.8
55	9.83010	9	9.96281	16	0.03719	9.86728	7	45	4 6.4
56	9.83018	8	9.96297	15	0.03703	9.86721	7	44	5 8.0 6 9.6
57	9.83026	8	9.96312	15	0.03688	9.86714		43	
58	9.83034	9	9.96327	15	0.03673	9.86707	7	42	8 12.8
59	9.83043	8	9.96342	15	0.03658	9.86700	6	41	9 14.4
60	9.83051	8	9.96357	16	0.03643	9.86694	7	40	
61	9.83059	8	9.96373	15	0.03627	9.86687	7	39	15
62	9.83067	9	9.96388	15	0.03612	9.86680	7	38	I 1.5
63	9.83076	8	9.96403	15	0.03597	9.86673	7	37	2 3.0 3 4.5
64	9.83084	8	9.96418	15	0.03582	9.86666	7	36	3 4.5 4 6.0
65	9.83092	8	9.96433	16	0.03567	9.86659	7	35	5 7.5
66	9.83100	9	9.96449	15	0.03551	9.86652	7	34	6 9.0
67	9.83109	8	9.96464	15	0.03536	9.86645	7	33	7 IO.5 8 I2.0
68	9.83117	8	9.96479	15	0.03521	9.86638	7	32	9 13.5
69	9.83125	8	9.96494	16	0.03506	9.86631	7	31	1
70	9.83133	8	9.96510	15	0.03490	9.86624	7	30	
71	9.83141	9	9.96525	15	0.03475	9.86617	7	29	9
72	9.83150	8	9.96540	15	0.03460	9.86610	7	28	1 0.9
73	9.83158	8	9.96555	15	0.03445	9.86603	7	27	2 1.8
74	9.83166	8	9.96570	16	0.03430	9.86596	7	26	3 2.7 4 3.6
75	9.83174	8	9.96586	15	0.03414	9.86589	7	25	5 4.5
76	9.83182	9	9.96601	15	0.03399	9.86582	7	24	6 5.4
77	9.83191	8	9.96616	15	0.03384	9.86575	7	23	7 6.3 8 7.2
78	9.83199	8	9.96631	15	0.03369	9.86568	7	22	8 7.2 9 8.1
79	9.83207	8	9.96646	16	0.03354	9.86561	7	21	
80	9.83215	8	9.96662	15	0.03338	9.86554	7	20	8
81	9.83223	9	9.96677	15	0.03323	9.86547	7	19	1 0.8
82	9.83232	8	9.96692	15	0.03308	9.86540	7	18	2 1.6
83	9.83240	8	9.96707	15	0.03293	9.86533	7	17	3 2.4
84	9.83248	8	9.96722	16	0.03278	9.86526	8	16	4 3.2
85 86	9.83256 9.83264	8	9.96738	15	0.03262	9.86518 9.86511	7	15	5 4.0 6 4.8
		8	9.96753	15	0.03247		7	14	7 5.6 8 6.4
87 88	9.83272	9	9.96768	15	0.03232	9.86504	7	13	
88 89	9.83281 9.83289	8	9.96783 9.96798	15	0.03217	9.86497	7	12 11	9 7.2
90	9.83297	8	9.96814	16	0.03202	9.86483	7	10	
91	9.83305	8	9.96829	15	0.03171	9.86476	7	09	7
91	9.83313	8	9.90829	15	0.03171	9.86469	7	08	1 0.7
93	9.83321	8	9.96859	15	0.03141	9.86462	7	07	2 1.4
94	9.83330	9	9.96874	15	0.03126	9.86455	7	06	3 2.1
94 95	9.83338	8	9.96890	16	0.03110	9.86448	7	05	4 2.8 5 3.5
96	9.83346	8	9.96905	15	0.03095	9.86441	7	04	6 4.2
97	9.83354	1	9.96920	15	0.03080	9.86434	7	03	7 4.9 8 5.6 9 6.3
98	9.83362	8	9.96935	15	0.03065	9.86427	7	02	8 5.6 9 6.3
99	9.83370	8	9.96950	15 16	0.03050	9.86420	7 7	OI	9 1 0.3
100	9.83378	0	9.96966	10	0.03034	9.86413	'	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.

O		Sin	d.	Tan	d. c.	Cot	Cos	d.]	P. P.
OI	00	9.83378		9.96966		0.03034	9.86413		100	
02 9.83395 8 9.99096 15 0.03004 9.86399 7 98 97 11 1.5 0.02969 9.86392 7 98 97 12 3.2 <	01			9.96981	-	0.03010	9.86406	1	99	
03 9.83431 8 9.970701 15 0.02989 9.80392 8 97 2 3.2 4.6 <td< th=""><th>02</th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></td<>	02									
04 9.83411 05 8 9.97026 9.83417 06 16 0.02971 0.02937 0.02938 0.02938 0.02938 0.02938 0.02938 0.02931 0.02	03	9.83403		9.97011		0.02989	9.86392		97	
o5 9.83419 of 9.83417 street 8 9.97072 ls 15 o.02948 of 9.86377 ls 7 yes 9.86377 ls 7 yes 6 yes 9.87078 ls 7 yes 6 yes 9.97072 ls 15 o.02943 yes 9.86370 ls 7 yes 6 yes 9.97078 ls 15 o.02913 yes 9.86370 ls 7 yes 9 yes 7 yes 9 yes 7 yes 8 yes 12 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 9 yes 16 yes 16 yes 9 yes 16 yes <th>04</th> <th>9.83411</th> <th>l .</th> <th>9.97026</th> <th>1</th> <th>0.02974</th> <th>9.86384</th> <th>l</th> <th>96</th> <th>3 4.8</th>	04	9.83411	l .	9.97026	1	0.02974	9.86384	l	96	3 4.8
oo 9.83425 09 8 9.97057 15 15 0.02943 0.02943 0.02963 0.02963 0.02963 0.02867 0.02863 0.02		9.83419		9.97042		0.02958	9.86377		95	4 6.4
07 9.83435 8 9.97072 15 0.02928 9.86363 7 93 7 11.2 9.9787 15 0.02913 9.86356 7 91 9 11.4 9.97102 15 0.0288 9.86349 7 91 9 11.4 9.97138 9.97138 15 0.02882 9.86335 7 91 9 11.4 9.97148 15 0.02882 9.863342 7 89 15 13.3 9.83476 8 9.97168 15 0.02852 9.863342 7 88 1 1.5 0.02852 9.863342 7 88 1 1.5 0.02852 9.863342 7 87 23 3.4 5 0.02852 9.863342 7 87 23 3.4 5 0.02716 9.86321 7 87 23 3.4 5 0.02716 9.86321 7 80 15 0.02716 9.86299 7 84 5 7 7 10.5 </th <th>06</th> <th>9.83427</th> <th></th> <th>9.97057</th> <th></th> <th>0.02943</th> <th></th> <th></th> <th>94</th> <th>5 8.0</th>	06	9.83427		9.97057		0.02943			94	5 8.0
10 9.8345 8 9.97102 15 0.02892 9.86349 7 91 9 14.44								1	93	
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16 9,83508 8 9,97209 16 0,02971 9,86299 7 84 6 9,5 6 9,029729 15 0,02716 9,86299 7 83 7 10,5 </th <th></th> <th></th> <th>8</th> <th></th> <th>15</th> <th></th> <th></th> <th>8</th> <th></th> <th>4 6.0</th>			8		15			8		4 6.0
17								7		5 7.5
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20 9.83540 8 9.97269 15 0.02731 9.86271 7 80 21 9.83548 8 9.97269 16 0.02715 9.86264 7 79 9 22 9.83556 9.997305 15 0.02700 9.86267 7 78 1 0.9 24 9.83573 8 9.97330 15 0.02670 9.862257 7 75 4 3.6 26 9.83581 8 9.97330 15 0.02655 9.86235 7 75 4 3.6 27 9.83581 8 9.97361 15 0.02659 9.86235 7 75 4 3.6 28 9.83597 8 9.97361 15 0.02639 9.86228 7 75 4 3.6 29 9.83613 8 9.97361 15 0.02699 9.86221 7 73 76 3.6 7.2 30 9.8										9 13.5
21 9.83548 9.97285 15 0.02715 9.86264 7 79 9 9 9 9 9 9 9	-							7		i
22 9.83556 8 9.97300 15 0.02700 9.86257 7 78 78 78 78 78 78 7			8		16			7		
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26 9.83589 8 9.97361 15 0.02638 9.86228 7 74 66 5.4 6.5 27 9.83597 8 9.97376 15 0.02624 9.86221 7 73 76 6.3 28 9.83693 8 9.97391 15 0.02609 9.86221 7 73 8 7.2 29 9.83613 8 9.97492 15 0.02593 9.86128 7 71 31 9.83629 8 9.97452 15 0.02594 9.86128 7 71 32 9.83637 8 9.97452 15 0.02593 9.86128 7 70 33 9.83638 8 9.97452 15 0.02588 9.86185 7 668 1 0.8 34 9.83653 8 9.97452 15 0.02533 9.86178 7 67 3 2.4 34 9.83653 8 9.97452 15 0.02538 9.86178 7 667 3 2.4 35 9.83661 8 9.97497 15 0.02533 9.86178 7 66 4 3.2 36 9.83669 8 9.97512 16 0.02593 9.86164 7 65 5 4.0 36 9.83669 8 9.97512 16 0.02488 9.86157 7 64 7 5.6 37 9.83677 8 9.97588 15 0.02487 9.86150 8 63 8 6.4 39 9.83693 8 9.97558 15 0.02457 9.86128 7 60 41 9.83701 8 9.97588 15 0.02412 9.86128 7 60 42 9.83717 8 9.97604 15 0.02361 9.86124 7 65 43 9.83733 8 9.97694 15 0.02381 9.86144 7 58 1 0.7 44 9.83733 8 9.97694 15 0.02366 9.86092 7 55 4 2.8 44 9.83733 8 9.97649 15 0.02361 9.86092 7 55 4 2.8 45 9.83741 8 9.97604 15 0.02366 9.86092 7 55 5 4 2.8 47 9.83757 8 9.97694 15 0.02351 9.86092 7 55 5 4 2.8 48 9.83765 8 9.97695 15 0.02336 9.86085 7 54 6 4.2 48 9.83757 8 9.97695 15 0.02336 9.86063 7 51		1			15	- 1		_		3 2.7
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28 9.83605 8 9.97391 15 0.02609 9.86214 7 72 8 7.22 8 7.22 8 9.81 30 9.83613 8 9.97421 15 0.02594 9.86200 8 7 71 72 9.81 31 9.83629 8 9.97437 15 0.02593 9.86192 69 8 32 9.83637 8 9.97452 15 0.02533 9.86185 7 68 1 0.8 34 9.83653 8 9.97487 15 0.02533 9.86178 7 66 4 3.2 4 35 9.83661 8 9.97497 15 0.02533 9.86171 7 66 4 3.2 4 36 9.83669 8 9.97512 16 0.02488 9.86177 7 64 7 56 5 4.0 37 9.83671 8 9.97538	27	9.83597		9.97376		0.02624	9.86221			7 6.3
30 9.83621 8 9.97421 15 0.02539 9.86202 7 7 70 8 31 9.83629 8 9.97452 15 0.02533 9.86185 7 68 1 0.8 3 32 9.83637 8 9.97467 15 0.02533 9.86178 7 66 3 2.4 4 9.83757 8 9.97582 15 0.02432 9.86150 7 66 4.8 9.97352 15 0.02432 9.86157 7 66 4.8 9.97582 15 0.02488 9.86157 7 66 4.8 9.97582 15 0.02488 9.86157 7 66 4.8 9.97582 15 0.02488 9.86157 7 64 7 5.6 6.4 8.8 9.97583 15 0.02488 9.86157 7 64 7 5.6 6.4 8.8 9.97583 15 0.02482 9.86150 8 62 9.722 9.86150 8 62 9.87532 15 0.02412 9.86150 8 62 9.722 9.86150 8 62 9.97583 15 0.02412 9.86150 8 62 9.722 9.86150 8 62 9.97593 15 0.02412 9.86150 7 60 9.83701 8 9.97588 16 0.02412 9.86121 7 59 7 7 60 9.83717 8 9.97649 15 0.02381 9.86107 8 57 2 1.44 9.83733 8 9.97649 15 0.02381 9.86092 7 55 4 2.8 8 49 9.83741 8 9.97649 15 0.02366 9.86092 7 55 5 3.5 46 9.83741 8 9.97649 15 0.02366 9.86092 7 55 5 3.5 46 9.83741 8 9.97649 15 0.02336 9.86085 7 54 6 4.2 47 9.83757 8 9.97695 15 0.02336 9.86085 7 54 6 4.2 47 9.83757 8 9.97695 15 0.02336 9.86085 7 54 6 4.2 48 9.83765 8 9.97695 15 0.02336 9.86085 7 54 6 6.2 9.83765 8 9.97695 15 0.02390 9.86063 7 51										8 7.2
30	29	9.83613		9.97406		0.02594	9.86207		71	9 8.1
31 9.83629 8 9.97437 15 0.02563 9.86192 7 68 1 0.8 32 9.83637 8 9.97457 15 0.02548 9.86185 7 66 2 1.6 34 9.83653 8 9.97487 15 0.02533 9.86177 7 66 4 3.2.4 35 9.83661 8 9.97497 15 0.02533 9.86164 7 66 4 3.2.4 36 9.83669 8 9.97512 16 0.02488 9.86157 7 66 4 3.2.4 37 9.83667 8 9.97512 16 0.02488 9.86157 7 64 6 4.8 38 9.83683 8 9.97543 15 0.02472 9.86150 8 63 8 6.4 40 9.83701 8 9.97584 15 0.02472 9.86128 7 60 4	30	9.83621		9.97421	- 1	0.02579	9.86200		70	
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33 9.83045 8 9.97467 15 0.02533 9.86178 7 66 3 2.4 34 9.83653 8 9.97482 15 0.02518 9.86171 7 66 4 3.2 35 9.83669 8 9.97512 15 0.02488 9.86167 7 64 6 48 7 5.6 4.0 64 7 5.6 4.8 7 5.6 4.8 7 5.6 4.8 7 5.6 4.8 6.2 9.86157 7 64 7 5.6 4.8 7 5.6 4.8 6.2 9.97538 15 0.024172 9.86150 8 62 9.7.2 39 9.83701 8 9.97558 15 0.02412 9.86128 7 60 7 7 60 7 7 60 7 7 4 9.83717 8 9.97694 15 0.023181 9.86121 7 59	32	9.83637		9.97452		0.02548	9.86185		68	
34	33	9.83645		9.97467		0.02533	9.86178		67	
37 9.83677 8 9.97528 16 0.02472 9.86150 8 63 8 0.4 7 5.6 8 63 8 9.97543 15 0.02472 9.86142 7 61 7 61 7 61 7 61 7 61 7 61 7 7 61 7 7 61 7 7 7 7 7 7 7 7 7			-							
37 9.83677 8 9.97528 16 0.02472 9.86150 8 63 8 0.4 7 5.6 8 63 8 9.97543 15 0.02472 9.86142 7 61 7 61 7 61 7 61 7 61 7 61 7 7 61 7 7 61 7 7 7 7 7 7 7 7 7										5 4.0
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43 9.83712 8 9.976619 15 0.02381 9.86107 8 57 2 1.4 7 85 1 0.7 15 0.02381 9.86107 8 57 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 4 2.8 3 2.9 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 3 2.1 4 2.8 3 2.9 3 2.1 3 2.1 3 2.1 4 2.8 4 2.8 8 9.97669 15 0.02351 9.86092 7 55 5 3.5 5 4 4.2 8 4 2.8 9.97699 16 0.02321 9.86078			8		16			7		
44 9.83733 8 9.97634 15 0.02361 9.86099 7 56 4 2.8 45 9.83741 8 9.97649 15 0.02361 9.86092 7 55 5 3.5 3.21 2.8 4.2 8 9.97649 15 0.023361 9.86092 7 55 5 3.5 5 3.5 3.21 <t< th=""><th></th><th></th><th></th><th></th><th>15</th><th></th><th></th><th>7</th><th></th><th>1 0.7</th></t<>					15			7		1 0.7
44 9.83741 8 9.97649 15 0.02361 9.86092 7 50 4 2.8 46 9.83749 8 9.97649 15 0.02351 9.86092 7 55 5 3.5 47 9.83757 8 9.97699 16 0.02321 9.86078 7 53 7 4.9 48 9.83765 8 9.97695 15 0.02305 9.86071 8 52 9 6.3 49 9.83773 8 9.97710 15 0.02209 9.86663 7 51					15			8		3 2.I
47 9.83757 8 9.97679 16 0.02321 9.86078 7 53 8 5.6 48 9.83765 8 9.97695 15 0.02305 9.86071 8 52 9 6.3 49 9.83773 8 9.97710 15 0.02290 9.86063 7 51										
47 9.83757 8 9.97679 16 0.02321 9.86078 7 53 8 5.6 48 9.83765 8 9.97695 15 0.02305 9.86071 8 52 9 6.3 49 9.83773 8 9.97710 15 0.02290 9.86063 7 51										$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
49 9.83773 8 9.97710 15 0.02290 9.80003 7 51			-		- 1					7 4.9
49 9.83773 8 9.97710 15 0.02290 9.80003 7 51						-				8 5.6
15										9 0.3
50 9.83781 9.97725 0.02275 9.86056 50	50	9.83781	٥		15	0.02275	9.86056	7	50	
Cos d. Cot d. c. Tan Sin d. P. P.			d.		d. c			d.		P. P.

	Sin	d.	Tan	d.c.	Cot	Cos	d.		P. P.
50	9.83781	8	9.97725	15	0.02275	9.86056	7	50	
51	9.83789	8	9.97740	15	0.02260	9.86049		49	
52	9.83797	8	9.97755	16	0.02245	9.86042	7 7	48	16
53	9.83805	8	9.97771	15	0.02229	9.86035	8	47	
54	9.83813	8	9.97786	15	0.02214	9.86027	7	46	I 1.6 2 3.2
55 56	9.83821 9.83829	8	9.97801 9.97816	15	0.02199	9.86020 9.86013	7	45	3 4.8
-		8		15			7	44	4 6.4
57 58	9.83837 9.83845	8	9.97831 9.97846	15	0.02169	9.86006 9.85999	7	43	5 8.0
59	9.83853	8	9.97862	16	0.02154	9.85991	8	42 41	6 9.6
60	9.83861	8	9.97877	15	0.02123	9.85984	7	40	7 II.2 8 I2.8
61	9.83869	8	9.97892	15	0.02108	9.85977	7	39	9 14.4
62	9.83877	8	9.97997	15	0.02093	9.85970	7	38	3
63	9.83885	8	9.97922	15	0.02078	9.85962	8	37	
64	9.83898	8	9.97938	16	0.02062	9.85955	7	36	15
65	9.83901	8	9.97953	15	0.02047	9.85948	7	35	1 1.5
66	9.83909	8	9.97968	15 15	0.02032	9.85941	7	34	2 3.0
67	9.83917	8	9.97983		0.02017	9.85934	8	33	3 4.5
68	9.83925	7	9.97998	15 15	0.02002	9.85926	7	32	4 6.0
69	9.83932	8	9.98013	16	0.01987	9.85919	7	31	5 7.5 6 9.0
70	9.83940	8	9.98029	15	0.01971	9.85912	7	30	6 9.0 7 10.5
71	9.83948	8	9.98044	15	0.01956	9.85905	8	29	8 12.0
72	9.83956	8	9.98059	15	0.01941	9.85897	7	28	9 13.5
73	9.83964	8	9.98074	15	0.01926	9.85890	7	27	
74	9.83972	8	9.98089	15	0.01911	9.85883	7	26	
75	9.83980	8	9.98104	16	0.01896	9.85876	8	25	
76	9.83988	8	9.98120	15	0.01880	9.85868	7	24	
77 78	9.83996	8	9.98135 9.98150	15	0.01865	9.85861 9.85854	7	23 22	8
79	9.84012	8	9.98165	15	0.01835	9.85847	7	21	1 0.8
80	9.84020	8	9.98180	15	0.01820	9.85839	8	20	2 1.6
81	9.84027	7	9.98195	15	0.01805	9.85832	7	19	3 2.4
82	9.84035	8	9.98211	16	0.01789	9.85825	7	18	4 3.2
83	9.84043	8	9.98226	15	0.01774	9.85817	8	17	5 4.0
84	9.84051	8	9.98241	15	0.01759	9.85810	7	16	6 4.8 7 5.6
85	9.84059	8	9.98256	15	0.01744	9.85803	7	15	8 6.4
86	9.84067	8	9.98271	15 16	0.01729	9.85796	7 8	14	9 7.2
87	9.84075	8	9.98287		0.01713	9.85788		13	
88	9.84083	8	9.98302	15 15	0.01698	9.85781	7 7	12	
89	9.84091	7	9.98317	15	0.01683	9.85774	8	II	7
90	9.84098	8	9.98332	15	0.01668	9.85766	7	10	I 0.7
91	9.84106	8	9.98347	15	0.01653	9.85759	7	09	2 I.4
92	9.84114	8	9.98362	16	0.01638	9.85752	7	08	3 2.1
93	9.84122	8	9.98378	15	0.01622	9.85745	8	07	4 2.8 5 3.5
94	9.84130	8	9.98393	15	0.01607	9.85737	7	06	6 4.2
95	9.84138	8	9.98408	15	0.01592	9.85730	7	05	7 4.9
96	9.84146	8	9.98423	15	0.01577	9.85723	8	04	8 5.6
97	9.84154	7	9.98438	15	0.01562	9.85715	7	03	9 6.3
98 99	9.84161	8	9.98453	16	0.01547	9.85708 9.85701	7	02 01	
100	9.84177	8	9.98484	15	0.01516	9.85693	8	00	
100		- 1		4.0			- d	-00	P. P.
	Cos	d.	Cot	d.c.	Tan	Sin	d.		P. P.

44°								135	
	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
00	9.84177		9.98484		0.01516	9.85693	-	100	
10	9.84185	8	9.98499	15	0.01501	9.85686	7	99	
02	9.84193	8	9.98514	15	0.01486	9.85679	7 8	98	40
03	9.84201	8	9.98529	15	0.01471	9.85671	7	97	16
04	9.84209		9.98544	15	0.01456	9.85664		96	1 1.6
05	9.84216	7	9.98560	16	0.01440	9.85657	7 8	95	2 3.2
06	9.84224	8	9.98575	15 15	0.01425	9.85649	7	94	3 4.8 4 6.4
07	9.84232	1 1	9.98590		0.01410	9.85642	7	93	4 6.4 5 8.0
о8	9.84240	8	9.98605	15	0.01395	9.85635	8	92	6 9.6
09	9 84248	7	9.98620	15	0.01380	9.85627	7	91	7 11.2
10	9.84255	8	9.98635	16	0.01365	9.85620	7	90	8 12.8
11	9.84263		9.98651		0.01349	9.85613	8	8 9	9 14.4
12	9.84271	8 8	9.98666	15	0.01334	9.85605	7	88	
13	9.84279	8	9.98681	15 15	0.01319	9.85598	7	87	
14	9.84287		9.98696		0.01304	9.85591	8	86	15
15	9.84295	8	9.98711	15	0.01289	9.85583	7	85	I 1.5
16	9.84302	7 8	9.98726	15 16	0.01274	9.85576	7	84	2 3.0
17	9.84310	8	9.98742	15	0.01258	9.85569	8	83	3 4.5
18	9.84318	8	9.98757	15	0.01243	9.85561	7	82	4 6.0
19	9.84326	8	9.98772	15	0.01228	9.85554	7	81	5 7.5 6 9.0
20	9.84334	7	9.98787	15	0.01213	9.85547	8	80	7 10.5
21	9.84341	1	9.98802	15	0.01198	9.85539		79	8 12.0
22	9.84349	8	9.98817	16	0.01183	9.85532	7 8	78	9 13.5
23	9.84357	8	9.98833	15	0.01167	9.85524	7	77	
24	9.84365	8	9.98848	15	0.01152	9.85517	7	76	
25	9.84373	7	9.98863	15	0.01137	9.85510	8	75	
26	9.84380	8	9.98878	15	0.01122	9.85502	7	74	
27	9.84388	8	9.98893	15	0.01107	9.85495	8	73	8
28	9.84396	8	9.98908	16	0.01092	9.85487	7	72	
29	9.84404	7	9.98924	15	0.01076	9.85480	7	71	2 0.8
30	9.84411	8	9.98939	15	6.01061	9.85473	8	70	3 2.4
31	9.84419	8	9.98954	15	0.01046	9.85465	7	69	4 3.2
32	9.84427	8	9.98969	15	0.01031	9.85458	8	68	5 4.0
33	9.84435	7	9.98984	15	0.01016	9.85450	7	67	6 4.8
34	9.84442	8	9.98999	16	0.01001	9.85443	7	66	7 5.6
35	9.84450	8	9.99015	15	0.00985	9.85436	8	65 64	8 6.4
36	9.84458	8	9.99030	15	0.00970	9.85428	7		9 7.2
37	9.84466	7	9.99045	15	0.00955	9.85421	8	63 62	l
38	9.84473	8	9.99060	15	0.00940	9.85413 9.85406	7	61	7
39	9.84481	8	9.99075	15	0.00925		7	60	
40	9.84489	8	9.99090	16	0.00910	9.85399	8		1 0.7
41	9.84497	7	9.99106	15	0.00894	9.85391	7	59	2 I.4 3 2.1
42	9.84504	8	9.99121	15	0.00879	9.85384 9.85376	8	58 57	4 2.8
43	9.84512	8	9.99136	15	1		7	1	5 3.5
44	9.84520	8	9.99151	15	0.00849	9.85369	8	56	6 4.2
45	9.84528	7	9.99166	15	0.00834	9.85361 9.85354	7	55 54	7 4.9
46	9.84535	8	9.99181	15	1		7	ŀ	8 5.6
47	9.84543	8	9.99196	16	0.00804	9.85347 9.85339	8	53 52	9 6.3
48	9.84551	7	9.99212 9.99227	15	0.00788	9.85339	7	5 ²	
49	9.84558	. 8		15	0.00758	9.85324	8	50	
50	9.84566	-1	9.99242 Cot	d. c.	Tan	Sin	d.	 —	P. P.
	Cos	d.	Cot	ı a. c.	ı ıan	. 3111	ı u.		1.1.

	Sin	d.	Tan	d. c.	Cot	Cos	d.		P. P.
50	9.84566		9.99242		0.00758	9.85324		50	
51	9.84574	8	9.99257	15	0.00743	9.85317	7	49	
52	9.84582	8	9.99237	15	0.00728	9.85309	8	48	
53	9.84589	7	9.99287	15	0.00713	9.85302	7	47	16
54	9.84597	8	9.99303	16	0.00697	9.85294	8	46	1 1.6
55	9.84605	8	9.99318	15	0.00682	9.85287	7	45	2 3.2
56	9.84612	7 8	9.99333	15	0.00667	9.85279	8	44	3 4.8
57	9.84620		9.99348	15	0.00652	9.85272	7	43	4 6.4
58	9.84628	8	9.99363	15	0.00637	9.85265	7	42	5 8.0 6 9.6
59	9.84635	7 8	9.99378	15 16	0.00622	9.85257	8 7	41	7 11.2
60	9.84643	8	9.99394		0.00606	9.85250	8	40	8 12.8
61	9.84651		9.99409	15	0.00591	9.85242		39	9 14.4
62	9.84659	8	9.99424	15	0.00576	9.85235	7 8	38	
63	9.84666	7 8	9.99439	15	0.00561	9.85227	7	37	
64	9.84674	8	9.99454	15	0.00546	9.85220	8	36	15
65	9.84682		9.99469	15 16	0.00531	9.85212	7	35	I 1.5
66	9.84689	7 8	9.99485	15	0.00515	9.85205	8	34	2 3.0
67	9.84697	8	9.99500		0.00500	9.85197	7	33	3 4.5
68	9.84705	7	9.99515	15 15	0.00485	9.85190	8	32	4 6.0
69	9.84712	8	9.99530	15	0.00470	9.85182	7	31	5 7.5
70	9.84720	8	9.99545	15	0.00455	9.85175	8	30	6 9.0 7 10.5
71	9.84728		9.99560	16	0.00440	9.85167	7	29	8 12.0
72	9.84735	7 8	9.99576	15	0.00424	9.85160	8	28	9 13.5
73	9.84743	8	9.99591	15	0.00409	9.85152	7	27	, , , , ,
74	9.84751	7	9.99606	15	0.00394	9.85145	8	26	
75	9.84758	8	9.99621	15	0.00379	9.85137	7	25	
76	9.84766	7	9.99636	15	0.00364	9.85130	8	24	
77	9.84773	8	9.99651	15	0.00349	9.85122	7	23	8
78	9.84781	8	9.99666	16	0.00334	9.85115	8	22	l
79	9.84789	7	9.99682	15	0.00318	9.85107	7	21	1 0.8 2 1.6
80	9.84796	8	9.99697	15	0.00303	9.85100	8	20	3 2.4
81	9.84804	8	9.99712	15	0.00288	9.85092	7	19	4 3.2
82	9.84812	7	9.99727	15	0.00273	9.85085	8	18	5 4.0
83	9.84819	8	9.99742	15	0.00258	9.85077	8	17	6 4.8
84	9.84827	8	9.99757	16	0.00243	9.85069	7	16	7 5.6
85 86	9.84835	7	9.99773	15	0.00227	9.85062	8	15 14	8 6.4
	9.84842	8	9.99788	15		9.85054	7		9 7.2
87 88	9.84850	7	9.99803	15	0.00197	9.85047	8	13	
89	9.84857 9.84865	8	9.99818 9.99833	15	0.00182	9.85039 9.85032	7	11	7
90		8		15	0.00152	9.85024	8	10	ł
	9.84873	7	9.99848	16			7		I 0.7 2 I.4
91	9.84880	8	9.99864	15	0.00136	9.85017	8	o9 o8	3 2.1
92 93	9.84888 9.84895	7	9.99879 9.99894	15	0.00121	9.85009	8	07	4 2.8
		8		15			7	06	5 3.5
94 95	9.84903	8	9.99909 9.99924	15	0.00091	9.84994 9.84986	8	05	6 4.2
95 96	9.84918	7	9.99924	15	0.00070	9.84979	7	04	7 4.9
97	9.84926	8	9.99955	16	0.00045	9.84971	8	03	8 5.6
98	9.84933	7	9.99935	15	0.00045	9.84964	7 8	02	9 6.3
99	9.84941	8	9.99970	15	0.00015	9.84956	7	01	
100	9.84949	8	10.00000	15	0.00000	9.84949	'	00	
	Cos	d.	Cot	d. c.	Tan	Sin	d.		P. P.
	CUS	· u.	COL	ı u. c.	1411	Om	u.		

TABLE XXVI.—Logarithmic Versed Sines and External Secants Log vs = $2\log\alpha^\circ + V$ Log exsec = $2\log\alpha^\circ + E$

Hun-		0	۰		Hun-		1	°	
dredths	Vers	V	E	Exsec	dredths	Vers	V	E	Exsec
			182					182	
00	Inf. neg.	725	725	Inf. neg.	00	6.18271	714	780	6.18278
02	2.78478	725	725	2.78478	02	.19991	713	782	.19998
04 06	3.38684	725 725	725 725	3.38684	04 06	.21678	713 712	785 787	. 21685
08	.98890	725	725	.98890	08	.24956	712	789	.24964
10	4.18272	725	725	4.18272	10	6.26549	711	791	6.26557
12	.34109	725	726	.34109	12	.28115	71 J	794	.28123
14	.47498	725	726	.47498	14	.29652	711	797	.29661
16	.59096	724	726	.59096	16	.31163	710	799	.31172
18	.69327	724	727	.69327	18	.33461	709	801	.33470
20	4.78478	724	727	4.78479	20	6.34107	709	804	6.34116
22	.86757	724	727	.86757	22	-35543	708	807	-35553
24 26	.94315 5.01267	724 724	728 729	.94315 5.01268	24 26	.36955	708 707	810 812	. 36965
28	.07704	724	729	.07705	28	.39713	707	815	.39724
30	5.13697	724	730	5.13697	30	6.41059	706	818	6.41070
32	.19302	724	731	.19303	32	.42385	706	821	.42397
34	.24568	723	731	.24569	34	. 43691	705	824	.43703
36	. 29533	723	732	.29534	36	.44977	704	827	. 44989
38	.34229	723	733	.34230	38	. 46246	704	830	. 46259
40	5.38684	723	734	5.38685	40	6.47496	703	833	6.47509
42	.42922	723	735	.42923	42	. 48728	703	836	.48741
44	.46962	722	735	.46964	44	49943	702	839	.49957
46	.50824	722	736	.50825	46	.51141	701	842	.51155
48 50	.54521 5.58066	722 722	737 739	5.58068	48 50	.52322 6.53488	700 700	845 849	6.53503
52	.61473	722	740	.61475	52	.54639	699	852	.54654
54	.64751	721	740	.64753	54	.55774	699	855	.55790
56	.67910	721	742	.67912	56	.56895	698	859	.56911
58	. 70958	721	743	. 70960	58	.58001	697	863	.58018
60	5.73902	721	745	5.73904	60	6.59093	697	866	6.59110
62	.76750	720	746	.76753	62	.60173	696	870	.60190
64	.79508	720	747	.79511	64	.61238	695	873	.61256
66 68	.82181	720	749	.82184	66	.62291	694	877	.62309
70	.84774 5.87292	720 719	750 752	.84777 5.87295	68 70	.63331 6.64359	694 693	881 884	6.64378
72	.89738	719	753	.89742	70	.65375	692	888	.65395
74	.92118	719	755	.92122	74	.66379	692	892	.66399
76	.94435	718	756	.94438	76	.67372	691	896	.67392
78	.96691	718	758	.96695	78	.68353	690	900	.68374
80	5.98890	718	760	5.98894	80	6.69323	689	903	6.69345
82	6.01034	717	762	6.01039	82	.70383	688	907	.70405
84 86	.03128	717	764 766	.03132	84 86	.71232	687 686	911	.71254
88	.05171	717 716	767	.05176	88	.72171	686	915	.72194
90	6.09120	716	769	6.09125	90	.73100 6.74019	685	919 924	6.74043
92	.11029	715	772	.11035	92	.74929	684	924	.74953
94	.12897	715	774	.12903	94	.75829	683	932	.75854
96	. 14726	715	776	.14732	96	.76718	682	936	.76743
98	.16517	714	778	.16523	98	.77601	681	941	.77627
100	6.18271	714	780	6.18278	100	6.78474	681	945	6.78500

TABLE XXVI.—Logarithmic Versed Sines and External Secants $\mbox{Log vs} = 2\log\alpha^\circ + V \qquad \mbox{Log exsec} = 2\log\alpha^\circ + E$

Hun-		2	٥		Hun-		3	٥	
dredths	Vers	V	E	Exsec	dredths	Vers	V	E	Exsec
		6.	182				6.182	6.183	
00	6.78474	681	945	6.78501	00	7.13687	626	221	7.13746
02	.79338	680	950	.79365	02	.14264	624	228	. 14324
04	.80194	679	954	.80221	04	.14837	623	234	.14898
06	.81041	678	958	.81069	06	.15406	621	241	.16468
08	.81880 6.82712	677 676	963 968	.81909 6.82741	08 10	. 15972 7. 16534	620 619	248 255	.16035 7.16598
12	.83535	675	973	.83565	12	.17093	618	255 261	.17157
14	.84350	674	978	.84381	14	.17648	616	268	.17713
16	.85158	673	982	.85189	16	.18199	614	275	. 18265
18	.85959	672	987	.85990	18	. 18747	613	283	.18814
20	6.86752	671	992	6.86784	20	7.19291	612	290	7.19359
22	.87538	670	997	.87570	22	. 18832	610	296	.19901
24 26	.88317	669 668	*002	.88350	24 26	.20370	609 607	303 311	. 20439
28	. 89854	667	011	.89888	28	.21435	606	318	.20975
30	6.90612	666	016	6.90647	30	7.21963	605	325	7.22035
32	.91364	665	022	.91400	32	.22488	603	333	.22561
34	.92110	664	027	.92146	34	.23010	602	340	. 23083
36	. 92849	663	032	.92886	36	. 23528	600	348	. 23603
38	.93582	662	037	.93619	38	. 24043	599	355	.24119
40	6.94308	66I	042	6.94347	40	7.24556	597	362	7.24632
42	. 95029	660	048	.95068	42	.25065	596	370	.25142
44 46	.95744 .96453	659 658	053 058	.95783	44 46	.25571 .26075	595 593	377 385	.25649 .26154
48	.90453	657	063	.97197	48	.26575	591	393	. 26655
50	6.97854	656	069	6.97895	50	7.27073	590	400	7.27154
52	.98546	655	075	.98588	52	. 27567	588	408	. 27649
54	.99232	654	081	.99275	54	.28059	587	416	.28142
56	.99913	652	286	-99957	56	.28549	585	424	. 28632
58	.00589	651	092	. 00633	58	.29035	583	432	.29120
60	7.01260	650	098	7.01304	60	7.29519	582	440	7.29605
62 64	.01925	649 648	103	.01971	62 64	.30000	581	448 456	.30087 .30566
66	.03241	646	115	.03288	66	.30478	579 577	464	.31043
68	.03891	645	121	.03939	68	.31427	575	472	.31517
70	7.04537	644	127	7.04585	70	7.31898	574	480	7.31988
72	.05178	643	133	.05227	72	. 32366	572	488	.32457
74	.05814	642	139 145	.05864	74	.32831	571	496	.32924
76 78	.06446	640 639	151	.06496	76 78	.33294	569 567	504 512	. 33388
80	7.07695	638	157	7.07747	1 80	7.34213	566	521	7.34309
82	.08314	637	163	.08366	82	.34669	564	529	.34766
84	.08927	636	169	.08981	84	.35122	562	538	. 35220
86	.09537	634	176	.09 5 91	86	-35574	560	547	. 35672
88	.10142	633	182	. 10197	88	. 36022	558	556	.36122
90	7.10743	632	189 195	7.10799	90	7.36469	557	564	7.36569
92	.11340	631 630	201	.11396	92	.36913	555	572 581	.37014
94 96	.11932	628	208	.11790	94 96	.37355 .37794	553 552	590	.37457 .37898
98	.13106	627	215	.13165	98	.38232	550	599	.38337
100	7.13687	626	22I * 183	7.13746	100	7.38667	548	6 08	7.38773
	,		4 183			, , , , , , ,	J /-		

		4	۰			-	5	۰	
Hun- dredths	Vers	Diff.	Exsec	Diff.	Hun- dredths	Vers.	Diff.	Exsec	Diff.
		100.		.001			.001		.001
00	7.38667	21,65	7.38773	21.75	00	7.58039	17.30	7.58204	17.40
02	.39100	21.55	.39207	21.60	02	.58385	17.30	.58552	17.35
04 06	.39531	21.45	.39639	.21.50	04 06	.58731	17.15	.58899	17.25
· 08	.39960	21.30		21.35	08	.59074	17.15	.59244	17.20
. 09	.40386	21.25	.40496 7.40922	21.30	10	.59417 7.59758	17.05	.59588 7.59930	17.10
12	.41233	21.10	.41346	21.20	12	.60098	17.00	.60271	17.05
14	.41654	21.05	.41767	21.05	14	,60436	16.90	.60611	17.00
16	.42072	20.90	.42187	21.00	16	.60773	16.85	.60949	16.90
18	.42488	20.80	.42604	20.85	18	.61109	16.80 16.70	.61287	16.90 16.75
20	7.42903	20.75	7.43020	20.65	20	7.61443	16.70	7.61622	16.75
22	.43315		.43433	20.60	22	.61777	16.55	.61957	16.65
24	.43726	20.55	.43845	20.50	24	.62108	16.55	.62290	16.60
26	.44134	20.35	-44255	20.35	26	.62439	16.50	.62622	16.55
28	.44541	20.25	.44662	20.30	28	.62769	16.40	.62953	16.50
30	7.44946	20.15	7.45068	20.20	30	7.63097	16.35	7.63283	16.40
32	.45349	20.05	.45472	20.10	32	.63424	16.25		16.35
34 36	.45750 .46149	19.95	.45874	20.05	34 36	.63749 .64074	16.25	.63938 .64264	16.30
38	.46546	19.85	.46673	19.90	38	.64397	16.15	.64589	16.25
40	7.46942	19.80	7.47070	19.85	40	7.64719	16.10	7.64912	16.15
42	•47335	19.65	.47465	19.75	42	.65040	16.05	.65235	16.15
44	.47727	19.60	.47858	19.65	44	.65360	16.00	.65556	16.05
46	.48118	19.55	.48249	19.55	46	.65678	15.90	.65876	16.00 15.90
48	.48506	19.40	. 48639	19.50	48	.65995		.66194	
50	7.48893	19.35	7.49027	19.40	50	7.66312	15.85	7.66512	15.90 15.85
52	.49278	19.15	.49413	19.30	52	.66627	15.70	.66829	15.75
54	.49661	19.10	-49797	19.15	54	.66941	15.60	.67144	15.70
56	.50043	18.95	.50180	19.05	56	.67253	15.60	.67458	15.65
58	.50422	18.95	.50561	19.00	58	.67565	15.55	.67771	15.60
60	7.50801	18.80	7.50941	18.90	60	7.67876	15.45	7.68083	15.55
62 64	.51177	18.75	.51319	18.80	62 64	.68185	15.40	.68394	15.50
66	.51552 .51926	18.70	.51695	18.75	66	.68800	15.35	.69013	15 45
68	.52297	18.55	.52443	18.65	68	.69107	15.35	.69320	15.35
70	7.52668	18.55	7.52814	18.55	70	7.69412	15.25	7.69627	15.35
72	.53036	18.40	.53184	18.50 18.40	72	.69716	15.20	.69932	15.25 15.25
74	.53403	18.30	.53552	18.35	74	.70019		.70237	15.15
76	.53769	18.20	.53919	18.25	76	.70320	15.05 15.05	.70540	15.15
78	.54133	18.10	.54284	18.20	78	.70621	15.00	.70843	15.05
80	7.54495	18.05	7.54648	18.10	80	7.70921	14.95	7.71144	15.00
82	.54856	17.90	.55010	18.05	82	.71220	14.85	.71444	14.95
84	.55216	17.90	.55371	17.95	84	.71517	14.85	.71743	14.95
86	.55574	17.80	.55730	17.90	86	.71814	14.80	.72042	14.85
88 90	.55930 7.56285	17.75	.56088 7.56444	17.80	88 90	.72110 7.72405	14.75	7.72635	14.80
90 92	.56639	17.70	.56799	17.75	90	.72698	14.65	.72930	14.75
94	.56991	17.65	.57153	17.70	94	.72991	14.65	.73225	14.75
96	.57342	17.55	.57505	17.60	96	.73283	14.60	.73518	14.65
98	.57691	17.45	.57855	17.50	- 98	73573	14.50	.73810	14.60
100	7.58039	17.40	7.58204	11.43	100	7.73863	14.30	7.74102	14.33

TABLE XXVI. — (Continued)

		6	۰				7	٥	
Hun- dredths		Diff.		Diff.	Hun- dredths		Diff.		Diff.
dreaths	Vers	.001	Exsec	.001	dreaths	Vers	.001	Exsec	.001
00	7.73863	14.45	7.74102	14.50	00	7.87238	12.40	7.87563	12.45
02	.74152	14.40	.74392	14.45	02	.87486	12.30	.87812	12.45
04	.74440	14.35	.74681	14.45	04	.87732	12.30	.88061	12.45
06	.74727	14.25	.74970	14.35	06	.87978	12.30	.88309	12.35
08	.75012	14.25	.75257	14.35	08	.88224	12.25	.88556	12.35
10 12	7.75297	14.20	7.75544	14.30	10 12	7.88469	12.20	7.88803	12.30
	.75581	14.20	.75830	14.20		.88713	12.15	.89049	12.25
14 16	.75865 .76147	14.10	.76114 .76398	14.20	14 16	.88956 .89199	12.15	.89294	12.25
18	.76428	14.05	.76681	14.15	18	.89199	12.10	.89539	12.15
20	7.76708	14.00	7.76963	14.10	20	7.89682	12.05		12.20
		14.00		14.05			12.00	7.90026	12.10
22 24	.76988 .77266	13.90	.77244 .77525	14.05	22 24	.89922 .90162	12.00	.90268	12.10
26	.77544	13.90	.77804	13.95	26	.90102	12.00	.90510	12.05
28	.77821	13.85	.78082	13.90	28	.90402	11.90	.90992	12.05
30	7.78097	13.80	7.78360	13.90	30	7.90878	11.90	7.91232	12.00
32	.78372	13.75	.78637	13.85	32	.91116	11.90	.91471	11.95
34	.78646	13.70	.78912	13.75	34	.91352	11.80	.91710	11.95
3 4 36	.78919	13.65	.79187	13.75	36	.91588	11.80	.91718	11.90
38	.79192	13.65	.79462	13.75	38	.91824	11.80	.92185	11.85
40	7.79463	13.55	7.79735	13.65	40	7.92058	11.70	7.92422	11.85
42	.79734	13.55	.80007	13.60	42	.92293	11.75	.92658	11.80
44	.80004	13.50	.80279	13.60	44	.92526	11.65	.92893	11.75
46	.80273	13.45	.80550	13.55	46	.92759	11.65	.93128	11.75
48	.80541	13.40	.80820	13.50	48	.92991	11.60	.93362	11.70
50	7.80809	13.40	7.81089	13.45	50	7.93223	11.60	7.93596	11.70
52	.81075	13.30 13.30	.81357	13.40	52	.93454	11.55	.93829	11.65
54	.81341		.81624	13.35	54	.93684	11.50	.94061	i
56	.81606	13.25 13.20	.81891	13.35	56	.93914	11.50	.94293	11.60
58	.81870	13.15	.82157	13.30 13.25	58	.94143	II.45 II.45	.94524	11.55
60	7.82133	13.15	7.82422	13.20	60	7.94372	11.35	7.94755	11.50
62	.82396		.82686	-	62	.94599	1	.94985	
64	.82657	13.05 13.05	.82950	13.20 13.10	64	.94827	11.40	.95214	11.45
66	.82918	13.05	.83212	13.10	66	.95054	11.35	-95443	11.45
68	.83179	12.95	.83474	13.10	68	.95280	11.25	.95671	11.40
70	7.83438	12.95	7.83736	13.10	70	7.95505	II.25	7.95899	11.40
72	.83697	12.85	.83996	13.00	72	.95730	11.25	.96126	11.30
74	.83954	12.85	.84256	12.90	74	95955	11.15	. 96352	11.30
76 78	.84211	12.85	.84514	12.95	76 78	.96178	11.20	.96578	11.25
78 80	.84468	12.75	.84773	12.85	80	.96402	11.10	.96803	11.25
	7.84723	12.75	7.85030	12.80		7.96624	11.10	7.97028	11.20
82	.84978	12.70	.85286	12.80	82	.96846	11.10	.97252	11.20
84 86	.85232 .85485	12.65	.85542 .85797	12.75	8 ₄ 86	.97068	11.05	.97476	11.15
88		12.65		12.75	88	.97289	11.00	.97699	11.10
88 90	.85738 7.85990	12.60	.86052 7.86306	12.70	90	.97509 7.97729	11.00	.97921 7.98143	11.10
90	.86241	12.55	.86558	12.60	92	.97948	10.95	.98365	11.10
94	.86491	12.50	.86811	12.65	94	.98167	10.95	.98585	11.00
94 96	.86741	12.50	.87062	12.55	94	.98385	10.90	. 98806	11.05
98	.86990	12.45	.87313	12.55	98	.98603	10.90	.99025	10.95
100	7.87238	12.40	7.87563	12.50	100	7.98820	10.85	7.99245	11.00

Hun-		8	•		Hun-		9	•	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	7.98820	10.80	7.99245		00	8.09032	9.60	8.09570	9.70
02	.99036	10.80	.99463	10.90	02	.09224	9.60	.09764	9.70
04	.99252	10.80	.99681	10.90	04	.09416	9.60	.09959	9.60
06	.99468	10.75	.99899	10.85	06	.09608	9.55	.10153	9.65
08	.99683	10.70	8.00116	10.85	08	.09799	9.50	.10346	9.70
10	7.99897	10.70	8.00333	10.80	10	8.09989	9.55	8.10540	9.60
12	8.00111	10.65	.00549	10.75	12		9.50	.10732	9.65
14	.00324	10.65	.00764	10.75	14 16	. 10370	9.45	.10925	9.55
16 18	.00537	10.60	.01193	10.70	18	.10559	9.45	.11110	9.60
20	8.00961	10.60	8.01407	10.70	20	8.10937	9.45	8.11499	9.55
		10.55	.01621	10.70		.11125	9.40	.11690	9.55
22 24	.01172	10.55	.01021	10.65	22 24	.11123	9.40	.11880	9.50
26	.01593	10.50	.02046	10.60	26	.11500	9.35	.12070	9.50
28	.01803	10.50	.02258	10.60	28	.11687	9.35	.12259	9.45
30	8,02012	10.45	8.02469	10.55	30	8.11874	9.35	8.12448	9.45
32	.02221	10.45	.02680	10.55	32	.12060	9.30	.12637	9.45
34	.02429	10.40	.02891	10.55	34	.12246	9.30	,12825	9.40
36	.02637	10.40	.03101	10.50	36	.12431	9.25 9.25	.13013	9.40
38	.02844	10.35	.03310	10.45	38	.12616	9.25	.13201	9.40
40	8.03051	10.30	8.03519	10.40	40	8.12801	9.20	8.13388	9.30
42	.03257	_	.03727	10.40	42	.12985	9.20	.13574	9.35
44	.03462	10.25	.03935	10.40	44	.13169	9.20	.13761	9.35
46	.03668	10.20	.04143	10.35	46	.13352	9.15	.13947	9.25
48	.03872	10.25	.04350	10.30	48	.13535	9.15	.14132	9.25
50	8.04077	10.15	8.04556	10.30	50	8.13718	9.10	8.14317	9.25
52	.04280	10.20	.04762	10.20	52	.13900	9.10	.14502	9.25
54	.04484	10.10	.04968	10.25	54	.14082	9.05	.14687	9.20
56 58	.04686	10.15	.05173	10.25	56 58	.14263	9.05	.14871	9.15
60		10.10	8.05582	10.20	60	8.14625	9.05	8.15238	9.20
	8.05091	10.05		10.15			9.00		9.10
62 64	.05292	10.05	.05785	10.20	62 64	.14805	9.00	.15420	9.15
66	.05693	10.00	.06191	10.10	66	.15165	9.00	.15785	9.10
68	.05893	10.00	.06394	10.15	68	.15344	8.95	.15967	9.10
70	8.06093	10.00	8.06595	10.05	70	8.15523	8.95	8.16148	9.05
72	.06292	9.95	.06797	10.10	72	.15702	8.95 8.90	. 16330	9.10
74	.06491	9.95	.06998	10.00	74	.15880	8.85	.16510	9.05
76	.06689	9.90	.07198	10.00	76	.16057	8.90	.16691	9.00
78	.06886	9.03	.07398	10.00	78	.16235	8.85	.16871	8.95
80	8.07084	9.80	8.07598	9.95	80	8.16412	8.80	8.17050	8.95
82	.07280	9.85	.07797	9.95	82	.16588	8.85	.17229	8.95
84	.07477	9.80	.07996	9.90	84	.16765	8.80	.17408	8.95
86	.07673	9.75	.08194	9.90	86	.16941	8.75	.17587	8.90
88	.07868	9.75	.08392	9.85	88	.17116	8.75	. 17765	8.90
90 92	8.08063 .08258	9.75	8.08589	9.85	90	8.17291 .17466	8.75	8.17943	8.85
	1	9.70		9.85	92		8.75	.18298	8.90
94 96	.08452	9.70	.08983	9.80	94 96	.17641	8.70	.18298	8.80
98	.08839	9.65	.09179	9.75	98	.17989	8.70	.18651	8.85
100	8.09032	9.65	8.09570	9.80	100	8.18162	8.65	8.18827	8.80

Hun-		10	o°		Hun-		11	l°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	8.18162	8.65	8.18827	8.80	00	8.26418	7.85	8.27223	8.00
02	. 18335	8.65	.19003	8.75	02	. 26575	7.85	. 27383	8.00
04	.18508	8.60	.19178	8.75	04	. 26732	7.85	.27543	8.00
06	.18680	8.65	.19353	8.75	06	. 26889	7.80	.27703	7.95
08 10	. 18853 8 . 19024	8.55	.19528 8.19703	8.75	08	. 27045 8. 27201	7.80	. 27862 8. 28021	7.95
12	.19196	8.60	.19877	8.70	12	.27357	7.80	.28180	7.95
14	.19367	8.55	.20050	8.65	14	.27513	7.80	. 28339	7.95
16	.19537	8.50	.20224	8.70	16	.27668	7.75	.28497	7.90
18	. 19708	8.55 8.50	. 20397	8.65 8.65	18	. 27823	7.75 7.75	. 28655	7.90
20	8.19878	-	8.20570	8.60	20	8.27978		8.28813	7.85
22	.20047	8.45	.20742		22	.28132	7.70	.28970	
24	.20217	8.50 8.45	.20914	8.60 8.60	24	. 28286	7.70	. 29128	7.90 7.80
26	. 20386	8.45	.21086	8.55	26	. 28440	7.70	.29284	7.85
28	. 20555	8.40	.21257	8.55	28	. 28594	7.65	.29441	7.85
30	8.20723	8.40	8.21428	8.55	30	8.28747	7.65	8.29598	7.80
32	. 20891	8.40	.21599	8.55	32	. 28900	7.65	.29754	7.75
34	.21059	8.35	.21770	8.50	34 36	.29053	7.65	.30065	7.80
36 38	.21220	8.35	.21940	8.50	38	. 29358	7.60	.30220	7.75
40	8.21560	8.35	8.22279	8.45	40	8.29510	7.60	8.30376	7.80
	.21726	8.30		8.45		. 29662	7.60		7.70
42 44	.21720	8.30	.22448	8.45	42 44	.29813	7 - 55	. 30530	7.75
46	.22058	8.30	,22786	8.45	46	. 29965	7.60	.30839	7.70
48	. 22224	8.30	. 22954	8.40	48	.30116	7.55	.30993	7.70
50	8.22389	8.25	8.23122	8.40	50	8.30266	7.50	8.31147	7.70
52	.22554	8.25	. 23290	8.40 8.35	52	.30417	7.55	.31300	7.65
54	.22718		.23457		54	. 30567	7.50	.31454	7.65
56	. 22882	8.20	.23624	8.35 8.35	56	.30717	7.45	. 31607	7.60
58	.23046	8.20	.23791	8.30	58	. 30866	7.50	.31759	7.65
60	8.23210	8.15	8.23957	8.30	60	8.31016	7.45	8.31912	7.60
62	.23373	8.15	.24123	8.30	62	.31165	7.45	.32064	7.60
64	. 23536	8.15	.24289	8.30	64 66	.31314	7.40	.32216	7.60
66	. 23699	8.10	.24455	8.25			7.45		7.55
68 70	. 23861 8 . 24023	8.10	. 24620 8. 24785	8.25	68 70	.31611 8.31759	7.40	.32519 8.32671	7.60
70	. 24185	8.10	.24949	8.20	72	.31907	7.40	.32822	7.55
74	.24346	8.05	.25114	8.25	74	.32054	7.35	.32972	7.50
76	.24507	8.05	.25278	8.20	76	.32201	7.35	.33123	7.55
78	.24668	8.05	.25441	8.15	78	. 32348	7.35 7.35	.33273	7.50
80	8.24829	8.00	8.25605	8.15	80	8.32495	7.35	8.33423	7.50
82	.24989		.25768	_	82	.32642		-33573	
84	.25149	8.00 7.95	. 25931	8.15	84	.32788	7.30	.33722	7.45 7.45
86	.25308	8.00	,26093	8.10	86	.32934	7.30	.33871	7.45
88	. 25468	7.95	.26255	8.10	88	.33080	7.30	.34020	7.45
90	8.25627	7.90	8.26417	8.10	90 92	8.33226 .33371	7.25	8.34169	7.45
92	.25785	7.95	.26579	8.05			7.25	.34466	7.40
94 96	.25944	7.90	.26740	8.10	94 96	.33516	7.25	.34400	7.40
98	.26260	7.90	.27062	8.00	98	.33806	7.25	.34762	7.40
100	8.26418	7.90	8.27223	8.05	100	8.33950	7.20	8.34909	7.35
100	0.20410	1	0.21223	1	1 200	0.00900	1	1 3.04339	I

TABLE XXVI. — (Continued)

Hun-		1	2ೆ (ಬ್ರ		Hun-		1	3°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff. .∞ı
00	8.33950	7.20	8.34909	7.40	00	8.40875	6.65	8.42002	6.85
02	.34094	7.20	.35057	7.40	02	.41008	6.60	.42139	6.80
04	.34238	7.20	.35204	7.35	04	.41140	6.65	.42275	6.80
06	.34382	7.15	.35351	7.30	06	.41273	6.60	.42391	6.80
08 10	.34525 8.34668	7.15	.35497 8.35644	7.35	08 10	.41405 8.41537	6.60	.42547 8.42683	6.80
12	.34811	7.15	.35790	7.30	12	.41537	6.60	.42818	6.75
14	.34954	7.15	.35936	7.30	14	.41801	6.60	.42953	6.75
16	.35096	7.10	.36082	7.30	16	.41933	6.60	.43088	6.75
18	.35238	7.10	.36227	7.25	18	.42064	6.55	.43223	6.75
20	8.35380	7.10	8.36372	7.25	20	8.42195	6.55	8.43358	6.75
22	.35522	7.10	.36517	7.25	22	.42326	6.55	.43492	6.70
24	.35664	7.10	. 36662	7.25	24	.42457	6.55	.43627	6.75
26	.35805	7.05 7.05	. 36807	7.25	26	.42587	6.55	.43761	6.70
28	.35946	7.05	. 36951	7.20	28	.42718	6.50	. 43895	6.65
30	8.36087	7.00	8.37095	7.20	30	8.42848	6.50	8.44028	6.70
32	.36227	7.05	.37239	7.20	32	.42978	6.45	.44162	6.65
34	.36368 .36508	7.00	.37383	7.15	34	.43107	6.50	.44295	6.65
36 38	.36648	7.00	.37520	7.15	36 38	.43237 .43366	6.45	.44428	6.65
40	8.36787	6.95	8.37812	7.15	40	8.43495	6.45	8.44694	6.65
	.36927	7.00	37955	7.15	42	.43624	6.45	.44827	6.65
42 44	.30927	6.95	.38098	7.15	44	.43024	6.45	.44959	6.60
46	.37205	6.95	.38240	7.10	46	.43882	6.45	.45091	6.60
48	.37344	6.95	.38382	7.10	48	.44010	6.40	.45223	6.60
50	8.37482	6.90	8.38524	7.10	50	8.44138	6.40 6.40	8.45355	6.60 6.60
′ 52	.37620	6.90 6.95	.38666	7.10 7.05	52	.44266	6.40	.45487	6.55
54	.37759	6.85	.38807	7.05	54	.44394	6.40	.45618	6.55
56	.37896	6.90	.38948	7.05	56	.44522	6.35	-45749	6.55
58	. 38034	6.85	. 39089	7.05	58	.44649	6.35	.45880	6.55
60	8.38171	6.90	8.39230	7.05	60	8.44776	6.35	8.46011	6.55
62	.38309	6.85	.39371	7.00	62 64	.44903 .45030	6.35	.46142 .46273	6.55
64 66	.38446 .38582	6.80	.39511	7.00	66	.45157	6.35	.46403	6.50
68	.38719	6.85	.39791	7.00	68	.45283	6.30	.46533	6.50
70	8.38855	6.80	8.39931	7.00	70	8.45410	6.35	8.46663	6.50
72	.38991	6.80 6.80	.40071	7.00 6.95	72	. 45536	6.30 6.30	.46793	6.50 6.50
74	.39127	6.80	.40210		74	. 45662	6.25	.46923	6.45
76	.39263	6.80	.40349	6.95	76	.45787	6.30	.47052	6.45
78	-39399	6.75	.40488	6.95	78	.45913	6.25	.47181	6.45
80	8.39534	6.75	8.40627	6.90	80	8.46038	6.25	8.47310	6.45
82	.39669	6.75	.40765	6.90	82	.46163	6.25	.47439	6.45
84 86	.39804	6.70	.40903 .41042	6.95	84 86	.46288	6.25	.47568 .47696	6.40
88	.39938	6.75		6.85	88	.46538	6.25	.47825	6.45
88 90	.40073 8.40207	6.70	.41179 8.41317	6.90	90	8.46662	6.20	8.47953	6.40
90	.40341	6.70	.41455	6.90	92	.46787	6.25	.48081	6.40
94	.40475	6.70	.41592	6.85	94	.46911	6.20	.48209	6.40
96	.40608	6.65 6.70	.41729	6.85 6.85	96	.47035	6.20	. 48337	6.40 6.35
98	.40742	6.65	.41866	6.80	98	.47158	6.20	.48464	6.35
100	8.40875	0.03	8,42002	0.00	100	8.47282		8.48591	- 100

TABLE XXVI. - (Continued)

	i	1.	4°		1	1		5°	
Hun-		Diff.	*	Diff.	Hun-		Diff.	9	Diff.
dredths	Vers]	.001	Exsec	.001	dredths	Vers	.001	Exsec	.001
00	8.47282	6.15	8.48591	6.40	00	8.53243	5.75	8.54748	5.95
02	.47405	6.15	.48719	6.35	02	•53358	5.75	.54867	5.95
04 06	.47528	6.15	. 48846	6.30	04	53473	5.70	.54986	5.95
	.47651	6.15	.48972	6.35	06	.53587	5.75	.55105	5.95
08 10	.47774 8.47897	6.15	.49099	6.35	08 10	.53702	5.70	.55224	5.90
10	.48019	6.10	8.49226 .49352	6.30	10	8.53816 -53931	5.75	8.55342 .55461	5.95
14	.48142	6.15	.49332	6.30	14	ı	5.70	1	5.90
16	.48264	6.10	.49604	6.30	16	.54045 .54159	5.70	- 55579 - 55697	5.90
18	.48386	6.10	. 49730	6.30	18	.54273	5.7C	.55815	5.90
20	8.48508	6.10	8.49855	6.25	20	8.54386	5.65	8.55933	5.90
22	.48629	6.05	.49981	6.30	22	.54500	5.70	.56051	5.90
24	.48751	6.10	.50105	6.20	24	.54613	5.65	.56168	5.85
26	.48872	6.05	.50231	6.30	26	.54727	5.70	.56285	5.85
28	. 48993	6.05	.50356	6.25	28	.54840	5.65	.56403	5.90
30	8.49114	6.05	8.50481	6.25	30	8.54953	5.65	8.56520	5.85
32	.49235	6.05	.50606	6.25	32	.55065	5.60	.56637	5.85
34	- 49355	6.00	.50730	6.20	34	.55178	5.65	.56753	5.80
36	.49486	6.05	.50864	6.20	36	.55290	5.60	.56870	5.85
38	. 49596	6.00	.50979	6.25	38	. 55403	5.65 5.60	. 56987	5.85 5.80
40	8.49716	6.00	8.51103	6.15	40	8.55515	5.60	8.57103	5.80
42	.49836	6.00	.51226		42	.55627		.57219	
44	.49956	5.95	.51350	6.20	44	-55739	5.60 5.60	-57335	5.80 5.80
46	.50075	6.00	.51474	6.15	46	.55851	5.55	·5745I	5.80
48	.50195	5.95	.51597	6.15	48	.55962	5.60	.57567	5.80
50	8.50314	5.95	8.51720	6.15	50	8.56074	5.55	8.57683	5.75
52	.50433	5.95	.51843	6.15	52	.56185	5.55	.57798	5.80
54	.50552	5.95	.51966	6.15	54	.56296	5.55	.57914	5.75
56 58	.50671	5.90	. 52089	6.10	56	.56407	5.55	.58029	5.75
60	.50789	5.95	. 52211	6.10	58 60	.56518	5.55	.58144	5 · 7 5
	8.50908	5.90	8.52333	6.15		8.56629	5 - 55	8.58259	5.75
62 64	.51026	5.90	.52456	6.10	62	.56740	5.50	.58374	5.75
66	.51144	5.90	.52578	6.10	64 66	. 56850 . 56960	5.50	.58489 .58603	5.70
68	.51380	5.90	.52821	6.05	68		5.50	.58717	5.70
70	8.51498	5.90	8.52943	6.10	70	.57070 8.57181	5.55	8.58832	5.75
72	.51615	5.85	.53064	6.05	70	.57290	5.45	.58946	5.70
74	.51732	5.85	.53186	6.10	74	.57400	5.50	.59060	5.70
76	.51849	5.85	.53307	6.05	76	.57510	5.50	.59174	5.70
78	.51966	5.85	.53428	6.05	78	.57619	5 - 45	.59288	5.70
80	8.52083	5.85	8.53548	6.00	80	8.57728	5.45	8.59401	
82	.52200	5.85	.53669	6.05	82	.57838	5.50	.59515	5.70
84	. 52316	5.80	.53790	6.05	84	-57947	5.45	.59628	5.65 5.65
8 6	-52433	5.80	.53910	6.00	8 6	. 58056	5.45 5.40	.59741	5.65
88	.52549	5.80	.54030	6.00	88	.58164	5.45	. 59854	5.65
90	8.52665	5.80	8.54150	6.00	90	8.58273	5.40	8.59967	5.65
92	.52781	5.75	.54270	6.00	92	.58381	5.45	.60080	5.65
94 96	.52896	5.80	.54390	5.95	94	.58490	5.40	.60193	5.60
98	.53012	5.75	.54509	6.00	96 98	.58598	5.40	.60305 .60418	5.65
100	8.53243	5.80	8.54748	5.95	100	8.58814	5.40	8.60530	5.60
200	0.33443	1	0.54748	- 1	100	0.50014		0.00330	

.,		16	S°		Hun-		17	7°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
-00	8.58814	100.	8.60530		-00	8.64043		8.65984	
02	.58922	5.40	.60642	5.60	02	.64145	5.10	.66090	5.30
02	.59030	5.40	.60754	5.60	04	.64246	5.05	.66196	5.30
06	.59137	5.35	.60866	5.60	06	.64347	5.05	.66301	5.25
08	.59244	5.35	.60978	5.60	о8	.64448	5.05	.66407	5.30
10	8.59352	5.40	8.61089	5.55 5.60	10	8.64549	5.05 5.05	8.66513	5.30
12	.59459	5.35 5.35	.61201	5.55	12	.64650	5.05	.66618	5.25
14	. 59566	5.35	.61312	5.60	14	.64751	5.00	.66723	5.30
16	. 59673	5.30	.61424	5.55	16	.64851	5.00	.66829	5.25
18	-59779	5.35	.61535	5.55	18	.64951	5.05	.66934	5.25
20	8.59886	5.30	8.61646	5.50	20	8.65052	5.00	8.67039	5.25
22	. 59992	5.35	.61756	5.55	22	.65152	5.00	.67144	5.20
24	.60099	5.30	.61867	5.55	24 26	.65252 .65352	5.00	.67248 .67353	5.25
26	.60205	5.30	.61978	5.50			5.00		5.25
28	.60311	5.30	.62088 8.62199	5.55	28	.65452 8.65551	4.95	.67458 8.67562	5.20
30 32	8.60417	5.30	.62309	5.50	30 32	.65651	5.00	.67666	5.20
	.60628	5.25	.62419	5.50	34	.65751	5.00	.67771	5.25
34 36	.60734	5.30	.62529	5.50	36	.65850	4.95	.67875	5.20
38	.60839	5.25	.62639	5.50	38	.65949	4.95	.67979	5.20
40	8.60945	5.30	8.62748	5 - 45	40	8.66048	4.95	8.68083	5.20
42	.61050	5.25	.62858	5.50	42	.66147	4.95	.68186	5.15
44	.61155	5.25	.62968	5.50	44	.66246	4.95	.68290	5.20
46	.61260	5.25	.63077	5.45	46	.66345	4.95	.68393	5.20
48	.61364	5.20	. 63786	5.45	48	.66444	4.95	.68497	
50	8.61469	5.25	8.63295	5.45	50	8.66542	4.90	8.68600	5.15 5.15
52	.61573	5.20	.63404	5 · 45 5 · 45	52	.66641	4.90	.68703	5.20
54	.61678	5.20	.63513	5.45	54	.66739	4.90	.68807	5.15
56	.61782	5.20	.63622	5.40	56	.66837	4.90	.68910	5.10
58	.61886	5.20	.63730	5.45	58	.66935	4.90	.69012	5.15
60	8.61990	5.20	8.63839	5.40	60	8.67033	4.90	8.69115	5.15
62	.62094	5.20	.63947	5.45	62	.67131	4.90	.69218	5.15
64 66	.62198 .62301	5.15	.64056	5.40	64 66	.67229 .67327	4.90	.69321	5.10
68	.62405	5.20	.64272	5.40	68	.67424	4.85	.69525	5.10
70	8.62508	5.15	8.64380	5.40	70	8.67521	4.85	8.69628	5.15
72	.62611	5.15	.64487	5.35	72	.67619	4.90	.69730	5.10
74	.62714	5.15	.64595	5.40	74	.67716	4.85	.69832	5.10
76	.62817	5.15	.64703	5.40	76	.67813	4.85	.69934	5.10
78	.62920	5.15	.64810	5.35	78	.67910	4.85	. 70036	5.10
80	8.63023	5.15	8.64917	5.35	80	8.68007	4.85	8.70137	5.10
82	.63126	5.15	.65024	5.35	82	.68104	1	.70239	1 -
84	.63228	5.10	.65132	5.40	84	.68200	4.80	.70340	5.05
86	.63330	5.15	.65238	5.35	86	.68297	4.80	.70442	5.05
88	.63433	5.10	.65345	5.35	88	.68393	4.85	.70543	5.05
90	8.63535	5.10	8.65452	5.35	90	8.68490	4.80	8.70644	5.05
92	.63637	5.10	.65559	5.30	92	.68586	4.80	.70745	5.05
94	.63739	5.05	.65665	5.30	94	.68682	4.80	.70846	5.05
96 98	.63840 .63942	5.10	.65771	5.35	96 98	.68778	4.80	.70947	5.05
100	8.64043	5.05	8.65984	5.30	100	8.68969	4.75	8.71149	5.05
100	8.04043	1	0.05984		1 100	0.00909	I	0.71149	I

		1	8°					9°	
Hun- dredths		Diff.		Diff.	Hun- dredths	ļ	Diff.	1	Diff.
dreaths	Vers	.coi	Exsec	.001	diedins	Vers	.001	Exsec	.001
00	8.68969	4.80	8.71149	5.00	00	8.73625		8.76058	
02	.69065	4.80	.71249	5.05	02	.73715	4.50	.76154	4.80
04 06	.69161 .69256	4.75	.71350	5.00	04 06	.73806	4.55 4.50	.76249	4.75 4.80
08		4.75	.71450	5.05	08	.73896	4.50	.76345	4.75
10	.69351 8.69447	4.80	.71551 8.71651	5.00	10	.73986 8.74077	4.55	.76440 8.76536	4.80
12	.69542	4.75	.71751	5.00	12	.74167	4.50	.76631	4.75
14	.69637	4.75	.71851	5.00	14	.74257	4.50	.76726	4.75
16	.69732	4.75 4.75	.71951	5.00	16	.74346	4.45	. 7682İ	4.75 4.75
18	.69827	4.70	.72051	4.95	18	.74436	4.50	.76916	4.75
20	8.69921	4.75	8.72150	5.00	20	8.74526	4.50	8.77011	4.75
22	.70016	4.70	.72250	4.95	22	.74616	4.45	.77106	4.75
24 26	.70110	4.75	.72349	5.00	24 26	.74705 .74794	4.45	.77201	4.75
28	.70299	4.70	.72548	4.95	28	.74884	4.50	.77390	4.70
30	8.70393	4.70	8.72647	4.95	30	8.74973	4.45	8.77485	4.75
32	.70487	4.70	.72746	4.95 4.95	32	.75062	4 - 45	.77579	4.70
34	.70581	4.70	. 72845	4.95	34	.75151	4.45	.77674	4.75
36	.70675	4.70	.72944	4.95	36	.75240	4 · 45 4 · 45	.77768	4.70
38	.70769	4.65	.73043	4.95	38	.75329	4.40	.77862	4.70
40	8.70862	4.70	8.73142	4.90	40	8.75417	4.45	8.77956	4.70
42 44	.70956 .71049	4.65	.73240 .73339	4.95	42 44	.75506 .75595	4.45	.78050	4.70
46	.71143	4.70	.73339	4.90	46	.75683	4.40	.78238	4.70
48	.71236	4.65	.73535	4.90	48	.75772	4 - 45	.78331	4.65
50	8.71329	4.65	8.73634	4.95	50	8.75860	4.40	8.78425	4.70
52	.71422	4.65	.73732	4.90	52	.75948	4.40	.78519	4.70
54	.71515	4.65	. 73830	4.90	54	.76036	4.40	.78612	4.70
56 58	.71608 .71701	4.65	.73928	4.85	56 58	.76124 .76212	4.40	.78706 .78799	4.65
60	8.71793	4.60	8.74123	4.90	60	8.76300	4.40	8.78892	4.65
62	.71886	4.65	.74221	4.90	62	.76387	4.35	.78985	4.65
64	.71978	4.60	.74221	4.85	64	.76475	4.40	.79078	4.65
66	.72071	4.65	.74416	4.90	66	. 76563	4.40	.79171	4.65
68	.72163	4.60	.74513	4.85	68	. 76650	4.35	.79264	4.65
70	8.72255	4.60	8.74610	4.85	70	8.76737	4.35	8.79357	4.60
72	.72347	4.60	.74707	4.85	72	.76825	4.35	.79449	4.65
74 76	.72439 .72531	4.60	.74804	4.85	74 76	.76912 .76999	4.35	.79542 .79635	4.65
78	.72531	4.55	.74901	4.85	78	.70999	4.35	.79727	4.60
80	8.72714	4.60	8.75095	4.85	80	8.77173	4.35	8.79819	4.60
82	.72806	4.60	.75192	4.85	82	.77260	4.35	.79912	4.65
84	.72897	4 · 55 4 · 55	.75288	4.80 4.85	84	.77346	4.30 4.35	.80004	4.60 4.60
86	.72988	4.60	- 75385	4.80	86	.77433	4.35	.80096	4.60
88	.73080	4.55	.75481	4.85	88	.77520	4.30	.80188 8.80280	4.60
90 92	8.73171 .73262	4.55	8.75578 .75674	4.80	90 92	8.77606 .77692	4.30	.80280	4.60
94	.73353	4.55	.75770	4.80	94	.77779	4.35	.80464	4.60
96	.73443	4.50	.75866	4.80	96	.77865	4.30	.80555	4.55
98	.73534	4.55 4.55	.75962	4.80 4.80	98	.77951	4.30	.80647	4.60 4.55
100	8.73625	4.33	8.76058	4.60	100	8.78037	4.30	8.80738	4.33

Hun-		20	٥		Hun-		21	۰	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
-00	8.78037		8.80738		- 00	8.82230		8.85214	
02	.78123	4.30	.80830	4.60	02	.82311	4.05	.85302	4.40
04	.78209	4.30	.80921	4.55	04	.82393	4.10	.85390	4.40
06	.78295	4.30	.81013	4.60	o6	.82475	4.10	.85477	4.35
08	. 78380	4.25	.81104	4.55	о8	.82556	4.05	.85564	4.35
10	8.78466	4.30 4.25	8.81195	4.55 4.55	10	8.82638	4.10	8.85652	4.40
12	.78551	4.30	.81286	4.55	12	.82719	4.05	.85739	4.35
14	. 78637	4.25	.81377	4.55	14	.82800	4.05	.85826	4.35
16 18	.78722	4.25	.81468	4.55	16 18	.82881 .82963	4.10	.85913	4.35
	.78807	4.25	.81559	4.50	20		4.05	8.86087	4.35
20	8.78892	4.25	8.81649	4.55		8.83044	4.05		4.35
22	.78977 .79062	4.25	.81740 .81831	4.55	22 24	.83125 .83205	4.00	.86174 .86261	4.35
24 26	.79002	4.25	.81921	4.50	26	.83286	4.05	.86347	4.30
28	.79232	4.25	.82011	4.50	28	.83367	4.05	.86434	4.35
30	8.79317	4.25	8.82102	4.55	30	8.83448	4.05	8.86520	4.30
32	.79402	4.25	.82192	4.50	32	.83528	4.00	.86607	4.35
34	.79486	4.20	,82282	4.50	34	.83609	4.05	.86693	4.30
36	.79571	4.25	.82372	4.50	36	.83689	4.00	.86780	4.35 4.30
38	.79655	4.20	.82462	4.50	38	.83769	4.05	.86866	4.30
40	8.79739	4.20	8.82552	4.50	40	8.83850	4.00	8.86952	4.30
42	.79823	4.25	.82642	4.50	42	.83930	4.00	.87038	4.25
44	.79908	4.25	.82732	4.50	44	.84010	4.00	.87123	4.25
46	.79992	4.20	.82822	4.45	46	.84090	4.00	.87210	4.30
48	.80076	4.15	.82911	4.50	48	.84170	4.00	.87296	4.30
50	8.80159 .80243	4.20	8.83001 .83090	4.45	50 52	8.84250 .84330	4.00	8.87382	4.30
52	.80243	4.20	.83180	4.50	_	.84410	4.00	.87554	4.30
54 56	.80327	4.20	.83269	4.45	54 56	.84489	3.95	.87639	4.25
58	.80494	4.15	.83358	4.45	58	.84569	4.00	.87725	4.30
60	8.80578	4.20	8.83447	4.45	60	8.84648	3.95	8.87810	4.25
62	.80661	4.15	.83536	4.45	62	.84728	4.00	.87896	4.30
64	.80744	4.15	.83625	4.45	64	.84807	3.95	.87981	4.25
66	.80827	4.15 4.15	.83714	4 . 45	66	.84886	3.95	.88067	4.30
68	.80911		.83803	4 . 45	68	.84966	3.95	.88152	4.25
70	8.80994	4.15	8.83892	4.45	70	8.85045	3.95	8.88237	4.25
72	.81077	4.10	.83981	4.40	72	.85124	3.95	.88322	4.25
74	.81159	4.15	.84069	4.45	74	.85203 .85282	3.95	.88407	4.25
76 78	.81242	4.15	.84158	4.40	76 78	.85360	3.90	.88577	4.25
80	8.81408	4.15	8.84335	4.45	80	8.85439	3.95	8.88661	4.20
80 82	.81490	4.10		4.40	82	.85518	3.95	.88746	4.25
84	.81490	4.15	.84423	4.40	84	.85596	3.90	.88831	4.25
86	.81655	4.10	.84599	4.40	86	. 85675	3.95	.88916	4.25
88	.81737	4.10	.84687	4.40	88	.85754	3.95	.89000	4.20
90	8.81820	4.15	8.84775	4.40	90	8.85832	3.90	8.89085	4.25
92	.81902	4.10	.84863	4.40	92	.85910	3.90	.89169	4.25
94	.81984	4.10	.84951	4.40	94	.85988	3.95	.89254	4.20
96	.82066	4.10	.85039	4.40	96	.86067	3.95	.89338	4.20
98	.82148	4.10	.85127	4.35	98	.86145	3.90	.89422	4.20
100	8.82230		8.85214		100	8.86223		8.89506	l

Hun-		2:	2°		Hun-		23	3°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	8.86223	2.00	8.89506	4.00	00	8 90034		8.93631	
02	.86301	3.90	.89590	4.20	02	.90109	3.75	.93712	4.05
04	.86379	3.90 3.85	.89674	4.20	04	.90183	3.70 3.70	.93793	4.05 4.05
06	.86456	3.90	.89758	4.20	06	.90257	3.75	.93874	4.05
08	.86534	3.90	.89842	4.20	08	.90332	3.70	.93955	4.00
10	8.86612	3.85	8.89926	4.20	10 12	8.90406	3.70	8.94035	4.05
12	.86689	3.90	.90010	4.15		.90480	3.70	.94116	4.05
14 16	.86767 .86844	3.85	.90093	4.20	14 16	.90554	3.70	.94197	4.00
18	.86922	3.90	.90261	4.20	18	.90702	3.70	.94277	4.05
20	8.86999	3.85	8.90344	4.15	20	8.90776	3.70	8.94438	4.00
	.87076	3.85	.90427	4.15	22	.90850	3.70	.94518	4.00
22 24	.87153	3.85	.90427	4.20	24	.90923	3.65	.94599	4.05
26	.87231	3.90	.90594	4.15	26	.90997	3.70	.94679	4.00
28	.87308	3.85	.90677	4.15	28	.91071	3.70	.94759	4.00
30	8.87385	3.85	8.90761	4.20	30	8.91144	3.65	8.94839	4.00
32	.87461	3.80 3.85	.90844	4.15 4.15	32	.91218	3.70	.94919	4.00 4.00
34	.87538	3.85	.90927		34	.91291	3.65	.94999	4.00
36	.87615	3.85	.91010	4.15 4.15	36	.91365	3.65	.95079	4.00
38	.87692	3.80	.91093	4.10	38	.91448	3.65	.95169	3.95
40	8.87768	3.85	8.91175	4.15	40	8.91511	3.65	8.95238	4.00
42	.87845	3.80	.91258	4.15	42	.91584	3.65	.95318	4.00
44	.87921	3.85	.91341	4.10	44	.91657	3.65	95398	4.00
46	.87998	3.80	.91423	4.15	46	.91730	3.65	.95478	3.95
48	.88074	3.80	.91506	4.15	48	.91803	3.65	. 95557	4.00
50 52	8.88150 .88226	3.80	8.91589 .91671	4.10	50 52	8.91876 .91949	3.65	8.95637 .95716	3.95
	.88302	3.80		4.10	54	.92022	3.65		3.95
54 56	.88378	3.80	.91753	4.15	54 56	.92022	3.65	.95795	4.00
58	.88454	3.80	.91918	4.10	58	.92167	3.60	.95954	3.95
60	8.88530	3.80	8.92000	4.10	60	8.92240	3.65	8.96033	3.95
62	.88606	3.80	.92082	4.10	62	.92313	3.65	.96112	3.95
64	.88682	3.80	.92165	4.15	64	.92385	3.60	.96192	4.00
66	.88758	3.80	.92247	4.10	66	.92457	3.60	.96271	3.95
68	.88833	3.75	.92328	4.05	68	.92530	1	. 96350	3.95
70	8.88909	3.80	8.92410	4.10	70	8.92602	3.60	8.96428	3.90
72	.88984	3.75	.92492	4.10	72	.92674	3.60	.96507	3.95
74	.89060	3 75	.92574	4.10	74	.92746	3.60	.96586	3.95
76 78	.89135	3.75	.92656	4.05	76 78	.92818	3.65	.96665	3.95
78 80	.89210	3.80	.92737	4.10	78 80	.92891	3.55		3.90
	8.89286	3.75	8.92819	4.05		8.92962	3.60	8.96822	3.95
82 84	.89361	3.75	.92900	4.10	82 84	.93034	3.60	.96901	3.90
86	.89436 .89511	3.75	.92982	4.05	86	.93106	3.60	.90979	3.95
88	.89586	3.75	.93145	4.10	88	.93250	3.60	.97136	3.90
90	8.89661	3.75	8.93226	4.05	90	8.93321	3.55	8.97215	3.95
92	.89735	3.70	.93307	4.05	92	.93393	3.60	.97293	3.90
94	.89810	3.75	.93388	4.05	94	.93465	3.60	.97371	3.90
96	.89885	3.75	.93469	4.05	96	.93536	3.55	.97450	3.95 3.90
98	.89960	3.75 3.70	.93550	4.05	98	.93607	3.55	.97528	3.90
100	8.90034	3.70	8.93631	4.53	100	8.93679	3.50	8.97606	3.30

Hun-		24	٥		Hun-		2	5°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
		100.		.001			.001		.001
00	8.93679	3.55	8.97606	3.90	00	8.97170	3.45	9.01443	3.75
02	.93750	3.55	.97684	3.90	02	.97239	3.40	.01518	3.80
04 06	.93821 .93892	3.55	.97762 .97840	3.90	04 06	.97307 .97375	3.40	.01594	3.75
08		3.60	.97918	3.90	08	.97443	3.40	.01744	3.75
10	.93964 8.94035	3.55	8.97995	3.85	10	8.97512	3.45	9.01819	3.75
12	.94106	3 55	.98073	3.90	12	.97580	3.40	.01895	3.80
14	.94177	3.55	.98151	3.90	14	.97648	3.40	.01970	3.75
16	.94247	3.50	.98229	3.90	16	.97716	3.40	.02045	3.75
18	.94318	3.55	.98306	3.85	18	.97784	3.40	.02120	3.75
20	8.94389	3.55	8.98384		20	8.97851		9.02195	3.75
22	.94460	3 55	.98461	3.85	22	.97919	3.40	.02270	3.75
24	. 94530	3.50	. 98539	3.90	24	97987	3.40	.02345	3.75 3.70
26	.94601	3.55 3.50	.98616	3.85	26	.98055	3.40	.02419	3.75
28	. 94671		.98693	3.90	28	.98122	3.40	.02494	3.75
30	8.94742	3.55 3.50	8.98771	3.85	30	8.98190	3.40	9.02569	3.75
32	.94812	3.50	.98848	3.85	32	.98257	3.40	.02644	3.70
34	.94882	3.55	. 98925	3.85	34	.98325	3.35	.02718	3.75
36	.94953	3.50	.99002	3.85	36 38	.98392	3.35	.02793	3.70
38	.95023	3.50	.99079	3.85	40	.98459	3.40	.02867	3.75
40	8.95093	3.50	8.99156	3.85		8.98527	3.35	9.02942	3.70
42	.95163	3.50	.99233	3.85	42	.98594	3.35	.03016	3.75
44	.95233	3.50	.99310	3.85	44 46	.98661 .98728	3.35	.03091	3.70
46	.95303	3.50	.99387	3.85			3.35		3.70
48 50	.95373 8.9544 3	3.50	.99464 8.99541	3.85	48 50	.98795 8.98862	3.35	9.03314	3.75
50 52	.95513	3.50	.99617	3.80	52	.98929	3.35	.03388	3.70
54	.95582	3.45	.99694	3.85	54	.98996	3.35	.03462	3.70
56 56	.95652	3.50	.99771	3.85	56	.99063	3.35	.03536	3.70
58	.95722	3.50	.99847	3.80	58	. 99130	3.35	.03610	3.70
60	8.95791	3.45	8.99924	3.85	60	8.99197	3.35	9.03684	3.70
62	.95861	3.50	9.00000	3.80	62	.99263	3.30	.03758	3.70
64	.95930	3.45	.00076	3.80	64	.99330	3.35	.03832	3.70
66	.96000	3.50	.00153	3.85	66	.99397	3.35	.03906	3.70
68	.96069		.00229	3.80	68	.99463	3.35	.03980	3.70
70	8.96138	3.45	9.00305	3.85	70	8.99530	3 30	9.04054	3.65
72	.96207	3.50	.00382	3.80	72	.99596	3.35	.04127	3.70
74	.96277	3.45	.00458	3.80	74	.99663	3.30	.04201	3.70
76 78	.96346	3.45	.00534	3.80	76 78	.99729	3.30	.04275	3.65
78 80		3.45	9.00686	3.80	80	.99795 8.99861	3.30		3.70
1	8.96484	3.45		3.80	82		3.35	9.04422	3.65
82 84	.96553 .96621	3.40	.00762	3.80	82 84	.99928 .99994	3.30	.04495	3.70
86	.96690	3.45	.00030	3.75	86	9.00060	3.30	.04642	3.65
88	.96759	3.45	.00989	3.80	88	,00126	3.30	.04715	3.65
90	8.96828	3.45	9.01065	3.80	90	9.00192	3.30	9.04789	3.70
92	.96896	3.40	.01141	3.80	92	.00258	3.30	.04862	3.65
94	. 96965	3.45	.01216	3.75	94	.00323	3.25	.04935	3.65
9 6	.97033	3.40	.01292	3.80	96	.00389	3.30	.05008	3.65
98	.97102	3.45	.01367	3.75 3.80	98	.00455	3.30	.05082	3.65
100	8.97170	3.45	9.01443	3.50	100	9.00521	5.50	9.05155	1

Hun-		20	6°		Hun-		2	7°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff. .∞ı	Exsec	Diff.
-00	9.00521		9.05155		00	9.03740		9.08752	
02	.00586	3.25	.05228	3.65	02	.03803	3.15	.08823	3.55
04	.00652	3.30	.05301	3.65	04	.03866	3.15	.08894	3.55
06	.00717	3.25	.05374	3.60	06	.03929	3.15	.08964	3.50 3.55
08	.00783	3.25	.05446	3.65	08	.03992	3.15	.09035	3.55
10	9.00848	3.30	9.05519	3.65	10	9.04055	3.15	9.09106	3.50
12	.00914	3.25	.05592	3.65	12	.04118	3.15	.09176	3.55
14	.00979	3.25	.05665	3.65	14	.04181	3.15	.09247	3.55
16 18	.01044	3.25	.05738	3.60	16 18	.04244	3.10	.09318	3.50
20		3.30		3.65	20		3.15		3.55
	9.01175	3.25	9.05883	3.60		9.04369	3.15	9.09459	3.50
22	.01240	3.25	.05955	3.65	22	.01432	3.10	.09529	3.50
24 26	.01305	3.25	.06028	3.65	24 26	.04494	3.15	.09599	3.55
		3.25		3.60	28		3.10		3.50
28 30	.01435 9.01500	3.25	.06173 9.06245	3.60	30	.04619 9.04682	3.15	9.09740	3.50
30	.01565	3.25	.06318	3.65	32	.04744	3.10	.09881	3.55
34	.01629	3.20	.06390	3.60	34	.04807	3.15	.09001	3.50
34 36	.01694	3.25	.06462	3.60	36	.04869	3.10	.10021	3.50
38	.01759	3.25	.06535	3.65	38	.04931	3.10	.10091	3.50
40	9.01824	3.25	9.06607	3.60	40	9.04993	3.10	9.10161	3.50
42	.01888	3.20	.06679	3.60	42	.05055	3.10	.10231	3.50
42	.01953	3.25	.00079	3.60	44	.05055	3.15	.10231	3.50
46	.02017	3.20	.06823	3.60	46	.05180	3.10	.10371	3.50
48	.02082	3.25	. 06895	3.60	48	.05242	3.10	.10441	3.50
50	9.02146	3.20	9.06968	3.65	50	9.05304	3.10	9.10511	3.50
52	.02210	3.20	.07039	3.55	52	05366	3.10	. 10581	3.50
54	.02275	3.25	.07111	3.60	54	.05127	3.05	. 10650	3.45
56	.02339	3.20	.07183	3.60	56	.05489	3.10	.10720	3.50
58	.02403	3.20	.07254	3.55 3.60	58	.05551	3.10	.10790	3.50
60	9.02467	3.20	9.07326		60	9.05613		9.10860	3.50
62	.02531	3.20	.07398	3.60	62	.05675	3.10	.10929	3.45
64	.02596	3.25	.07469	3.55	64	.05736	3.05	.10999	3.50
66	.02660	3.20	.07541	3.60	66	.05798	3.10	.11068	3.45
68	.02723	3.15	.07613	3.60	68	.05859	3.05	.11138	3.50
70	9.02787	3.20	9.07684	3.55 3.60	70	9.05921	3.10	9.11207	3.45
72	.02851	3.20	.07756	3.55	72	.05982	3.10	.11277	3.30
74	.02915	3.20	.07827	3.55	74	.06044	3.05	.11346	3.45
76	.02979	3.20	.07898	3.60	76	.06105	3.05	.11415	3.45
78	.03043	3.15	.07970	3.55	78	.06166	3.10	.11485	3.45
80	9.03196	3.20	9.08041	3.55	80	9.06228	3.05	9.11554	3.45
82	.03170	3.15	.08112	3.60	82	.06289	3.05	.11623	3 45
84 86	.03233	3.20	.08184	3.55	84 86	.06350	3.05	.11692	3.50
	.03297	3.15	.08255	3.55		.06411	3.05	.11762	3.45
88	.03360	3.20	.08326	3.55	88	.06472	3.05	.11831	3.45
90 92	9.03424	3.15	9.08397 .08468	3.55	90 92	9.06533	3.05	9.11900	3.45
•		3.15		3.55			3.05		3.45
94 96	.03550	3.20	.08539	3.55	94 96	.06655	3.05	.12038	3.45
98	.03677	3.15	.08681	3.55	98	.06777	3.05	.12107	3.45
100		3.15	9.08752	3.55	100	9.06838	3.05	9.12245	3.45
100	9.03740		9.06752		100	9.00038		9.12245	

Hun-		28	•		Hun-		29	°	
dredths	Vers	Diff.	Exsec	Dıff.	dredths	Vers	Diff.	Exsec	Diff.
		100.		.001	00		.001	0	.001
00	9.06838	3.05	9.12245	3.40		9.09823	2.95	9.15641	3.35
02	.06899	3.05	.12313	3.45	02 04	.09882	2.90	.15708	3.35
04 06	.07020	3.00	.12451	3.45	.06	.09999	2.95	.15842	3.35
08	.07081	3.05	.12520	3.45	o8	.10057	2.90	.15909	3.35
10	9.07141	3.00	9.12588	3.40	10	9 10115	2.90	9.15976	3 · 35 3 · 35
12	07202	3.05	12657	3 45	12	.10174	2.90	.16043	3.30
14	.07263	3.00	.12726	3.40	14	.10232	2.95	.16109	3.35
16	.07323	3.00	.12794	3.45	16 18	.10291	2.90	.16176 .16243	3.35
18	.07383	3.05		3.40	20	.10349	2.90	9.16309	3.30
20	9.07444	3.00	9.12931	3.45		9.10407	2.90		3.35
22	.07504	3.00	.13000	3.40	22 24	.10465	2.90	.16376	3.35
24 26	.07504	3.05	.13137	3.45	26	,10581	2.90	.16509	3.30
28	.07685	3.00	.13205	3.40	28	.10639	2.90	. 16576	3.35
30	9.07745	3.00	9.13273	3.40	30	9.10697	2.90	9.16642	3.30 3.35
32	.07805	3.00	.13341	3.45	32	.10755	2.90	.16709	3.30
34	.07865	3.00	.13410	3.40	34	.10813	2.90	.16775	3.35
36	.07925	3.00	.13478	3.40	36	.10871	2.90	.16842	3.30
38	.07985	3.00	. 13546	3.40	38	.10929	2.90	.16908	3.30
40	9.08045	3.00	9.13614	3.40	40	9.10987	2.90	9.16974	3.35
42	.08105	3.00	.13682	3.40	42 44	.11045	2.85	.17041	3.30
44 46	.08165	3.00	.13750	3.40	46	.11160	2.90	.17173	3.30
48	.08284	2.95	.13886	3.40	48	.11218	2.90	.17239	3.30
50	9.08344	3.00	9.13954	3.40	50	9.11275	2.85	9.17306	3.35
52	.08404	3.00	.14022	3.40	52	.11333	2.85	.17372	3.30
54	.08463	3.00	.14090	3.40	54	.11390	2.90	.17438	3.30
56	.08523	3.00	.14158	3.40	56	.11448	2.85	.17504	3.30
58	.08583	2.95	.14226	3.35	58	.11505	2.90	.17570	3.30
60	9.08642	2.95	9.14293	3.40	60	9.11563	2.85	9.17636	3.30
62	.08701	3.00	.14361	3.40	62 64	.11620 .11677	2.85	.17702	3.30
64 66	.08761	2.95	.14429	3.35	66	.11735	2.85	.17834	3.30
68	.08880	3.00	.14564	3.40	68	.11792	2.85	.17900	3.30
70	9.08939	2.95	9.14632	3.40	70	9.11849	2.85	9.17966	3.30
72	.08998	2.95 2.95	.14699	3.35	72	.11906	2.85	.18031	3.30
74	.09057	2.95	.14767	3.35	74	.11963	2,85	.18097	3.30
76	.09116	3.00	.14834	3.40	76	.12020	2.85	.18163	3.30
78	.09176	2.95	.14902	3.35	78	.12077	2.85	.18229	3.25
80	9.09235	2.95	9.14969	3.35	80	9.12134	2.85	9.18294	3.30
82	.09294	2.95	.15036	3.40	8 ₂ 8 ₄	.12191	2.85	.18360	3.30
84 86	.09353	2.95	.15104	3.35	86	.12246	2.85	.18491	3.25
88	.09472	2.90	.15238	3.35	88	.12362	2.85	.18557	3.30
90	9.09529	2.95	9.15305	3.35	90	9.12419	2.85	9.18622	3.25
92	.09588	2.95	.15373	3.40	92	.12476	2.80	.18688	3.25
94	.09647	2.95	.15440	3.35	94	.12532	2.85	.18753	3.25
96	.09706	2.90	.15507	3.35	96	.12589	2.85	.18818	3.30
98	.09764	2.95	.15574	3.35	98	.12646	2.80		3.25
100	9.09823	I	9.15641	1	100	9.12702	l	9.18949	1

Hun-		30)°		Hun-		3:	L°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.12702	2.85	9.18949	3.25	00	9.15483	2.70	9.22176	3.20
02	.12759	2.80	.19014	3.30	02	. 15537	2.75	.22240	3.20
04	.12815	2.85	.19080	3.25	04	.15592	2.75	. 22304	3.15
06	.12872	2.80	.19145	3.25	06	.15647	2.70	. 22367	3.20
08	.12928	2.85	.19210	3.25	08	.15701	2.75	.22431	3.20
10 12	9.12985 .13041	2.80	9.19275 .19341	3.30	10 12	9.15756 .15810	2.70	9.22495	3.15
	- 1	2.80	.19341	3.25	14	. 15865	2.75	.22622	3.20
14 16	.13097	2.80	.19400	3.25	16	.15919	2.70	.22685	3.15
18	.13210	2.80	.19536	3.25	18	.15973	2.70	.22749	3.20
20	9.13266	2.80	9.19601	3.25	20	9.16028	2.75	9.22812	3.15
22	. 13322	2.80	.19666	3.25	22	.16082	2.70	.22876	3.20
24	.13378	2.80	.19731	3.25	24	.16136	2.70	.22939	3.15
26	.13434	2.80 2.80	.19796	3.25	26	.16190	2.70	.23003	3.20
28	.13490		19861	3.25	28	.16244		. 23066	3.15
30	9.13546	2.80	9.19926	3.25	30	9.16299	2.75	9.23129	3.15
32	.13602	2.80	.19990	3.25	32	.16353	2.70	.23193	3.20
34	.13658	2.80	. 20055	3.25	3.4	.16407	2.70	. 23256	3.15
36	.13714	2.80	.20120	3.25	36	.16461	2.70	. 23319	3.15
38	.13770	2.80	. 20185	3.20	38	. 16515	2.70	. 23383	3.15
40	9.13826	2.80	9.20249	3.25	40	9.16569	2.70	9.23446	3.15
42	.13882	2.75	. 20314	3.25	42	.16623	2.65	.23509	3.15
44	.13937	2.80	.20379	3.20	44	.16676	2.70	.23572	3.15
46	.13993	2.80	.20443	3.25	46	.16730	2.70	. 23635	3.15
48	.14049	2.75	. 20508	3.20	48	.16784	2.70	. 23698	3.15
50	9.14104	2.80	9.20572	3.25	50	9.16838 .16892	2.70	9.23761	3.15
52		2.80		3.20	52		2.65	.23824	3.15
54 56	.14216	2.75	.20701	3.25	54 56	.16945 .16999	2.70	.23887	3 15
58	.14327	2.80	. 20830	3.20	58	.17053	2.70	.24013	3.15
60	9.14382	2.75	9.20895	3.25	60	9.17106	2.65	9.24076	3.15
62	.14437	2.75	.20959	3.20	62	.17160	2.70	.24139	3.15
64	.14493	2.80	.21023	3.20	64	.17213	2.65	.24139	3.15
66	.14548	2.75	.21088	3.25	66	.17267	2.70 2.65	.24265	3.15
68	.14603	2.75	.21152	3.20	68	.17320		. 24328	3.15
70	9.14659	2.80	9.21216	3.20	70	9.17374	2.70 2.65	9.24390	3.10
72	.14714	2.75	.21280	3.25	72	.17427	2.65	.24453	3.15
74	.14769	2.75	.21345	3.20	74	.17480	2,70	.24516	3.10
76	.14824	2.75	.21409	3.20	76	.17534	2.65	. 24578	3.15
78	.14879	2.75	.21473	3.20	78	.17587	2.65	. 24641	3.15
80	9.14934	2.75	9.21537	3.20	80	9.17640	2.65	9.24704	3.10
82	.14989	2.75	.21601	3.20	82	.17693	2.70	.24766	3.15
84	.15044	2.75	.21665	3.20	84	.17747	2.65	.24829	3.10
86	.15099	2.75	.21729	3.20	86	.17800	2.65	24891	3.15
88 90	.15154	2.75	.21793	3.20	88	.17853	2.65	.24954	3.15
90	9.15209 .15264	2.75	9.21857	3.20	90 92	9.17906	2.65	9.25017	3.10
94	.15319	2.75	.21921	3.20	92	.18012	2.65	.250/9	3.10
94 96	.15373	2.70	.22049	3.20	94 96	.18065	2.65	.25141	3.15
98	.15428	2.75	.22112	3.15	98	.18118	2.65	.25266	3.10
100	9.15483	2.75	9.22176	3.20	100	9.18171	2.65	9.25329	3.15
	334-3		,,0			7.202/1		J.=33=9	

Hun-		3	2°		Hun-		3:	3°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.18171	2.60	9.25329	3.10	00	9.20771	2.60	9.28412	
02	.18223	2.65	.25391	3.10	02	.20823	2.55	.28473	3.05
04	. 18276	2.65	. 25453	3.10	04	.20874	2.55	.28534	3.05
06	. 18329	2.65	.25515	3.15	06	.20925	2.55	.28595	3.05
о8	. 18382	2.65	.25578	3.10	08	. 20976	2.55	.28656	3.05
10 12	9.18435 .18487	2.60	9.25640	3.10	10 12	9.21027	2.55	9.28717	3.05
14	.18540	2.65	.25764	3.10	14	.21129	2.55	. 28839	3.05
16	.18592	2.60	.25826	3.10	16	.21129	2.55	.28900	3.05
18	. 18645	2.65 2.65	.25889	3.15	18	.21231	2.55 2.55	.28961	3.05 3.00
20	9.18698	2.60	9.25951	3.10	20	9.21282	2.50	9.29021	3.05
22	.18750	2.65	.26013	3.10	22	.21332	2.55	.29082	3.05
24	.18803	2.60	.26075	3.10	24	.21383	2.55	.29143	3.00
26	.18855	2.60	.26137	3.10	26	.21434	2.55	. 29203	3.05
28	.18907	2.65	.26199 9.26261	3.10	28	.21485	2.50	.29264	3.05
30 32	9.18960 .19012	2.60	.26323	3.10	30 32	9.21535	2.55	9.29325	3.00
34	.19064	2.60	.26384	3.05	34	.21637	2.55	.29446	3.05
36	.19117	2.65	.26446	3.10	36	.21687	2.50	.29507	3.05
38	.19169	2.60	. 26508	3.10	38	.21738	2.55	. 29567	3.00 3.05
40	9.19221	2.60	9.26570	3.10	40	9.21788	2.55	9.29628	3.00
42	.19273	2.60	. 26632	3.10	42	.21839	2.50	.29688	3.05
44	.19325	2.60	. 26694	3.05	44	.21889	2.55	.29749	3.00
46	. 19377	2.65	.26755	3.10	46	.21940	2.50	.29809	3.05
48	.19430	2.60	.26817	3.10	48	.21990	2.55	.29870	3.00
50 52	9.19482	2.60	9.26879 .26940	3.05	50 52	9.22041	2.50	9.29930	3.00
54	.19586	2.60	.27002	3.10	54	.22141	2.50	.30051	3.05
56	.19637	2.55	.27064	3.10	56	.22192	2.55	.30111	3.00
58	.19689	2.60	.27125	3.05	58	.22242	2.50	.30171	3.00
60	9.19741	2.60	9.27187	3.05	60	9.22292	2.50	9.30232	3.00
62	.19793	2.60	.27248	3.10	62	.22342	2.50	.30292	3.00
64	.19845	2.60	.27310	3.10	64	.22392	2.50	.30352	3.00
66	.19897	2.55	.27371	3.10	66	.22442	2.55	.30412	3.05
68	.19948	2.60	.27433	3.05	68	.22493	2.50	.30473	3.00
70 73	9.20000	2 60	9.27494	3.05	70 72	9.22543	2.50	9.30533	3.00
74	.20103	2.55	.27617	3.10	74	.22643	2.50	.30653	3.00
74 76	.20103	2.55	.27678	3.05	74	.22693	2.50	.30713	3.00
78	.20206	2.55	.27739	3.05	78	.22743	2.50 2.50	.30773	3.00
80	9.20258	2.55	9.27801	3.05	80	9.22793	2.50	9.30833	3.00
82	.20309	2.60	.27862	3.05	82	.22843	2.45	.30893	3.00
84	. 20361	2.55	.27923	3.05	84	. 22892	2.43	.30953	3.00
86	.20412	2.60	.27984	3.10	86	.22942	2.50	.31013	3.00
88	.20464	2.55	.28046	3.05	88	.22992	2.50	.31073	3.00
90 92	9.20515	2.55	9.28107	3.05	90 92	9.23042	2.45	9.31133	3.00
94	.20618	2.60	.28229	3.05	94	.23141	2.50	.31253	3.00
94 96	.20669	2.55	.28229	3.05	94	.23141	2.50	.31313	3.00
98	.20720	2.55 2.55	.28351	3.05	98	.23240	2.45	.31373	3.00
100	9.20771	55	9.28412	3.03	100	9.23290	2.30	9.31433	3.00

Hun-		34	L°		Hun-		38	5°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.23290		9.31433		00	9.25731		9.34395	
02	. 23340	2.50	.31492	2.95	02	.25779	2.40	-34454	2.95
04	.23389	2.45	.31552	3.00	04	.25827	2.40	.34512	2.90 2.95
06	·23439	2.45	. 31612	3.00	06	. 25875	2.40	.34571	2.95
о8	.23488	2.50	.31672	2.95	o8	. 25923	2.40	. 34630	2.90
10	9.23538	2.45	9.31731	3.00	10	9.25971	2.40	9.34688	2.95
12	.23587	2.45	.31791	3.00	12	. 26019	2.40	.34747	2 90
14	.23636	2.50	. 31851	2.95	14	. 26067	2,40	.34805	2.95
16 18	. 23686	2.45	.31910	3.00	16 18	.26115	2.40	.34864	2.90
20	.23735	2.45	.31970	3.00		.26163	2.40	34922	2.95
	9.23784	2.50	9.32030	2.95	20	9.26211	2.35	9.34981	2.90
22	. 23834	2.45	. 32089	3.00	22	.26258	2.40	.35039	2.95
24 26	.23883	2.45	.32149	2.95	24 26	.26306	2.40	. 35098	2.90
		2.45	_	3.00		. 26354	2.40	.35156	2.95
28 30	.23981 9.24030	2.45	.32268 9.32327	2.95	28	. 26402 9. 26449	2.35	.35215	2.90
32	.24079	2.45	. 32387	3.00	30 32	.26497	2.40	9.35273 .35331	2.90
34	.24129	2.50	.32446	2.95	-		2.40	1	2.95
36	.24129	2.45	.32440	3.00	34 36	.26545	2.35	.35390	2.90
38	.24227	2.45	. 32565	2.95	38	.26640	2.40	.35506	2.90
40	9.24276	2.45	9.32624	2.95	40	9.26687	2.35	9.35565	2.95
42		2.45	. 32684	3.00			2.40		2.90
44	.24325	2.45	. 32084	2.95	42	. 26735 . 26782	2.35	. 35623	2.90
46	.24422	2.40	.32802	2.95	44 46	,26830	2.40	-35739	2.90
48	. 24471	2.45	.32861	. 2.95	48	.26877	2.35	.35798	2.95
50	9.24520	2.45	9.32921	3.00	50	9.26924	2.35	9.35856	2.90
52	.24569	2.45	. 32980	2.95	52	.26972	2.40	.35914	2.90
54	.24618	2.45	. 33039	2.95	54	. 27019	2.35	.35972	2.90
56	.24666	2.40	.33098	2.95	56	. 27066	2.35	. 36030	2.90
58	.24715	2.45	.33158	3.00	58	.27114	2.40	. 36088	2.90
60	9.24764	2.45	9.33217	2.95	60	9.27161	2.35	9.36146	2.90
62	.24813	2.45	. 33276	2.95	62	.27208	2.35	. 36204	2.90
64	. 24861	2.40	.33335	2.95	64	.27255	2.35	.36262	2.90
66	.24910	2.45	. 33394	2.95 2.95	66	. 27302	2.35	.36320	2.90
68	24958		. 33453		68	. 27349	2.35	.36378	2.90
70	9.25007	2.45	9.33512	2.95 2.95	70	9.27396	2.35	9.36436	2.90
72	.25055	2.45	.33571	2.95	72	.27444	2.35	.36494	2.90
74	.25104	2.40	.33630	2.95	74	.27491	2.35	.36552	2.90
76	.25152	2.45	.33689	2.95	76	.27538	2.35	.36610	2.90
78	.25201	2.40	. 33748	2.95	78	. 27585	2.35	.36668	2.90
80	9.25249	2.40	9.33807	2.95	80	9.27632	2.30	9.36726	2.90
82	. 25297	2.45	. 33866	2.95	82	.27678	2.35	. 36784	2.90
84 86	.25346	2.40	. 33925	2.95	84	. 27725	2.35	.36842	2.90
	.25394	2.40	.33984	2.90	86	.27772	2.35	.36900	2.85
88 90	.25442	2.45	. 34042	2.95	88	.27819	2.35	.36957	2.90
90 92	9.2549I .25539	2.40	9.34101 .34160	2.95	90 92	9.27866 .27913	2.35	9.37015	2.90
		2.40		2.95	1 *		2.30		2.90
94 96	.25587	2.40	.34219	2.90	94 96	. 27959 . 28006	2.35	.37131	2.85
98	.25683	2.40	.34277	2.95	98	.28053	2.35	.37246	2.90
100	9.25731	2.40	9 · 34395	2.95	100	9.28099	2.30	9.37304	2.90
100	9.25731		9 - 34395		100	9.28099		1 9.37304	<u> </u>

Hun-		36	°°		Hun-		3	7°	
dredths	Vers	Diff.	Exsec	Diff. .∞ı	dredths	Vers	Diff.	Exsec	Diff. .∞ı
00	9.28099		9.37304	2.85	00	9.30398		9.40163	- 0-
02	.28146	2.35	.37361		02	.30444	2.30	. 40220	2.85
04	.28193	2.35	.37419	2.90	04	.30489	2.25	. 40277	2.85
06	. 28239	2.30	-37477	2.90	06	.30534	2.25	. 40334	2.85
о8	. 28286		-37534		08	. 30579		. 40390	
10	9.28332	2.30	9.37592	2.90	10	9.30624	2.25	9.40447	2.85
12	.28379	2.30	. 37649	2.90	12	.30670	2.30	.40503	2.85
14	.28425	2.35	37707	2.85	14	.30715	2.25	. 40560	2.85
16	.28472	2.30	.37764	2.90	16	.30760	2.25	.40617	2.80
18	.28518	2.35	.37822	2.85	18	.30805	2.25	.40673	2.85
20	9.28565	2.30	9.37879	2.90	20	9.30850	2.25	9.40730	2.80
22	.28611	2.30	. 37937	2.85	22	. 30895	2.25	.40786	2.85
24	. 28657	2.35	37994	2.90	24	.30940	2.25	.40843	2.80
26	. 28704	2.30	.38052	2.85	26	. 30985	2.25	.40899	2.85
28	.28750	2.30	.38109	2.90	28	.31030	2.25	.40956	2.80
30	9.28796 .28842	2.30	9.38167 .38224	2.85	30	9.31075	2.25	9.41012	2.85
32		2.35		2.85	32	.31120	2.25	.41069	2.80
34	. 28889	2.30	.38281	2.90	34	.31165	2.25	.41125	2.85
36 38	.28981	2.30	.38396	2.85	36 38	.31210	2.20	.41182	2.80
40	9.29027	2.30	9.38453	2.85	40	9.31299	2.25	9.41294	2.80
	.29073	2.30	.38511	2.90			2.25		2.85
42 44	.29073	2.30	.38568	2.85	42 44	.31344	2.25	.41351	2.80
46	.29165	2.30	.38625	2.85	46	.31433	2.20	.41464	2.85
48	.29211	2.30	.38682	2.85	48	.31478	2.25	.41520	2.80
50	9.29257	2.30	9.38739	2.85	50	9.31523	2.25	9.41576	2.80
52	.29303	2.30	.38797	2.90	52	.31567	2.20	.41632	2.80
54	.29349	2.30	.38854	2.85	54	.31612	2.25	.41689	2.85
56	. 29395	2.30	.38911	2.85	56	.31657	2.25	.41745	2.80
58	.29441	2.30	. 38968	2.85	58	.31701	2.20	.41801	2.80
60	9.29487	2.30	9.39025	2.85	60	9.31746	2.20	9.41857	2.85
62	29533	_	. 39082		62	.31790		.41914	-
64	. 29578	2.25	. 391 39	2.85 2.85	64	.31835	2.25	.41970	2.80
66	. 29624	2.30	.39196	2.85	66	.31879	2.25	. 42026	2.80
68	. 29670	2.30	.39253	2.85	68	.31924	2.20	. 42082	2.80
70	9.29716	2.25	9.39310	2.85	70	9.31968	2.25	9.42138	2.80
72	.29761	2.30	.39367	2.85	72	.32013	2.20	.42194	2.80
74	.29807	2.30	.39424	2.85	74	. 32057	2.20	. 42250	2.85
76	.29853	2.25	.39481	2.85	76	.32101	2.25	.42307	2.80
78		2.30	.39538	2.85	78	.32146	2.20	.42363	2.80
80	9.29944	2.25	9.39595	2.85	80	9.32190	2.20	9.42419	2.80
82	. 29989	2.30	.39652	2.85	82	.32234	2.20	. 42475	2.80
84 86	.30035	2.25	. 39709	2.85	84 86	.32278	2.25	.42531	2.80
88	.30126	2.30	.39700	2.85	88	.32323	2.20	.42643	2.80
90	9.30171	2.25	9.39880	2.85	90	9.32411	2.20	9.42699	2.80
92	.30217	2.30	.39936	2.80	92	.32455	2.20	.42755	2.80
94	.30262	2.25	-39993	2.85	94	.32499	2.20	.42810	2.75
96	.30308	2.30	. 40050	2.85	96	.32543	2.20	.42866	2.80
98	.30353	2.25	.40107	2.85	98	.32587	2.20	.42922	2.80
100	9.30398	2.25	9.40163	2.00	100	9.32631	2.20	9.42978	⊿.00

Hun-		38	3°		Hun-		39)°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.32631	2.20	9.42978	2.80	00	9.34802	2.15	9.45752	2.75
02	.32675	2.20	.43034	2.80	02	.34845	2.15	.45807	2.75
04	.32719	2.20	.43090	2.80	04	.34888	2.15	.45862	2.75
o6 o8	.32763	2.20	.43146	2.80	06	.34930	2.15	.45917	2.75
10	.32807 9.32851	2.20	. 43202 9 · 43257	2.75	80 10	.34973 9.35016	2.15	.45972 9.46027	2.75
12	.32895	2.20	.43313	2.80	12	.35058	2.10	.46082	2.75
14	.32939	2.20	.43369	2.80	14	.35101	2.15	.46137	2.75
16	.32983	2.20	.43425	2.80	16	.35144	2.15	.46192	2.75
18	.33027	2.15	.43480	2.15	18	.35186	2.10	. 46247	2.75
20	9.33070	2.20	9.43536	2.80	20	9.35229	2.15	9.46302	2.75
22	.33114	2,20	.43592	2.75	22	.35272	2.10	. 46357	2.75
24 26	.33158	2.20	.43647	2.80	24 26	.35314	2.15	. 46412 . 46467	2.75
28	.33245	2.15	.43703 .43759	2.80	28	·35357 ·35399	2.10	.46522	2.75
30	9.33289	2.20	9.43814	2.75	30	9.35442	2.15	9.46576	2.70
32	-33333	2.20	.43870	2.80	32	.35484	2.10	.46631	2.75
34	.33376	2.15	. 43926	2.80	34	. 35526	2.10	.46686	2.75
36	.33420	2.20	.43981	2.75	36	. 35569	2.15	46741	2.75 2.75
38	.33463	2.20	.44037	2.75	38	.35611	2.15	.46796	2.75
40	9.33507	2.15	9.44092	2.80	40	9.35654	2.10	9.46851	2.70
42	33550	2.20	.44148	2.75	42	.35696	2.10	.46905	2.75
44 46	· 33594 · 33637	2.15	. 44203	2.80	44 46	.35738 .35780	2.10	.46960	2.75
48	.33681	2.20	.44239	2.75	48	.35823	2.15	.47070	2.75
50	9.33724	2.15	9.44370	2.80	50	9.35865	2.10	9.47124	2.70
52	.33768	2.20	-44425	2.75	52	.35907	2.IO 2.IO	.47179	2.75 2.75
54	.33811	2.15	.44481		54	-35949	2.10	-47234	2.70
56	.33854	2.13	.44536	2.75	56	.35991	2.15	. 47288	2.75
58	.33898	2.15	.44592	2.75	58	.36034	2.10	-47343	2.75
60	9.33941	2.15	9.44647	2.75	60	9.36076	2.10	9.47398	2.70
62 64	.33984	2.20	.44702	2.80	62	.36118	2.10	.47452	2.75
66	.34026	2.15	.44758	2.75	64 66	.36202	2.10	.47507 .47562	2.75
68	.34114	2.15	.44868	2.75	68	.36244	2.10	.47616	2.70
70	9.34157	2.15	9.44924	2.80	70	9.36286	2.10	9.47671	2.75
72	.34200	2.15	-44979	2.75 2.75	72	.36328	2.IO 2.IO	.47725	2.70 2.75
74	.34244	2.15	. 45034	2.80	74	.36370	2.10	.47780	2.70
76 78	.34287	2.15	.45090	2.75	76 78	.36412	2.10	.47834	2.75
70 80	.34330	2.15	.45145	2.75	78 80	.36454	2.10		2.75
82	9.34373	2.15	9.45200	2.75		9.36496	2.10	9.47944	2.70
84	.34416 .34459	2.15	.45255	2.80	82 84	.36538 .36579	2.05	.47998	2.75
86	. 34502	2.15	.45366	2.75	86	.36621	2.10	.48107	2.70
88	-34545	2.15	.45421	2.75	88	.36663	2.10	.48161	2.70
90	9.34588	2.15 2.15	9.45476	2.75 2.75	90	9.36705	2.10	9.48216	2.75 2.70
92	.34631	2.15	.4548I	2.75	92	.36747	2.10	.48270	2.75
94	.34674	2.10	.45586	2.80	94	.36788	2.10	.48325	2.70
96 98	.34716 .34759	2.15	.45642	2.75	96 98	.36830	2.10	. 48379	2.70
100	9.34802	2.15		2.75	100	9.36913	2.05	9.48488	2.75
100	9.34002		9.45752	1	1 100	9.30913	1	9.40400	

Hun-			10°		Hun-		4	1°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff. .∞ı
00	9.36913	2.10	9.48488	2.70	00	9.38968	2.05	9.51190	2.67
02	. 36955		. 48542	2.70	02	. 39009	2.05	.51243	2.65
04	. 36997	2.10	. 48597	2.75	04	. 39049	2.00	.51297	2.70 2.70
06	. 37038	2.10	. 48651	2.70	06	. 39090	2.00	.51351	2.70
о8	. 37080	2.05	. 48705	2.75	08	.39130	2.05	. 51405	2.70
· 10	9.37121	2.10	9.48760	2.70	10	9.39171	2.00	9.51459	2.65
12	.37163	2.05	.48814	2.70	12	. 39211	2.00	.51512	2.70
14	.37204	2.10	. 48868 . 48922	2.70	14 16	. 39251	2.05	.51566	2.65
16 18	.37246	2.05	. 48922	2.75	18	.39292	2.00	.51619	2.70
20	9.37329	2.10	.49031	2.70	20	9.39372	2.00		2.70
		2.05		2.70			2.05	9.51727	2.65
22 24	.37370	2.10	.49085	2.70	22 24	.39413	2.00	.51780	2.70
26	-37453	2.05	.49194	2.75	26	39453	2.00	.51887	2.65
28	-37494	2.05	. 49248	2.70	28	39534	2.05	.51941	2.70
30	9.37536	2.10	9.49302	2.70	30	9.39574	2.00	9.51995	2.70
32	.37577	2.05	.49356	2.70	32	.39614	2.00	.52048	2.65
34	.37618	2.05	.49410	2.70	34	39654	2.00	.52102	2.70
36	.37659	2.05	. 49465	2.75	36	. 39694	2.00	.52155	2.65
38	.37701	2.10	.49519	2.70	38	-39735	2.05	. 52209	2.70
40	9.37742	2.05	9.49573	2.70	40	9.39775		9.52262	-
42	.37783	2.05	.49627	2.70	42	.39815	2.00	.52316	2.70
44	.37824	2.05	. 49681	2.70	44	. 39855	2.00	. 52369	2.65 2.70
46	.37865	2.05	-49735	2.70	46	. 39895	2.00	.52423	2.70
48	.37906		. 49789		48	-39935		. 52476	2.65
50	9.37948	2.10	9.49843	2.70	50	9.39975	2.00	9.52529	2.70
52	.37989	2.05	. 49897	2.70	52	.40015	2.00	.52583	2.65
54	. 38030	2.05	. 49951	2.70	54	.40055	2.00	. 52636	2.70
56	.38071	2.05	.50005	2.70	56	.40095	2.00	.52690	2.65
58	. 38112	2.05	.50059	2.70	58	.40135	2.00	.52743	2.65
60	9.38153	2.05	9.50113	2.70	60	9.40175	2.00	9.52796	2.70
62	. 38194	2.05	.50167	2.70	62	.40215	2.00	.52850	2.65
64 66	. 38235 . 38276	2.05	.50221	2.70	64 66	. 40255 . 40294	1.95	.52903	2.65
68		2.05	.50275	2.70	68		2.00	. 52956	2.70
70	.38317	2.00	.50329 9.50383	2.70	70	9.40374	2.00	. 53010 9. 53063	2.65
72	.38398	2.05	.50437	2.70	72	.40414	2.00	.53116	2.65
74	.38439	2.05	.50491	2.70	74	.40454	2.00	.53170	2.70
76	.38480	2.05	. 50544	2.65	76	.40493	1.95	.53223	2.65
78	. 38521	2.05	.50598	2.70	78	40533	2.00	.53276	2.65 2.70
80	9.38562	2.05	9.50652	2.70	80	9.40573	2.00	9.53330	
82	.38602	2.00	. 50706	2.70	82	.40613	2,00	.53383	2.65
84	. 38643	2.05	.50760	2.70	84	. 40652	1.95	.53436	2.65 2.65
86	. 38684	2.05	.50814	2.70	86	.40692	2.00 1.95	.53489	2.65
88	. 38724		. 50867	2.70	88	. 40731	2.00	.53542	2.70
90	9.38765	2.05	9.50921	2.70	90	9.40771	2.00	9.53596	2.70
92	. 38806	2.00	.50975	2.70	92	.40811	1.95	.53649	2.65
94	. 38846	2.05	.51029	2.70	94	. 40850	2.00	.53702	2.65
96	. 38887	2.05	.51083	2.65	96	.40890	1.95	-53755	2.65
98	.38928	2.00	.51136	2.70	98	.40929	2.00	.53808	2.65
100	9.38968		9.51190		100	9.40969	1	9.53861	

Hundredths 00 9.409 02 .410 04 .410 06 .410 08 .411 12 .412 14 .412 16 .412 18 .433 20 9.413 22 .414 24 .414 26 .412 28 .415	1.95 8.8 2.00 1.95 2.00 2.00 1.95 2.00 2.	Exsec 9.53861 53915 53968 54021 54074 9.54127 54128 54232 54286 54339 9.54392 54445 54455	Diff. .001 2.70 2.65 2.65 2.65 2.65 2.65 2.65 2.65 2.65	Hundredths 00 02 04 06 08 10 12 14 16 18 20	Vers 9.42918 .42957 .42995 .43033 .43072 9.43110 .43149 .43187 .43225 .43264	Diff. .001 1.95 1.90 1.90 1.95 1.90 1.95 1.90 1.95	Exsec 9.56505 .56558 .56611 .56663 .56716 9.56768 .56821 .56873 .56926 .56979	Diff. .001 2.65 2.65 2.60 2.65 2.60 2.65 2.60 2.65 2.65
02 .410 04 .410 06 .410 08 .411 10 9.411 12 .412 14 .412 18 .413 20 9.413 22 .414 24 .414 26 .414	1.95 8.8 2.00 1.95 2.00 2.00 1.95 2.00 2.	.53915 .53968 .54021 .54074 9.54127 .54180 .54232 .54286 .54339 9.54392 .54445 .54498	2.65 2.65 2.65 2.65 2.65 2.60 2.70 2.65 2.65 2.65	02 04 06 08 10 12 14 16	.42957 .42995 .43033 .43072 9.43110 .43149 .43187 .43225	1.90 1.90 1.95 1.90 1.95 1.90 1.90	.56558 .56611 .56663 .56716 9.56768 .56821 .56873 .56926	2.65 2.60 2.65 2.60 2.65 2.60 2.65 2.65
04 .410 06 .410 08 .411 10 9.411 12 .412 14 .412 18 .413 20 9.413 22 .414 24 .414 26 .414	8 2.00 1.95 2.00 1.95 2.00 1.95 1.95 2.00 1.95 2.00 1.95 1.95 2.00 1.95 1.95 1.95 2.00 1.95	.53968 .54021 .54074 9.54127 .54180 .54232 .54286 .54339 9.54392 .54445 .54498	2.65 2.65 2.65 2.65 2.65 2.60 2.70 2.65 2.65 2.65	04 06 08 10 12 14 16	.42995 .43033 .43072 9.43110 .43149 .43187 .43225	1.90 1.90 1.95 1.90 1.95 1.90 1.90	. 56611 . 56663 . 56716 9. 56768 . 56821 . 56873 . 56926 . 56979	2.65 2.60 2.65 2.60 2.65 2.60 2.65 2.65
06 .410 08 .411 10 9.411 12 .412 14 .412 16 .412 18 .413 20 9.413 22 .414 24 .414 26 .414	1.95 2.00 1.95 1.95 2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.0	.5402I .54074 9.54127 .54180 .54232 .54286 .54339 9.54392 .54445 .54498	2.65 2.65 2.65 2.65 2.60 2.70 2.65 2.65 2.65	06 08 10 12 14 16	.43033 .43072 9.43110 .43149 .43187 .43225	1.90 1.95 1.90 1.95 1.90 1.90	. 56663 . 56716 9. 56768 . 56821 . 56873 . 56926 . 56979	2.60 2.65 2.60 2.65 2.60 2.65 2.65
08 .411 10 9.411 12 .412 14 .412 16 .412 18 .413 20 9.413 22 .414 24 .414 26 .414	2.00 1.95 1.95 2.00 1.95	.54074 9.54127 .54180 .54232 .54286 .54339 9.54392 .54445 .54498	2.65 2.65 2.65 2.60 2.70 2.65 2.65	08 10 12 14 16 18	.43072 9.43110 .43149 .43187 .43225	1.95 1.90 1.95 1.90 1.90	.56716 9.56768 .56821 .56873 .56926 .56979	2.65 2.60 2.65 2.60 2.65 2.65
10 9.411 12 .412 14 .412 16 .412 18 .413 20 9.413 22 .414 26 .414	1.95 1.95 2.00 1.95 2.00 1.95 2.00 1.95 1.95 2.00 1.95 1.95 2.00 1.95 1.95 2.00 1.95	9.54127 .54180 .54232 .54286 .54339 9.54392 .54445 .54498	2.65 2.65 2.60 2.70 2.65 2.65 2.65	10 12 14 16 18	9.43110 .43149 .43187 .43225	1.90 1.95 1.90 1.90	9.56768 .56821 .56873 .56926 .56979	2.65 2.60 2.65 2.65
12 .412 14 .412 16 .412 18 .413 20 9.413 22 .414 24 .414	1.95 2.00 1.95 1.95 1.95 2.00 3.3 1.95 1.95 1.95 1.95 1.95 1.95 1.95 1.95	.54180 .54232 .54286 .54339 9.54392 .54445 .54498	2.65 2.60 2.70 2.65 2.65 2.65	12 14 16 18	.43149 .43187 .43225	1.95 1.90 1.90 1.95	. 56821 . 56873 . 56926 . 56979	2.60 2.65 2.65
14 .412 16 .412 18 .413 20 9.413 22 .414 24 .414 26 .414	2.00 1.95 1.95 2.00 1.95 1.95 1.95 1.95 1.95 2.00 1.95 2.00 1.95	.54232 .54286 .54339 9.54392 .54445 .54498	2.70 2.65 2.65 2.65	14 16 18	. 43187 . 43225	1.90 1.95	. 56873 . 56926 . 56979	2.65 2.65
16 .412 18 .443 20 9.413 22 .414 24 .414 26 .414	1.95 1.95 2.00 1.95 1.95 1.95 1.95 2.00 1.95 2.00	.54286 .54339 9.54392 .54445 .54498	2.65 2.65 2.65	16 18	. 43225	1.95	. 56926 . 56979	2.65
18 .413 20 9.413 22 .414 24 .414 26 .414	1.95 2.00 1.95 1.95 1.95 1.95 2.00 1.95	·54339 9·54392 ·54445 ·54498	2.65 2.65	18			. 56979	
20 9.413 22 .414 24 .414 26 .414	2.00 1.95 1.95 1.95 1.95 2.00 1.95	9 · 54392 · 54445 · 54498	2.65			T 00		
22 .414 24 .414 26 .414	1.95 1.95 1.95 2.00 1.95	· 54445 · 54498	- 1		9.43302		9.57031	2.60
24 .414 26 .414	1.95 30 2.00 20 1.95	. 54498	2.65	22	.43340	1.90	.57084	2.65
26 .414	30 1.95 2.00 1.95			24	.43378	1.90	.57136	2.60
28 475	1.95		2.65	26	43417	1.95	.57189	2.65
	1.95	. 54604	2.65	28	. 43455	1.90	.57241	
30 9.415		9.54657	2.65	30	9.43493	1.90	9.57294	2.65
32 .415	98 I.95 I.95	.54710	2.65	32	.43531	1.90 1.90	.57346	2.65
34 .416	37 1.95	.54763		34	. 43569		.57399	2.60
36 .416	70 1.05	.54816	2.65	36	. 43608	1.95	.57451	2.60
38 .417	2.00	. 54869	2.65	38	. 43646	1.90	.57503	2.65
40 9.417	1.95	9.54922	2.65	40	9.43684	1.90	9.57556	2.60
42 .417	94 T.05	. 54975	2.65	42	. 43722	1.90	. 57608	2.65
44 .418	33 тоб	. 55028	2.65	44	.43760	1.90	.57661	2.60
46 .418	1.95	. 55081	2.65	46	. 43798	1.90	.57713	2.65
48 .419		.55134	2.65	48	. 43836	1.90	. 57766	2.60
50 9.419	50 1.05	9.55187	2.65	50	9.43874	1.90	9.57818	2.60
52 .419	1.93	. 55240	2.60	52	.43912	1.90	.57870	2.65
54 .420 56 .420	67 1.95	. 55292	2.65	54 56	. 43950	1.90	.57923	2.60
58 .421	6 1.95	.55398	2.65	58	.43900	1.90	.58027	2.60
60 9.421	1.90	9.55451	2.65	60	9.44064	1.90	9.58080	2.65
62 .421	1.95	.55505	2.70	62	.44102	1.90	.58132	2.60
64 .423	1.93	. 55557	2.60	64	.44140	1.90	.58184	2.60
66 .422		FF600	2.60	66	.44177	1.85	.58237	2.65
68 .423		==660	2.65	68	.44215	1.90	. 58289	2.60
70 9.42	1 1.93	0 55575	2.65	70	9.44253	1.90	9.58341	2.65
72 .423	77 1.95		2.65	72	.44291	1.90	. 58394	2.60
74 .42				74	.44329		.58446	2.60
76 .42	55 1.95	.55873	2.65	76	.44366	1.85	. 58498	2.60
78 .42	94 1.90		2.65	78	.44404	1.90	. 58550	2.65
80 9.42	32 1.95	9.55979	2.60	80	9.44442	1.90	9.58603	2.60
82 .42		.56031	2.65	82	. 44480	1.85	.58655	2.60
84 .420		.56084	2.65	84	.44517	1.90	.58707	2.60
86 .42	1 1.93	.56137	2.60	86	.44555	1.90	.58759	2.65
88 .42	1.90		2.65	88	.44593	1.85	.58812	2.60
90 9.42 92 .42	6. 1.90		2.65	90 92	9.44630	1.90	9.58864	2.60
1 1	1.93		2.60			1.85	.58968	2.60
94 .42 96 .42	1.90	#6.000	2.65	94 96	.44705	1.90	.59020	2.60
98 .42		-60	2.65	98	.44781	1.90	.59073	2.65
100 9.42		9.56505	2.60	100	9.44818	1.85	9.59125	2.00

Hun-		44	۰		Hun-		45	٥	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.44818	1.90	9.59125	2.60	- 00	9.46671	1.85	9.61722	2.60
02	. 44856	1.85	.59177	2.60	02	. 46708	1.80	.61774	2.60
04	. 44893	1.90	. 59229	2.60	04	. 46744	1.85	.61826	2.60
о6	.44931	1.85	. 59281	2.60	06	. 46781	1.80	.61878	2.55
08	. 44968	1.85	-59333	2.60	08 10	.46817 9.46854	1.85	.61929 9.61981	2.60
10 12	9.45005	1.90	9.59385 .59437	2.60	10	.46890	1.80	.62033	2.60
	.45080	1.85	.59490	2.65	14	.46927	1.85	.62085	2.60
14 16	.45118	1.90	.59542	2.60	16	.46963	1.80	.62136	2.55
18	45155	1.85	.59594	2.60	18	.47000	1.85	.62188	2.60
20	9.45192	1.85	9.59646	2.60	20	9.47036	1.80	9.62240	2.60
22	. 45230	1.90	.59698	2.60	22	.47072	1.80	.62291	2.55
24	.45267	1.85	.59750	2.60	24	.47109	1.85	.62343	2.60
26	.45304	1.85	.59802	2.60	26	.47145	1.80	.62395	2.60
28	.45342	1.90	. 59854		28	. 47182	1.85	.62446	2.55
30	9.45379	1.85	9.59906	2.60	30	9.47218	1.80	9.62498	2.60
32	. 45416	1.85	.59958	2.60	32	. 47254	1.85	.62550	2.55
34	. 45453	1.85	.60010	2.60	34	.47291	1.80	.62601	2.60
36	.45490	1.05	.60062	2.60	36	-47327	1.80	.62653	2.60
38	.45528	1.85	.60114	2.60	38	.47363	1.80	.62705	2.55
40	9.45565	1.85	9.60166	2.60	40	9.47399	1.85	9.62756	2.60
42	. 45602	1.85	.60218	2.60	42	.47436	1.80	. 62808	2.55
44	. 45639	1.85	.60270	2.60	44	.47472	1.80	.62859	2.60
46	. 45676	1.85	_	2.60	46	. 47508	1.80	.62911	2.60
48	.45713	1.85	.60374 9.60426	2.60	48	.47544 9.47580	1.80	.62963	2.55
50 52	9.45750 .45787	1.85	.60478	2.60	50 52	.47616	1.80	,63066	2.60
		1.85	.60530	2.60	54	.47653	1.85	.63117	2.55
54 56	.45824 .45861	1.85	.60582	2.60	56	.47689	1.80	.63169	2.60
58	. 45898	1.85	.60634	2.60	58	.47725	1.80	.63220	2.55
60	9.45935	1.85	9.60686	2.60	60	9.47761	1.80	9.63272	
62	.45972	1.85	.60738	2.60	62	. 47797	1.80	.63323	2.55
64	.46009	1.85	.60790	2.60	64	47833	1.80	.63375	2.60
66	. 46046	1.85	.60841	2.55	66	. 47869	1.80	.63427	2.55
68	.46083	-	.60893	2.60	68	. 47905	1.80	.63478	2.60
70	9.46120	1.85	9.60945	2.60	70	9.47941	1.80	9.63530	2.55
72	.46157	1.85	.60997	2.60	72	-47977	1.80	.63581	2.60
74	.46194	1.80	.61049	2.60	74	.48013	1.80	.63633	2.55
76	,46230	1.85	.61101	2.60	76 78	.48049	1.80	.63684	2.60
78	.46267	1.85		2.55	80	9.48121	1.80	9.63787	2.55
80	9.46304	1.85	9.61204	2.60		. 48156	1.75	.63839	2.60
82 84	. 46341	1.85	.61256	2.60	82 84	.48192	1.80	.63890	2.55
86	.46378 .46414	1.80	.61360	2.60	86	.48228	1.80	.63941	2.55
88	.46451	1.85	.61412	2.60	88	.48264	1.80	.63993	2.60
90	9.46488	1.85	9.61464	2.60	90	9.48300	1.80	9.64044	2.55
92	.46524	1.80	.61515	2.55	92	. 48336	1.80	.64096	2.60
94	.46561	1.85	.61567	2.60	94	. 48371	1.75	.64147	2.55
96	.46598	1.85	.61619	2.60	96	. 48407	1.80	.64199	2.55
98	. 46634	1.80	.61671	2.55	98	. 48443	1.80	. 64250	2.55
100	9.46671	1.03	9.61722		100	9.48479	1	9.64301	1

Hun-		46	0		Hun-		4'	7°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.48479	1.75	9.64301	2.60	00	9.50243	1.75	9.66865	0.55
02	.48514	1.75	. 64353		02	.50278		.66916	2.55
04	. 48550	1.80	.64404	2.55	04	.50313	I.75 I.75	.66967	2.55 2.55
06	. 48586	1.75	. 64456	2.55	06	. 50347	1.70	.67018	2.55
08	. 48621	1.80	. 64507	2.55	o8	. 50382	1.75	. 67069	2.55
10	9.48657	1.80	9.64558	2.60	10	9.50417	1.75	9.67120	2.55
12	.48693	1.75	.64610	2.55	12	.50452	1.75	.67171	2.55
14	.48728	1.80	.64661	2.60	14	.50487	1.70	. 67222	2.55
16 18	. 48764 . 48799	1.75	.64713	2.55	16	.50521 .50556	1.75	.67273	2.60
		1.80		2.55	I .		1.75		2.55
20	9.48835	1.75	9.64815	2.60	20	9.50591	1.70	9.67376	2.55
22	.48870	1.80	.64867	2.55	22	.50625 .50660	1.75	. 67427	2.55
24 26	.48906 .48941	1.75	.64918	2.55	24 26	.50695	1.75	.67478	2.55
28	- 1	1.80		2.60	1		1.70	.67580	2.55
30	.48977 9.49012	1.75	9.65021	2.55	28 30	.50729 9.50764	1.75	9.67631	2.55
30	.49012	1.80	.65123	2.55	30	.50799	1.75	.67682	2.55
	. 49083	1.75	.65175	2.60		.50833	I.70	.67733	2.55
34 36	.49119	1.80	.65226	2.55	34 36	. 50868	1.75	.67784	2.55
38	.49154	1.75	.65277	2.55	38	.50902	1.70	.67835	2.55
40	9.49189	1.75	9.65328	2.55	40	9.50937	1.75	9.67886	2.55
42	.49225	1.80	.65380	2.60	42	.50971	1.70	.67937	2.55
44	.49223	1.75	.65431	2.55	44	.51006	1.75	.67988	2.55
46	. 49295	1.75	.65482	2.55	46	.51040	1.70	.68039	2.55
48	.49331	1.80	.65534	2.60	48	.51075	1.75	.68090	2.55
50	9.49366	1.75	9.65585	2.55	50	9.51109	1.70	9.68141	2.55
52	.49401	I.75 I.80	.65636	2.55	52	.51144	1.75	.68192	2.55 2.55
54	. 49437		. 65687	2.55	54	.51178	,	.68243	1
56	. 49472	I.75 I.75	.65739	2.55	56	.51213	1.75	. 68294	2.55 2.55
58	- 49507	1.75	.65790	2.55	58	.51247	1.70	. 68345	2.55
60	9.49542	1.75	9.65841	2.55	60	9.51281	1.75	9.68396	2.55
62	-49577	1.80	. 65892	2.60	62	.51316	1.70	. 68447	2.55
64	.49613	1.75	. 65944	2.55	64	.51350	1.70	.68498	2.55
66	.49648	1.75	.65995	2.55	66	.51384	1.75	.68549	2.55
68	.49683	1.75	.66046	2.55	68	.51419	1.70	.68600	2.55
70	9.49718	1.75	9.66097	2.55	70	9.51453	1.70	9.68651	2.55
72	49753	1.75	.66148	2.60	72	.51487	1.75	1	2.55
74	.49788	1.75	. 66200	2.55	74 76	.51522	1.70	.68753 .68804	2.55
76 78	. 49823 . 49858	1.75	.66302	2.55	78	.51556	1.70	. 68855	2.55
80	9.49893	1.75	9.66353	2.55	80	9.51624	1.70	9.68905	2.50
82	,49928	1.75	,66404	2.55	82	.51659	1.75	.68956	2.55
84	.49928	1.75	.66455	2.55	84	.51693	1.70	.69007	2.55
86	.49998	1.75	.66507	2.55	86	.51727	1.70	.69058	2.55
88	.50033	1.75	.66558	2.55	88	.51761	1.70	.69109	2.55
90	9.50068	1.75	9.66609	2.55	90	9.51795	1.70	9.69160	2.55
92	.50103	1.75	.66660	2.55	92	.51829	1.70	.69201	2.55
94	.50138	1.75	.66711	2.55	94	.51863	1.70	.69262	2.55
96	.50173	1.75	.66762	2.55	96	.51898	1.70	.69313	2.55 2.55
98	.50208	I.75 I.75	.66813	2.55	98	. 51932	I.70	.69364	2.55
100	9.50243	73	9.66865		100	9.51966		9.69415	

		48	۰	ī	u		49	٥	
Hun- dredths	77	Diff.	Exsec	Diff.	Hun- dredths	Vers	Diff.	Exsec	Diff.
	Vers	.001		.001			.001	Lixsec	.001
00	9.51966	1.70	9.69415	2.50	00	9.53648	1.70	9.71954	2.55
02	. 52000	1.70	.69465	2.55	02	. 53682	1.65	.72005	2.50
04	.52034	1.70	.69516 .69567	2.55	04 06	.53715	1.65	. 72055 . 72106	2.55
06		1.70	.69618	2.55	08	.53781	1.65	. 72157	2.55
08 10	.52102 9.52136	1.70	9.69669	2.55	10	9.53815	1.70	9.72208	2.55
12	.52170	1.70	.69720	2.55	12	. 53848	1.65	.72258	2.50
14	.52204	1.70	.69771	2.55	14	.53881	1.65	.72309	2.55
16	. 52238	1.70	.69822	2.55	16	.53914	1.65 1.65	. 72360	2.55
18	.52271	1.70	.69872	2.55	18	-53947	1.65	.72410	2.55
20	9.52305	1.70	9.69923	2.55	20	9.53980	1.65	9.72461	2.55
22	.52339	1.70	.69974	2.55	22	.54013	1.65	.72512	2.50
24	.52373	1.70	. 70025	2.55	24 26	. 54046	1.70	.72562	2.55
26	.52407	1.70	.70076	2.55		. 54080	1.65	.72613	2.55
28	.5244I 9.52475	1.70	.70127 9.70177	2.50	28 30	.54113 9.54146	1.65	.72664 9.72714	2.50
30 32	.52508	1.65	.70228	2.55	32	.54179	1.65	.72765	2.55
34	.52542	1.70	.70279	2.55	34	.54212	1.65	. 72816	2.55
36	.52576	1.70	.70330	2.55	36	.54245	1.65	.72866	2.50
38	.52610	1.70	. 70381	2.55	38	. 54278	1.65	.72917	2.55 2.55
40	9.52643	1.70	9.70431	2.55	40	9.54311	1.65	9.72968	2.50
42	. 52677		.70482	2.55	42	. 54344	1.65	.73018	2.55
44	.52711	1.70	.70533	2.55	44	.54377	1.60	. 73069	2.55
46	.52745	1.65	.70584	2.55	46	.54409	1.65	.73120	2.50
48	.52778	1.70	.70635	2.50	48	.54442	1.65	.73170	2.55
50	9.52812	1.70	9.70685	2.55	50 52	9.54475 .54508	1.65	9.7322I .7327I	2.50
52	.52879	1.65	.70787	2.55	54	.54541	1.65	.73321	2.50
54 56	.52079	1.70	.70838	2.55	54 56	.54574	1.65	73372	2.55
58	.52946	1.65	.70889	2.55	58	.54607	1.65	.73423	2.55
60	9.52980	1.70	9.70939	2.50	60	9.54639	1	9.73474	2.55
62	.53014	1.70	.70990	2.55	62	.54672	1.65	.73524	2.50
64	.53047	1.65	.71041	2.55	64	.54705	1.65	.73575	2.55 2.55
66	.53081	1.65	.71092	2.50	66	.54738	1.65	.73626	2.50
68	.53114	1.70	.71142	2.55	68	.54771	1.60	.73676	2.55
70	9.53148	1.65	9.71193	2.55	70	9.54803	1.65	9.73727	2.55
72	.53181	1.70	.71244	2.55	72	.54836	1.65	.73778	2.50
74 76	.53215	1.65	.71295	2.50	74 76	.54869	1.60	.73879	2.55
78	.53240	1.70	.71396	2.55	78	.54934	1.65	.73929	2.50
80	9.53315	1.65	9.71447	2.55	80	9.54967	1.65	9.73980	2.55
82	.53348	1.65	.71498	2.55	82	-54999	1.60	.74031	2.55
84	.53382	1.70	.71548	2.50	84	.55032	1.65	.74081	2.50
86	.53415	1.65	.71599	2.55	86	.55065	1.65	.74132	2.55
88	-53449	1.65	.71650	2.50	88	.55097	1.65	.74182	2.55
90	9.53482	1.65	9.71700	2.55	90	9.55130	1.60	9.74233	2.55
92	.53515	1.70	.71751	2.55	92	.55162	1.65	.74284	2.50
94	.53549	1.65	.71802	2.55	94 96	.55195	1.65	·74334 ·74385	2.55
96 98	.53582 .53615	1.65	.71853	2.50	98	.55226	1.60	.74305	2.50
100	9.53648	1.65	9.71954	2.55	100	9.55293	1.65	9.74486	2.55
100	9.53048	1	1 9.71954	1	1 100	9.33293	1	9.74400	1

		50	0°				51	L°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	Hun- dredths	Vers	Diff.	72	Diff.
	Vers	.001		.001			.001	Exsec	.001
00	9.55293	1.60	9.74486	2.50	00	9.56900	1.60	9.77013	2.50
02 04	. 55325 . 55358	1.65	.74536 .74587	2.55	02 04	. 56932 . 56963	1.55	. 77063	2.55
06	.55330	1.60	.74638	2.55	06	. 56995	1.60	.77114 .77164	2.50
08	.55423	1.65	.74688	2.50	o8	.57027	1.60	.77215	2.55
10	9.55455	1.60 1.60	9 74739	2.55	10	9.57059	1.55	9.77265	2.50
12	. 55487	1.65	.74789	2.55	12	.57090	1.60	.77316	2.55 2.50
14	. 55520	1.60	.74840	2.50	14	.57122	1.60	. 77366	2.55
16 18	. 55552 . 55 585	1.65	.74890 .74941	2.55	16 18	.57154 .57185	1.55	.77417	2.50
20	9.55617	1.60	9.74992	2.55	20	9.57217	1.60	9.77518	2.55
22	.55649	1.60	.75042	2.50	22	.57249	1.60	.77568	2.50
24	.55682	1.65	.75042	2.55	24	.57249	1.55	.77508	2.55
26	.55714	1.60	.75143	2.50	26	.57312	1.60	.77669	2.50
28	. 55746	1.60	.75194	2.55	28	.57343	I.55 I.60	.77720	2.55
30	9.55779	1.65 1.60	9.75244	2.50	30	9.57375	1.60	9.77770	2.50
32	.55811	1.60	.75295	2.50	32	57407	1.55	.77821	2.50
34	-55843	1.60	.75345	2.55	34	. 57438	1.60	.77871	2.55
36 38	. 558 75 . 55908	1.65	.75396 .75447	2.55	36 38	.57470 .57501	1.55	.77922	2.50
40	9.55940	1.60	9.75497	2.50	40	9.57533	1.60	9.78023	2.55
42	-55972	1.60	.75548	2.55	42	.57564	1.55	.78073	2.50
44	.56004	1.60	.75598	2.50	44	.57596	1.60 1.55	.78124	2.55
46	. 56036	1.60 1.65	.75649	2.55	46	. 57627	1.55	.78174	2.50
48	. 56069	1.60	. 75699	2.50	48	. 57659	1.55	. 78225	2.55
50	9.56101	1.60	9.75750	2.55 2.50	50	9.57690	1.55	9.78275	2.50
52	. 56133	1.60	.75800	2.55	52	.57721	1.60	. 78326	2.50
54 56	. 56165 . 56197	1.60	.75851	2.50	54	.57753	1.55	. 78376	2.55
58	.56229	1.60	.7590I .75952	2.55	56 58	.57784 .57816	1.60	.78427	2.50
60	9.56261	1.60	9.76002	2.50	60	9.57847	1.55	9.78527	2.50
62	.56293	1.60	. 76053	2.55	62	.57878	1.55	.78578	2.55
64	.56325	1.60	.76103	2.50	64	.57910	1.60	. 78628	2.50
66	. 56357	1.60	.76144	2.55 2.50	66	.57941	1.55	. 78679	2.55
68	. 56390	1.60	.76204	2.50	68	.57972	1.60	. 78729	2.50
70	9.56422	1.60	9.76255	2.55	70	9.58004	1.55	9.78780	2.50
72	.56454	1.55	. 76306	2.50	72	. 58035	1.55	. 78830	2.55
74 76	. 56485 . 56517	1.60	.76356	2.55	74 76	. 58066 . 58097	1.55	.78881	2.50
78	.56549	1.60	.76457	2.50	78	.58129	1.60	.78982	2.55
80	9.56581	1.60	9.76508	2.55	80	9.58160	1.55	9.79032	2.50
82	.56613	1.60	.76558	2.50	82	.58191	I.55 I.55	.79083	2.55
84	. 56645	1.60	. 76609	2.55	84	. 58222	1.55	.79133	2.50
86	56677	1.60	.76659	2.50	86	. 58253	1.60	.79184	2.55
88	. 56709	1.60	.76710	2.50	88	. 58285	1.55	.79234	2.55
90 92	9.56741 .56773	1.60	9.76760	2.55	90 92	9.58316 .58347	1.55	9.79285 -79335	2.50
92	.56804	1.55	.76861	2.50	92	.58378	1.55	. 79335	2.55
96	.56836	1.60	.76912	2.55	94 96	.58409	1.55 1.55	.79386	2.50
98	. 56868	1 60 1.60	.76962	2.50	98	.58440	1.55	. 79487	2.55
100	9.56900	1.00	9.77013	2.55	100	9.58471	1.55	9.79537	2.50

Hun-		52	2°		Hun-		53	3°	
dredths	Vers	Diff.	Exsec	Dıff.	dredths	Vers	Diff.	Exsec	Dıff.
- 00	9.58471		9.79537		-00	9.60008		9.82062	
02	. 58502	1.55	.79588	2.55	02	. 60039	1.55	.82113	2.55
04	. 58534	1.60	. 79638	2.50	04	.60069	1.50	.82163	2.50
06	. 58565	I.55 I.55	. 79689	2.55	06	.60100	I.55 I.50	.82214	2.55 2.50
о8	. 58596	1.55	. 79739	2.55	о8	.60130	1.50	.82264	2.55
10	9.58627	1.55	9.79790	2.50	10	9.60160	1.55	9.82315	2.50
12	. 58658	1.55	.79840	2.55	12	.60191	1.50	.82365	2.55
14	.58689	1.55	.79891	2.50	14	.60221	1.50	.82416	2.50
16 18	. 58720 . 58751	1.55	.79941	2.55	16 18	.60251 .60282	1.55	.82466 .82517	2.55
20		1.55		2.50	20		1.50		2.55
	9.58782	1.50	9.80042	2.55		9.60312	1.50	9.82568	2.50
22 24	.58812	1.55	.80093 .80143	2.50	22 24	.60342 .60372	1.50	.82618 .82669	2.55
26	.58874	1.55	.80143	2.55	26	.60403	1.55	.82719	2.50
28	.58905	1.55	.80244	2.50	28	.60433	1.50	.82770	2.55
30	9.58936	1.55	9.80295	2.55	30	9.60463	1.50	9.82820	2.50
32	.58967	1.55	.80345	2.50	32	.60493	1.50	.82871	2.55
34	. 58998	1.55	.80395	2.50	34	.60523	1.50	.82921	2.50
36	.59029	1.55	.80446	2.55	36	.60554	1.55	.82972	2.55
38	. 59059	1.50 1.55	.80496	2.50	38	.60584	I.50 I.50	.83022	2.50 2.55
40	9.59090	1.55	9.80547	2.50	40	9.60614	1.50	9.83073	2.50
42	.59121		.80597	2.55	42	.60644	1.50	.83123	2.55
44	.59152	I.55 I.55	.80648	2.50	44	.60674	1.50	.83174	2.55
46	.59183	1.50	.80698	2.55	46	.60704	1.50	.83225	2.50
48	.59213	1.55	. 80749	2.50	48	.60734	1.50	.83275	2.55
50	9.59244	1.55	9.80799	2.55	50	9.60764	1.55	9.83326	2.50
52	.59275	1.55	.80850	2.50	52	.60795	1.50	.83376	2.55
54	. 59306	1.50	.80900	2.50	54	.60825 .60855	1.50	.83427	2.50
56 58	. 59336 . 59367	1.55	.80950 .81001	2.55	56 58	.60885	1.50	.83477 .83528	2.55
60	9.59398	1.55	9.81052	2.55	60	9.60915	1.50	9.83579	2.55
62		1.50	.81102	2.50	62	.60945	1.50	.83629	2.50
64	.59428	1.55	.81153	2.55	64	.60945	1.50	.83680	2.55
66	.59490	1.55	.81203	2.50	66	.61005	1.50	.83730	2.50
68	.59520	1.50	.81254	2.55	68	.61035	1.50	.83781	2.55
70	9.59551	1.55	9.81304	2.50	70	9.61065	I.50 I.50	9.83831	2.50
72	.59581	I.50 I.55	.81355	2.55 2.50	72	.61095	1.50	.83882	2.55 2.55
74	.59612		.81405	2.55	74	.61124	1.50	.83933	2.50
76	. 59643	1.55	.81456	2.55	76	.61154	1.50	.83983	2.55
78	. 59673	1.55	.81507	2.50	78	.61184	1.50	.84034	2.50
80	9.59704	1.50	9.81557	2.55	80	9.61214	1.50	9.84084	2.55
82	-59734	1.55	.81608	2.50	82	.61244	1.50	.84135	2.55
84	. 59765	1.50	.81658	2.55	84	.61274	1.50	.84186	2.50
86	-59795	1.55	.81709	2.50	86	.61304	1.50	.84236	2.55
88	.59826	1.50	.81759	2.55	88 90	.61334	1.45	.84287	2.50
90 92	9.59856 .59887	1.55	9.81810	2.50	90 92	9.61363	1.50	9.84337	2.55
-		1.50	.81911	2.55	92	.61423	1.50	.84439	2.55
94 96	.59917	1.55	.81911	2.50	94 96	.61423	1.50	.84489	2.50
98	.59948	1.50	.82012	2.55	98	.61483	1.50	.84540	2.55
100	9.60008	1.50	9.82062	2.50	100	9.61512	1.45	9.84590	2.50

		54	4.0				-	- 0	
Hun-			1.		Hun-		5) °	
dredths	Vers	Diff. .001	Exsec	Diff. .001	dredths	Vers	Diff. .∞ı	Exsec	Diff.
00	9.61512	1.50	9.84590	2.55	00	9.62984	1.45	9.87125	2.55
02	.61542	1.50	.84641	2.55	02	.63013		.87176	
04	.61572	1.50	.84692	2.50	04	. 63042	I.45 I.45	.87227	2.55 2.50
о6	.61602	1.45	.84742	2.55	06	.63071	1.50	.87277	2.55
08	.61631	1.50	.84793	2.55	08	.63101	1.45	. 87328	2.55
10	9.61661	1.50	9.84844	2.50	10 12	9.63130	1.45	9.87379	2.55
12	.61691	1.45	.84894	2.55		.63159	1.45	.87430	2.50
14 16	.61720	1.50	.84945	2.55	14 16	.63188 .63217	1.45	.87480	2.55
18	.61750 .61780	1.50	.84996 .85046	2.50	18	.63217	1.45	.87531 .87582	2.55
20	9.61809	1.45		2.55	20	9.63275	1.45		2.55
		1.50	9.85097	2.50			1.45	9.87633	2.55
22 24	.61839 .61868	1.45	.85147 .85198	2.55	22 24	.63304 .63333	1.45	.8768.4 .87735	2.55
26	.61898	1.50	.85249	2.55	26	.63362	1.45	.87785	2.50
28	.61928	1.50	.85299	2.50	28	.63391	1.45	.87846	2.55
30	9.61957	1.45	9.85350	2.55	30	9.63420	1.45	9.87887	2.55
32	.61987	1.50	.85401	2.55	32	.63448	I.40	.87938	2.55
34	.62016	1.45	.85451	2.50	34	.63477	1.45	.87989	2.55
36	.62046	1.50	.85502	2.55	36	.63506	1.45	.88040	2.55
38	.62075	I.45	.85553	2.55	38	.63535	1.45	. 88090	2.50
40	9.62105	1.50	9.85603	2.50	40	9.63564	I.45	9.88141	2.55
42	.62134	1.45	.85654	2.55	42	.63593	1.45	.88192	2.55
44	.62164	1.50	.85705	2.55	44	.63622	1.45	.88243	2.55
46	.62193	I.45 I.50	.85755	2.50	46	.63651	1.45	.88294	2.55
48	.62223	_	.85806		48	.63679	1.40	. 88345	2.55
50	9.62252	I.45 I.50	9.85857	2.55	50	9.63708	I.45 I.45	9.88395	2.50 2.55
52	.62282	I.45	.85907	2.55	52	.63737	1.45	.88446	2.55
54	.62311	1.45	. 85958	2.55	54	.63766	1.45	.88497	2.55
56	.62340	1.50	.86009	2.55	56	.63795	1.40	. 88548	2.55
58	.62370	1.45	.86060	2.50	58	.63823	1.45	. 88599	2.55
60	9.62399	1.50	9.86110	2.55	60	9.63852	1.45	9.88650	2.55
62	.62429	1.45	.86161	2.55	62	.63881	1.45	.88701	2.55
64	.62458	1.45	.86212	2.50	64	.63910	1.40	.88752	2.55
66	.62487	1.50	.86262	2.55	66	.63938	1.45	.88803	2.55
68	.62517	1.45	.86313	2.55	68	.63967	1.45	.88854	2.50
70	9.62546	1.45	9.86364	2.55	70 72	9.63996 .64025	1.45	9.88904	2.55
72	.62575	1.45		2.50	· ·		1.40	.88955	2.55
74 76	.62604 .62634	1.50	.86465 .86516	2.55	74 76	.64053 .64082	1.45	.89006	2.55
78	.62663	1.45	.86567	2.55	78	.64111	1.45	.89057	2.55
80	9.62692	1.45	9.86617	2.50	80	9.64139	1.40	9.89159	2.55
82	.62722	1.50	.86668	2.55	82	.64168	1.45	.80210	2.55
84	.62751	1.45	.86719	2.55	84	.64197	1.45	.89210	2.55
86	.62780	1.45	.86770	2.55	86	.64225	1.40	.89312	2.55
88	.62809	1.45	.86820	2.50	88	.64254	1.45	.89363	2.55
90	9.62838	1.45	9.86871	2.55	90	9.64282	1.40	9.89414	2.55
92	.62868	1.50	.86922	2.55	92	.64301	1.45	.89455	2.55
94	.62897	1.45	.86973	2.55	94	.64339	I.40	.89516	2.55
96	.62926	I.45 I.45	.87023	2.50	96	.64368	I.45 I.40	.89567	2.55 2.55
98	.62955	1.45	.87074	2.55	98	. 64396	1.45	.89618	2.55
100	9.62984		9.87125		100	9.64425		9.89669	- 33

Hun-		5	6°		Hun-		5	7°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.64425	1.40	9.89669	2.55	00	9.65836	1.35	9.92225	2.55
02	. 64453	1.45	.89720	2.55	02	.65863	1.35	.92276	2.55
04	.64482	1.43	.89771	2.55	04	.65891	1.40	. 92327	2.60
06	.64510	1.45	.89822	2.55	06	.65919	1.40	.92379	2.55
о8	.64539	1.40	.89873	2.55	08	. 65947	1.40	.92430	2.55
10 12	9.64567 .64596	1.45	9.89924 .89975	2.55	10 12	9.65975	1.40	9.92481	2.55
		1.40		2.55		-	1.40		2.55
14 16	64624	1.45	.90026 .90077	2.55	14 16	.66031 .66059	1.40	.92584	2.60
18	.64681	1.40	.90128	2.55	18	.66086	1.35	.92686	2.55
20	9.64709	1.40	9.90179	2.55	20	9.66114	1.40	9.92738	2.60
22	64738	1.45	.90230	2.55	22	.66142	1.40	.92789	2.55
24	.64766	1.40	.90281	2.55	24	.66170	1.40	.92840	2.55
26	.64794	I.40 I.45	.90332	2.55	26	.66198	1.40	.92892	2.60 2.55
28	.64823		.90383	2.55	28	.66225	1.35	.92943	
30	9.64851	I.40 I.40	9.90434	2.55 2.55	30	9.66253	I.40 I.40	9.92994	2.55 2.60
32	.64880	1.40	. 90485	2.55	32	.66281	1.40	. 93046	2.55
34	.64908	1.40	.90536	2.55	34	.66309	1.35	.93097	2.60
36	.64936	1.40	.90587	2.55	36	.66336	1.40	.93149	2.55
38	.64964	1.45	.90638	2.55	38	.66364	1.40	.93200	2.55
40	9.64993	1.40	9.90689	2.60	40	9.66392	1.35	9.93251	2.60
42	.65021	1.40	.90741	2.55	42	.66419	1.40	.93303	2.55
44 46	.65049 .65077	1.40	.90792	2.55	44 46	.66447 .66475	1.40	.93354 .93405	2.55
48	.65106	1.45	.90894	2.55		.66502	1.35		2.60
50	9.65134	1.40	9.90945	2.55	48 50	9.66530	1.40	9.93457	2.55
52	.65162	1.40	.90996	2.55	52	.66558	1.40	.93560	2.60
54	.65190	1.40	.91047	2.55	54	.66585	1.35	.93611	2.55
56	.65218	1.40	.91098	2.55	56	.66613	1.40	.93663	2.60
58	.65247	I.45 I.40	.91149	2.55 2.60	58	.66640	I.35 I.40	.93714	2.55 2.60
60	9.65275	1.40	9.91201	2.55	60	9.66668	1.40	9.93766	2.55
62	.65303	1.40	.91252		62	.66696		.93817	2.60
64	. 65331	1.40	.91303	2.55 2.55	64	.66723	I.35 I.40	. 93869	2.55
66	.65359	1.40	.91354	2.55	66	.66751	1.35	.93920	2.55
68	. 65387	1.40	.91405	2.55	68	.66778	1.40	.93971	2.60
70	9.65415	1.45	9.91456	2.60	70	9.668o6 .66833	1.35	9.94023	2.55
72	.65444	1.40	.91508	2.55	72		1.40	.94074	2.60
74 76	.65472 .65500	1.40	.91559	2.55	74 76	.66861 .66888	1.35	.94126	2.55
78 78	.65528	1.40	.91661	2.55	78	.66916	1.40	.94229	2.60
80	9.65556	1.40	9.91712	2.55	80	9.66943	1.35	9.94281	2.60
82	.65584	1.40	.91764	2.60	82	.66971	1.40	.94332	2.55 2.60
84	.65612	1.40	.91815	2.55	84	.66998	1.35	.94384	2.55
86	.65640	I.40 I.40	.91866	2.55 2.55	86	.67026	I.40 I.35	.94435	2.60
88	.65668	1.40	.91917		88	.67053	1.35	.94487	2.55
90	9.65696	1.40	9.91968	2.55	90	9.67080	1.35	9.94538	2.55
92	.65724	1.40	.92020	2.55	92	.67108	1.35	.94590	2.55
94	.65752	1.40	.92071	2.55	94	.67135	1.40	.94641	2.60
96	.65780	1.40	.92122	2.55	96	.67163	1.35	.94693	2.60
98	.65808	I.40	.92173	2.60	98	.67190	1.35	·94745	2.55
100	9.65836		9.92225	1	100	9.67217		9.94796	

TABLE XXVI. — (Continued)

		5	8°		1		5	9°	
Hun-		Diff.	1	Diff.	Hun-		Diff.		Diff.
dredths	Vers	.001	Exsec	.001	dredths	Vers	.001	Exsec	.001
00	9.67217	1.40	9.94796	2.60	00	9.68571	1.35	9.97387	2.60
02	. 67245	1.35	.94848	2.60	02	.68598	1.30	. 97439	2.60
04	.67272	1.35	.94900	2.55	04	.68624	1.35	.97491	2.60
06	.67299	1.40	.94951	2.60	06	.68651	1.35	-97543	2.60
08 10	.67327 9.67354	1.35	.95003	2.55	08	.68678 9.68705	1.35	9.97595	2.60
10	.67381	1.35	9.95054	2.60	12	.68731	1.30	.97699	2.60
14	.67408	1.35	.95158	2.60	14	.68758	1.35	.97751	2.60
16	.67436	1.40	.95150	2.55	16	.68785	1.35	.97/51	2.60
18	.67463	1.35	.95261	2.60	18	.68811	1.30	.97855	2.60
20	9.67490	1.35	9.95313	2.60	20	9.68838	1.35	9.97908	2.65
22	.67517	1.35	.95364	2.55	22	.68865	1.35	.97960	2.60
24	.67545	1.40	.95416	2.60	24	.68892	1.35	.98012	2.60
26	.67572	1.35	.95468	2.60	26	.68918	1.30	.98064	2.60
28	.67599	1.35	.95520	2.60	28	. 68945	1.35	.98116	2.60
30	9.67626	1.35	9.95571	2.55	30	9.68971	1.30	9.98168	2.60
32	.67653	1.35	.95623	2.60	32	. 68998	1.35	.98220	2.60
34	.67681	1.40	.95675	2.60	34	.69025	1.35	.98273	2.65
36	. 67708	1.35	.95726	2.55	36	.69051	1.30	.98325	2.60
38	. 67735	1.35 1.35	.95778	2.60	38	. 69078	I.35 I.30	. 98377	2.60
40	9.67762		9.95830	2.60	40	9.69104		9.98429	
42	. 67789	1.35	.95882		42	.69131	1.35	. 98481	2.60 2.65
44	.67816	1.35	.95934	2.60	44	.69158	1.35	.98534	2.60
46	.67843	I.35 I.35	.95985	2.55 2.60	46	.69184	I.30 I.35	.98586	2.60
48	. 67870		.96037	2.60	48	.69211		. 98638	2.60
50	9.67897	I.35 I.40	9.96089	2.60	50	9.69237	I.30 I.35	9.98690	2.65
52	.67925	1.35	.96141	2.60	52	.69264	1.30	.98743	2.60
54	.67952	1.35	.96193	2.55	54	.69290	1.35	.98795	2.60
56	.67979	1.35	.96244	2.60	56	.69317	1.30	.98847	2.60
58	.68006	1.35	. 96296	2,60	58	.69343	1.35	. 98899	2.65
60	9.68033	1.35	9.96348	2.60	60	9.69370	1.30	9.98952	2.60
62	.68060	1.35	. 96400	2.60	62	. 69396	1.35	. 9900.1	2.60
64	.68087	1.35	.96452	2.60	64	.69423	1.30	. 99056	2.65
66	.68114	1.35	. 96504	2.60	66	. 69449	1.35	.99109	2.60
68	.68141	1.35	.96556	2.55	68	.69476	1.30	.99161	2.60
70 72	.68195	1.35	9.96607 .96659	2.60	70 72	9.69502 .69528	1.30	9.99213	2.65
	.68222	1.35		2.60			1.35	.99266	2.60
74 76	.68222	1.30	.96711 .96763	2.60	74 76	.69555 .69581	1.30	.99318 .99371	2.65
78	.68275	1.35	.96815	2.60	78	.69608	1.35	.99371	2.60
80	9.68302	1.35	9.96867	2.60	80	9.69634	1.35	9.99475	2.60
82	.68329	1.35	.96919	2.60	82	,69660	1.30		2.65
84	.68356	1.35	.96919	2.60	84	.69687	1.35	.99528 .99580	2.60
86	.68383	1.35	.97023	2.60	86	.69713	1.30	.99633	2.65
88	.68410	1.35	.97075	2.60	88	.69739	1.30	.99685	2.60
90	9.68437	1.35	9.97127	2.60	90	9.69766	1.35	9.99738	2.65
92	.68463	1.30	.97179	2.60	92	.69792	1.30	.99790	2.60 2.65
94	.68490	1.35	.97231	2.60	94	.69818	1.30	. 99843	-
96	.68517	1.35	.97283	2.60 2.60	96	.69844	1.30	.99895	2.60 2.60
98	68544	I.35 I.35	.97335	2.60	98	.69871	1.35	.99947	2.65
100	9.68571	*.33	9.97387	2.00	100	9.69897	1.30	0.00000	2.03

Hun-		60)°		Hun-		6:	1°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.69897	1.30	0.00000	2.65	00	9.71197	1.30	0.02640	2.65
02	. 69923	1.30	.00053	2.60	02	.71223	1.25	.02693	2.65
04	. 69949	1.35	.00105	2.65	04	.71248	1.30	.02746	2.65
06	. 69976	1.30	.00158	2.60	06	.71274	1.30	.02799	2.65
о8	.70002	1.30	.00210	2.65	08	.71300	1.25	.02852	2.65
10 12	9.70028	1.30	0.00263	2.60	10 12	9.71325	1.30	0.02905	2.65
	.70054	1.35	.00315	2.65		.71351	1.30	.02958	2.70
14 16	. 70081 . 70107	1.30	.00368	2.60	14 16	.71377	1.25	.03012	2.65
18	.70107	1.30	.00420	2.65	18	.71402 .71428	1.30	.03065	2.65
20	9.70159	1.30	0.00526	2.65	20		1.30		2.65
		1.30		2.60		9.71454	1.25	0.03171	2.65
22 24	. 70185 . 70211	1.30	.00578	2.65	22 24	.71479	1.30	.03224	2.70
26	.70211	1.30	.00684	2.65	26	.71530	I.25	.03278	2.65
28	.70264	1.35	.00736	2.60	28	.71556	1.30	.03384	2.65
30	9.70290	1.30	0.00789	2.65	30	9.71582	1.30	0.03437	2.65
32	.70316	1.30	.00842	2.65	32	.71607	1.25	.03491	2.70
34	.70342	1.30	.00894	2.65	34	.71633	1.30	.03544	2.65
36	.70368	1.30	.00947	2.65	36	.71658	1.25	.03597	2.65
38	. 70394	1.30	.01000	2.65	38	.71684	1.30	.03651	2.65
40	9.70420	1.30	0.01052	2.60	40	9.71709	1.25	0.03704	2.65
42	. 70446	1.30	.01105	2.65	42	.71735	1.30	.03757	2.65
44	.70472	1.30	.01158	2.65	44	.71760	1.25	.03811	2.70
46	. 70498	I.30 I.30	.01211	2.65	46	.71786	1.30	.03864	2.65 2.65
48	.70524	-	.01263	1	48	.71811	-	.03917	
50	9.70550	1.30	0.01316	2.65 2.65	50	9.71837	1.30	0.03971	2.70
52	.70576	1.30	.01369	2.65	52	.71862	1.30	.04024	2.70
54	. 70602	1.30	.01422	2.65	54	.71888	1.25	.04078	2.65
56	. 70628	1.30	.01475	2.65	56	.71913	1.30	.04131	2.65
58	.70654	1.30	.01528	2.60	58	.71939	1.25	.04184	2.70
60	9.70680	1.30	0.01580	2.65	60	9.71964	1.30	0.04238	2.65
62	.70706	1.30	.01633	2.65	62	.71990	1.25	.04291	2.70
64 66	.70732	1.30	.01686	2.65	64 66	.72015	1.30	.04345	2.65
68	.70758	1.30	.01739	2.65		.72041	1.25	.04398	2.70
70	.70784 9.70810	1.30	.01792	2.65	68 70	.72066 9.72091	1.25	.04452 0.04505	2.65
72	.70835	1.25	.01898	2.65	70 72	.72117	1.30	.04559	2.70
74	.70861	1.30	.01951	2.65			1.25	.04539	2.65
76	.70887	1.30	.02004	2.65	74 76	.72142 .72167	1.25	.04666	2.70
78	.70913	1.30	.02056	2.60	78	.72193	1.30	.04720	2.70
80	9.70939	1.30	0.02109	2.65	80	9.72218	1.25	0.04773	2.65
82	-70965	1.30	.02162	2.65	82	.72243	1.25	.04827	2.70
84	.70991	1.30	.02215	2.65	84	.72269	1.30	.04880	2.65
86	.71016	1.25	.02268	2.65	86	.72294	1.25	.04934	2.70
88	.71042	1.30	.02321	2.65	88	. 72319	1.25	.04988	2.70
90	9.71068	1.30	0.02374	2.65	90	9.72345	1.30	0.05041	2.65
92	71094	I.30 I.30	.02427	2.65 2.65	92	.72370	1.25	.05095	2.70 2.70
94	.71120	1.25	.02480	2.70	94	. 72395		.05149	2.65
96	.71145	1.25	.02534	2.70	96	.72420	1.25	,05202	2.70
98	.71171	1.30	.02587	2.65	98	. 72446	1.25	.05256	2.70
100	9.71197		0.02640		100	9.72771		0.05310	

TABLE XXVI. — (Continued)

		65	2°				63	3°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	Hun- dredths	Vers	Diff.	Exsec	Diff.
		.001		100.			.001		.001
00	9.72471	1.25	0.05310	2.70	00	9.73720	1.25	0.08015	2.75
02	.72496	1.25	.05364	2.65	02	.73745	1.20	.08070	2.70
04 06	.72521 .72547	1.30	.05417	2.70	04 06	. 7 3769 . 73794	1.25	.08124	2.75
08	.72572	1.25	.05525	2.70	08	.73819	1.25	.08233	2.70
10	9.72597	1.25	0.05579	2.70	10	9.73844	1.25	0.08288	2.75
12	.72622	I.25 I.25	.05633	2.70 2.65	12	. 73868	I.20 I.25	.08343	2.75
14	.72647	1.25	.05686	2.70	14	. 73893	I.25	.08397	2.75
16	.72672	I.30	.05740	2.70	16	.73918	1.20	.08452	2.70
18	.72698	1.25	.05794	2.70	18	.73942	1.25	.08506	2.75
20	9.72723	1.25	0.05848	2.70	20	9.73967	1.25	0.08561	2.75
22 24	.72748	1.25	.05902	2.70	22 24	.73992	1.20	.08616	2.70
26	.72773 .72798	1.25	.05956	2.70	26	.74016 .74031	1.25	.08715	2.75
28	.72823	1.25	.06064	2.70	28	.74065	1.20	.08780	2.75
30	9.72848	1.25	0.06118	2.70	30	9.74090	1.25	0.08835	2.75
32	. 72873	I.25 I.25	.06172	2.70	32	.74115	I.25 I.20	.08889	2.70
34	.72898	I.25	.06226	2.70	34	.74139	1.25	.08944	
36	.72923	I.25	.06280	2.70	36	.74164	1.25	.08999	2.75
38	.72948	1.25	.06334	2.70	38	.74188	1.25	.09054	2.70
40	9.72973	1.30	0.06388	2.70	40	9.74213	1.20	0.09108	2.75
42	.72999	1.25	.06442	2.70	42	.74237	1.25	.09163	2.75
44 46	. 73024	1.25	.06496	2.70	44 46	. 74262 . 74286	1.20	.09218	2.75
48	.73049	1.25	.06604	2.70	48	.74311	1.25	.09273	2.75
50	9.73099	1.25	0.06658	2.70	50	9.74335	1.20	0.09383	2.75
52	.73123	I.20	.06712	2.70	52	.74360	I.25 I.20	.09438	2.75
54	.73148	1.25	.06766	2.70	54	.74384	1	.09493	2.75
56	.73173	I.25 I.25	.06820	2.70	56	.74409	I.25 I.20	.09548	2.75 2.70
58	.73198	1.25	.06874	2.75	58	74433	1.25	.09602	2.75
60	9.73223	1.25	0.06929	2.70	60	9.74458	1.20	0.09657	2.75
62	. 73248	1.25	.06983	2.70	62	. 74482	1.25	.09712	2.75
64 66	. 73273 . 73298	1.25	.07037	2.70	64	.74507 .74531	1.20	.09767	2.80
68		1.25	.07146	2.75	68	.74556	1.25	.09823	2.75
70	. 73323 9 · 73348	1.25	0.07200	2.70	70	9.74580	1.20	0.09933	2.75
72	-73373	1.25	.07254	2.70	72	.74604	1.20	.09988	2.75
74	.73398	I.25 I.20	.07308	2.75	74	. 74629	I.25	. 10043	2.75
76	.73422	I.20	.07363	2.70	76	. 74653	I.20	.10098	2.75 2.75
78	-73447	1.25	.07417	2.70	78	. 74678	1.20	. 10153	2.75
80	9.73472	1.25	0.07471	2.75	80	9.74702	1.20	0.10208	2.75
82 84	.73497	1.25	.07526	2.70	82 84	. 74726	1.25	.10263	2.80
86	.73522 .73547	1.25	.07580	2.70	86	.74751 .74775	1.20	.10319	2.75
88	.73547	1.20	.07689	2.75	88	.74799	1.20	.10374	2.75
90	9.73596	1.25	0.07743	2.70	90	9.74824	1.25	0.10484	2.75
92	.73621	1.25	.07798	2.75	92	.74848	I.20 I.20	.10540	2.80
94	.73646	1.25	.07852	2.70	94	.74872	1.20	. 10595	2.75
96	.73671	I.25 I.20	.07906	2.70	96	.74896	I.25	.10650	2.75 2.75
98	73695	1.25	.07961	2.70	98	.74921	1.20	. 10705	2.80
100	9.73720		0.08015	1	100	9.74945		0.10761	1

Hun-		64	۰		Hun-		65	°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
-00	9.74945		0.10761		00	9.76146		0.13551	
02	.74969	I.20	.10816	2.75	02	.76170	I.20	. 13608	2.85
04	74993	I.20	. 10871	2.75 2.80	04	.76194	I.20 I.20	. 13664	2.80
06	.75018	I.25 I.20	. 10927	2.75	06	.76218	1.15	. 13720	2.85
о8	. 75042	1.20	. 10982	2.80	08	.76241	1.20	.13777	2.80
10	9.75066	1.20	0.11038	2.75	10	9.76265	1.20	0.13833	2.85
12	. 75090	1.25	.11093	2.80	12	. 76289	1.20	. 13890	2.80
14	.75115	1.20	.11149	2.75	14	.76313	1.15	. 13946	2.85
16	.75139	1.20	.11204	2.80	16 18	. 76336 . 76360	1.20	.14003	2.80
18	.75163	1.20		2.75	20		1.20		2.85
20	9.75187	1.20	0.11315	2.80		9.76384	1.20	0.14116	2.80
22	.75211	1.20	.11371	2.75	22	.76408	1.15	.14172	2.85
24 26	.75235 .75260	1.25	.11426	2.80	24 26	.76431 .76455	1.20	.14229	2.80
28		1.20	1 1	2.75	28	.76479	1.20	.14342	2.85
30	.75284 9.75308	1.20	0.11537	2.80	30	9.76502	1.15	0.14398	2.80
32	·75332	1.20	.11649	2.80	32	.76526	1.20	.14455	2.85
34	.75356	1.20	.11704	2.75	34	.76550	1.20	.14512	2.85
36	.75380	I.20	.11760	2.80	36	.76573	1.15	.14568	2.80
38	.75404	1.20	.11816	2.80	38	.76597	1.20	.14625	2.85
40	9.75428	1.20	0.11871	2.75	40	9.76620	1.15	0.14682	2.85
42	.75452	1.20	.11927	2.80	42	.76644	1.20	. 14738	2.80
44	.75476	I.20	.11983	2.80	44	.76668	1.20	.14795	2.85
46	.75500	I.20 I.20	.12039	2.80	46	.76691	I.15 I.20	.14852	2.85
48	.75524		.12094	2.75	48	.76715		.14909	2.85
50	9.75549	I.25 I.20	0.12150	2.80	50	9.76738	I.15 I.20	0.14966	2.85
52	-75573	1.20	.12206	2.80	52	.76762	1.15	.15022	2.85
54	.75597	1.20	.12262	2.80	54	.76785	1.20	.15079	2.85
56	.75621	I.20	.12318	2.75	56	.76809	1.20	.15136	2.85
58	75645	1.20	.12373	2.80	58	.76833	1.15	.15193	2.85
60	9.75669	1.15	0.12429	2.80	60	9.76856	1.20	0.15250	2.85
62	.75692	1.20	.12485	2.80	62	.76880	1.15	. 15307	2.85
64 66	.75716	1.20	.12541	2.80	64	.76903	1.20	. 15364	2.85
	.75740	1.20	.12597	2.80	66	.76927	1.15	.15421	2.85
68 70	.75764	I.20	.12653	2.80	68 70	.76950	1.20	.15478	2.85
70 72	9.75788	1.20	0.12709	2.80	70	9.76974 .76997	1.15	0.15535	2.85
74	.75836	1.20	.12821	2.80	74	.77021	I.20	.15649	2.85
76	.75860	1.20	.12877	2.80	76	.77044	1.15	.15049	2.85
78	.75884	1.20	.12933	2.80	78	.77068	1.20	.15764	2.90
80	9.75908	1.20	0.12989	2.80	80	9.77091	1.15	0.15821	2.85
82	-75932	1.20	.13046	2.85	82	.77114	1.15	. 15878	2.85
84	.75956	1.20	.13102	2.80	84	.77138	I.20	.15935	2.85
86	.75980	I.20 I.15	.13158	2.80	86	.77161	1.15	.15992	2.85
88	.76003	1.20	.13214	2.80	88	.77185	1.15	.16049	2.90
90	9.76027	1.20	0.13270	2.80	90	9.77208	1.15	0.16107	2.90
92	.76051	1.20	. 13326	2.85	92	.77231	1.20	.16164	2.85
94	. 76075	1.20	.13383	2.80	94	77255	1.15	.16221	2.90
96	.76099	1.20	.13439	2.80	96	.77278	1.15	.16279	2.85
98	.76123	1.15	.13495	2.80	98	.77301	I.20	.16336	2.85
100	9.76146		0.13551	l .	100	9.77325	1	0.16393	

TABLE XXVI. — (Continued)

		6	6°		Hun-		6'	7°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.77325	1.15	0.16393	2.90	00	9.78481	1.15	0.19293	2.95
02	. 77348	1.15	. 16451	2.85	02	. 78504	1.15	. 19352	2.90
04	.77371	1.15	. 16508	2.90	04	. 78527	1.15	. 19410	2.95
06	-77395	1.15	. 16566	2.85	06	. 78550	1.10	. 19469	2.95
08	.77418	1.15	. 16623	2.90	08	.78572	1.15	. 19528	2.95
10 12	9.7744I .77465	1.20	0.16681	2.85	10	9.78595 .78618	1.15	0.19587	2.90
14	.77488	1.15	.16796	2.90	14	.78641	1.15	.19704	2.95
16	.77511	1.15	.16853	2.85	16	.78664	1.15	.19763	2.95
18	.77534	1.15	.16911	2.90	18	.78687	1.15	.19822	2.95
20	9.77558	1.20	0.16969	2.90	20	9.78710	1.15	0.19881	2.95
22	.77581	1.15	.17026	2.85	22	. 78732	1.10	.19939	2.90
24	.77604	1.15	.17084	2.90	24	.78755	1.15	.19998	2.95
26	.77627	I.15 I.20	.17142	2.90	26	.78778	1.15	.20057	2.95
28	.77651	1.10	.17199	2.90	28	.78801	1.10	.20116	2.95
30	9.77674	1.15	0.17257	2.90	30	9.78823	1.15	0.20175	2.95
32	.77697	1.15	.17315	2.85	32	.78846	1.15	.20234	2.95
34	.77720	1.20	.17372	2.90	34	. 78869	1.15	20293	2.95
36 38	.77744	1.15	.17430	2.90	36 38	.78892 .78915	1.15	.20352	3.00
-	.77767	1.15	.17488	2.90	40		1.10		2.95
40	9.77790	1.15	0.17546	2.90		9.78937	1.15	0.20471	2.95
42	.77813 .77836	1.15	.17604	2.90	42	. 78960 . 78983	1.15	. 20530	2.95
44 46	.77859	1.15	.17662	2.90	44 46	.79005	1.10	.20509	2.95
48	.77882	1.15	.17778	2.90	48	.79028	1.15	. 20708	3.00
50	9.77906	1.20	0.17836	2.90	50	9.79051	1.15	0.20767	2.95
52	.77929	1.15	.17894	2 90	52	.79073	1.10	.20826	2.95
54	.77952	1.15	.17952	2.90	54	.79096	1.15	.20885	2.95
56	.77975	1.15	. 18010	2.90	56	.79119	1.15	. 20945	3.00
58	.77998	1.15	. 18068	2.90	58	.79141	1.15	.21004	3.00
60	9.78021	1.15	0.18126	2.90	60	9.79164	1.15	0.21064	2.95
62	. 78044	1.15	.18184	2.90	62	.79187	1.15	. 21123	3.00
64	. 78067	1.15	.18242	2.90	64	. 79209	1.15	.21183	2.95
66	. 78090	1.15	.18300	2.90	66	. 79232	1.15	.21242	3.00
68	.78113	1.15	. 18358	2.95	68 70	.79255	1.10	.21302 0.21361	2.95
70 72	9.78136 .78159	1.15	0.18417	2.90	70 72	9.79277	1.15	.21421	3.00
74	.78182	1.15	.18533	2.90	74	.79322	1.10	.21480	2.95
76	.78205	1.15	.18592	2.95	76	.79345	1.15	.21540	3.00
78	.78228	1.15	.18650	2.90	78	.79368	1.15	.21600	3.00 2.95
80	9.78251	1.15	0.18708	2.90	80	9.79390	1.15	0.21659	
82	.78274	1.15	.18767	2.95	82	.79413		.21719	3.00
84	.78297	1.15	. 18825	2.90	84	-79435	1.10	.21779	3.00
86	. 78320	1.15	. 18883	2.90	86	. 79458	1.15	.21839	2.95
88	.78343	1.15	. 18942	2.90	88	.79480	1.15	. 21898	3.00
90	9.78366	1.15	0.19000	2.95	90	9.79503	1.10	0.21958	3.00
92	.78389	1.15	.19059	2.90	92	.79525	1.15	.22018	3.00
94	.78412	1.15	.19117	2.95	94	.79548	1.10	.22078	3.00
96 98	.78435	1.15	.19176	2.90	96 9 8	.79570	1.15	.22138	3.00
	.78458	1.15	.19234	2.95	-	.79593	1.10	0.22258	3.00
100	9.78481	l	0.19293	!	100	9.79615		0.22258	i

TABLE XXVI. — (Continued)

				-		1			
Hun-		68	3°		Hun-		69)°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
		.001		.001			.001		.001
00	9.79615	1.15	0.22258	3.00	00	9.80729	1.10	0.25296	3.05
02	.79638	1.10	. 22318	3.00	02	.80751	1.10	.25357	3.10
04 06	.79660 .79683	1.15	. 22378	3.00	04 06	.80773 .80795	1.10	.25419	3.05
08	.79705	1.10	. 22498	3.00	08	.80817	1.10	.25542	3.10
10	9.79708	1.15	0.22558	3.00	10	9.80839	1.10	0.25604	3.10
12	.79750	1.10	.22618	3.00	12	.80861	1.10	.25666	3.10
14	.79772	1.10	.22678	3.00	14	.80883	1.10	.25727	3.05
16	.79795	1.15	.22739	3.05	16	.80905	1.10	.25789	3.10
18	.79817	I.10 I.15	.22799	3.00	18	.80927	I.10 I.10	. 25851	3.10
20	9.79840	1.10	0.22859	-	20	9.80949	1.10	0.25913	-
22	.79862		.22920	3.05	22	.80971		. 25975	3.10
24	.79884	1.10	. 22980	3.00	24	.80993	I.10 I.10	. 26037	3.10
26	.79907	1.15	. 23041	3.05	26	.81015	1.10	. 26099	3.10
28	.79929	1.15	.23101	3.00	28	.81037	1.10	. 26161	3.10
30	9.79952	1.10	0.23161	3.05	30	9.81059	1.05	0.26223	3.10
32	-79974	1.10	.23222	3.00	32	.81080	1.10	.26285	3.10
34	.79996	1.15	.23282	3.05	34	.81102	1.10	. 26347	3.10
36 38	.80019 .80041	1.10	.23343	3.00	36 38	.81124 .81146	1.10	.26409	3.10
40		1.10	0.23464	3.05	40	9.81168	1.10		3.10
	9.80063	1.10		3.00			1.10	0.26533	3.15
42 44	.80085 .80108	1.15	.23524	3.05	42 44	.81190 .81212	1.10	. 26596	3.10
46	.80108	1.10	.23646	3.05	46	.81234	1.10	.26720	3.10
48	.80152	1.10	.23706	3.00	48	.81256	1.10	.26783	3.15
50	9.80175	1.15	0.23767	3.05	50	9.81277	1.05	0.26845	3.10
52	.80197	I.10 I.10	.23828	3.05	52	.81299	I.IO I.IO	. 26907	3.10
54	.80219		. 23889	3.05	54	.81321		. 26970	3.15
56	.80241	1.10	. 23949	3.00	56	.81343	I.10 I.10	. 27032	3.10 3.15
58	.80264	1.13	.24010	3.05	58	.81365	1.10	. 27095	3.10
60	9.80286	1.10	0.24071	3.05	60	9.81387	1.05	0.27157	3.15
62	.80308	1.10	.24132	3.05	62	.81408	1.10	.27220	3.15
64	.80330	1.10	. 24193	3.05	64	.81430	1.10	.27273	3.15
66	.80352	1.15	.24254	3.05	66	.81452	1.10	.27345	3.15
68	.80375	1.10	.24315	3.05	68	.81474	1.10	. 27408	3.15
70 72	9.80397	1.10	0.24376	3.05	70 72	9.81496 .81517	1.05	0.27471	3.10
	80419	1.10	.24437	3.05			1.10	.27533	3.15
74 76	.80441 .80463	1.10	.24498	3.05	74 76	.81539 .81561	1.10	.27596	3.15
78	.80485	1.10	. 24621	3.10	78	.81583	1.10	.27722	3.15
80	9.80508	1.15	0.24682	3.05	80	9.81604	1.05	0.27785	3.15
82	.80530	1.10	.24743	3.05	82	.81626	1.10	.27848	3.15
84	.80552	1.10	.24743	3.05	84	.81648	1.10	.27911	3.15
86	.80574	1.10	.24866	3.10	86	.81670	1.10	.27974	3.15
88	.80596		.24927	3.05	88	.81691	_	. 28037	
90	9.80618	I.10 I.10	0.24988	3.05	90	9.81713	I.IO I.IO	0.28100	3.15
92	.80640	1.10	.25050	3.10	92	.81735	1.05	.28163	3.15
94	.80662	1.10	.25111	3.10	94	.81756	1.10	.28226	3.20
96	.80684	1.15	.25173	3.05	96	.81778	1.10	. 28290	3.15
98	.80707	1.10	.25234	3.10	98	.81800	1.05	. 28353	3.15
100	9.80729	ļ	9.25296	1	100	9.81821	1	0.28416	1

Hun-		70	0°		Hun-		7:	L°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.81821	1.10	0.28416	3.15	00	9.82894	1.05	0.31630	3.25
02	.81843	1.10	. 28479	3.13	02	.82915	1.05	.31695	3.25
04	.81865	1.10	. 28543	3.20	04	.82936	1.10	.31760	3.30
06	.81886	1.10	. 28606	3.20	06	. 82958	1.05	.31826	3.25
о8	.81908	1.05	.28670	3.15	о8	.82979	1.05	.31891	3.30
10	9.81929	1.10	0.28733	3.20	10	9.83000	1.05	0.31957	3.25
12	.81951	1.10	.28797	3.15	12	.83021	1.05	.32022	3.30
14 16	.81973	1.05	.28860	3.20	14 16	.83042 .83064	1.10	.32088	3.25
18	.81994 .82016	1.10	.28924	3.15	18	.83085	1.05	.32153	3.30
20		1.05		3.20	20	9.83106	1.05		3.30
	9.82037	1.05	0.29051	3.15			1.05	0.32285	3.25
22	.82058 .82080	1.10	.29114	3.20	22 24	.83127 .83148	1.05	.32350	3.30
24 26	.82080	1.10	.29178	3.20	26	.83148	1.05	.32482	3.30
28	.82124	1.10	.29306	3.20	28	.83191	1.10	.32548	3.30
30	9.82124	1.05	0.29370	3.20	30	9.83212	1.05	0.32614	3.30
32	.82167	1.10	.29434	3.20	32	.83233	1.05	.32680	3.30
34	.82188	1.05	.29498	3.20	34	.83254	1.05	.32746	3.30
36	.82210	1.10	.29562	3.20	36	.83275	1.05	.32812	3.30
38	.82231	1.05	. 29626	3.20	38	.83296	1.05	. 32878	3.30
40	9.82253		0.29690	3.20	40	9.83317	1.05	0.32944	3.30
42	.82274	1.05	. 29754		42	.83338		.33010	
44	. 82296	1.10	.29818	3.20	44	.83359	1.05	.33076	3.30
46	.82317	1.10	. 29882	3.20	46	.83381	1.05	.33142	3.35
48	. 82339	1.05	. 29946	3.20	48	.83402	1.05	. 33209	3.30
50	9.82360	1.05	0.30010	3.25	50	9.83423	1.05	0.33285	3.30
52	.82381	1.10	.30075	3.20	52	.83444	1.05	.33341	3.35
54	.82403	1.05	.30139	3.20	54	.83465	1.05	.33408	3.30
56 58	.82424	1.10	.30203	3.25	56 58	.83486 .83507	1.05	·33474 ·33541	3.35
60	9.82467	1.05	0.30332	3.20	60	9.83528	1.05	0.33607	3.30
		1.10		3.25	62		1.05		3.35
62 64	.82489 .82510	1.05	. 30397 . 30461	3.20	64	.83549 .83570	1.05	.33674 .33741	3.35
66	.82531	1.05	.30526	3.25	66	.83591	1.05	.33807	3.30
68	.82553	1.10	.30590	3.20	68	.83612	1.05	.33874	3.35
70	9.82574	1.05	0.30655	3.25	70	9.83633	1.05	0.33941	3.35
72	.82595	1.05	.30720	3.25	72	.83654	1.05	. 34008	3.35
74	.82617	1.10	.30784	3.20	74	.83675	1.05	.34075	3.35
76	.82638	1.05	. 30849	3.25 3.25	76	.83696	1.05	.34142	3.35 3.35
78	.82660	1.10	.30914	3.25	78	.83717	1.05	.34209	3.35
80	9.82681	1.05	0.30979	3.25	80	9.83738	1.05	0.34276	3.35
82	.82702	1.10	. 31044	3.25	82	.83759	1.05	34343	3.35
84	.82724	1.10	.31109	3.25	84	.83780	1.00	.34410	3.35
86	.82745	1.05	.31174	3.25	86	.83800	1.05	34477	3.35
88	.82766	1.05	.31239	3.25	88	.83821	1.05	.34544	3.35
90 92	9.82787	1.10	0.31304 .31369	3.25	90 92	9.83842 .83863	1.05	.34679	3.40
	.82830	1.05		3.25	1 1	.83884	1.05	.34746	3.35
94 96	.82830	1.05	.31434	3.25	94 96	.83905	1.05	.34740	3.40
98	.82873	1.10	.31499	3.25	98	.83926	1.05	.34881	3.35
100	9.82894	1.05	0.31630	3.30	100	9.83947	1.05	0.34948	3.35
	g.02094		0.01000			J. 93541		1	1

Hun-		7	2°		Hun-		73	3°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
		.001		.001			.001		.001
00	9.83947	1.05	0.34948	3.40	00	9.84981	1.00	0.38387	3.50
02	.83968	1.00	.35016	3.40	02	.85001	I.00	. 38457	3.50
04 06	.83988 .84009	1.05	.35084 .35151	3.35	04 06	.85021 .85042	1.05	.38527 .38597	3.50
08	.84030	1.05	.35219	3.40	08	.85062	1.00	.38668	3.55
10	9.84051	1.05	0.35287	3.40	10	9.85083	1.05	0.38738	3.50
13	.84072	I.05 I.05	.35354	3.35	12	.85104	1.05	.38809	3.55
14	.84093	I.00	.35422	3.40	14	.85124	1.00	. 38879	3.50
16	.84113	1.05	. 35490	3.40	16	.85144	I.00	. 38949	3.50
18	.84134	1.05	35558	3.40	18	.85165	1.00	. 39020	3.50
20	9.84155	1.05	0.35626	3.40	20	9.85185	1.00	0.39090	3.55
22	.84176	1.05	. 35694	3.40	22	.85205	1.05	.39161	3.55
24 26	.84197 .84217	1.00	.35762 .35830	3.40	24 26	.85226 .85246	1.00	.39232	3.55
28	.84238	1.05	.35899	3.45	28		1.05	.39303	3.50
30	9.84259	1.05	0.35967	3.40	30	.85267 9.85287	1.00	·39373 •.39444	3.55
32	.84280	1.05	.36035	3.40	32	.85307	1.00	.39515	3.55
34	.84300	1.00	.36103	3.40	34	.85328	1.05	.39586	3.55
36	.84321	1.05	.36172	3.45	36	.85348	1.00	.39667	3.55
38	.84342	1.05	.36240	3.40	38	.85368	I.00 I.05	.39728	3.55 3.60
40	9.84363	1.00	0.36309	3.40	40	9.85389	1.00	0.39800	3.55
42	.84383	1.05	. 36377	3.45	42	.85409	1.00	. 39871	3.55
44	.84404	1.05	. 36446	3.40	44	.85429	1.05	.39942	3.55
46	.84425	1.00	.36514	3.45	46	.85450	1.00	.40013	3.60
48 50	.84445 9.84466	1.05	.36583 0.36652	3.45	48	.85470	1.00	.40085	3.55
52	.84487	1.05	.36721	3.45	50 52	9.85490 .85511	1.05	0.40156	3.60
54	.84507	1.00	.36789	3.40	54	.85531	1.00	.40299	3.55
56	.84528	1.05	.36858	3 · 45	56	.85551	1.00	.40371	3.60
58	.84549	I.05 I.00	. 36927	3 · 45 3 · 45	58	.85572	I.05	.40443	3.60
60	9.84569	1.05	0.36996		60	9.85592	1.00	0.40514	3.55 3.60
62	. 84590	_	. 37065	3.45	62	.85612		.40586	
64	.84611	I.05 I.00	.37134	3.45 3.50	64	.85632	1.00	.40658	3.60 3.60
66	.84631	1.05	. 37204	3.45	66	.85653	1.00	.40730	3.60
68	.84652	1.00	.37273	3.45	68	.85673	1.00	. 40802	3.60
70 72	9.84672 .84693	1.05	0.37342 .374II	3.45	70 72	9.85693 .85713	1.00	.40946	3.60
74	.84714	1.05	.37481	3.50	74	.85733	1.00	.41018	3.60
76	.84734	1.00	.37461	3.45	74 76	.85754	1.05	.41018	3.60
78	.84755	1.05	.37619	3.45	78	.85774	1.00	.41163	3.65
80	9.84775	1.00	0.37689	3.50	80	9.85794	1.00	0.41235	3.60
82	.84796	1.05	.37759	3.50	82	.85814	1.00	.41307	3.60
84	.84816	I.00 I.05	.37828	3.45 3.50	84	.85834	I.00	.41380	3.65
86	.84837	1.00	.37898	3.50	86	.85855	1.05	.41452	3.65
88	.84857	1.05	. 37968	3.45	88	.85875	1.00	.41525	3.65
90 92	9.84878 .84899	1.05	0.38037	3.50	90	9.85895	1.00	0.41598	3.60
	.84919	1.00	.38107	3.50	92	.85915	1.00	.41670	3.65
94 96	.84919	1.05	.38177	3.50	94 96	.85935 .85955	1.00	.41743	3.65
98	.84960	1.00	.38317	3.50	98	.85975	1.00	.41889	3.65
100	9.84981	1.05	0.38387	3.50	100	9.85996	1.05	0.41962	3.65

TABLE XXVI. — (Continued)

		7/	10				7	5°	
Hun- dredths		Diff.	_	Diff.	Hun- dredths		Diff.		Diff.
areaths	Vers	.001	Exsec	.001	dredths	Vers	.001	Exsec	.001
00	9.85996	1.00	0.41962	3.65	00	9.86992	1.00	0.45693	3.80
02	.86016	1.00	. 42035	3.65	02	.87012	1.00	. 45769	3.85
04 06	.86036 .86056	1.00	. 42108	3.65	04 06	.87032 .87052	1.00	. 45846	3.80
08	.86076	1.00		3.65	08	.87032	-95	.45922	3.85
10	9.86096	1.00	. 42254 0. 42328	3.70	10	9.87091	1.00	- 45999 0. 46075	3.80
12	.86116	1.00	.42401	3.65	12	.87111	1.00	.46152	3.85
14	.86136	1.00	. 42474	3.65	14	.87131	1.00	.46228	3.80
16	.86156	I.00	. 42548	3.70 3.65	16	.87150	.95 1.00	. 46306	3.90
18	.86176	1.00	. 42621	3.70	18	.87170	1.00	. 46383	3.85
20	9.86196	1.00	0.42695	3.65	20	9.87190	.95	0.46460	3.85
22	.86216	I.00	. 42768	3.70	22	.87209	1.00	. 46537	3.85
24	. 86236	1.05	. 42842	3.70	24	.87229	1.00	.46614	3.85
26	.86257	1.00	. 42916	3.70	26	.87249	.95	.46691	3.90
28 30	.86277 9.86297	1.00	.42990 0.43064	3.70	28 30	.87268 9.87288	1.00	.46769 o.46846	3.85
32	.86317	1.00	.43138	3.70	32	.87308	1.00	.46923	3.85
34	.86337	1.00	.43212	3.70	34	.87327	-95	.47001	3.90
36	.86357	1.00	.43286	3.70	36	.87347	1.00	.47079	3.90
38	.86377	I.00	.43360	3.70	38	.87367	1.00 -95	.47156	3.85
40	9.86397	1.00	0.43434	3.75	40	9.87386	1.00	0.47234	3.90
42	.86417		. 43509	3.70	42	.87406	.95	.47312	3.90
44	.86436	.95	. 43583	3.70	44	.87425	1.00	.47390	3.90
46	.86456	1.00	. 43657	3.75	46	.87445	1.00	.47468	3.90
48	.86476	1.00	. 43732	3.70	48	.87465	.95	.47546	3.90
50 52	9.86496 .86516	I.00	0.43806	3.75	50 52	9.87484 .87504	1.00	.47702	3.90
54	.86536	1.00	.43956	3.75	54	.87523	.95	.47781	3.95
56	.86556	1.00	. 44030	3.70	56	.87543	1.00	.47859	3.90
58	.86576	I.00 I.00	.44105	3.75	58	.87562	.95	.47938	3.95
60	9.86596	1.00	0.44180	3.75	60	9.87582	1	0.48016	3.95
62	.86616		. 44255	3.75	62	.87601	.95 1.00	. 48095	3.90
64	.86636	I.00 I.00	. 44330	3.75 3.75	64	.87621	1.00	.48173	3.95
66	.86656	.95	.44405	3.80	66	.87641	.95	.48252	3.95
68	.86675	1.00	.44481	3.75	68	.87660	1.00	0.48410	3.95
70 72	9.86695 .86715	1.00	0.44556 .44631	3.75	70 72	9.87680 .87699	.95	.48489	3.95
74	.86735	I.00	.44706	3.75	74	.87719	1.00	.48568	3.95
76	.86755	1.00	.44782	3.80	76	.87738	- 95	.48647	3.95
78	.86775	1.00	. 44857	3.75	78	.87758	1.00	.48727	4.00
80	9.86795	1.00	0.44933	3.80	80	9.87777	.95	0.48806	3.95
82	.86814	.95	. 45009	3.80	82	.87796	-95	. 48885	4.00
84	.86834	I.00	. 45084	3.75 3.80	84	.87716	.95	.48965	3.95
86	.86854	1.00	.45160	3.80	86	.87835	1.00	.49044	4.00
88	.86874	1.00	.45236	3.80	88	.87855	.95	.49124	4.00
90 92	9.86894 .86913	-95	0.45312	3.80	90 92	9.87874 .87894	1.00	.49284	4.00
	.86933	1.00	. 45388	3.80	1 -	.87913	.95	.49364	4.00
94 96	.86933	I.00	.45404	3.80	94 96	.87933	1.00	.49444	4.00
98	.86973	1.00	.45617	3.85	98	.87952	.95	.49525	4.05
100	9.86992	.95	0.45693	3.80	100	9.87971	.95	0.49604	3.95

		76	٥		Hun-	77°			
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
	- 0	.001	0.49604	001	-00	9.88933	001	0.53724	100.
00	9.87971	1.00		4.00			-95		4.25
02	.87991	.95	. 49684 . 49764	4.00	02 04	.889 52 .88971	.95	. 53809 . 53894	4.25
04 06	.88010 .88030	1.00	.49704	4.05	o ₄	.88990	.95	-53979	4.25
		.95	. 49925	4.00	08	.89009	.95	.54064	4.25
08	.88049 9.88068	.95	0.50006	4.05	10	9.89028	-95	0.54149	4.25
10	.88088	1.00	.50087	4.05	12	.89047	-95	.54234	4.25
	.88107	.95	.50167	4.00	14	.89066	.95	.54320	4.30
14 16	.88126	. 95	.50248	4.05	16	.89085	.95	.54405	4.25
18	.88146	1.00	. 50329	4.05	18	.89104	.95	.54491	4.30
20	9.88165	.95	0.50410	4.05	20	9.89123	.95	0.54576	4.25
	.88184	.95	.50491	4.05	22	.89142	.95	.54662	4.30
22	.88204	1.00	.50572	4.05	24	.89142	-95	.54748	4.30
24 26	.88223	.95	.50654	4.10	26	.89180	.95	.54834	4.30
28	.88242	.95	.50735	4.05	28	.89199	-95	.54920	4.30
30	9.88262	1.00	0.50817	4.10	30	9.89218	.95	0.55006	4.30
32	.88281	.95	.50898	4.05	32	.89237	.95	.55092	4.30
	.88300	.95	.50980	4.10	34	.89256	.95	.55179	4.35
34 36	.88320	1.00	.51061	4.05	36	.89275	.95	.55265	4.30
38	.88339	.95	.51143	4.10	38	.89294	.95	-55352	4.35
40	9.88358	.95	0.51225	4.10	40	9.89313	.95	0.55439	4.35
42	.88377	.95	.51307	4.10	42	.89332	.95	.55525	4.30
44	.88397	1.00	.51389	4.10	44	.89351	.95	.55612	4.35
46	.88416	.95	.51471	4.10	46	.89369	.90	. 55699	4.35
48	.88435	.95	.51553	4.10	48	.89388	.95	. 55786	4.35
50	9.88454	.95	0.51636	4.15	50	9.89407	.95	0.55874	4.40
52	.88474	.95	.51718	4.10	52	.89426	.95	. 55961	4.35 4.35
54	.88493	1	.51801	4.10	54	.89445	1	. 56048	4.40
56	.88512	.95 .95	.51883	4.15	56	.89464	· 95 · 95	.56136	4.40
58	.88531	.95	.51966	4.15	58	.89483	.95	. 56224	4.35
60	9.88550	1.00	0.52049	4.15	60	9.89502	.90	0.56311	4.40
62	.88570		.52132	1	62	.89520		. 56399	4.40
64	.88589	.95	.52215	4.15 4.15	64	.89539	. 95	. 56487	4.40
66	.88608	·95	.52298	4.15	66	.89558	·95	.56575	4.40
68	.88627	.95	.52381	4.15	68	.89577	-95	. 56663	4.45
70	9.88646	.95	0.52464	4.15	70	9.89596	.95	0.56752	4.40
72	.88665	1.00	. 52547	4.20	72	.89615	.90	. 56840	4.45
74	.88685	.95	. 52631	4.15	74	.89633	-95	. 56929	4.40
76 -0	.88704	.95	.52714	4.20	76	.89652	.95	.57017	4.45
78	.88723	.95	.52798	4.20	78	.89671	. 95	.57106	4.45
80	9.88742	.95	0.52882	4.20	80	9.89690	.95	0.57195	4.45
82	.88761	.95	. 52966	4.15	82	.89709	.90	.57284	4.45
84	.88780	.95	. 53049	4.20	84	.89727	-95	.57373	4.45
86	.88799	.95	.53133	4.25	86	.89746	.95	. 57462	4.45
88	.88818	1.00	. 53218	4.20	88	.89765	.95	.57551	4.50
90	9.88838	.95	0.53302 .53386	4.20	90 92	9.89784	.90	0.57641	4.45
92		.95		4.20	-		.95	.57730	4.50
94 06	.88876 .88895	.95	.53470	4.25	94 96	.89821	.95	.57820	4.50
96 98	.88914	.95	.53555	4.20	98	.89840	.95	.57910	4.45
100	9.88933	.95	0.53724	4.25	100	9.89877	.90	0.58089	4.50
100	1 9.00933	•	0.33724		. 100	· 9.09077	1	0.30009	

Hun-		7:	8°		Hun-		7	9°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.89877		0.58089	4.55	00	9.90805	.90	0.62745	
02	.89896	.95	.58180	4.50	02	.90823		. 62842	4.85
04	.89915	.95	. 58270	4.50	04	. 90842	.95	. 62938	4.80 4.80
06	.89933	.95	. 58360	4.55	06	. 90860	.95	. 63036	4.80
о8	.89952	.95	. 58451	4.50	o8	.90879	.90	.63132	4.85
10 12	9.89971 .89990	.95	0.58541	4.55	10 12	9.90897	.90	0.63229	4.85
1		.90		4.55			.95		4.85
14 16	.90008	.95	. 58723	4.55	14 16	.90934	.90	.63423	4.90
18	.90046	.95	.58905	4.55	18	.90970	. 90	.63618	4.85
20	9.90064	.90	0.58996	4.55	20	9.90989	-95	0.63716	4.90
22	.90083	.95	.59087	4.55	22	.91007	.90	.63814	4.90
24	.90102	.95	.59178	4.55	24	.91025	.90	.63912	4.90
26	.90120	.90	.59270	4.60	26	.91044	.95	.64010	4.90
28	.90139	- 95	. 59362	4.60	28	.91062	. 90	.64108	4.90
30	9.90157	.90	0.59453	4.55	30	9.91080	.90	0.64207	4.95
32	.90176	- 95 - 95	-59545	4.60	32	.91099	·95	.64305	4.90
34	.90195		. 59637	4.60	34	.91117	.90	. 64404	
36	.90213	.90	.59729	4.65	36	.91135	.90	.64503	4.95 4.95
38	.90232	.90	. 59822	4.60	38	.91153	.95	.64602	4.95
40	9.90250	.95	0.59914	4.65	40	9.91172	.90	0.64701	5.00
42	. 90269	. 95	.60007	4.60	42	.91190	.90	.64801	5.05
44	.90288	.90	.60099	4.65	44	.91218	.90	. 64900	5.00
46	.90306	.90	.60192	4.60	46	.91226	-95	. 65000	5.00
48	.90324	.95	.60284	4.70	48	.91245	.90	.65100	5.00
50 52	9.90343	.95	0.60378 .60471	4.65	50 52	9.91263	.90	0.65200	5.00
54	.90380	.90	.60564	4.65		.91201	.90	.65400	5.00
56 56	.90390	.95	.60658	4.70	54 56	.91299	. 90	.65500	5.00
58	.90417	.90	.60751	4.65	58	.91336	.95	.65601	5.05
60	9.90436	.95	0.60845	4.70	60	9.91354	.90	0.65702	5.05
62	.90455	.95	. 609.38	4.65	62	.91372	.90	.65802	5.00
64	.90473	. 90	.61032	4.70	64	.91390	.90	.65903	5.05
66	.90492	.95	.61126	4.70	66	.91408	.90	. 66005	5.05
68	.90510	. 90	.61221	4.75	68	.91427	.95	.66106	5.05
70	9.90529	·95	0.61315	4.70	70	9.91445	.90	0.66207	5.05 5.10
72	.90547	.90	.61409	4.75	72	.91463	.90	.66309	5.10
74	.90565	.95	.61504	4.75	74	.91481	.90	.66411	5.10
76 78	.90584	.90	.61599	4.70	76	.91499	.90	.66513	5.10
		.95	.61693	4.75	78	.91517	.95		5.10
80	9.90621	.90	0.61788	4.75	80	9.91536	.90	0.66717	5.15
82 84	.90639	.95	.61883	4.80	82	.91554	.90	.66820	5.10
86	.90658	.90	.61979	4.75	84 86	.91572	.90	.66922	5.15
88	.90695	.95	.62169	4.75	88	.91590	. 90	.67128	5.15
90	9.90713	.90	0.62265	4.80	90	9.91626	. 90	0.67231	5.15
92	.90731	.90	.62361	4.80	92	.91644	.90	.67335	5.20
94	.90750	.95	.62457	4.80	94	.91662	.90	.67438	5.15
96	.90768	.90	.62543	4.80	96	.91680	.90	.67542	5.20
98	.90787	·95	. 62649	4.80 4.80	98	.91698	.90 .90	.67646	5.20 5.15
100	9.90805	.90	0.62745	4.00	100	9.91716	. 90	0.67749	3.13

Hun-		8	0°		Hun-		8:	ı°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff. .001
- 00	9.91716		0.67749		00	9.92612		0.73179	
02	.91735	-95	.67854	5.25	02	. 92630	.90	.73292	5.65
04	.91753	.90 .90	.67958	5.20 5.20	04	. 92647	.85	. 73406	5.70 5.70
о6	.91771	.90	.68062	5.25	06	.92665	.90	.73520	5.70
о8	.91789	.90	.68167	5.25	08	. 92683	.90	. 73634	5.75
10	9.91807	.90	0.68272	5.25	10	9.92701	.85	0.73749	5.70
12	.91825	.90	.68377	5.25	12	.92718	.90	.73863	5.75
14	.91843	.90	.68482	5.25	14	.92736	.90	.73978	5.75
16 18	.91861	.90	.68587	5.30	16 18	.92754	.85	.74093	5.75
	.91879	.90		5.30	20	.92771	.90	.74208	5.80
20	9.91897	.90	0.68799	5.25		9.92789	.90	0.74324	5.80
22	.91915	.90	. 68904	5.30	22	.92807	.85	.74440	5.80
24 26	.91933	.90	.69010	5.35	24 26	.92824 9284 2	.90	.74556	5.85
		.90		5.30	28		.90		5.85
28	.91969 9.91987	.90	0.69330	5.35	30	.92860 9.92877	.85	.74788	5.85
30 32	.92005	.90	.69436	5.30	32	.92895	.90	.75022	5.85
-	.92023	.90	.69543	5.35	34	.92913	.90	.75139	5.85
34 36	.92023	.90	.69650	5.35	36	.92913	.85	.75256	5.85
38	.92059	.90	.69758	5.40	38	.92948	.90	.75373	5.85
40	9.92077	.90	0.69865	5.35	40	9.92966	.90	0.75491	5.90
42	.92095	.90	.69973	5.40	42	.92983	.85	.75609	5.90
44	.92093	.90	.70080	5.35	44	.93001	.90	.75727	5.90
46	.92130	.95	.70189	5 45	46	.93018	.85	.75846	5.95
48	.92148	.90	.70297	5.40	48	. 93036	.90	.75965	5.95
50	9.92166	.90	0.70405	5.40	50	9.93054	.90	0.76083	5.90
52	.92184	.90	.70514	5.45 5.45	52	.93071	.85	.76203	6.00 5.95
54	.92202		.70623		54	. 93089		.76322	6.00
56	.92220	.90	.70732	5.45 5.45	56	.93106	.85	.76442	5.95
58	.92238	.90	.70841	5.45	58	. 93124	.90	.76561	6.05
60	9.92256	.90	0.70950	5.50	60	9.93142	.85	0.76682	6.00
62	.92274	.85	.71060	5.45	62	.93159	.85	.76802	6.00
64	.92291	.90	.71169	5.50	64	. 93176	.90	.76922	6.05
66	.92309	.90	.71279	5.50	66	.93194	.90	.77043	6.10
68	. 92327	.90	.71389	5.55	68	.93212	.85	.77165	6.05
70	9.92345	.90	0.71500	5.50	70	9.93229	.90	0.77286	6.05
72	.92363	.90	.71610	5.55	72	.93247	.85	.77407	6.10
74 76	.92381	.85	.71721	5.55	74 76	.93264	.90	.77529	6.10
78	.92398 .92416	.90	.71943	5.55	78	.93282	.85	.77651	6.15
80	9.92434	.90	0.72054	5.55	80		.90	0.77896	6.10
82	.92452	.90	.72166	5.60	82	9.93317	.85	.78019	6.15
84	.92432	.90	.72278	5.60	84	·93334 ·93352	.90	.78142	6.15
86	.92487	.85	.72389	5 55	86	.93369	.85	.78265	6.15
88	.92505	.90	.72502	5.65	88	.93387	.90	. 78389	6.20
90	9.92523	.90	0.72614	5.60	90	9.93404	.85	0.78513	6.20
92	.92541	.90	.72726	5.60 5.65	92	.93422	.90	.78637	6.20
94	.92559	.90	. 72839		94	.93439		.78761	
96	.92576	.85	.72952	5.65 5.65	96	.93457	.90	. 78886	6.25 6.25
98	.92594	.90	. 73065	5.70	98	-93474	.90	.79011	6.25
100	9.92612		0.73179		100	9.93492		0.79136	

		8	2 °		Hun-		8	3°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
- 00	9.93492		0.79136		00	9.94356		0.85766	
02	.93509	.85	.79261	6.25 6.30	02	-94373	.85 .85	.85907	7.05
04	.93526	.85 .90	.79387	6.30	04	.94390	.85	.86048	7.05
06	-93544	.85	.79513	6.35	∘6	.94407	.85	.86190	7.10
08	.93561	.90	.79640	6.30	o8	.94424	.90	.86332	7.10
10	9.93579	.85	0.79766	6.35	10 12	9.94442	.85	0.86474 .86616	7.10
12	.93596	.90	.79893	6.35		94459	.85	.86759	7.15
14 16	.93614 .93631	.85	.80020	6.35	14 16	.94476 .94493	.85	.86903	7.20
18	.93648	.85	.80275	6.40	18	.94493	.85	.87046	7.15
20	9.93666	.90	0.80403	6.40	20	9.94527	.85	0.87190	7.20
	. 93683	.85	.80531	6.40	22	.94544	.85	.87335	7.25
22 24	.93003	.85	.80659	6.40	24	.94544	.85	.87470	7.25
26	.93718	.90	.80788	6.45	26	.94578	.85	.87625	7.25
28	93735	.85	.80917	6.45	28	.94595	.85	.87770	7.25
30	9.93752	.85	0.81046	6.45	30	9.94612	.85	0.87916	7.30
32	.93770	.90	.81176	6.50	32	.94629	.85 .85	.88062	7.30
34	.93787	.85	.81306	6.50	34	.94646	_	.88209	7.35
36	.93804	.85	.81436	6.50	36	.94663	.85 .85	.88356	7.35
38	.93822	.90 .85	.81567	6.55 6.50	38	.94680	.85	.88504	7.40
40	9.93839	.85	0.81697	6.60	40	9.94697	.85	0.88651	7.45
42	. 93856	_	.81829		42	.94714	.85	.88800	7.40
44	. 93874	.90 .85	.81960	6.55	44	.94731	.85	.88948	7.45
46	. 93891	.85	.82092	6.60	46	.94748	.85	.89097	7.50
48	. 93908	.90	.82224	6.60	48	.94765	.85	.89247	7.50
50	9.93926	.85	0.82356	6.60	50	9.94782	.85	0.89397	7.50
52	-93943	.85	.82488	6.65	52	.94799	.85	.89547	7.50
54	. 93960	.85	.82621	6.70	54	.94816	.85	.89697 .89848	7.55
56 58	.93977	.90	.82755 .82888	6.65	56 58	.94833 .94850	.85	.00000	7.60
60	93995	.85	0.83022	6.70	60	9.94867	.85	0.90152	7.60
	9.94012	.85		6.70			.85		7.60
62 64	.94029	.90	.83156	6.70	62 64	.94884 .94901	.85	.90304	7.65
66	.94047	.85	.83425	6.75	66	.94901	.85	.90437	7.65
68	.94004	.85	.83560	6.75	68	94935	.85	.90764	7.70
70	9.94098	.85	0.83696	6.80	70	9.94952	.85	0.90918	7.70
72	.94115	.85	.83831	6.85	72	.94969	.85	.91072	7.70
74	.94133	.90	.83968	6.85	74	.94986	.85	.91227	7.75
76	.94150	.85	.84104	6.80	76	.95003	.85	.91383	7.80
78	.94167	.85	.84241	6.85	78	.95020	.85	.91538	7.75
80	9.94184	.85 .85	0.84378	6.85	80	9.95037	.80	0.91694	7.85
82	.94201		.84515		82	.95053		.91851	7.85
84	.94219	.90	.84653	6.90	84	.95070	.85	.92008	7.90
86	.94236	.85	.84791	6.90	86	.95087	.85	.92166	7.90
88	.94253	.85	.84929	6.95	88	.95104	.85	.92324	7.90
90	9.94270	.85	0.85068	6.95	90	9.95121	.85	0.92482	7.95
92	.94287	.85	.85207	6.95	92	.95138	.85	.92641	8.00
94	.94304	.90	.85346	7.00	94	.95155	.80	.92801	8.00
96 98	.94322	.85	.85486	7.00	96 98	.95171 .95188	.85	.92961	8.00
100		.85		7.00	100		.85	0.93282	8.05
100	9.94356		0.85766		100	9.95205	1	0.93262	

**		84	0		Hun-		85	0	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
		.001		100.			.001		100.
00	9.95205	.85	0.93282	8.05	00	9.96040	.80	1.02010	9.50
02	.95222	.85	-93443	8.10	02	.96056	.85	.02200	9.55
-04 -06	.95239	.85	.93605 .93767	8.10	04 06	.96073 .96089	.80	.02391	9.60
08	.95256	.80	.93930	8.15	08	.96106	.85	.02775	9.60
10	.95272 9.95289	.85	0.94093	8.15	10	9.96122	.80	1.02968	9.65
12	.95306	.85	.94257	8.20 8.20	12	.96139	.85 .80	.03162	9.70 9.70
14	.95323	.85	.94421		14	.96155		.03356	
16	.95340	.85 .80	.94586	8.25 8.25	16	.96172	.85 .80	.03551	9.75 9.80
18	.95356	.85	.94751	8.30	18	.96188	.85	.03747	9.85
20	9.95373	.85	0.94917	8.30	20	9_96205	.80	1.03944	9.85
22	.95390	.85	.95183	8.35	22	.96221	.85	.04141	9.90
24	.95407	.85	.95250	8.35	24 26	.96238	.80	.04339	9.95
26	.95424	.80	.95417	8.40		.96254	.85	.04538	10.00
28	.95440	.85	.95585	8.45	28 30	.96271 9.96287	.80	.04738 1.04938	10.00
30 32	9.95457 .95474	.85	.95922	8.40	32	.96304	.85	.05140	10.10
-	.95491	.85	.95922	8.50	34	.96320	.80	.05342	10.10
34 36	.95507	.80	.96262	8.50	3 4 36	.96337	.85	.05544	10.10
38	.95524	.85	.96432	8.50	38	.96353	.80	.05748	10.20
40	9.95541	.85	0.96603	8.55	40	9.96369	.85	1.05953	10.25
42	-95557	.80	.96775		42	.96386	1 "	.06158	
44	.95574	.85	.96947	8.60 8.65	44	. 96402	.8o .85	.06364	10.30
46	.95591	.85 .85	.97120	8.65	46	.96419	.80	.06571	10.35
48	.95608	.80	.97293	8.70	48	.96435	.80	.06779	10.40
50	9.95624	.85	0.97467	8.70	50	9.96451	.85	1.06987	10.50
52	.95641	.85	.97641	8.75	52	.96468	.80	.07197	10.50
54	.95658	.80	.97816	8.80	54	.96484	.85	.07407	10.55
56 58	.95674 .95691	.85	.97992	8.80	56 58	.96517	.80	.07830	10.60
60	9.95708	.85	0.98345	8.85	60	9.96533	.80	1.08043	10.65
62		.80	.98522	8.85	62	.96550	.85	.08257	10.70
64	.95724 .95741	.85	.98700	8.90	64	.96566	.80	.08472	10.75
66	.95758	.85	.98879	8.95	66	.96582	.80	.08687	10.75
68	.95774	.80	.99058	8.95	68	.96599	.85	.08904	10.85
70	9.95791	.85	0.99237	8.95	70	9.96615	.80	1.09121	10.85
72	.95807	.80	.99418	9.05	72	.96632	.80	.09340	10.95
74	.95824	.85	.99599	9.05	74	.96648	.80	.09559	11.00
76	.95841	.80	.99780	9.03	76	.96664 .96680	.80	.10000	11.05
78	.95857	.85	.99963	9.15	78		85]	11.15
80	9.95874	.85	1.00146	9.15	80	9.96697	.80	1.10223	11.15
82	.95891	.80	.00329	9.20	82 84	.96713	.80	.10446	11.25
84 86	.95907	.85	.00513	9.25	86	.96729	.85	.10896	11.25
88	.95940	.80	.00883	9.25	88	.96762	.80	.11122	11.30
90	9.95957	.85	1.01069	9.30	90	9.96778	.80	1.11349	11.35
92	.95973	.80	.01256	9.35	92	.96795	.85	.11578	II.45 II.45
94	.95990	.85	.01444	9.40	94	.96811	1	.11807	
96	.96007	.85	.01633	9.45	96	.96827	.80	.12038	11.55
98	. 96023	85	.01821	9.45	98	.96843	85	.12269	- 11.60
100	9.96040		1.02010	3.43	100	9.96860	1	1.12501	1

Hun-		86	ő°		Hun-		8	37°	
dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.96860	.80	1.12501	11.70	00	9.97665	.8c	1.25785	
02	.96876		.12735		02	.97681		. 26092	15.35
0.4	.96892	.80 .80	. 12969	11.70	0.1	.97697	.80	.26400	13.40
06	. 96908	.85	.13205	11.85	06	.97713	.80	.26710	15.50
08	.96925	.80	.13442		08	.97729	.80	.27022	
10	9.96941	.80	1.13680	11.90	10	9.97745	.80	1.27336	15.70
12	.96957	.So	.13010	12.05	12	.97761	.80	. 27652	15.95
14	.96973	.85	.14160	12.05	14	.97777	.80	. 27971	16.00
16	.96990	.80	.14401	12.15	16	-97793	.80	. 28291	16.15
18	.97006	.80	11011	12.20	18	.97809	.80	. 28614	16.25
20	9.97022	.80	1.14888	12.25	20	9.97825	.80	1.28939	16.35
22	.97038	.80	.15133	12.30	22	.97841	.80	. 29266	16.45
24	.97054	.85	.15379	12.35	24	.97857	.80	- 29595	16.55
26	.97071	.80	.15626	12.45	26	.97873	.80	. 29926	16.70
28	.97087	.80	.15875	12.50	28	.97889	.75	. 30260	16.80
30	9.97103	.80	1.16125	12.55	30	9.97904	.80	1.30596	16.95
32	.97119	.80	.16376	12.65	32	.97920	.80	.30935	17.05
34	.97135	.80	. 16883	12.70	34 36	.97936	.80	.31276	17.15
36 38	.97151	.85	.17138	12.75	38	.97952 .97968	.80	.31019	17.30
40		.80		12.80	40		.80		17.45
	9.97184	.80	1.17394	12.90		9.97984	.80	1.32314	17.55
42	.97200	.80	.17652	12.90	42	.98000	.So	.32665	17.65
44 46	.97216	.80	.17910	13.10	44 46	.98016 .98031	.75	.33018	17.85
		.80		13.10	48		.80	-33375	17.90
48 50	.97248 9.97264	.80	1.18697	13.15	50	.98047 9.98063	.80	.33733 I.34095	18.10
52	.97280	.80	.18961	13.20	52	. 98079	.80	.34460	18.25
54	.97297	.85	. 19228	13.35	54	.98095	.80	.34827	18.35
56	.97313	.80	.19495	13.35	56	.98111	.80	.35197	18.50
58	.97329	.80	.19764	13.45	58	.98126	- 75	.35570	18.65
60	9.97345	.80	I.20035	13.55	60	9.98142	.80	1.35946	18.80
62	.97361	.80	.20307	13.60	62	.98158	.80	.36325	18.95
64	.97377	.80	.20580	13.65	64	.98174	.80	.36707	19.10
66	.97393	.80	. 20855	13.75	66	.98190	.80	.37092	19.25
68	.97409	.80	.21132	13.85	68	.98205	-75	.37481	19.45
70	9.97425	.80	1.21410	13.90	70	9.98221	.80	1.37872	19.55
72	.97441	.80 .80	.21690	14.00	72	.98237	.80	.38267	19.75
74	-97457		.21971	14.05	74	.98253		. 38665	19.90
76	-97473	.80	. 22254	14.15	76	. 98268	-75 .80	. 39067	20.10
78	.97489	.80	. 22539	14.25	78	.98284	.80	.39472	20.45
80	9.97505	.80	1.22825		80	9.98300	.80	1.39881	20.60
82	.97521		.23113	14.40	82	.98316		.40293	20.80
84	.97537	.80	. 23403	14.50	84	.98331	. 75 . 80	.40709	20.80
86	-97553	.80	.23695	14.65	86	.98347	.80	.41128	21.20
88	.97569	.80	. 23988	14.75	88	.98363	.80	.41552	21.35
90	9.97585	.80	I.24283	14.75	90	9.98379	.75	1.41979	21.35
92	.97601	.80	. 24580	14.90	92	.98394	.80	.42410	21.75
94	.97617	.80	.24878	14.95	94	.98410	.80	.42845	21.95
96 98	.97633	.80	.25179	15.10	96	.98426	.80	.43284	22.20
,	.97649	.80	. 25481	15.20	98	.98442	.75	.43728	22.35
100	9.97665		1.25785		100	9.98457		1.44175	

		88	3°		Hun-		89)°	
Hun- dredths	Vers	Diff.	Exsec	Diff.	dredths	Vers	Diff.	Exsec	Diff.
00	9.98457	.80	1.44175	22.60	00	9.99235	.80	1.75050	44.65
02	.98473	.80	. 44627	22.85	02	.99251	.75	-75943	45.50
04	.98489	.75	. 45084	23.05	04	.99266	.80	.76853	46.50
06	.98504	.80	45545	23.25	06	.99282	.75	.77783	47.45
08	.98520	.80	.46010	23.55	08	.99297	.75	.78732	48.50
10 12	9.98536 .98551	. 75	1.46481 .46956	23.75	10 12	9.99312	.80	1.79702 .80694	49.60
	.98567	.80	.47436	24.00	14	.99343	.75	.81707	50.65
14 16	.98583	.80	.47430	24.25	16	.99343	.80	.82744	51.85
18	.98598	.75	.48411	24.50	18	.99374	.75	.83806	53.10
20	9.98614	.80	1.48906	24.75	20	9.99389	-75	1.84894	54.40
22	.98630	.80	.49407	25.05	22	.99405	.80	.86009	55.75
24	.98645	- 75	.49913	25.30	24	.99420	.75	.87152	57.15
26	.98661	.80	.50425	25.60 25.85	26	.99435	.75 .80	.88326	58.70 60.15
28	. 98676	.75	. 50942		28	.99451		.89531	1
30	9.98692	.8o .8o	1.51466	26.20 26.45	30	9.99466	.75 .75	1.90770	61.95 63.70
32	.98708	.75	.51995	26.80	32	.99481	.80	.92044	65.60
34	.98723	.80	. 52531	27.10	34	.99497	.75	.93356	67.55
36	.98739	.80	. 53073	27.40	36	.99512	.75	.94707	69.70
38	. 98755	.75	. 53621	27.75	38	.99527	.80	.96101	72.00
40	9.98770	.80	1.54176	28.10	40	9.99543	-75	1.97541	74.35
42	. 98786	.75	. 54738	28.40	42	.99558	.75	.99028	77.00
44	.98801	.80	.55306	28.80	44	.99573	.80	2.00568	79.70
46	.98817	.75	.55882	29.15	46	.99589	.75	.02162	82.75
48	.98832 9.98848	.80	.56465 1.57056	29.55	48 50	.99 6 04 9.99619	.75	.03817	85.90
50 52	.98864	.80	.57654	29.90	52	.99635	.80	.07323	89.40
54	.98879	.75	.58261	30.35	54	.99650	- 75	.09187	93.20
56	.98895	.80	.58875	30.70	56	.99665	.75	.11133	97.30
58	.98910	.75 .80	. 59498	31.15	58	.99680	.75 .80	.13168	101.75
60	9.98926		1.60130	1 -	60	9.99696		2.15302	
62	.98941	.75	.60770	32.00	62	.99711	.75	.17545	112.15
64	.98957	.80	.61419	32.45	64	.99726	.75 .80	.19909	118.20
6 6	.98972	.80	.62078	32.95 33.45	66	.99742	.75	.22406	132.40
68	.98988	.75	.62747	33.90	68	-99757	.75	.25054	140.90
70	9.99003	.80	1.63425	34.45	70	9.99772	.75	2.27872	150.60
72	.99019	-75	.64114	34.95	72	.99787	.75	.30884	161.70
74	.99034	.80	.64813	35.50	74	.99802	.80	.34118	174.55
76 78	.99050	.75	.65523	36.10	76 78	.99818	.75	.37609	189.70
80	9.99081	.80	1.66978	36.65	80	9.99848	-75		207.70
82		.75		37.25	82		.75	2.45557	229.55
84	.99096	.80	.67723	37.90	84	.99863	.80	.50148	256.55
86	.99112	-75	.69252	38.55	86	.99894	.75	.61093	290.70
88	.99143	.80	.70036	39.20	88	.99909	-75	.67803	335.50
90	9.99158	.75	1.70834	39.90	90	9.99924	.75	2.75736	396.65
92	.99174	.80	.71646	40.60	92	.99939	·75	.85443	485.45 625.45
94	.99189	.75	.72473	42.15	94	.99954	.80	.97952	881.20
96	.99204	.80	.73316	42.15	96	.99970	.75	3.15576	1505.90
98	.99220	.75	.74174	43.80	98	. 99985	.75	. 45694	
100	9.99235	1	1.75050		100	0.00000	1	∞	1

TABLE XXVII. — Natural Sines, Tangents, Cotangents and Cosines

Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
0.0	0.0000		0.0000	17	inf.		1.0000	0	90.0	
1	0.0017	17	0.0017	18	572.9572		1.0000	0	9	
2	0.0035	17	0.0035	17	286.4777		1.0000	0	8	
3	0.0052	18	0.0052	18	190.9842		1.0000	0	7	
4	0.0070	17	0.0070	17	143.2371		1,0000	0	6	
5 6	0.0087	18	0.0087	18	95.4895		0.9999	1	5 4	
	0.0122	17	0.0122	17	81.8470			0		
7	0.0122	18	0.0122	18	71.6151		0.9999	0	3 2	
9	0.0157	17	0.0157	17	63.6567		0.9999	0	ī	
1.0	0.0175	18	0.0175	18	57.2900		0.9998	I	89.0	
1	0.0192	17	0.0192	17	52.0807		0.9998	0	9	
2	0.0209	17	0.0209	17	47.7395		0.9998	0	8	18
3	0.0227	18 17	0.0227	18 17	44.0661		0.9997	I 0	7	1 1.8
4	0.0244	18	0.0244	18	40.9174		0.9997	0	6	2 3.6 3 5.4
5	0.0262	17	0.0262	17	38.1885		0.9997	I	5	3 3.4
6	0.0279	18	0.0279	18	35.8006		0.9996	0	4	5 9.0
7	0.0297	17	0.0297	17	33.6935		0.9996	1	3	6 10.8
8 9	0.0314	18	0.0314	18	31.8205		0.9995	0	2 I	7 12.6
2.0	0.0332	17	0.0332	17	28.6363		0.9994	1	88.0	8 14.4 9 16.2
		17		18				I	9	9 10.2
I 2	0.0366	18	0.0367	17	27.2715 26.0307		0.9993	0	8	
3	0.0401	17	0.0402	18	24.8978		0.9992	I	7	
4	0.0419	18	0.0419	17	23.8593		0.9991	I	6	
5	0.0436	17 18	0.0437	18 17	22.9038	9555 8821	0.9990	I 0	5	
6	0.0454	17	0.0454	18	22.0217	8168	0.9990	I	4	
7	0.0471	17	0.0472	17	21.2049	7584	0.9989	I	3	
8	0.0488	18	0.0489	18	20.4465	7062	0.9988	ī	2	
9	0.0506	17	0.0507	17	19.7403	6592	0.9987	I	I	
3.0	0.0523	18	0.0524	18	19.0811	6166	0.9986	I	87.0	17
1	0.0541	17	0.0542	17	18.4645	5782	0.9985	I	9	I I.7 2 3.4
2	0.0558	18	0.0559	18	17.8863	5431	0.9984	1	8 7	2 3.4 3 5.1
3	0.0576	17	0.0577	17	17.3432	5113		I	6	4 6.8
4 5	0.0593	17	0.0594	18	16.8319 16.3499	4820	0.9982	1	5	5 8.5
6	0.0628	18	0.0629	17	15.8945	4554	0.9980	1	4	6 10.2
7	0.0645	17	0.0617	18	15.4638	4307	0.9979	I	3	7 11.9 8 13.6
8	0.0663	18	0.0664	17 18	15.0557	4081 3872	0.9978	I	2	9 15.3
9	0.0680	17 18	0.0682	17	14.6685	3678	0.9977	I	1	5 , =5.5
4.0	0.0698	17	0.0699	18	14.3007	3500	0.9976	2	86.0	
1	0.0715	17	0.0717	17	13.9507	3333	0.9974	I	9	
2	0.0732	18	0.0734	18	13.6174	3178	0.9973	I	8	
3	0.0750	17	0.0752	17	13.2996	3034	0.9972	I	7	
4	0.0767	18	0.0769	18	12.9962	2900	0.9971	2	6	
5 6	0.0785	17	0.0787	18	12.7062 12.4288	2774	0.9969	I	5	
		17		17		2656	*	2	4	
7 8	0.0819	18	0.0822	18	12.1632	2545	0.9966 0.9965	1	3 2	
9	0.0854	17	0.0857	17	11.6645	2442	0.9963	2	ī	
5.0	0.0872	18	0.0875	18	11.4301	2344	0.9962	I	85.0	
- <u></u>		d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	
	Cosin	d.	Cotan	d.	Tan	ı d.	Sin	d.	Deg.	

Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P	. P.
5.0	0.0872		0.0875		11.4301		0.9962	-	85.0		
1	0.0889	17	0.0892	17	11.2048	2253	0.9960	2	9		
2	0.0906	17	0.0910	18	10.9882	2166 2085	0.9959	I 2	8		
3	0.0924	18 17	0.0928	18 17	10.7797	2008	0.9957	1	7		
4	0.0941	17	0.0945	18	10.5789	1935	0.9956	2	6		
5	0.0958	18	0.0963	18	10.3854	1866	0.9954	2	5		
6	0.0976	17	0.0981	17	10.1988	1801	0.9952	1	4		
7	0.0993	18	0.0998	18	10.0187	1739	0.9951	2	3		
8	0.1011	17	0.1016	17	9.8448 9.6768	1680	0.9949	2	2 I		
9	0.1028	17	0.1033	18		1624		2	84.0		
6.0	0.1045	18	0.1051	18	9.5144	1572	0.9945	2			18
1	0.1063	17	0.1069	17	9.3572 9.2052	1520	0.9943	1	9 8	I	1.8
2	0.1080	17	0.1086	18	9.0579	1473	0.9942	2	7	2	3.6
3	0.1097	18	0.1122	18	8.9152	1427	0.9938	2	6	3	5.4
4 5	0.1113	17	0.1122	17	8.7769	1383	0.9936	2	5	4	7.2
6	0.1149	17	0.1157	18 18	8.6427	1342	0.9934	2 2	4	5 6	9.0
7	0.1167	18	0.1175		8.5126	1301	0.9932		3	7	10.8
8	0.1184	17 17	0.1192	17	8.3863	1263 1227	0.9930	2 2	2	8	14.4
9	0.1201	18	0.1210	18	8.2636	1193	0.9928	3	1	9	16.2
7.0	0.1219	17	0.1228	18	8.1443	1158	0.9925	2	83.0		
1	0.1236	17	0.1246	17	8.0285	1127	0.9923	2	9		
2	0.1253	18	0.1263	18	7.9158	1096	0.9921	2	8		
3	0.1271	17	0.1281	18	7.8062	1066	0.9919	2	7		
4	0.1288	17	0.1299	18	7.6996	1038	0.9917	3	6		
5	0.1305	18	0.1317	17	7 5958	1011	0.9914	2	5		
6	0.1323	17	0.1334	18	7 4947	985	0.9912	2	4		
7 8	0.1340 0.1357	17	0.1352 0.1370	18	7.3962 7.3002	960	0.9910	3	3 2		
9	0.1374	17	0.1370	18	7.2066	936	0.9907	2	1		
8.0	0.1392	18	0.1405	17	7.1154	912	0.9903	2	82.0		17
1	0.1409	17	0.1423	18	7.0264	890	0.9900	3	9	1	1.7
2	0.1409	17	0.1423	18	6.9395	869	0.9898	2	8	2	3.4
3	0.1444	18	0.1459	18 18	6.8548	847 828	0.9895	3	7	3	5.1
4	0.1461	17	0.1477	}	6.7720	l	0.9893	2	6	4	6.8
5	0.1478	17 17	0.1495	18 17	6.6912	808 790	0.9890	3 2	5	5	8.5
6	0.1495	18	0.1512	18	6.6122	772	0.9888	3	4	7	11.9
7	0.1513	17	0.1530	18	6.5350	754	0.9885	3	3	8	13.6
8	0.1530	17	0.1548	18	6.4596	737	0.9882	2	2	9	15.3
9	0.1547	17	0.1566	18	6.3859	721	0.9880	3	1	l	
9.0	0.1564	18	0.1584	18	6.3138	706	0.9877	3	81.0	Ì	
1	0.1582	17	0.1602	18	6.2432	690	0.9874	3	9 8		
2	0.1599	17	0.1620 0.1638	18	6.1742	676	0.9871	2	7		
3	0.1633	17	0.1655	17	6.0405	661	0.9866	3	6		
4 5	0.1650	17	0.1655	18	5.9758	647	0.9863	3	5	l	
6	0.1668	18	0.1691	18	5.9124	634	0.9860	3	4	l	
7	0.1685	17	0.1709		5.8502	622	0.9857	3	3		
8	0.1702	17	0.1727	18	5.7894	608 597	0.9854	3	2		
9	0.1719	17	0.1745	18	5.7297	584	0.9851	3	I		
10.0	0.1736		0.1763		5.6713	J-4	0.9848		80.0	<u> </u>	
	Cosin	đ.	Cotan	d.	Tan	d.	Sin	d.	Deg.		

Deg.	Sin	d.	Tan	d.	Cotan	đ.	Cosin	đ.		P. P.
10.0	0.1736		0.1763		5.6713		0.9848	_	80.0	
1	0.1754	18	0.1781	18	5.6140	573	0.9845	3	9	
2	0.1771	17	0.1799	18 18	5.5578	562	0.9842	3	8	
3	0.1788	17 17	0.1817	18	5.5026	552 540	0.9839	3	7	
4	0.1805	17	0.1835	18	5.4486	531	0.9836	3	6	
5	0.1822	18	0.1853	18	5 - 3955	520	0.9833	4	5	1 10
6	0.1840	17	0.1871	19	5 - 3435	511	0.9829	3	4	1 1.9
7	0.1857	17	0.1890	18	5.2924	502	0.9826	3	3	2 3.8
8	0.1874	17	0.1908	18	5.2422	493	0.9823	3	2 I	3 5.7
9	0.1891	17	0.1926	18	5.1929	483		4	79.0	4 7.6
11.0	0.1908	17	0.1944	18	5.1446	476	0.9816	3		5 9.5
I	0.1925	17	0.1962	18	5.0970	466	0.9813	3	9	6 11.4
2	0.1942	17	0.1980 0.1998	18	5.0504 5.0045	459	0.9810	4	7	7 13.3 8 15.2
3	0.1959	18		18		451		3	6	9 17.1
4	0.1977 0.1994	17	0.2016	19	4.9594 4.9152	442	0.9803	4	5	7, -,
5 6	0.1994	17	0.2053	18	4.8716	436	0.9796	3	4	
7	0.2028	17	0.2071	18	4.8288	428	0.9792	4	3	
8	0.2026	17	0.2071	18	4.7867	421	0.9792	3	2	
9	0.2062	17	0.2107	18	4.7453	414	0.9785	4	1	
12.0	0.2079	17	0.2126	19	4.7046	407	0.9781	4	78.0	
1	0.2096	17	0.2144	18	4.6646	400	0.9778	3	9	18
2	0.2113	17	0.2144	18	4.6252	394	0.9774	4	8	1 1.8
3	0.2130	17	0.2180	18	4.5864	388	0.9770	4	7	2 3.6
4	0.2147	17	0.2199	19	4.5483	381	0.9767	3	6	3 5.4
5	0.2164	17	0.2217	18	4.5107	376	0.9763	4	5	4 7.2
ŏ l	0.2181	17	0.2235	18	4.4737	370	0.9759	4	4	5 9.0
7	0.2198	17	0.2254	19	4.4373	364	0.9755	4	3	6 10.8
8	0.2215	17	0.2272	18	4.4015	358	0.9751	4	2	7 12.6 8 14.4
9	0.2233	18	0.2290	18	4.3662	353	0.9748	3	1	9 16.2
13.0	0.2250	17	0.2309	19	4.3315	347	0.9744	4	77.0	
1	0.2267	17	0.2327	18	4.2972	343	0.9740	4	9	
2	0.2284	17	0.2345	18	4.2635	337	0.9736	4	8	
3	0.2300	16	0.2364	19 18	4.2303	332	0.9732	4	7	
4	0.2317	17	0.2382		4.1976	327	0.9728	4	6	
5	0.2334	17	0.2401	19	4.1653	323 318	0.9724	4	5	
6	0.2351	17	0.2419	19	4.1335	313	0.9720	5	4	17
7	0.2368	17	0.2438	18	4.1022	309	0.9715	4	3	1 1.7
8	0.2385	17	0.2456	19	4.0713	305	0.9711	4	2	2 3.4
9	0.2402	17	0.2475	18	4.0408	300	0.9707	4	1	3 . 5.1
14.0	0.2419	17	0.2493	19	4.0108	296	0.9703	4	76.0	4 6.8 5 8.5
1	0.2436	17	0.2512	18	3.9812	292	0.9699	5	9	6 10.2
2	0.2453	17	0.2530	19	3.9520	288	0.9694	4	8	7 11.9
3	0.2470	17	0.2549	19	3.9232	285	0.9690	4	7	8 13.6
4	0.2487	17	0.2568	18	3.8947	280	0.9686	5	6	9 15.3
5 6	0.2504	17	0.2586	19	3.8667	276	0.9681	4	5	
1 1	0.2521	17	0.2605	18	3.8391	273		4	4	
7 8	0.2538	16	0.2623	19	3.8118	270	0.9673	5	3 2	
9	0.2554 0.2571	17	0.2661	19	3.7848 3.7583	265	0.9664	4	1	
15.0	0.2588	17	0.2679	18	3.7321	262	0.9659	5	75.0	
	Cosin	d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

TABLE XXVII. - (Continued)

Deg.	Sin	đ.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
		u.		<u>u.</u>		a.		a.		P. P.
15.0	0.2588	17	0.2679	19	3.7321	259	0.9659	4	75.0	
I	0.2605	17	0.2698	19	3.7062	256	0.9655	5	9 8	
3	0.2639	17	0.2717	19	3.6806 3.6554	252	0.9650 0.9646	4	7	
		17		18		249		5		19
4	0.2656	16	0.2754	19	3.6305 3.6059	246	0.9641	5	6	I I.9
5 6	0.2689	17	0.2792	19	3.5816	243	0.9632	4	5 4	2 3.8
	0.2706	17	0.2811	19		240	0.9627	5		3 5.7
7 8	0.2723	17	0.2830	19	3.5576 3.5339	237	0.9622	5	3	4 7.6 5 9.5
9	0.2740	17	0.2849	19	3.5105	234	0.9617	5	1	5 9.5 6 11.4
16.0	0.2756	16	0.2867	18	3.4874	231	0.9613	4	74.0	7 13.3
		17		19		228		5		8 15.2
I	0.2773	17	0.2886	19	3.4646	226	0.9608	5	9	9 17.1
3	0.2807	17	0.2905	19	3.4420 3.4197	223	o.9603 o.9598	5	7	
		16		19		220		5	6	
4 5	0.2823	17	0.2943	19	3.3977 3.3759	218	0.9593	5	5	
6	0.2857	17	0.2981	19	3.3544	215	0.9583	5	4	18 1 1.8
	0.2874	17	0.3000	19	-	212	0.9578	5		I I.8 2 3.6
7 8	0.2890	16	0.3000	19	3.3332 3.3122	210	0.9573	5	3 2	3 5.4
9	0.2907	17	0.3038	19	3.2914	208	0.9568	5	1	4 7.2
17.0	0.2924	17		19	3.2709	205	0.9563	5	73.0	5 9.0
		16	0.3057	19		203		5		6 10.8
1	0.2940	17	0.3076	20	3.2506	201	0.9558	5	9	7 12.6
3	0.2957	17	0.3096 0.3115	19	3.2305 3.2106	199	0.9553	5	7	8 14.4
		16	. 1	19	1	196		6	6	9 16.2
4	0.2990	17	0.3134	19	3.1910 3.1716	194	0.9542	5	5	
5 6	0.3024	17	0.3133	19	3.1524	192	0.9532	5	4	
	0.3040	16		19		190	0.9527	5		17
7 8	0.3040	17	0.3191	20	3.1334 3.1146	188	0.9521	6	3 2	1 1.7
9	0.3074	17	0.3230	19	3.0961	185	0.9516	5	ī	2 3.4
18.0	0.3090	16	0.3249	19	3.0777	184	0.9511	5	72.0	3 5.1
1		17		20		182		6		4 6.8
1 2	0.3107	16	0.3269 0.3288	19	3.0595	180	0.9505	5	9	5 8.5
3	0.3123	17	0.3200	19	3.0237	178	0.9494	6	7	6 10.2
- 1	0.3156	16		20	3.0061	176	0.9489	5	6	7 II.9 8 I3.6
4 5	0.3130	17	0.3327 0.3346	19	2.9887	174	0.9483	6	5	9 15.3
6	0.3173	17	0.3340	19	2.9714	173	0.9478	5	4	7 -3.3
7	0.3206	16	0.3385	20	2.9544	170	0.9472	6	3	
8	0.3223	17	0.3303	19	2.9375	169	0.94/2	6	3 2	
9	0.3239	16	0.3424	20	2.9208	167	0.9461	5	ī	16
19.0	0.3256	17	0.3443	19	2.9042	166	0.9455	6	71.0	1 1.6
1	0.3272	16	0.3463	20	2.8878	164	0.9449	6	9	2 3.2
2	0.3272	17	0.3403	19	2.8716	162	0.9444	5	8	3 4.8
3	0.3305	16	0.3502	20	2.8556	160	0.9438	6	7	5 8.0
4	0.3322	17	0.3522	20	2.8397	159	0.9432	6	6	6 9.6
5	0.3338	16	0.3541	19	2.8239	158	0.9432	6	5	7 11.2
6	0.3355	17	0.3561	20	2.8083	156	0.9421	5	4	8 12.8
7	0.3371	16	0.3581	20	2.7929	154	0.9415	6	3	9 14.4
8	0.3387	16	0.3600	19	2.7776	153	0.9409	6	2	
9	0.3404	17	0.3620	20	2.7625	151	0.9403	6	1	
20.0	0.3420	16	0.3640	20	2.7475	150	0.9397	6	70.0	
	Cosin	d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
20.0	0.3420	17	0.3640	19	2.7475	149	0.9397	6	70.0	
I	0.3437	16	0.3659	-	2.7326		0.9391	6	9	
2	0.3453	16	0.3679	20 20	2.7179	147 145	0.9385	6	8	
3	0.3469	17	0.3699	20	2.7034	145	0.9379	6	7	. 22
4	0.3486	16	0.3719	20	2.6889		0.9373	6	6	I 2.2
5	0.3502	16	0.3739	20	2.6746	143 141	0.9367	6	5	2 4.4
6	0.3518	17	0.3759	20	2.6605	141	0.9361	7	4	3 6.6
7	0.3535	16	0.3779	20	2.6464	139	0.9354	6	3	4 8.8
8	0.3551	16	0.3799	20	2.6325	138	0.9348	6	2	5 11.0
9	0.3567	17	0.3819	20	2.6187	136	0.9342	6	1	6 13.2
21.0	0.3584	16	0.3839	20	2.6051	135	0.9336	6	69.0	7 15.4
1	0.3600	16	0.3859		2.5916		0.9330		9	8 17.6 9 19.8
2	0.3616	17	0.3879	20 20	2.5782	I34 I33	0.9323	7	8	9 19.8
3	0.3633	16	0.3899	20	2.5649	132	0.9317	6	7	
4	0.3649	16	0.3919	20	2.5517		0.9311		6	
5	0.3665	16	0.3939	20	2.5386	13I 129	0.9304	7	5	. 21
6	0.3681	16	0.3959	20	2.5257	128	0.9298	7	4	I 2.I
7	0.3697	17	0.3979	21	2.5129	127	0.9291	6	3	2 4.2
8	0.3714	16	0.4000	20	2.5002	127	0.9285	7	2	3 6.3
9	0.3730	16	0.4020	20	2.4876	125	0.9278	6	1	4 8.4
22.0	0.3746	16	0.4040	21	2.4751	124	0.9272		68.0	5 10.5
1	0.3762		0.4061		2.4627		0.9265	7	9	6 12.6 7 14.7
2	0.3778	16	0.4081	20	2.4504	123	0.9259	6	8	7 14.7 8 16.8
3	0.3795	17 16	0.4101	20 21	2.4383	12I 12I	0.9252	7	7	9 18.9
4	0.3811		0.4122		2.4262		0.9245	7	6	9 20.9
5	0.3827	16 16	0.4142	20 21	2.4142	120	0.9239	6	5	
6	0.3843	16	0.4163	20	2.4023	119 117	0.9232	7	4	
7	0.3859	16	0.4183	21	2.3906		0.9225	1	3	17
8	0.3875	16	0.4204	20	2.3789	117 116	0.9219	6	2	I I.7
9	0.3891	16	0.4224	21	2.3673	114	0.9212	7	1	2 3.4
23.0	0.3907	16	0.4245	20	2.3559	114	0.9205		67.0	3 5.I 4 6.8
1	0.3923		0.4265		2.3145		0.9198	7	9	4 6.8 5 8.5
2	0.3939	16	0.4286	21	2.3332	113	0.9191	7	8	6 10.2
3	0.3955	16 16	0.4307	2I 20	2.3220	II2 III	0.9184	7	7	7 11.9
4	0.3971		0.4327		2.3109		0.9178	1	6	8 13.6
5	0.3987	16	0.4348	21	2.2998	III	0.9171	7	5	9 15.3
6	0.4003	16 -16	0.4369	2I 2I	2.2889	109	0.9164	7	4	
7	0.4019		0.4390		2.2781		0.9157	7	3	
8	0.4035	16 16	0.4411	21	2.2673	108	0.9150	7	2	
9	0.4051	16	0.4431	21	2.2566	106	0.9143	8	1	I 16
24.0	0.4067	16	0.4452	21	2.2460	105	0.9135	1	66.0	2 3.2
1	0.4083		0.4473		2.2355	-	0.9128	7	9	3 4.8
2	0.4099	16	0.4494	2I 2I	2.2251	104	0.9121	7	8	4 6.4
3	0.4115	16 16	0.4515	2I 2I	2.2148	103	0.9114	7	7	5 8.0
4	0.4131		0.4536		2.2045		0.9107		6	6 9.6
5	0.4147	16 16	0.4557	2I 2I	2.1943	102	0.9100	7 8	5	7 11.2
6	0.4163	16	0.4578	21	2.1842	101	0.9092	7	4	8 12.8
7	0.4179		0.4599		2.1742		0.9085	1	3	9 14.4
8	0.4195	16	0.4621	22 21	2.1642	100	0.9078	7 8	2]
9	0.4210	15 16	0.4642	21	2.1543	99 98	0.9070	7	1	
امعما	0.4226	10	0.4663	-1	2.1445	90	0.9063		65.0	
25.0										

TABLE XXVII. — (Continued)

		_				-		,	_	
Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
25.0	0.4226	16	0.4663	21	2.1445	97	0.9063	7	65.0	
1	0.4242	16	0.4684	22	2.1348	97	0.9056	8	9	1
2	0.4258	16	0.4706	21	2.1251	96	0.9048	7	8	1
3	0.4274	15	0.4727	21	2.1155	95	0.9041	8	7	23
4	0.4289	16	0.4748	22	2.1060	95	0.9033	7	6	I 2.3
5	0.4305	16	0.4770	21	2.0965	93	0.9026	8	5	2 4.6
6	0.4321	16	0.4791	22	2.0872	94	0.9018	7	4	3 6.9
7	0.4337	15	0.4813	21	2.0778	92	0.9011	8	3	4 9.2
8	0.4352	16	0.4834	22	2.0686	92	0.9003	7	2	5 11.5
9	0.4368	16	0.4856	21	2.0594	91	0.8996	8	I	6 13.8
26.0	0.4384	15	0.4877	22	2.0503	90	0.8988	8	64.0	7 16.1 8 18.4
1	0.4399	16	0.4899	}	2.0413	1	0.8980		9	8 18.4
2	0.4415	16	0.4921	22	2.0323	90	0.8973	7 8	8	9 20.7
3	0.4431	15	0.4942	2I 22	2.0233	90 88	0.8965	8	7	
4	0.4446	16	0.4964	l	2.0145		0.8957	l	6	
5	0.4462	16	0.4986	22	2.0057	88	0.8949	8	5	22
6	0.4478	15	0.5008	22 21	1.9970	87	0.8942	7 8	4	I 2.2
7	0.4493	1	0.5029	1	1.9883	87	0.8934	Į.	3	2 4.4
8	0.4509	16 15	0.5051	22	1.9797	86	0.8926	8	2	3 6.6
9	0.4524	16	0.5073	22 22	1.9711	86	0.8918	8	1	4 8.8
27.0	0.4540	1	0.5095		1.9626	85	0.8910	í	63.0	5 11.0
1	0.4555	15	0.5117	22	1.9542	84	0.8902	8	9	6 13.2
2	0.4571	16	0.5139	22	1.9458	84	0.8894	8	l š	7 15.4 8 17.6
3	0.4586	15	0.5161	22	1.9375	83	0.8886	8	7	9 19.8
4	0.4602	16	0.5184	23	1.9292	83	0.8878	8	6	9 19.0
5	0.4617	15	0.5206	22	1.9210	82	0.8870	8	5	
ĕ	0.4633	16	0.5228	22	1.9128	82	0.8862	8	4	
7	0.4648	15	0.5250	22	1.9047	81	0.8854	8	3	16
8	0.4664	16	0.5272	22	1.8967	80	0.8846	8	2	1 1.6
9	0.4679	15	0.5295	23	1.8887	80	0.8838	8	1	2 3.2
28.0	0.4695	16	0.5317	22	1.8807	80	0.8829	9	62.0	3 4.8
1	0.4710	15	0.5340	23	1.8728	79	0.8821	8	9	4 6.4
2	0.4710	16	0.5362	22	1.8650	78	0.8813	8	8	5 8.0 6 9.6
3	0.4741	15	0.5384	22	1.8572	78	0.8805	8	7	6 9.6 7 II.2
4	0.4756	15	0.5407	23	1.8495	77	0.8796	9	6	8 12.8
5	0.4750	16	0.5430	23	1.8418	77	0.8788	8	5	9 14.4
6	0.4772	15	0.5452	22	1.8341	77	0.8780	8	4	21 -4.4
7	0.4802	15	0.5475	23	1.8265	76	0.8771	9		
8	0.4802	16	0.5498	23	1.8190	75	0.8763	8	3 2	
9	0.4833	15	0.5520	22	1.8115	75	0.8755	8	í	15
29.0	0.4848	15	0.5543	23	1.8040	75	0.8746	9	61.0	1 1.5
		15		23		74		8		2 3.0
1	0.4863	16	0.5566	23	1.7966	73	0.8738	9	9 8	3 4.5
3	o.4879 o.4894	15	0.5589 0.5612	23	1.7820	73	0.8729 0.8721	8	7	4 6.0 5 7.5
		15		23		73		9		5 7.5 6 9.0
4	0.4909	15	0.5635	23	1.7747	72	0.8712	8	6	7 10.5
5 6	0.4924	15	0.5658 0.5681	23	1.7675 1.7603	72	0.8704 0.8695	9	5	8 12.0
	0.4939	16		23		71		9	4	9 13.5
7	0.4955	15	0.5704	23	1.7532	71	0.8686	8	3	
8	0.4970	15	0.5727	23	1.7461	70	o.8678 o.8669	9	2 I	
	0.4985	15	0.5750	24		70		9		
30.0	0.5000		0.5774		1.7321		0.8660		60.0	
	Cosin	đ.	Cotan	d.	Tan	đ.	Sin	d.	Deg.	Y

TABLE XXVII. — (Continued)

Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
30.0	0.5000		0.5774		I.732I		0.8660	_	60.0	
1	0.5015	15	0.5797	23	1.7251	70	0.8652	8	9	
2	0.5030	15	0.5820	23	1.7182	69	0.8643	9	8	
3	0.5045	15	0.5844	24	1.7113	69 68	0.8634	9	7	24
4	0.5060	15	0.5867	23	1.7045		0.8625	9	6	I 2.4
5	0.5075	15	0.5890	23	1.6977	68 68	0.8616	9	5	2 4.8
6	0.5090	15 15	0.5914	24 24	1.6909	67	0.8607	9	4	3 7.2 4 9.6
7	0.5105	-	0.5938		1.6842		0.8599	-	3	5 12.0 6 14.4
8	0.5120	15	0.5961	23	1.6775	67 66	0.8590	9	2	
9	0.5135	15 15	0.5985	24 24	1.6709	66	0.8581	9	1	7 16.8 8 19.2
31.0	0.5150	-	0.6009		1.6643	66	0.8572	9	59.0	9 21.6
1	0.5165	15	0.6032	23	1.6577		0.8563		9	
2	0.5180	15	0.6056	24	1.6512	65	0.8554	9	8	25
3	0.5195	15 15	0.6080	24 24	1.6447	65 64	0.8545	9	7	1 2.5
4	0.5210	-	0.6104		1.6383		0.8536		6	2 5.0
5	0.5225	15	0.6128	24	1.6319	64 64	0.8526	10 9	5	3 7.5 4 10.0
6	0.5240	15 15	0.6152	24 24	1.6255	64	0.8517	9	4	
7	0.5255	-	0.6176	-	1.6191	63	0.8508	9	3	6 15.0
8	0.5270	15 14	0.6200	24	1.6128	62	0.8499	9	2	7 17.5 8 20.0
9	0.5284	15	0.6224	24 25	1.6066	63	0.8490	10	1	8 20.0 9 22.5
32.0	0.5299	-	0.6249	-	1.6003	62	0.8480	9	58.0	313
1	0.5314	15	0.6273	24	1.5941	61	0.8471	1	9	1 26
2	0.5329	15	0.6297	24	1.5880	62	0.8462	9	8	I 2.6
3	0.5344	15 14	0.6322	25 24	1.5818	61	0.8453	10	7	2 5.2
4	0.5358		0.6346	-	1.5757	60	0.8443		6	3 7.8
5	0.5373	15 15	0.6371	25	1.5697	60	0.8434	9	5	4 10.4 5 13.0
6	0.5388	14	0.6395	24 25	1.5637	60	0.8425	10	4	5 13.0 6 15.6
7	0.5402		0.6420		1.5577	60	0.8415	9	3	7 18.2
8	0.5417	15 15	0.6445	25 24	1.5517	59	0.8406	10	2	8 20.8 9 23.4
9	0.5432	14	0.6469	25	1.5458	59	0.8396	9	I	9123.4
33.0	0.5446	15	0.6494	25	1.5399	59	0.8387	10	57.0	
1	0.5461	-	0.6519		1.5340	58	0.8377	9	9	I I.5
2	0.5476	15	0.6544	25 25	1.5282	58	0.8368	10	8	2 3.0
3	0.5490	15	0.6569	25	1.5224	58	0.8358	IO	7	3 4.5
4	0.5505	14	0.6594	25	1.5166	58	0.8348	9	6	4 6.0 5 7.5
5	0.5519	15	0.6619	25 25	1.5108	57	0.8339	10	5	5 7.5 6 9.0
6	0.5534	14	0.6644	25	1.5051	57	0.8329	9	4	7 10.5
7	0.5548	15	0.6669	25	1.4994	56	0.8320	10	3	8 12.0 9 13.5
8	0.5563	14	0.6694	26	1.4938	56	0.8310	10	2 1	9 1 13.3
9	0.5577	15	0.6720	25	1.4882	56	0.8300	10		
34.0	0.5592	14	0.6745	26	1.4826	56	0.8290	9	56.0	I 1.4
1	0.5606	15	0.6771	25	1.4770	55	0.8281	10	9	2 2.8
2	0.5621	13	0.6796	26 26	1.4715	56	0.8271	10	8	3 4.2
3	0.5635	15	0.6822	25	1.4659	54	0.8261	10	7	4 5.6 5 7.0
4	0.5650	14	0.6847	26	1.4605	55	0.8251	10	6	5 7.0 6 8.4
5 6	0.5664	14	0.6873	26	1.4550	54	0.8241	10	5	7 9.8
	0.5678	15	0.6899	25	1.4496	54	0.8231	10	4	
7	0.5693	14	0.6924	26	I.4442	54	0.8221	10	3	9 12.6
8 9	0.5707 0.572I	14	0.6950	26	1.4388	53	0.8211	9	2 I	
35.0	0.5721	15	0.7002	26	1.4335	54	0.8202	10	55.0	
<u> </u>	Cosin	đ.	Cotan	d.	Tan	d.	Sin	d.	Deg.	
L	COSIII	u.	Cotan	u.	1 an	l u.	I OIII	1 a.	Lock.	1

Deg.	Sin	d.	Tan	d.	Cotan	d.	Cosin	d.		P. P.
35.0	0.5736		0.7002	26	1.4281	52	0.8192	11	55.0	
1	0.5750	14	0.7028		1.4229		0.8181		9	
2	0.5764	14	0.7054	26 26	1.4176	53	0.8171	10	8	
3	0.5779	15	0.7080		1.4124	52	0.8161	10	7	27
4	0.5793	14	0.7107	27	1.4071	53	0.8151	10	6	1 2.7
5	0.5807	14	0.7133	26	1.4019	52	0.8141	10	5	2 5.4 3 8.1
6	0.5821	14	0.7159	26	1.3968	51	0.8131	10	4	
7	0.5835	14	0.7186	27	1.3916	52	0.8121	10	3	
8	0.5850	15	0.7212	26	1.3865	51	0.8111	10	2	5 13.5 6 16.2
9	0.5864	14	0.7239	27	1.3814	51	0.8100	11	1	7 18.9 8 21.6
36.0	0.5878	14	0.7265	26	1.3764	50	0.8090	10	54.0	
		14		27		51	0.8080	10		9 24.3
I 2	0.5892	14	0.7292	27	1.3713	50	0.8070	10	9	
	0.5906 0.5920	14	0.7319	27	1.3663 1.3613	50	0.8059	11	7	28
3		14		27		49		10	1	1 2.8
4	0.5934	14	0.7373	27	1.3564	50	0.8049	10	6	2 5.6 3 8.4
5 6	0.5948	14	0.7400	27	1.3514	49	0.8039	II	5	4 11.2
	0.5962	14	0.7427	27	1.3465	49	1	10	4	5 14.0
7	0.5976	14	0.7454	27	1.3416	49	0.8018	11	3	
8	0.5990	14	0.7481	27	1.3367	48	0.8007	10	2	7 19.6 8 22.4
9	0.6004	14	0.7508	28	1.3319	49	0.7997	11	53.0	9 25.2
37.0	0.6018	14	0.7536	27	1.3270	48	0.7986	IO	103.0	* ' '
1	0.6032		0.7563		1.3222		0.7976	1	9	1 29
2	0.6046	14	0.7590	27	1.3175	47 48	0.7965	II	8	I 2.9
3	0.6060	14	0.7618	28 28	1.3127	48	0.7955	11	7	2 5.8
4	0.6074	14	0.7646		1.3079		0.7944		6	3 8.7
5	0.6088	14	0.7673	27	1.3032	47	0.7934	10	5	4 11.6
6	0.6101	13	0.7701	28	1.2985	47	0.7923	II	4	5 14.5 6 17.4
7	0.6115	14	0.7729	28	1.2938	47	0.7912		3	
8	0.6129	14	0.7757	28	1.2892	46	0.7902	10	2	8 23.2
9	0.6143	14	0.7785	28	1.2846	46	0.7891	11	ı	9 26.I
38.0	0.6157	14	0.7813	28	1.2799	47	0.7880	11	52.0	
1	0.6170	13	0.7841	28	1.2753	46	0.7869	11	9	14
I 2	0.6184	14	0.7869	28	1.2708	45	0.7859	10	8	I I.4
3	0.6198	14	0.7898	29	1.2662	46	0.7848	11	7	2 2.8
1 -	0.6211	13	0.7926	28	1.2617	45	0.7837	11	6	3 4.2 4 5.6
4	0.6211	14	0.7920	28	I.2572	45	0.7837	11	5	
5 6	0.6239	14	0.7983	29	1.25/2	45	0.7815	11	4	5 7.0
1	0.6252	13	0.8012	29	i	45	0.7804	11	1	7 9.8 8 II.2
7 8	0.6252	14	0.8012	28	1.2482	45	0.7804	11	3 2	9 12.6
9	0.6280	14	0.8040	29	1.2437	44	0.7782	11	. 1	
		13	0.8098	29		44		II	51.0	
39.0	0.6293	14		29	1.2349	44	0.7771	11	1	I 1.3
I	0.6307	13	0.8127	29	1.2305	44	0.7760	11	9	2 2.6
2	0.6320	14	0.8156	29	1.2261	43	0.7749	11	8	3 3.9
3	0.6334	13	0.8185	29	1.2218	44	0.7738	11	7	4 5.2
4	0.6347	14	0.8214	29	1.2174	43	0.7727	11	6	5 6.5 6.8
5 6	0.6361	13	0.8243	30	1.2131	43	0.7716	111	5	7 9.I 8 10.4
	0.6374	14	0.8273	29	1.2088	43	0.7705	11	4	
7	0.6388	13	0.8302	30	1.2045	43	0.7694	11	3	9 11.7
8	0.6401	13	0.8332	29	1.2002	43	0.7683	11	2	1
9	0.6414	14	0.8361	30	1.1960	42	0.7672	12	I	
40.0	0.6428		0.8391		1.1918		0.7660		50.0	
	Cosin	d.	Cotan	d.	Tan	d.	Sin	đ.	Deg.	
	1 000111	,	1		1			1	1 - 5	1

TABLE XXVII. — (Continued)

Deg.	Sin	d.	Tan	đ.	Cotan	đ.	Cosin	d.		P. P.
40.0	0.6428		0.8391		1.1918		0.7660		50.0	
1	0.6441	13	0.8421	30	1.1875	43	0.7649	II	9	
2	0.6455	14	0.8451	30	1.1833	42	0.7638	II	8	
3	0.6468	13	0.8481	30	1.1792	41	0.7627	11	7	31
		13	0.8511	30	1	42	0.7615	12	6	I 3.I 2 6.2
4	0.6481	13	0.8541	30	1.1750	42	0.7604	II	5	3 9.3
5 6	0.6508	14	0.8571	30	1.1667	41	0.7593	11	4	4 12.4
		13		30		41		12		5 15.5
7	0.6521	13	0.8601	31	1.1626	41	0.7581	II	3	
8	0.6534	13	0.8632	30	1.1585	41	0.7570	II	2 I	7 21.7 8 24.8
9	0.6547	14		31	1.1544	40	0.7559	12		9 27.9
41.0	0.6561	13	0.8693	31	I.1504	41	0.7547	11	49.0	
Ī	0.6574		0.8724		1.1463		0.7536	12	9	
2	0.6587	13	0.8754	30	1.1423	40	0.7524	II	8	32
3	0.6600	13	0.8785	31	1.1383	10	0.7513	12	7	1 3.2 2 6.4
4	0.6613	13	0.8816	31	1.1343		0.7501		6	3 9.6
5	0.6626	13	0.8847	31	1.1303	40	0.7490	II	5	4 12.8
6	0.6639	13	0.8878	31	1.1263	10	0.7478	12	4	5 16.0
7	0.6652	13	0.8910	32	I.1224	39	0.7466	12	3	
8	0.6665	13	0.8911	31	1.1184	40	0.7455	11	2	7 22.4 8 25.6
9	0.6678	13	0.8972	31	1.1145	39	0.7443	12	1	9 28.8
		13		32	1.1106	39		12	48.0	
42.0	0.6691	13	0.9004	32		39	0.7431	II		
1	0.6704	13	0.9036	31	1.1067	39	0.7420	12	9	33
2	0.6717	13	0.9067	32	1.1028	38	0.7408	12	8	1 3.3 2 6.6
3	0.6730	13	0.9099	32	1.0990	39	0.7396	II	7	
4	0.6743		0.9131	32	1.0951	38	0.7385	12	6	3 9.9 4 13.2
5	0.6756	13 13	0.9163	32	1.0913	38	0.7373	12	5	5 16.5
6	0.6769	13	0.9195	33	1.0875	38	0.7361	12	4	6 19.8
7	0.6782		0.9228		1.0837		0.7349	12	3	7 23.1 8 26.4
8	0.6794	12	0.9260	32	1.0799	38	0.7337	12	2	8 26.4 9 29.7
9	0.6807	13	0.9293	33	1.0761	38	0.7325	II	1	9 1 29.7
43.0	0.6820	13	0.9325	32	1.0724	37	0.7314		47.0	
	0.6833	13		33	1.0686	38	0.7302	12	9	34
1	0.6845	12	0.9358	33	1.0649	37	0.7290	12	8	I 3.4 2 6.8
2	0.6858	13	0.9391	33	1.0612	37	0.7278	12	7	
3		13	1	33		37	1	12	6	3 IO.2 4 I3.6
4	0.6871	13	0.9457	33	1.0575	37	0.7266	12	1	
5	0.6884	12	0.9490	33	1.0538	37	0.7254	12	5 4	6 20.4
6	0.6896	13	0.9523	33	1.0501	37	0.7242	12		7 23.8
7	0.6909	12	0.9556	34	1.0464	36	0.7230	12	3	
8	0.6921	13	0.9590	33	1.0428	36	0.7218	12	2	9 (30.6
9	0.6934	13	0.9623	34	1.0392	37	0.7206	13	1	
44.0	0.6947	12	0.9657		1.0355	36	0.7193	12	46.0	13
1	0.6959		0.9691	34	1.0319		0.7181	12	9	I I.3
2	0.6972	13	0.9725	34	1.0283	36	0.7169	12	8	2 2.6
3	0.6984	12	0.9759	34	1.0247	36	0.7157	12	7	3 3.9
4	0.6997	13	0.9793	34	1.0212	35	0.7145	(6	4 5.2 5 6.5
5	0.7009	12	0.9827	34	1.0176	36	0.7133	12	5	6: 7.8
6	0.7022	13	0.9861	34	1.0141	35	0.7120	13	4	7 9.1
	1	12	0.9896	35	1.0105	36	0.7108	12	3	
8	0.7034	12	0.9930	34	1.0070	35	0.7096	12	2	9 11.7
9	0.7040	13	0.9930	35	1.0075	35	0.7083	13	I	
		12		35		35	0.7071	12	45.0	
45.0	0.7071		1.0000		I.0000			_	-	
1	Cosin	d.	Cotan	d.	Tan	d.	Sin	d.	Deg.	

TABLE XXVIII. — NATURAL VERSED SINES AND EXTERNAL SECANTS

Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
0.0	.0000	.0000	5.0	.0038	.0038	10.0	.0152	.0154	15.0	.0341	.0353
т,	.0000	.0000	т,	. 0040	. 0040	.т	.0155	.0157	.r	.0345	.0358
.2	.0000	.0000	. 2	.0041	.0041	. 2	.0158	.0161	.2	.0350	,0363
-3	.0000	.0000	-3	.0043	.0043	.3	.0161	.0164	.3	.0354	.0367
.4	.0000	0000	.4	.0044	.0045	.4	.0164	.0167	.4	.0359	.0372
-5	.0000	.0000	-5	.0046	.0046	5	.0167	.0170	-5	.0364	.0377
.6	.0001	.0001	.6	.0048	.0048	.6	.0171	.0174	.6	.0368	.0382
.7	.0001	.0001	.7	.0049	.0050	.7	.0174	.0177	.7	.0373	.0388
.8	.0001	1000.	.8	.0051	.0051	.8	.0177	.0180	.8	.0378	.0393
.9	.0001	.0001	.9	.0053	.0053	.9		.0184	.9	. 0383	.0398
1.0	.0002	.0002	6.0	.0055	.0055	11.0	.0184	.0187	16.0	.0387	.0403
.I	.0002	.0002	.I	.0057	.0057	Ι.	.0187	.0191	.I	.0392	.0408
.2	.0002	.0002	.2	.0058	.0059	.2	.0190	.0194	.2	.0397	.0413
.3	.0003	.0003	-3		1	-3	.0194	.0198	-3	.0402	.0419
.4	.0003	.0003	.4	.0062	.0063	-4	.0197	.0201	-4	.0407	.0424
.5 .6	.0003	.0003	.5 .6	.0066	.0067	.5 .6	.0201	.0209	.5 .6	.0412	.0429
	.0004	.0004	.7	.0068	.0069	.7	.0204	.0212			
.7 .8	.0004	.0004	.8	.0008	.0009	.8	.0208	.0212	.7 .8	.0422	.0440
.9	.0005	.0005	.9	.0072	.0073	.9	.0215	.0220	.9	.0432	.0451
2.0	.0006	.0006	7.0	.0075	.0075	12.0	.0219	.0223	17.0	.0437	.0457
т.	.0007	.0007	.1	.0077	.0077	τ.	.0222	.0227	.1	.0442	.0463
.2	.0007	.0007	.2	.0079	.0079	.2	.0222	.0231	.2	.0442	.0468
.3	.0008	.0008	-3	.0081	.0082	.3	.0230	.0235	.3	.0452	.0474
.4	.0009	.0009	.4	.0083	.0084	.4	.0233	.0239	.4	.0458	.0480
.5	.0010	.0010	.5	.0086	.0086	.5	.0237	.0243	-5	.0463	.0485
.6	.0010	.0010	.6	.0088	.0089	.6	.0241	.0247	.6	.0468	.0491
.7	.0011	.0011	.7	.0090	.0091	.7	.0245	.0251	.7	.0473	.0497
.8	.0012	.0012	.8	.0093	.0093	.8	.0249	.0255	.8	.0479	.0503
.9	.0013	.0013	.9	.0095	.0096	.9	.0252	.0259	.9	.0484	. 0509
3.0	.0014	.0014	8.0	.0097	.0098	13.0	.0256	.0263	18.0	. 0489	.0515
.т	.0015	.0015	.I	.0100	.0101	.r	. 0260	.0267	.I	. 0495	.0521
.2	.0016	.0016	.2	.0102	.0103	.2	. 0264	.0271	.2	. 0500	.0527
-3	.0017	.0017	.3	.0105	.0106	-3	. 0268	.0276	.3	.0506	.0533
.4	.0018	.0018	.4	.0107	.0108	.4	.0272	. 0280	-4	.0511	.0539
.5	.0019	.0019	.5	.0110	.0111	.5	.0276	.0284	-5	.0517	.0545
.6	.0020	.0020	.6	.0112	.0114	.6	.0280	. 0288	.6	.0522	.0551
.7	.0021	.0021	.7	.0115	.0116	.7	.0285	.0293	.7	.0528	.0557
.8 .9	.0022	.0022	.8 .9	.0118	.0119	.8 .9	.0289	. 0297 . 0302	.8 .9	.0534	.0564
4.0			9.0			.9 14.0			.9 19.0	.0539	.0570
1	.0024	.0024		.0123	.0125		.0297	.0306		. 0545	.0576
.1	.0026	.0026	. I . 2	.0126	.0127	. I . 2	.0301	.0311	.I .2	.0551	.0583
.3	.0027	.0027	.3	.0129	.0133	.3	.0310	.0315	.3	.0556	.0595
.4	.0030	.0030	.4	.0134	.0136	.4	.0314	.0324	.4	.0568	.0602
.5	.0030	.0030	.5	.0134	.0139	.5	.0314	.0324	·4 ·5	.0574	.0608
.6	.0032	.0032	.6	.0140	.0142	.6	.0323	.0334	.6	.0579	.0615
.7	.0034	.0034	.7	.0143	.0145	.7	.0327	.0338	.7	. 0585	.0622
.8	.0035	.0035	.8	.0146	.0148	.8	.0332	.0343	.8	.0591	.0628
.9	.0037	. 0037	.9	.0149	.0151	.9	. 0336	. 0348	.9	.0597	. 0635
5.0	.0038	. 0038	10.0	.0152	.0154	15.0	.0341	.0353	20.0	.0603	.0642

TABLE XXVIII. — Natural Versed Sines and External Secants

Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
20.0	. 0603	.0642	25.0	.0937	. 1034	30.0	.1340	.1547	35.0	. 1808	.2208
.ı	. 0609	.0649	. т	.0944	. 1043	, г	.1348	.1559	. 1	. 1819	.2223
.2	.0615	.0655	.2	.0952	.1052	.2	. 1357	. 1570	.2	. 1829	. 2238
.3	.0621	.0662	.3	.0959	.1061	-3	.1366	.1582	.3	. 1839	. 2253
.4	.0627	.0669	.4	.0967	.1070	.4	.1375	. 1594	.4	. 1849	. 2268
5	. 0633	.0676	.5	.0974	.1079	-5	.1384	. 1606	- 5	. 1859	. 2283
.6	. 0639	.0683	.6	.0982	.1089	.6	. 1393	. 1618	.6	.1869	. 2299
.7	.0646	.0690	.7	. 0989	.1098	.7	.1401	. 1630	.7	.1879	.2314
.8	.0651	. 0697	.8	. 0997	.1107	.8	.1410	.1642	.8	1889	.2329
.9	.0658	.0704	.9	.1004	.1117	.9	. 1419	. 1654	.9	.1900	.2345
21.0	.0664	.0711	26.0	.1012	.1126	31.0	. 1428	. 1666	36.0	. 1910	. 2361
.1	.0670	.0719	. 1	.1020	.1135	. 1	. 1437	. 1679	. 1	.1920	.2376
.2	. 0677	.0726	.2	. 1027	.1145	.2	. 1446	.1691	. 2	. 1930	.2392
.3	.0683	.0733	-3	.1035	.1155	-3	. 1455	.1703	.3	.1941	.2408
.4	. 0689	.0740	-4	. 1043	.1164	.4	.1464	.1716	.4	.1951	.2424
-5	.0696	.0748	-5	. 1051	.1174	-5	.1474	.1728	-5	.1961	.2440
.6	.0702	.0755	.6	.1058	.1184	.6	.1483	.1741	.6	.1972	.2456
.7	.0709	.0763	.7	.1066	.1194	.7	.1492	. 1753	.7	.1982	.2472
.8	.0715	.0770	.8	.1074	.1203	.8	.1501	1766	.8	.1993	.2489
.9	.0722	.0778	.9	.1082	.1213	.9	.1510	.1779	.9	.2003	.2505
22.0	.0728	.0785	27.0	. 1090	.1223	32.0	.1520	.1792	37.0	.2014	.2521
.I	.0735	.0793	.1	. 1098	.1233	. 1	. 1529	. 1805	Ι.	.2024	.2538
.2	.0741	.0801	.2	.1106	.1243	.2	.1538	.1818	.2	. 2035	.2554
-3	.0748	.0808	.3	.1114	.1253	-3	.1547	.1831	-3	.2045	.2571
.4	.0755	.0816	.4	.1122	.1264	.4	. 1557	. 1844	-4	. 2056	.2588
.5	.0761	.0824	-5	.1130	.1274	.5	.1566	. 1857	- 5	. 2066	.2605
.6	.0768	.0832	.6	.1138	.1284	.6	.1575	.1870	.6	. 2077	. 2622
.7	.0775	.0840	.7	.1146	.1294		. 1585	.1883		. 2088	.2639
.8	.0781	.0848	.8	.1154	.1305		. 1594	.1897	.8	. 2098	. 2656
.9	. 0788	. 0856	.9	.1162	.1315	1	.1604	.1910	.9	.2109	.2673
23.0	.0795	.0864	28.0	.1171	.1326	ľ	.1613	.1924	38.0	.2120	, 2690
Ţ.	.0802	.0872	.1	.1179	.1336		.1623		. 1	. 2131	.2708
.2	.0809	.0880	.2	.1187	.1347		. 1632		.2	.2141	.2725
.3	.0816	.0888	-3	.1195	.1357		.1642		-3	.2152	
.4	.0822	.0896	-4	.1204	.1368		.1652		.4	.2163	
.5 .6	.0829	.0904	.6	.1212	.1379		.1661	.1992	.5 .6	.2174	
	_	.0913	1	1	1		.1680	1	1	.2196	1
.7 .8	.0843	.0921	.7	.1229	.1401		.1690	1	.7	.2207	.2831
.9	.0857	.0929	.9	.1237	.1412		.1700		.9	.2218	
24.0	.0865	.0946	29.0	. 1254	.1434	1	.1710			.2229	1
			1	.1262		1	-		1.1	.2240	
.1	.0872	.0955	I.I	.1202	.1445		.1719	1	.2	.2251	1
.2	.0879	.0963	.2	.1271	.1450		.1729			.2262	
	.0893	.0972	-	.1288	.1478		.1749	1		.2273	1 -
.4	.0893	.0989	.4	.1200	.1490		.1759	1	.5	.2284	
.5 .6	.0900	.0939	.6	.1305	.1501		.1769			.2295	
1	.0915	.1007	1	.1314	.1512		.1779	1 -		.2306	
.7 .8	.0913	.1007	.7	.1314	.1524		.1789			.2317	
.9	.0922	.1025	.9	.1331	.1535		.1798			.2328	
25.0	.0937	.1034	30.0	.1340	.1547	35.0	. 1808	.2208	40.0	. 2340	.3054

$\begin{array}{ll} \textbf{TABLE} & \textbf{XXVIII.} - \textbf{Natural Versed Sines and External} \\ \textbf{Secants} \end{array}$

Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
40.0	.2340	.3054	45.0	. 2929	.4142	50.0	.3572	-5557	55.0	.4264	.7434
т.	.2351	.3073	. т	. 2941	.4167	. т	. 3586	.5590	. 1	.4279	. 7478
.2	.2362	.3093	. 2	. 2954	.4192	.2	- 3599	. 5622	. 2	.4293	.7522
-3	.2373	.3102	-3	.2966	.4217	.3	.3612	. 5655	-3	.4307	. 7566
-4	.2385	.3131	-4	. 2978	. 4242	.4	. 3626	. 5688	.4	. 4322	.7610
-5	.2396	.3151	-5	. 2991	. 4267	-5	. 3639	.5721	-5	.4336	.7655
.6	.2407	.3171	.6	.3003	.4293	.6	.3653	.5755	.6	·4350	. 7700
.7	.2419	.3190	.7	.3016	.4318	.7	. 3666	. 5788	.7	.4365	. 7745
.8	.2430	.3210	.8	.3028	-4344	.8	.3680	. 5822	.8	.4379	.7791
.9	.2441	.3230	.9	.3041	. 4370	.9	. 3693	. 5856	.9	-4394	. 7837
41.0	. 2453	.3251	46.0	.3053	.4396	51.0	.3707	. 5890	56.0	. 4408	. 7883
.1	.2464	.3270	.I	. 3066	.4422	ı.	. 3720	. 5925	. 1	. 4423	. 7929
.2	.2476	. 3291	.2	.3079	-4448	. 2	.3734	. 5959	. 2	. 4437	. 7976
-3	.2487	.3311	-3	.3091	4474	-3	.3748	.5994	-3	.4452	.8033
.4	. 2499	.3331	.4	.3104	.4501	.4	.3761	. 6029	-4	. 4466	.8070
.5	.2510	.3352	.5	.3116	.4527	.5	.3775	. 6064	.5	.4481	.8118
.6	.2522	∙3373	.6	.3129	·4554	.6	.3789	.6099	.6	·4495	.8166
.7	. 2534	·3393	.7	.3142	. 4581	.7	.3802	.6135	.7	.4510	.8214
.8	.2545	.3414	.8	.3155	.4608	.8	.3816	.6171	.8	.4524	.8263
.9	. 2557	-3435	.9	.3167	. 4635	.9	. 3830	.6207	.9	4539	.8312
42.0	. 2569	.3456	47.0	.3180	.4663	52.0	. 3843	.6243	57.0	4554	.8361
I.	. 2580	.3478	ı.	. 3 193	.4690	.I	.3857	.6279	.I	. 4568	.8410
.2	.2592	-3499	.2	.3206	.4718	.2	.3871	6316	.2	.4583	.8460 .8510
-3	.2604	.3520	.3	.3218	.4746	.3	.3885	.6353	.3	.4598	
-4	.2615	.3542	-4	.3231	-4774	-4	. 3899	.6390	-4	.4612 .4627	.8561 .8612
.5 .6	.2627	.3563	.5 .6	.3244	.4802	.5 .6	.3912 .3926	. 6427 . 6464	.5 .6	.4642	.8663
4 1	.2651	.3607		.3270	1 1	.7		.6502	.7	.4656	.8714
.7 .8	. 2663	.3629	.7 .8	.3283	.4859	.8	.3940 .3954	. 6540	.8	.4671	.8766
.9	. 2675	.3651	.9	.3296	.4916	9.	.3968	. 6578	.9	.4686	.8818
43.0	. 2686	.3673	48.0	. 3309	-4945	53.0	.3982	.6616	58.0	.4701	.8871
Ι.	. 2698	.3696	.1	.3322	.4974	.1	.3996	.6655	.1	.4716	.8924
.2	.2710	.3718	.2	-3335	.5003	.2	.4010	. 6694	.2	4730	.8977
.3	.2722	.3741	.3	.3348	.5032	.3	.4024	.6733	.3	-4745	.9031
.4	.2734	3763	.4	.3361	.5062	.4	. 4038	.6772	.4	.4760	.9084
.5	.2746	.3786	.5	-3374	.5092	5	.4052	.6812	.5	-4775	.9139
.6	.2758	.3809	.6	.3387	.5121	.6	.4066	. 6852	.6	.4790	.9194
.7	.2770	.3832	.7	.3400	.5151	.7	.4080	. 6892	.7	. 4805	.9249
.8	.2782	. 3855	.8	.3413	.5182	.8	. 4094	.6942	.8	.4820	.9304
.9	.2794	.3878	.9	.3426	.5212	.9	.4108	.6972	.9	. 4835	.9360
44.0	. 2807	. 3902	49.0	- 3439	.5243	54.0	.4122	.7013	59.0	. 4850	.9416
I.	. 2819	.3925	.τ	-3453	.5273	. 1	.4136	.7054	.I	.4865	-9473
.2	. 2831	-3949	.2	. 3466	.5304	.2	.4150	. 7095	.2	.4880	.9530
.3	.2843	-3972	-3	-3479	-5335	-3	.4165	.7137	-3	.4895	.9587
.4	. 2855	.3996	-4	.3492	. 5366	-4	.4179	.7179	.4	.4910	.9645
.5 .6	.2868	.4020	-5	.3506	.5398		.4193	.7221	.5	.4925	.9703
	.2880	.4044	.6	.3519	.5429	.6	.4207	.7263	.6	.4940	.9762
.7	. 2892	.4069	.7	.3532	.5461	.7	.4221	.7305	.7 .8	.4955	.9821
.8 .9	.2904	.4093	.8	.3545	· 5493 · 5525	. 8 .9	.4236	.7348	9. e.	.4970	.9880
45.0			50.0	3559	_	1	.4264	·7434	60.0		1.0000
20.0	.2929	.4142	30.0	.3572	-5557	1 00.0	.4204	• 1454	00.0	.3000	12.0000

TABLE XXVIII. — Natural Versed Sines and External Secants

Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
60.0	.5000	1.0000	65.0	.5774	1.3662	70.0	.6580	1.9238
.1	.5015	.0061	.1	. 5790	.3751	.1	.6596	.9379
.2	. 5030	.0122	.2	. 5805	.3841	.2	.6613	.9521
-3	.5045	.0183	.3	.5821	.3931	.3	.6629	.9665
-4	.5061	.0245	-4	.5837	.4022	-4	.6645	.9811
.5 .6	.5076	1.0308	.5 .6	. 5853	1.4114	.5 .6	.6662	1.9957
1	.5091	.0371		. 5869	.4207		.6678	2.0106
.7 .8	.5106	.0434	.7 .8	. 5885	.4300	.7 .8	.6695	.0256
.9	.5121 .5137	.0498	.9	.5901 .5917	· 4395 · 4490	9.9	.6711 .6728	.0406
61.0		1.0627	66.0			71.0		2.0716
	.5152			.5933	.4586		.6744	
. I . 2	.5167	.0692	Ι.	. 5949	. 4683	I.	.6761	.0872
.3	.5182 .5198	.0757	.2	.5965 .5981	.4780	.2	.6777 .6794	.1030
		.0890				1	.6810	
.4 .5	.5213	1.0957	·4 ·5	.5997 .6013	.4978 1.5078	.4	.6827	.1352 2.1515
.6	.5244	.1025	.6	.6029	.5180	.5 .6	.6844	.1681
.7	.5259	.1023	.7	.6045	.5282	.7	.6860	.1848
.8	.5239	.1162	.8	.6061	.5384	.8	.6877	.2017
.9	.5290	.1231	.9	.6077	.5488	.9	.6893	.2188
62.0	.5305	.1301	67.0	.6093	1.5593	72.0	.6910	2.2361
.1	.5321	.1371	.1	.6109	.5699	.1	.6926	.2535
.1	.5321	.13/1	.1	.6125	.5805	.1	.6943	.2535
.3	.5352	.1513	.3	.6141	.5913	.3	.6960	.2891
.4	.5367	.1584	.4	.6157	.6022	4	.6976	.3072
.5	.5383	1.1657	.5	.6173	1.6131	.5	.6993	2.3255
.6	.5398	.1730	.6	.6189	.6242	.6	.7010	.3440
.7	.5414	. 1803	.7	.6205	.6354	.7	.7026	.3628
.8	.5429	.1877	.8	.6222	.6466	.8	.7043	.3817
.9	.5445	. 1952	.9	.6238	. 6580	.9	. 7060	.4009
63.0	. 5460	I.2027	68.0	.6254	1.6695	73.0	.7076	2.4203
.т	. 5476	.2103	.1	.6270	.6811	. I	.7093	- 4399
.2	. 5491	.2179	.2	. 6286	.6927	. 2	.7110	. 4598
.3	.5507	. 2256	.3	. 6303	.7046	.3	.7126	.4789
.4	.5522	. 2333	-4	.6319	.7165	-4	.7143	.5003
.5	. 5538	1.2412	.5	.6335	1.7285	.5	.7160	2.5209
.6	.5554	.2490	.6	.6351	.7407	.6	.7177	.5418
.7 .8	.5569	.2570	.7	.6367	.7529	.7	.7193	.5629
.8 .9	.5585 .5601	.2650	.8 .9	. 6384 . 6400	.7653	.8	.7210 .7227	.5843
64.0	.5616	1.2812	69.0	.6416	.7904	74.0	.7244	2.6280
.1	.5632	.2894	.1	.6433	.8032	.1	.7260	.6502
.1	.5648	.2894	.1	.6449	.8032	.1	.7200	.6728
.3	. 5663	.3060	.3	.6465	.8291	.3	.7294	.6955
.4	.5679	.3144	.4	.6482	.8422	.4	.7311	.7186
.5	.5695	1.3228	.5	.6498	1.8554	.5	.7328	2.7420
.6	.5711	.3314	.6	.6514	.8688	.6	.7344	.7657
.7	.5726	.3400	.7	.6531	.8824	.7	.7361	.7897
.8	.5742	.3486	.8	.6547	.8960	.8	.7378	.8140
.9	. 5758	-3574	.9	. 6563	. 9099	.9	.7395	.8387
65.0	-5774	1.3662	70.0	. 6580	1.9238	75.0	.7412	2.8637

TABLE XXVIII. — Natural Versed Sines and External Secants

Angle	Vers	Exsec	Angle	Vers	Exsec	Angle	Vers	Exsec
75.0	.7412	2.8637	80.0	.8264	4.7588	85.0	.9128	10.4737
ı.	.7429	.8890	.1	.8281	.8164	. т	.9146	.7073
.2	.7446	.9147	.2	.8298	.8751	.2	.9163	.9506
.3	.7462	.9408	٠3	.8315	.9351	-3	.9181	11.2043
4	.7479	.9672	.4	.8332	.9963	.4	.9198	. 4690
-5	.7496	2.9939	-5	.8350	5.0589	.5	.9215	11.7455
.6	.7513	3.0211	.6	.8367	.1227	.6	.9233	12.0346
.7	.7530	.0486	.7	.8384	.1880	.7	.9250	.3371
.8	.7547	.0765	.8	.8401	.2546	.8	.9268	.6541
.9	.7564	. 1048	.9	.8418	.3228	.9	.9285	.9865
76.0	.7581	3.1336	81.o	.8436	5.3925	86.o	.9302	13.3356
т.	.7598	.1627	ı.	.8453	.4637	ı.	.9320	.7026
.2	.7615	.1923	.2	.8470	. 5366	.2	.9337	14.0889
.3	.7632	.2223	-3	.8487	.6111	.3	.9355	.4961
.4	.7649	.2527	.4	.8505	.6874	.4	.9372	.9260
.5	. 7666	3.2837	-5	.8522	5.7655	.5	.9390	15.3804
.6	.7683	.3150	.6	.8539	.8454	.6	.9407	.8616
.7	.7700	.3469	.7	.8556	.9273	.7	.9424	16.3720
.8	.7716	.3792	.8	.8574	6.0112	.8	.9442	.9142
.9	.7733	.4121	.9	.8591	.0972	.9	.9459	17.4915
77.0	.7750	3.4454	82.0	.8608	6.1853	87.0	.9477	18.1073
.1	.7767	.4793	. т	.8626	.2757	. т	.9494	.7656
.2	.7785	.5137	.2	.8643	.3684	.2	.9512	19.4709
.3	.7802	.5486	.3	.8660	.4635	.3	.9529	20.2285
.4	.7819	.5841	1.4	.8677	.5611	.4	.9546	21.0444
-5	.7836	3.6202	.5	.8695	6.6613	.5	.9564	21.9256
.6	.7853	.6569	.6	.8712	.7642	.6	.9581	22.8802
.7	.7870	.6942	.7	.8729	.8700	.7	.9599	23.9179
.8	.7887	.7320	.8	.8747	.9787	.8	.9616	25.0499
.9	.7904	.7706	.9	.8764	7.0905	.9	.9634	26.2898
78.0	.7921	3.8097	83.0	.8781	7.2055	88.o	.9651	27.6537
Ι.	.7938	.8496	.1	.8799	.3238	.1	.9668	29.1612
.2	.7955	.8901	.2	.8816	.4457	.2	.9686	30.8362
-3	.7972	.9313	-3	.8833	.5711	-3	.9703	32.7083
.4	.7989	.9732	.4	.8851	.7004	-4	.9721	34.8145
-5	.8006	4.0159	-5	.8868	7.8337	-5	.9738	37.2016
.6	.8023	.0593	.6	.8885	.9711	.6	.9756	39.9296
.7	.8041	.1034	-7	.8903	8.1129	.7	.9773	43.0775
.8	.8058	.1484	.8	.8920	.2593	.8	.9791	46.7500
.9	.8075	. 1942	.9	.8937	.4105	.9	.9808	51.0903
79.0	.8092	4.2408	84.0	.8955	8.5668	89.0	.9825	56.2987
.τ	.8109	.2883	.1	.8972	.7283	.1	.9843	62.6646
.2	.8126	.3367	.2	.8989	.8955	.2	.9860	70.6221
-3	.8143	.3860	-3	.9007	9.0685	.3	.9878	80.8532
.4	.8160	.4362	-4	.9024	.2477	.4	.9895	94 - 4947
.5	.8178	4.4874	-5	.9042	9.4334	.5	.9913	113.5930
.6	.8195	. 5396	.6	.9059	.6261	.6	.9930	142.2406
.7	.8212	.5928	.7	.9076	.8260	.7	.9948	189.9868
.8	.8229	.6470	.8	.9094	10.0336	.8	.9965	285.4795 571.9581
.9	.8246	.7023	.9	.9111	.2493	.9	.9983	
80.0	.8264	4.7588	85.0	.9128	10.4737	90.0	1.0000	- ∞

TABLE XXIX

	Seconds in decimals of a degree														
Sec.	Degree	Sec.	Degree	Sec.	Degree	Sec.	Degree	Sec.	Degree	Sec.	Degree				
ı	0.00028	11	0.00306	21	0.00584	31	0.00862	41	0.01139	51	0.01417				
2	0.00056	12	0.00334	22	0.00612	32	0.00890	42	0.01167	52	0.01445				
3	0.00083	13	0.00361	23	0.00639	33	0.00917	43	0.01195	53	0.01473				
4	0.00111	14	0.00389	24	0.00667	34	0.00945	44	0.01222	54	0.01500				
5	0.00139	15	0.00417	25	0.00695	35	0.00973	45	0.01250	55	0.01528				
6	0.00167	16	0.00445	26	0.00723	36	0.01000	46	0.01278	56	0.01556				
7	0.00195	17	0.00473	27	0.00751	37	0.01028	47	0.01306	57	0.01584				
8	0.00222	18	0.00500	28	0.00778	38	0.01056	48	0.01334	58	0.01612				
9	0.00250	19	0.00528	29	0.00806	39	0.01083	49	0.01361	59	0.01639				
10	0.00278	20	0.00556	30	0.00834	40	0.01111	50	0.01389	60	0.01667				

TABLE XXX

	Minutes in decimals of a degree													
Min.	Degree	Min.	Degree	Min.	Degree	Min.	Degree	Min.	Degree	Min.	Degree			
I	0.01667		0.18333		0.35000		0.51667		0.68333	51	0.85000			
3	0.03333	13	0.20000	23	0.36667	33	0.53333	43	0.70000 0.71667		0.86667			
4 5	0.06667		0.23333	24 25	0.40000		0.56667		0.73333	54 55	0.90000			
6	0.10000	16	0.26667	26	0.43333	36	0.60000	46	0.76667	56	0.93333			
7 8	0.11667	1 1	0.28333		0.45000		0.61667		0.78333		0.95000			
9	0.15000		0.31667		0.48333	39 40	0.65000		0.81667 0.83333	59 60	0.9833			

From Roberts' "Track Formulæ and Tables."

CHAPTER IV

LOCATION THEORIES AND TABLES

For problems relating to improvements of existing lines exact data and volumes of discussion of methods will be available. The methods here suggested are for use in locating new lines for which precise data respecting motive power, business, or expense are indeterminate. Most of the problems will relate to saving in operation of freight trains. A single locomotive may be assumed, since in the solution of problems the results will be practically the same relatively for any probable differences in locomotives. It must be remembered that not all of the trains will be affected by probable changes in ruling grades; the engineer must use his judgment in determining what trains will be affected. trains must be considered in estimating the cost of distance, rise and fall, and curvature. The formulas given in what follows are based on the full discussion of the subjects in the author's "Elements of Railroad Engineering."

Tractive Effort. — For approximate computations the tractive effort of a locomotive may be assumed to be

$$T_b = \frac{146 \, H}{S}$$
 pounds,
 $T_c = \frac{P d^2 L}{D}$ pounds,
 $T_a = \frac{W}{4.25}$ pounds if W is pounds,

in which H is the square feet of heating surface.

or

or

S is the speed in miles per hour.

P is the mean effective pressure in the cylinders.

d is the diameter of the piston.

L is the length of the stroke.

D is the diameter of the drive wheels.

W is the weight on the drive wheels.

 T_b is to be used for speeds above that for which $T_b = T_c$ when P is 85 per cent of the working boiler pressure, and is known as the boiler

cent of the boiler pressure. It is the tractive effort of adhesion and all that the locomotive can exert under normal conditions regardless of the values of T_b and T_c . T_c is called the cylinder tractive effort. T_a has been known to be as high as $\frac{W}{3}$, with sand on the track, and it is probably as low as $\frac{W}{5}$ under unfavorable conditions of track. Theoretic values of T_b for a particular consolidation locomotive are

tabulated in Table XXXIII. Resistance. — Resistance to motion on a straight level track varies with speed and weight per car of train; it may be taken from Table XXXII. Grade resistance or acceleration is given by $R_q = 20 r$, in which R_a is resistance in pounds per ton and r is the rate per cent of grade expressed as a whole or mixed number; thus for a 2 per cent grade r is 2.0, etc. Curve resistance in pounds per ton varies with the degree of curve, somewhat with speed, being less as the speed is greater, and with the rigid wheel base of the car or locomotive. It may be averaged for a train at

$$R_c = 0.4 + 0.35 D$$

in which R_c is curve resistance in pounds per ton and D is the degree of curve. This is an empirical equation that does not vanish when D is o as it should to be mathematically correct. Ruling grades or others likely ever to become ruling because of the curves on them should be reduced or "compensated" in rate per cent through all curves as follows: For 1° curves reduce 0.04 per cent; for curves from 2° to 4° reduce 0.03 D per cent; for curves of 5° and over reduce 0.025 D per Greater reductions will do no harm unless they make a steeper ruling grade necessary.

To Find the Maximum Load a Locomotive can Haul on a Given Grade at a Given Speed. - From Table XXXII find the train resistance for an assumed or known car weight at the given speed; add the grade resistance = 20 r, and divide the tractive effort for the given speed by the sum; subtract the weight of engine and tender. The values for a particular consolidation engine are tabulated in Table XXXIV.

Pusher Grade.— To find the grade up which two similar locomotives can haul the load that one can haul on a given grade. If X be the rate of grade sought,

$$X = \frac{\frac{1.9 T}{W + 2E} - R_t}{\frac{20}{20}},$$

in which R_t is train resistance in pounds per ton, T is the tractive effort of one locomotive, W is the weight of the train and E the weight of one locomotive and tender both in tons. If there are to be three locomotives the corresponding pusher grade is

$$X = \frac{\frac{2.85 T}{W + 3 E} - R_t}{\frac{20}{20}}.$$

To Find the Length of Up Grade Required to Reduce the Speed from S_1 to S_2 Miles an Hour for a Given Locomotive and Train. — This is the so-called momentum or velocity grade problem and finds the length of grade steeper than the ruling grade that can still be operated if a sufficient velocity of approach may be had.

Let r be the rate of the grade steeper than that for which the locomotive is loaded. Find the tractive effort for the average speed; add the weight of the train and locomotive for gross load W in tons; find the train resistance R_t for the train at the average speed; find the quantity

$$V = \frac{1}{20} \left(\frac{T}{W} - R_t \right);$$

find the velocity heads for the speeds S_1 and S_2 from Table XXXI, then

$$L \text{ stations} = \frac{\text{difference in velocity heads}}{r - V};$$

V is the virtual grade, or grade that the locomotive can work at the given speed with the given load. If the steep grade differs only a little from the ruling grade for the given S_2 , the result is inaccurate but errs on the safe side, giving a grade somewhat shorter than true theory indicates.

Grades for Unbalanced Traffic. — If traffic is pretty certain to be permanently unbalanced with respect to direction of haul the grade against the lighter traffic may be steeper than that against the heavier traffic if economy of construction will result. The same number of engines and cars must go both ways, hence the lighter traffic trains will have a higher resistance per ton because the average car weight will be less. Having the ruling grade against the heavy traffic determined, the corresponding grade for a traffic in the opposite direction is found as follows:

Find the load that the assumed or known locomotive can haul behind the tender at a speed of about ten miles an hour on the ruling grade against the heavy traffic, using an assumed or known car weight to determine train resistance. If there is much variation in the traffic subtract the weight of the cars (taken at about 18 tons per car for preliminary purposes) from the load, reduce the remaining live or freight load by the assumed percentage of unbalancing, add the car weights and get the new total load and average car weight. Find the train resistance for the new car weight. If R_t be that resistance, T the tractive effort of the locomotive, E the weight of engine and tender and L the load behind the tender, then the grade, G, against the lighter traffic may be

$$G = \frac{1}{20} \left(\frac{T}{L+E} - R_t \right).$$

The caboose or way car has not been considered. For a greater degree of precision than such problems generally warrant its weight should be included with the engine weight E.

Elements for Estimating.—1. Distance. — To estimate the cost of operating extra distance or the saving due to reducing distance assume a probable average train mile cost and assume a number of trains per day over the distance under consideration. All trains going both ways are to be included. Then if C be the train mile cost in dollars, M the miles of extra distance under consideration, and N the number of daily trains, the annual cost of operating the M miles, or the annual saving by omitting M miles, is given approximately by

$$K = 156 C \cdot M \cdot N$$

for moderate changes in distance.

The limit of justifiable expenditure to reduce the distance in miles is $\frac{K}{r}$, where r is the going rate of interest which should be taken somewhat higher than the nominal rate specified in the company's bonds. In the formula it should be used as a decimal, thus 8 per cent = 0.08. For large changes in long lines the coefficient may be increased up to, say, 315 for a change involving the addition of a whole division.

The average train mile cost for the United States is not far from \$1.55 in 1914. The figures for the year have not been computed at this writing. The cost has been increasing for a number of years, but recent economies have checked this increase somewhat. In 1908 the average cost was about \$1.47. The Interstate Commerce Commission divides the country into three great districts for reporting savings and expenses, the Eastern, Southern, and Western. The Eastern district comprises that portion of the country bounded on the west by the northern and western shores of Lake Michigan to Chicago, thence by a line to Peoria, thence to East St. Louis, thence down the Mississippi River to the

mouth of the Ohio River; and on the south by the Ohio River from its mouth to Parkersburg, West Virginia, thence by a line to the southwestern corner of Maryland, thence by the Potomac River to its mouth. The Southern district comprises the territory south of the Eastern district and east of the Mississippi River. The Western district includes the remainder of the United States, exclusive of Alaska and insular possessions.

The Commission also divides the railroads into three classes:

- I. Roads with annual gross operating revenues of \$1,000,000 or more.
- II. Roads with annual gross operating revenues of \$100,000 or more but less than \$1,000,000.
- III. Roads with annual gross operating revenues of less than \$100,000. Average train mile costs for the three classes in the three districts may be taken for purposes of estimating as follows (1914):

District	Class I	Class II	Class III
Eastern	\$ 1.60	\$1.19	\$I.02
Southern	1.38	1.15	1.10
Western	1.59	1.52	I.45

2. Rise and Fall. — Rise and fall between any two points is the total vertical feet of rising grade with its corresponding vertical feet of fall. If the two points are at different levels it requires a round trip to realize the rise and fall due to this difference. In calculating the cost of rise and fall as between two lines, only the cost of the difference in rise and fall is of consequence and hence the following rule is satisfactory though inaccurate for a train going one way.

To find the rise and fall between two points add all vertical feet of rising grades and all vertical feet of falling grades and divide by two.

Three classes of rise and fall are recognized:

- Class A. Rise and fall of small amounts on light grades apparently not felt by the locomotive, requiring no apparent change in effort, only varying the speed a little.
- Class B. Rise and fall requiring the full power of the locomotive in the ascent, the shutting off of steam in the descent, but no use of brakes.
- Class C. Rise and fall requiring the whole power of the locomotive in the ascent and the use of brakes and sometimes of sand on the descent.

If C be the train mile cost, N the number of daily trains (all trains both ways) and f the number of feet of rise and fall, the annual cost for operation may be estimated as follows — the result being in dollars.

Class A. $K_1 = 0.25 f \cdot C \cdot N$. Class B. $K_1 = 1.2 f \cdot C \cdot N$.

Class C. $K_1 = f \cdot \hat{C} \cdot N \times$ the factor of the following table.

Grade	0.4 and under	0.5	0.67	1.0	1.5	2.0	2.5	3.0	3.5	4.0
Cost factor	2.4	2.9	3.6	4.2	4.6	4.8	4.9	5.0	5.05	5.1

The limit of justifiable expenditure to reduce the rise and fall by f feet is $\frac{K_1}{r}$, where r is the going rate of interest which should be somewhat larger than the rate of the company's bonds, and in the formula is to be expressed as a decimal, *i.e.*, 8 per cent = 0.08.

3. Curvature. — If C be the train mile cost and N the number of daily trains (all trains both ways) the annual operating cost saved by eliminating D degrees of curvature is found as follows, the result being in dollars:

$$K_2 = DC$$
 (0.11 $N + 2.55$),

and the limit of justifiable expenditure to eliminate D° of curvature is $\frac{K_2}{r}$, in which r is the going rate of interest expressed as a decimal and should be somewhat larger than that carried by the company's bonds.

4. Ruling Grade. — This is the most important of the four elements of location. The value of reducing the ruling grade from one rate to another is found by finding the saving in train miles due to the larger loads possible on the lighter grades and is assumed to be approximately proportional to the reduction in number of train miles. The ruling grade determines the weight of train for the whole operating division on which the grade occurs. The relative number of trains on two different ruling grades are assumed to be inversely as the loads behind the tender. To find the load behind the tender see page 259. If W be the train weight for ruling grade g and g and g be the train weight for ruling grade g and g and g be the train weight for ruling grade g and

given business on g', the number of trains to do the same business on g will be

$$N = \frac{W'}{W} N'.$$

If g' is steeper than g, the saving in daily trains one way will be N' - N, and the total train miles saved will be 2 (N' - N) L, L being the length of the division in miles. Having found this, substitute in the following formula for annual saving due to reduction in ruling grade from g' to g, C being the train mile cost on g'.

$$K_3 = 730 LC \left(0.43 (N' - N) - \frac{W - W'}{10 W'} N \right).$$

The N's of the foregoing discussion include only those full weight trains affected by the change. If the grade reduction is obtained at the expense of distance the extra distance should be figured against the improvement considering all trains to be run on the g grade and a train mile cost somewhat larger than C, say $\left(1 + \frac{W}{20\ W'}\right)C$, which supposes that about half the total trains may be affected. Precision is impossible. If rise and fall is reduced by the change the reduction should be credited to the change considering all trains for the g' grade at a train mile cost of C.

Table XXXV gives the relative number of trains for a consolidation locomotive for various grades. To use it for a reduction from an 0.8 per cent grade to a 0.6 per cent grade, there being 10 daily trains on the 0.8 per cent grade, divide the tabular quantity under 12 miles opposite 0.8 by that opposite 0.6 and multiply by 10. In any problem the maximum hauling capacity would probably be considered and hence the lower speeds. For fast freights slightly higher speeds may be considered. The limit of justifiable expenditure to reduce the ruling grade of the division from g' to g is $\frac{K_3}{r}$, in which r is the going interest rate expressed as a decimal and should be somewhat larger than the nominal rate carried by the company's bonds.

Cost of Pusher Service. — When helper engines must be maintained at intermediate points on a line the annual cost in dollars may be estimated as follows if the helpers can be kept busy:

$$K_4 = 155 \cdot N \cdot M,$$

in which N is the number of trains helped daily and M is the length of the pusher incline in miles. If the helper engine is not kept busy, say, making 100 miles a day, the part of 100 miles not run may be estimated to cost half as much per mile as the miles that are run.

TABLE XXXI. — VELOCITY HEADS IN FEET FOR SPEED IN MILES PER HOUR

Formula: $h = 0.035 s^2$

Speed.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
	0.00	0.00	0.00	0.00	0.01	0.01	0.01	0.02	0.02	0.03
1	0.03	0.04	0.05	0.06	0.07	0.08	0.09	0.10	0.11	0.13
2	0.14	0.15	0.17	0.19	0.20	0.22	0.24	0.26	0.27	0.29
3	0.31	0.34	0.36	0.38	0.40	0.43	0.45	0.48	0.51	0.53
4 5	0.56 0.87	0.59	0.02	0.03	1.02	1.06	0.74 1.10	0.77	0.81	0.84 I.22
6	1.26	1.30	1.35	1.39	1.43	1.48	1.52	1.57	1.62	1.67
7	1.72	1.76	1.81	1.87	1.92	1.97	2.02	2.08	2.13	2.18
8	2.24	2.30	2.35	2.41	2.47	2.53	2.59	2.65	2.71	2.77
9	2.84	2.90	2.96	3.03	3.09	3.16	3.23	3.29	3.36	3.43
10 11	3.50 4.24	3.57 4.31	3.64	3.71 4.47	3.79 4.55	3.86	3.93 4.71	4.01 4.79	4.08	4.16 4.96
12	5.04	5.12	5.21	5.29	5.38	5.47	5.56	5.65	5.73	5.82
13	5.91	6.01	6.10	6.19	6.28	6.38	6.47	6.57	6.66	6.76
14	6.86	6.96	7.06	7.16	7.26	7.36	7.46	7.56	7.67	7.77
15	7.87	7.98	8.09	8.19	8.30	8.41	8.52	8.63	8.74	8.85
16 17	8.96 10.11	9.07	9.18	9.30	9.41	9.53 10.72	9.64 10.84	9.76 10.97	9.88	10.00 II.2I
18	11.34	II.47	11.59	11.72	11.85	11.98	12.11	12.24	12.37	12.50
19	12.64	12.77	12.90	13.04	13.17	13.31	13.45	13.58	13.72	13.86
20	14.00	14.14	14.28	14.42	14.57	14.71	14.85	15.00	15.14	15.29
21	15.44	15.58	15.73	15.88	16.03	16.18	16.33	16.48	16.63	16.79
22	16.94	17.10	17.25	17.41	17.56	17.72	17.88	18.03	18.19	18.35
23	18.52	18.68	18.84	19.00	19.17	19.33	19.50	19.66	19.82	19.99
24 25	20.16 21.88	20.33	20.50	20.67	20.84	21.01	21.18 22.94	21.35 23.12	21.53	21.70 23.48
26	23.66	23.84	24.03	24.21	24.40	24.58	24.77	24.95	25.14	25.33
27	25.52	25.70	25.90	26.09	26.28	26.47	26.66	26.86	27.05	27.25
28	27.44	27.64	27.83	28.03	28.23	28.43	28.63	28.83	29.03	29.23
29	29.44	29.64	29.84	30.05	30.25	30.46	30.67	30.88	31.08	31.29
30 31	31.50 33.64	31.71	31.92 34.07	32.I3 34.29	32.35 34.51	32.56 34.73	32.78 34.96	32.98 35.18	33.20	33.42 35.62
32	35.84	36.06	36.29	36.52	36.74	36.97	37.19	37.42	35.40 37.65	37.88
33	38.11	38.34	38.58	38.81	39.05	39.27	39.51	39.75	39.98	40.22
34	40.46	40.70	40.94	41.18	41.42	41.66	41.90	42.14	42.38	42.63
35	42.87	43.12	43.37	43.61	43.86	44.11	44.36	44.61	44.86	45.11
36	45.36	45.61	45.87	46.12	46.38	46.63	46.88	47.14	47.40	47.66
37 38	47.9I 50.54	48.18 50.81	48.43	48.70 51.34	48.96	49.22 51.88	49.48 52.16	49.74 52.42	50.0I 52.69	50.28 52.96
39	53.24	53.51	53.78	54.06	54.34	54.61	54.89	55.17	55.44	55.72
35	0.0	I.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0
40	56.00	58.84	61.74	64.72	67.76	70.88	74.06	77.32	80.64	84.03
50 60	87.50 126.00	91.03	94.64	98.31	102.06	105.77	109.75	113.72	117.74	121.83 166.63
70	171.50	130.23	134.54	138.92 186.52	143.36	147.87	152.45	157.11 207.52	161.84 212.94	218.42
80	224.00	229.60	235.33	241.10	246.95	257.88	258.84	264.9I	271.04	218.42
90	283.50	289.82	296.23	302.70	309.25	315.86	322.55	329.31	336.15	343.05
100	350.00									

Note. — For the table the theoretical heads have been increased 4.63 per cent to allow for the energy of the rotating wheels.

TABLE XXXII.—Train Resistance at Different Speeds and for Trains of Various Average Car Weights

Speed,				Tr	ain r e	sistan	ce, po	unds j	per to	n *				Speed,
miles per hour	15 tons	20 tons	25 tons	30 tons	35 tons	40 tons	45 tons	50 tons	55 tons	60 tons	65 tons	70 tons	75 tons	miles per hour
5	7.6	6.8	6.0	5·4	4.8	4·4	4.0	3.7	3·5	3·3	3.2	3.1	3.0	5
6	7.7	6.9	6.1	5·5	4.9	4·4	4.1	3.8	3·5	3·3	3.2	3.1	3.0	6
7	7.8	7.0	6.2	5·5	5.0	4·5	4.1	3.8	3.6	3·4	3.2	3.1	3.1	7
8 9 10	8.0 8.1 8.2 8.3	7.1 7.2 7.3	6.3 6.4 6.5 6.6	5.6 5.7 5.8 5.9	5.0 5.1 5.2 5.3	4.6 4.6 4.7 4.8	4.2 4.2 4.3 4.3	3.9 3.9 4.0	3.6 3.6 3.7 3.7	3.4 3.4 3.5 3.5	3·3 3·3 3·3	3.2 3.2 3.2 3.3	3.I 3.I 3.2	9 10
12	8.4	7.5	6.7	6.0	5.4	4.8	4.4	4.0	3.8	3.6	3·4	3.3	3.3	12
13	8.6	7.6	6.8	6.1	5.5	4.9	4.5	4.1	3.8	3.6	3·5		3.3	13
14	8.7	7.8	6.9	6.2	5.5	5.0	4.5	4.2	3.9	3.7	3·5		3.4	14
15	8.8	7.9	7.0	6.3	5.6	5.1	4.6	4.2	3.9	3.7	3.6	3.5	3.4	15
16	9.0	8.0	7.1	6.4	5.7	5.1	4.7	4.3	4.0	3.8	3.6	3.5	3.5	16
17	9.1	8.1	7.2	6.5	5.8	5.2	4.8	4.4	4.1	3.9	3.7	3.6	3.5	17
18	9.3	8.3	7.4	6.6	5.9	5.3	4.8	4.5	4.1	3.9	3.7	3.7	3.6	18
19 20 21 22	9.4 9.6 9.7 9.9	8.4 8.5 8.7 8.8	7.5 7.6 7.7 7.9	6.7 6.8 6.9	6.0 6.1 6.2 6.3	5.4 5.5 5.6 5.7	4.9 5.0 5.1 5.2	4.5 4.6 4.7 4.8	4.2 4.3 4.3 4.4	4.0 4.0 4.1 4.2	3.8 3.9 3.9 4.0	3.7 3.8 3.9 3.9	3.6 3.7 3.8 3.8	19 20 21 22
23	10.0	9.0	8.0	7.I	6.4	5.8	5.3	4.9	4.5	4.3	4.I	4.0	3.9	23
24	10.2	9.1	8.1	7.3	6.6	5.9	5.4	4.9	4.6	4.3	4.2	4.1	4.0	24
25	10.4	9.3	8.3	7.4	6.7	6.0	5.5	5.0	4.7	4.4	4.2	4.1	4.0	25
26 27 28 29	10.5 10 7 10.9	9.4 9.6 9.7 9.9	8.4 8.5 8.7 8.8	7.5 7.7 7.8 7.9	6.8 6.9 7.0	6.1 6.2 6.3 6.5	5.6 5.7 5.8 5.9	5.1 5.2 5.3 5.4	4.8 4.8 4.9	4.5 4.6 4.7 4.8	4.3 4.4 4.5 4.6	4.3 4.4 4.5	4.1 4.2 4.3 4.4	26 27 28 29
30	11.3	10.0	9.0	8.0	7·3	6.6	6.0	5.5	5.1	4.9	4.7	4.5	4.5	30
31	11.4	10.2	9.1	8.2	7·4	6.7	6.1	5.6	5.2	5.0	4.8	4.6	4.5	31
32	11.6	10.4	9.3	8.3	7·5	6.8	6.2	5.8	5.3	5.0	4.9	4.7	4.6	32
33	11.8	10.5	9.4	8.5	7.6	7.0	6.3	5.9	5·4	5.2	5.0	4.8	4.7	33
34	12.0	10.7	9.6	8.6	7.8	7.1	6.5	6.0	5·5	5.3	5.1	4.9	4.8	34
35	12.3	10.9	9.7	8.8	7.9	7.2	6.6	6.1	5·7	5.4	5.2	5.0	4.9	35
36	12.5	11.1	9.9	8.9	8.0	7.4	6.7	6.2	5.8	5.5	5.3	5.1	5.0	36
37	12.7	11.2	10.0	9.0	8.2	7.5	6.9	6.4	5.9	5.6	5·4	5.2	5.1	37
38	12.9	11.4	10.2	9.2	8.3	7.6	7.0	6.5	6.0	5.7	5·5	5.3	5.2	38
39	13.1	11.6	10.4	9.4	8.5	7.8	7.1	6.6	6.2	5.8	5.6	5.4	5.3	39
40	13.4	11.8	10.6	9.5	8.6	7.9	7.3	6.8	6.3	6.0	5·7	5.6	5.5	40

^{*} Column headings indicate the average car weights.

This table from experiments of Professor Edward C. Schmidt of the University of Illinois. See Transactions of the American Society of Mechanical Engineers for 1910.

TABLE XXXIII

Tractive Effort in Pounds of the Consolidation Locomotive, Having the Characteristics Given Below, for Different Speeds. Nearest 50 Pounds

Speed	0.0	10.0	20.0	30.0
0.0 0.5 1.0 1.5 2.0 3.5 3.0 3.5 4.5 5.0 5.5 6.5 7.0 7.5 8.5 9.0	spunod ooo'oS	50,000 50,000 48,700 44,800 43,100 41,500 38,650 37,350 36,150 35,000 32,950 32,950 32,950 32,950 29,500 28,750	28,000 27,330 26,700 26,050 25,450 24,900 24,350 23,350 22,400 21,950 21,950 21,150 20,750 20,000 19,650 19,300 19,000	18,650 18,330 18,050 17,300 17,500 16,950 16,950 16,500 15,800 15,850 15,150 14,750 14,750 14,750 14,350 14,350 14,350

Consolidation locomotive.
Weight on drivers: 210,000 pounds.
Weight of engine and tender: 400,000 pounds.
Cylinders: 28" diam. by 32" stroke.
Heating surface: 3837 sq. ft.
Diameter drive wheels: 63".

Boiler working pressure: 163 pounds.

For this locomotive:

 $T_e = 55,174$ pounds (say 55,000 pounds);

 $T_a = 49,412$ pounds (say 50,000 pounds);

 $T_b = 50,000$ pounds at II.2 mi./hr., and as T_a limits the effort, this will be taken as constant and equal to 50,000 pounds at speeds below II mi./hr.

TABLE XXXIV

NET LOADS IN TONS OF 2000 POUNDS BEHIND THE TENDER OF THE CONSOLIDATION LOCOMOTIVE OF TABLE XXXIII, ON GIVEN GRADES AT GIVEN SPEEDS

Speed Grade	Under 11 mi	15	20	25	30	35	40
0.00 .05 .10	11430 9234 7736	7918 6468 5458	5400 4467 3800	3873 3246 2787	2908 2464 2131	2224 1905 1660	1718 1487
.15 .20 .25	6650 5825 5177	4714 4142 3690	3300 2911 2600	2435 2158 1934	1872 1665 1495	1467 1310 1179	1305 1159 1039 938
.30 .35 .40	4655 4225 3866	3323 3019 2764	2346 2134 1954	1748 1592 1459	1354 1235 1132	1070 977 896	853 779 715
.45 .50 .55	3560 3297 3068	2546 2358 2194	1800 1667 1550	1345 1245 1158	1043 966 897	826 764 709	659 609 565
.60 .65 .70	2868 2691 2533	2050 1922 1808	1447 1356 1274	1080 1011 949	836 782 733	660 616 577	525 490 457
.75 .80 .85	2331 2391 2263 2148	1706 1613 1529	1274 1200 1133 1073	893 842 795	688 648 611	541 508 478	428 401 376
.90 .95 1.00	2042 1946 1858	1453 1382 1318	1017 967	753 714 678	577 546	450 425 401	353 332 313
.05 .10	1776 1702	1259 1204	920 877 837 800	645 615 586	517 491 466	380 359	295 278 262
.15 .20 .25	1632 1567 1507	1153 1106 1062	765 733	559 534	443 422 402	341 323 306	247 233
.30 .35 .40	1450 1398 1348	982 946	703 675 649	511 489 469	383 365 348	291 276 262	220 208 197
.45 .50 .55	1302 1258 1217	911 879 849	624 600 578	449 431 414	333 318 304	249 237 226	186 175 166
.60 .65 .70	1178 1141 1106	820 793 768	557 537 518	397 382 367	291 278 266	214 204 194	156 147 139
.75 .80 .85	1072 1041 1011	743 720 698	500 483 467	353 340 327	255 244 234	185 176 167	131 123 116
.90 .95 2.00	982 955 929	677 657 637	451 436 422	315 303 292	224 214 205	159 151 143	109 102 96

The average car weight for this table is 45 tons.

TABLE XXXV. — RELATIVE NUMBER OF TRAINS TO DO THE SAME BUSINESS TONNAGE ON DIFFERENT GRADES, FOR DIFFERENT SPEEDS. COMPUTED FROM TABLE XXXIV

Speed Grade	Under 11 mi.	15	20	25	30	35	40
0.00	0.34	0.49	0.72	I.00	1.33	I.74	2.25
0.05	0.42	0.60	0.87	1.19	1.57	2.03	2.60
0.10	0.50	0.71	I.02	1.39	1.81	2.33	2.96
0.15	0.58	0.82	1.17	1.59	2.07	2.64	3.34
0.20	0.66	0.93	1.33	1.79	2.32	2.95	3.72
0.25	0.75	1.05	1.49	2.00	2.59	3.29	4.12
0.30	0.83	1.16	1.65	2.21	2.86	3.61	4.53
0.35	0.92	1.28	1.81	2.43	3.13	3.96	4.96
0.40	1.00	I.40	1.98	2.65	3.42	4.31	5.41
0.45	1.09	I.52	2.15	2.87	3.71	4.68	5.87
0.50	1.17	1.64	2.32	3.11	4.00	5.06	6.35
0.55	1.26	1.76	2.49	3 · 34	4.31	5 - 45	6.84
0.60	I.35	1.89	2.67	3.58	4.62	5.86	7.36
0.65	I.44	2.01	2.85	3.82	4.94	6.28	7.89
0.70	1.53	2.14	3.03	4.07	5.27	6.70	8.46
0.75	1.62	2.27	3.22	4.33	5.62	7.15	9.03
0.80	1.71	2.40	3.41	4.59	5.97	7.61	9.64
0.85	1.80	2.53	3.60	4.86	6.33	8.09	10.28
0.90	1.89	2.66	3.80	5.13	6.70	8.59	10.95
0.95	1.99	2.80	4.00	5.41	7.08	9.10	11.64
1.00	2.08	2.93	4.20	5.70	7.48	9.64	12.35
1.05	2.18	3.07	4.41	5.99	7.87	10.17	13.10
1.10	2.27	3.21	4.62	6.29	8.30	10.77	13.91
1.15	2.37	3.35	4.83	6.60	8.73	11.34	14.76
1.20	2.47	3.50	5.05	6.92	9.16	11.97	15.65
I.25	2.57	3.64	5.27	7.24	9.62	12.63	16.59
1.30	2.67	3.79	5.50	7 - 57	10.09	13.29	17.57
1.35	2.77	3.94	5.73	7.91	10.59	14.01	18.59
1.40	2.87	4.09	5.96	8.24	II.II	14.76	19.63
1.45	2.97	4.24	6.20	8.61	11.61	15.53	20.79
1.50	3.07	4.40	6.44	8.97	12.16	16.31	22.09
1.55	3.18	4.55	6.69	9.34	12.72	17.11	23.29
1.60	3.28	4.71	6.94	9.74	13.29	18.07	24.78
1.65	3.39	4.87	7.20	10.12	13.91	18.95	26.30
I.70	3.50	5.03	7.46	10.53	14.53	19.93	27.82
1.75	3.61	5.20	7.73	10.95	15.16	20.90	29.51
1.80	3.71	5.37	8.00	11.37	15.84	21.97	31.43
1.85	3.82	5 - 54	8.28	11.82	16.52	23.15	33 - 33
1.90	3.94	5.71	8.57	12.27	17.26	24.32	35 - 47
1.95	4.05	5.88	8.87	12.76	18.07	25.60	37.90
2.00	4.16	6.07	9.16	13.24	18.86	27.04	40.27

TABLE XXXVI. — Pusher Grades

The tabular quantities are pusher grades for the through grades indicated at the side and top of table. Computed for the Consolidation Engine of Table XXXIII.

Through grade	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.0 I.0 2.0	0.187 1.889 3.359	0.369						1.404 2.939		

Feet		·	Feet		T .:	Feet	ъ.	, ,.	Feet	-	
per	Feet	Incli- nation.	per	Feet per	Incli- nation,	per	Feet per	Incli- nation.	per	Feet per	Incli- nation,
sta- tion	mile	deg.	sta- tion	mile	deg.	sta- tion	mile	deg.	sta- tion	mile	deg.
00	.000	.000	50	26.400	.286	1.00	52.800	.573	1.50	79.200	.859
0I 02	.528 1.056	.006	51 52	26.928 27.456	.292	I.01 I.02	53.328 53.856	.579 .584	1.51	79.728 80.256	.865
	1.584	1	53	27.984	.304	1.03	54.384	1	1.52	80.784	
03 04	2.112	.017	53 54	28.512	.304	I.04	54.912	.596	I.53	81.312	.877 .882
05	2.640		55	29.040	.315	1.05	55.440		1.55	81.840	.888
06	3.168		56	29.568	.321	1.06	55.968	1	1.56	82.368	.894
07	3.696		57	30.096	.327	1.07	56.496	.613	1.57	82.896	.899
08	4.224	.046	58	30.624	.332	1.08	57.024	.619	1.58	83.424	.905
09	4.752		59	31.152	. 338	1.09	57.552		1.59	83.952	.911
10	5.280		60	31.680		1.10	58.080	.630	1.60	84.480	.917
11	5.808	_	61	32.208	.349	I.II	58.608	1	1.61	85.008	.922
12	6.336	1	62	32.736		1.12	59.136		1.62	85.536	.928
13 14	6.864 7.392	.074	63 64	33.264 33.792	.361	1.13	59.664 60.192	.648	1.63	86.064 86.592	.934
1 1	7.920		65	34.320	1	1.15	60.720	1	1.65	87.120	.939
15 16	8.448		66	34.848	.378	1.15	61.248		1.66	87.120	·945 ·951
17	8.976		67	35.376	.384	1.17	61.776	.670	1.67	88.176	.957
18	9.504	.103	68	35.904	.390	1.18	62.304	.676	1.68	88.704	.962
19	10.032		69	36.432		1.19	62.832	.682	1.69	89.232	.968
20	10.560	.115	70	36.960	.401	1.20	63.360	.688	1.70	89.760	.974
21	11.088		71	37.488		1.21	63.888		1.71	90.288	.980
22	11.616	1	72	38.016		1.22	64.416		1.72	90.816	.985
23	12.144	1	73	38.544		1.23	64.944)	1.73	91.344	.991
24	12.672		74	39.072		1.24	65.472 66.000	.710 .716	1.74	91.872	.997
25 26	13.200 13.728		75 76	39.600 40.128		1.25	66.528		1.75	92.400 92.928	I.002 I.008
27	14.256		77	40.656	1	1.27	67.056		1.77	93.456	
28	14.230		78	41.184		1.28	67.584		1.78	93.430	1.020
29	15.312		79	41.712		1.29	68.112	-739	1.79	94.512	1.026
30	15.840	.172	80	42.240	. 458	1.30	68.640	.745	1.80	95.040	1.031
31	16.368		81	42.768	. 464	1.31	69.168		1.81	95.568	1.037
32	16.896		82	43.296		1.32	69.696	1	1.82	96.096	1.043
33	17.424		83	43.824	.476	1.33	70.224		1.83	96.624	1.048
34	17.952	.195	84	44.352 44.880	.481	1.34	70.752 71.280		1.84	97.152 97.680	1.054
35	18.480	Į l	85 86			1.35 1.36	71.808	·773	1.86	98.208	
36 37	19.008 19.536	1	87	45.408 45.936	.493 .498	1.30	72.336	.779	1.80	98.736	1.066
38	20.064	, ,	88	46.464	.504	1.38	72.864	.791	1.88	99.264	1.077
39	20.592		89	46.992	.510	1.39	73.392	.796	1.89	99.792	1.083
40	21.120		90	47.520	.516	1.40	73.920	.802	1.90	100.320	1.089
41	21.648	.235	91	48.048	.521	1.41	74.448	.808	1.91	100.848	1.094
42	22.176		92	48.576		1.42	74.976	.814	1.92	101.376	1.100
43	22.704		93	49.104	.533	1.43	75.504	.819	1.93	101.904	1.106
44	23.232		94	49.632	-539	1.44	76.032	.825	1.94	102.432	I.III
45	23.760		95	50.160	-544	1.45	76.560	.831 .836	1.95	102.960	1.117
46 47	24.288 24.816		96 9 7	50.688 51.216	.550	1.46	77.088 77.616	.842	1.96 1.97	103.488 104.016	I.123 I.129
47	25.344	1	98	51.744	.561	1.48	78.144	.848	1.98	104.544	1.134
40 49	25.344		99	52.272	.567	1.49	78.672	.854	1.99	104.544	I.134 I.140
50	26.400		1.00	52.800	.573	1.50	79.200		2.00	105.600	1.146
ب		(_					

CHAPTER V

ESTIMATING AND CONSTRUCTION TABLES

TABLE XXXVIII

Relative prices in place that can be paid for articles for the same purpose lasting N and N' years. The article lasting N years is assumed to cost \$1.00 or one unit. Interest 4 per cent.

Example. — If a lasts 10 years and costs 50 cents, there may be paid for b lasting 7 years 50 \times 0.74 = 37 cents.

		_		_	_		_	_	_	_	37	A
\setminus N		1	1	_	- 1		1				N	Amount
	5	6	7	8	9	10	11	12	13	14	/ 27/	\$1.00 at
N'		- !										comp'd int.
5	1.00	0.85	0.74	0.66	0.60	0.55	0.51	0.47	0.45	0.42		1.21665
6	1.18	1.00	0.87	0.78	0.70	0.65	0.60	0.56	0.52	0.50	6	1.26532
7	1.35	1.14	1.00	0.89	0.81	0.74	0.69	0.64	0.60	0.57		1.31593
8	1.51	1.28	1.12	1.00	0.91	0.83	0.77	0.72	0.67	0.64		1.36857
9	1.67	1.42	1.24	1.10	1.00	0.92	0.85	0.79	0.74	0.70		1.42331
10	1.82	1.55	1.35	1.20	1.09	1.00	0.93	0.86	0.81	0.77		1.48024
11	1.97	1.67	1.46	1.30	1.18	1.08	1.00	0.93	0.88	0.83		1.53945
12	2.11	1.79	1.56		1.26	1.16	1.07	1.00	0.94	0.89	12	1.60103
13	2.43	1.90	1.66	1.48	1.34	1.23	1.14	1.06	1.00	0.95	13	1.66507
14	2.37	2.01	1.76	1.57	1.42	1.30	1.21	1.13	1.06	1.00	14	1.73167
15	2.50	2.12	1.85		1.50	1.37	1.27	1.18	1.11	1.05		1.80094
16	2.62	2.22	1.94		1.57	1.44	1.33	1.24	1.17	1.10	16	1.87297
17	2.73	2.32	-		1.64	1.50	1.39	1.30	1.22	1.15		1.94790
18	2.84	2.41	2.11	1.88	1.70	1.56	1.44	1.35	1.27	1.20	18	2.02581
19	2.95	2.50	2.19	1.95	1.77	1.62	1.50	1.40	1.32	1.24	19	2.10685
20	3.05	2.59	2.26		1.83	1.68	1.55	1.45	1.36	1.29	20	2.19112
21	3.15	2.68					1.60	1.49	1.40	1.33	21	2.27876
22	3.25	2.76		1				1.54	1.45	1.37	22	2.36991
23	3.34	2.83						1.58	1.49	1.41	23	2.46471
24	3.42	2.91			2.05	1.88	1.74	1.62	1.53	1.44	24	2.56330
25	3.51	2.98			_		1.78	1.66	1.56	1.48	25	2.66583
ستنسا	5.5-			-	_		_					

TABLE XXXVIII. — (Continued)

N' N	15	16	17	18	19	20	21	22	23	24	25	$N_{N'}$
5	0.40	0.38	0.37	0.35	0.34	0.33	0.32	0.31	0.30	0.29	0.28	5
6	0.47	0.45	0.43	0.41	0.40	0.39	0.37	0.36	0.35	0.34	0.34	6
7	0.54	0.52	0.49	0.47	0.46	0.44	0.43	0.42	0.40	0.39	0.38	7
8	0.61	0.58	0.55	0.53	0.51	0.50	0.48	0.47	0.45	0.44	0.43	8
9	0.67	0.64	0.61	0.59	0.57	0.55	0.53	0.51	0.50	0.49	0.48	9
10	0.73	0.70	0.67	0.64	0.62	0.60	0.58	0.56	0.55	0.53	0.52	10
11	0.79	0.75	0.72	0.69	0.67	0.64	0.62	0.61	0.59	0.57	0.56	11
12	0.84	0.81	0.77	0.74	0.71	0.69	0.67	0.65	0.63	0.62	0.60	12
13	0.90	0.86	0.82	0.79	0.76	0.73	0.71	0.69	0.67	0.65	0.64	13
14	0.95	0.91	0.87	0.83	0.80	0.78	0.75	0.73	0.71	0.69	0.68	14
15	1.00	0.95	0.91	0.88	0.85	0.82	0.79	0.77	0.75	0.73	0.71	15
16	1.05	1.00	0.96	0.92	0.89	0.86	0.83	0.81	0.78	0.76	0.75	16
17	1.09	1.04	1.00	0.96	0.93	0.90	0.87	0.84	0.82	0.80	0.78	17
18	1.14	1.09	1.04	1.00	0.96	0.93	0.90	0.88	0.85	0.83	0.81	18
19	1.18	1.13	1.08	1.04	1.00	0.97	0.94	0.91	0.88	0.86	0.84	19
20	1.22	1.17	1.12	1.07	1.03	1.00	0.97	0.94	0.91	0.89	0.87	20
21	1.26	1.20	1.15	1,11	1.07	1.03	I.00	0.97	0.94	0.92	0.90	21
22	1.30	1.24	1.19	1.14	1.10	1.06	1.03	1.00	0.97	0.95	0.92	22
23	1.34	1.27	1.22	1.17	1.13	1.09	1.06	1.03	1.00	0.97	0.95	23
24	1.37	1.31	1.25	1.20	1.16	I.12	1.08	1.06	1.03	1.00	0.98	24
25	1.41	1.34	1.28	1.23	1.19	1.15	I.II	1.08	1.05	I.02	1.00	25

TABLE XXXIX

Relative prices in place that can be paid for articles for the same purpose lasting N and N' years. The article lasting N years is assumed to cost \$1.00 or one unit. Interest 5 per cent.

Example. — If a lasts 10 years and costs 60 cents, there may be paid for b lasting 12 years, $60 \times 1.15 = 79$ cents.

N'	5	6	7	8	9	10	11	12	13	14	N N'	Amount \$1.00 at comp'd int.
5	I.00	0.85					0.52	0.49	0.46			1.27628
6	1.17	1.00	0.88	0.79	0.71	0.66	0.61	0.57	0.54	0.51	6	1.34009
7	I.34	I.I4	1.00	0.90	0.81	0.75	0.70	0.65	0.62	0.58	7	1.40710
8	1.49	1.27	I.I2	1.00	0.91	0.84	0.78	0.73	0.69	0.65	8	1.47745
9	1.64	1.40	1.23	1.10	1.00	0.92	0.86	0.80	0.76	0.72	9	1.55132
10	1.78	1.52	1.33	1.19	1.09	1.00	0.93	0.87	0.82	0.78	10	1.62889
11	1.92	1.64	1.44	1.29	1.17	1.08	1.00	0.94	0.88	0.84	11	1.71034
12	2.05	1.75	I.53	I.37	I.25	1.15	1.07	1.00	0.94	0.90	12	1.79585
13	2.17	1.85	1.62	1.45	I.32	I.22	1.13	1.06	1.00	0.95	13	1.88564
14	2.29	1.95	1.71	1.53	1.39	1.28	1.19	I.I2	1.05	1.00	14	1.97993
15	2.40	2.04	1.79	1.61	1.46	1.34	1.25	1.17	1.10	1.05	15	2.07892
16	2.50	2.14	1.87	1.68	I.52	1.40	1.30	1.22	1.15	1.09	16	2.18287
17	2.60	2.22	1.95	1.74	1.59	1.46	1.36	1.27	1.20	1.14	17	2.29202
18	2.70	2.30	2.02	1.81	1.64	1.51	1.41	1.32	I.24	1.18	18	2.40662
19	2.79	2.38	2.09	1.87	1.70	1.56	1.45	1.36	I.29	I.22	19	2.52695
20	2.88	2.46	2.15	1.93	1.75	1.61	1.50	1.41	1.33	1.25	20	2.65330
21	2.96	2.53	2.22	1.98	1.80	1.66	1.54	I.45	1.36	I.29	21	2.78596
22	3.04	2.59	2.27	2.04	1.85	1.70	1.58	I.49	1.40	1.33	22	2.92526
23	3.12	2.66	2.33	2.09	1.90	1.75	1.62	I.52	1.44	1.36	23	3.07152
24	3.19	2.72	2.38	2.13	1.94		1.66	1.56	1.47	I.39	24	3.22510
25	3.26	2.78	2 44	2.18	1.98	1:83	I-70	1.59	I 50	I.42	25	3.38635

TABLE XXXIX. - (Continued)

.V.	15	16	17	18	19	20	21	22	23	24	25	$N_{N'}$
5 6	0.42	0.40	0.38	0.37	0.36	0.35	0.34	0.33	0.32	0.31	0.31	5 6
7	0.56	0.53	0.51	0.49	0.48	0.46	0.45	0.44	0.43	0.42	0.41	7
8	0.62	0.60	0.57	0.55	0.53	0.52	0.50	0.49	0.48	0.47	0.46	8
9 10	0.68	0.66	0.63	0.61	0.59	0.57	0.55	0.54	0.53	0.52	0.50	9 10
11	0.80	0.77	0.74	0.71	0.69	0.67	0.65	0.59	0.62	0.60	0.55	11
12	0.85	0.77	0.74	0.76	0.73	0.07	0.69	0.67	0.66	0.64	0.59	12
13	0.90	0.87	0.83	0.80	0.78	0.75	0.73	0.71	0.70	0.68	0.67	13
14	0.95	0.91	0.88	0.85	0.82	0.79	0.77	0.75	0.73	0.72	0.70	14
15	1.00	0.96	0.92	0.89	0.86	0.83	0.81	0.79	0.77	0.75	0.74	15
16	1.04	1.00	0.96	0.93	0.90	0.87	0.85	0.82	0.80	0.79	0.77	16
17	1.09	I.04	1.00	0.96	0.93	0.90	0.88	0.86	0.84	0.82	0.80	17
18 19	1.13	1.08	I.04 I.07	I.00 I.03	0.97 1.00	0.94	0.91	0.89	0.87	0.85	0.83	18 19
20	1.20	1.12	1.11	1.03	1.03	1.00	0.94	0.92	0.90	0.90	0.88	20
21	I.24	1.15	1.11	1.10	1.03	1.03	1.00	0.95	0.92	0.93	0.91	21
22	1.27	I.2I	1.17	1.13	1.09	1.06	1.03	1.00	0.98	0.95	0.93	22
23	1.30	I.24	1.20	1.15	I.I2	1.08	1.05	1.02	1.00	0.98	0.96	23
24	1.33	1.27	1.22	1.18	1.14	1.11	1.08	1.05	1.02	1.00	0.98	24
25	1.36	I 30	1.25	1.21	I.I7	1.13	I.IO	1.07	I.04	I.02	I.00	25

Volumes of Triangular Prisms. — Table XL. In railroad earth-work the volume of a given length of cut or fill is given by the average end area method as $l \times \frac{A_1 + A_2}{2}$ in which l is the length, usually 100 feet, and A_1 and A_2 are the cross-section areas at the two ends. This is equivalent to $\frac{l}{2}A_1 + \frac{l}{2}A_2$ and Table XL is made on this basis with 100 for l. Hence the volumes are for 50-foot lengths and are to be used twice, once on one side of a station section for the part of the station

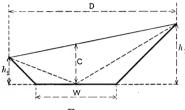


FIG. 25.

volume on that side, and once on the other side as part of the station volume on that side.

The commonest formula for the cross-section area of a 3-level section is $A = \frac{c}{2}D + \frac{w}{4}$ $(h_1 + h_2)$. This is equivalent to the area of two triangles of bases c and $\frac{w}{2}$ and altitudes D and $h_1 + h_2$ or it may be taken as three triangles of bases D and $\frac{w}{2}$ and altitudes c, h_1 and h_2 .

Whence the volume in cubic yards for a 50-foot length is

$$V_{50} = 50 \frac{c}{2 \times 27} D + 50 \frac{w}{4 \times 27} (h_1 + h_2)$$
$$= \frac{25}{27} cD + \frac{25}{27} \frac{w}{2} (h_1 + h_2).$$

D is the sum of the slope stake distances. The table is made to give the quantity $\frac{2}{2}\frac{\pi}{2} \cdot x \cdot y$, in which x is the base or altitude and y is the altitude or base of the triangular base or end of a triangular prism.

In using the table for such work the x numbers at the side of the page should be used for heights c and $\frac{w}{2}$ and the y numbers at the top for D and $h_1 + h_2$. The quantities are given for only whole numbers of y

from I to 9 inclusive, but are given to hundredths so that for y = 50 or 70, etc., ten times the tabular values for 5 or 7, etc., are taken and for y = 0.5 and 0.7, etc., one-tenth the tabular values for 5 and 7 are taken.

Example. — The cross-section notes of two stations show

Sta.
 L
 C
 R

$$762$$
 $\frac{-3.6}{13.6}$
 -4.2
 $\frac{-5.3}{15.3}$
 763
 $\frac{-4.8}{14.8}$
 -5.7
 $\frac{-6.4}{16.4}$

the minus sign indicating a cut. The volume between stations 762 and 763 is had from the tables as follows:

For 762.
$$D = 13.6 + 15.3 = 28.9$$
, done mentally,
 $c = 4.2$,
 $w = 20$, $\frac{w}{2} = 10$,
 $h_1 + h_2 = 8.9$.

From Table XL opposite
$$x = 4.2$$
 under 2 take 10 \times 7.78 = 77.8

$$\frac{w}{2}$$
 = 10 : opposite x = 10.0 under 8 take 1 \times 74.00 = 74.00

under 9
$$\frac{1}{10} \times 83.33 = 8.33$$

Total $194.8 = 194.8$

For 763.
$$D = 14.8 + 16.4 = 31.2$$
,
 $c = 5.7$,
 $w = 20$, $\frac{w}{2} = 10$,
 $h_1 + h_2 = 11.2$.

Opposite
$$x = 5.7$$
 take $10 \times 15.83 = 158.3$
 $1 \times 5.28 = 5.3$
 $\frac{1}{10} \times 10.56 = 1.1$
 $\frac{70}{2} = 10$.

: opposite
$$x = 10$$
 take $10 \times 9.72 = 97.2$
 $1 \times 9.72 = 9.7$
 $\frac{1}{10} \times 19.44 = \frac{1.9}{273.5}$
Total for sta.

273.5 468.3

If the length between two sections is 50 feet, take $\frac{1}{2}$ the result from the tables; if 40 feet, take $\frac{4}{10}$ the result, and so on. For a single right

prism of any length take that portion of the tabular quantity that the length is of 50.

Prismoidal Correction. — Table XLI. To get the volume of a station of earthwork by the prismoidal formula, get it by the average end area method and subtract the prismoidal correction. That is, get the volume from Table XL, and subtract the correction of Table XLI. The correction is for full stations of 100 feet; for shorter lengths use proportional parts of the tabular quantities. The arguments of the table $C_1 - C_0$ and $D_1 - D_0$ are the differences in center heights and total widths respectively of the two end sections.

Level Section Volumes. — Table XLII. This table is used only in preliminary estimates and gives the volumes in cubic yards for 100-foot lengths for varying center heights. Its use will be evident.

TABLE XL. — Volumes of Triangular Prisms 50 Feet in Length

X	I	2	3	4	5	6	7	8	9	Y_X
.1	.09	. 19	.28	-37	.46	.56	.65	.74	.83	.1
.2	.19	.37	.56	.74	.93	1.11	1.30	1.48	1.67	.2
-3	. 28	.56	.83	I.II	1.39	1.67	1.94	2.22	2.50	-3
-4	-37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	-4
.5	.46	.93	1.39	1.85	2.31	2.78	3.24	3.70	4.17	-5
.6	. 56	I.II	1.67	2.22	2.78	3.33	3.89	4.44	5.00	.6
-7	.65	1.30	1.94	2.59	3.24	3.89	4.54	5.19	5.83	.7
.8 .9	·74 .83	1.48 1.67	2.22	2.96 3.33	3.70 4.17	4 · 44 5 · 00	5.19 5.83	5.93 6.67	6.67 7.50	.8 .9
1.0	-93	1.85	2.78	3.70	4.63	5.56	6.48	7.41	8.33	1.0
	I.02	2.04			5.09	6.11		8.15		
. I . 2	1.02	2.04	3.06	4.07	5.56	6.67	7.13 7.78	8.89	9.17 10.00	. I . 2
.3	1.20	2.41	3.61	4.81	6.02	7.22	8.43	9.63	10.83	.3
.4	1.30	2.59	3.89	5.19	6.48	7.78	9.07	10.37	11.67	-4
-5	I.39	2.78	4.17	5.56	6.94	8.33	9.72	II.II	12.50	-5
.6	1.48	2.96	4.44	5.93	7.41	8.89	10.37	11.85	13.33	.6
.7	1.57	3.15	4.72	6.30	7.87	9.44	11.02	12.59	14.17	.7
.8	1.67	3.33	5.00	6.67	8.33	10.00	11.67	13.33	15.00	.8
.9	1.76	3.52	5.28	7.04	8.80	10.56	12.31	14.07	15.83	.9
2.0	1.85	3.70	5.56	7.41	9.26	II.II	12.96	14.81	16.67	2.0
ı.	I.94	3.89	5.83	7.78	9.72	11.67	13.61	15.56	17.50	. І
.2	2.04	4.07	6.11	8.15 8.52	10.19	12.22 12.78	14.26 14.91	16.30 17.04	18.33	.2
.3	- 1		6.67							.3
.4 .5	2.22 2.3I	4.44	6.94	8.89 9.26	II.II II.57	13.33	15.56 16.20	17.78 18.52	20.00	.4 .5
.6	2.41	4.81	7.22	9.63	12.04	14.44	16.85	19.26	21.67	.6
7	2.50	5.00	7.50	10.00	12.50	15.00	17.50	20.00	22.50	.7
.8	2.59	5.19	7.78	10.37	12.96	15.56	18.15	20.74	23.33	.8
.9	2.69	5.37	8.06	10.74	13.43	16.11	18.80	21.48	24.17	.9
3.0	2.78	5.56	8.33	II.II	13.89	16.67	19.44	22.22	25.00	3.0
ı.	2.87	5.74	8.61	11.48	14.35	17.22	20.09	22.96	25.83	ı.
. 2	2.96	5.93	8.89	11.85	14.81	17.78	20.74	23.70	26.67	.2
.3	3.06	6.11	9.17	12.22	15.28	18.33	21.39	24.44	27.50	-3
-4	3.15	6.30	9.44	12.59	15.74	18.89	22.04	25.19	28.33	-4
·5 ·6	3.24	6.48	9.72	12.96	16.20 16.67	19.44	22.69 23.33	25.93 26.67	29.17 30.00	.5 .6
.7	3.43	6.85	10.28	13.70	17.13	20.56	23.98	27.41	30.83	.7
.8	3.52	7.04	10.26	13.70	17.13	21.11	24.63	28.15	31.67	.8
.9	3.61	7.22	10.83	14.44	18.06	21.67	25.28	28.89	32.50	.9
4.0	3.70	7.41	II.II	14.81	18.52	22.22	25.93	29.63	33.33	4.0
ı.	3.80	7.59	11.39	15.19	18.98	22.78	26.57	30.37	34.17	.ı
. 2	3.89	7.78	11.67	15.56	19.44	23.33	27.22	31.11	35.00	.2
.3	3.98	7.96	11.94	15.93	19.91	23.89	27.87	31.85	35.83	-3
4	4.07	8.15	12.22	16.30	20.37	24.44	28.52	32.59	36.67	-4
.5 .6	4.17	8.33	12.50	16.67	20.83	25.00	29.17	33.33	37.50	·5
	4.26	8.52	12.78	17.04	21.30	25.56	29.81	34.07	38.33	.6
.7 .8	4 · 35 4 · 44	8.70 8.89	13.06 13.33	17.41 17.78	21.76	26.11 26.67	30.46 31.11	34.81 35.56	39. 17 40.00	.7 .8
.9	4.44	9.07	13.33	18.15	22.22	27.22	31.11	36.30	40.83	.9
5.0	4.63	9.26	13.89	18.52	23.15	27.78	32.41	37.04	41.67	5.0
	7.03	3.20	-3.09	20.32	23.13	21.10	32.41	37.54	42.07	-

Y										Y
$X \setminus$	I	2	3	4	5	6	7	8	9	\angle_X
5.1	4.72	9.44	14.17	18.89	23.61	28.33	33.06	37.78	42.50	5.1
.2	4.81	9.63	14.44	19.26	24.07	28.89	33.70	38.52	43.33	.2
-3	4.91	9.81	14.72	19.63	24.54	29.44	34.35	39.26	44.17	.3
.4	5.00	10.00	15.00	20.00	25.00 25.46	30.00 30.56	35.00 35.65	40.00 40.74	45.00 45.83	-4
.5 .6	5.19	10.19	15.26	20.74	25.40	31.11	36.30	41.48	46.67	.5 .6
.7	5.28	10.56	15.83	21.11	26.39	31.67	36.94	42.22	47.50	.7
.8	5.37	10.74	16.11	21.48	26.85	32.22	37.59	42.96	48.33	.8
.9	5.46	10.93	16.39	21.85	27.31	32.78	38.24	43.70	49.17	.9
6.0	5.56	11.11	16.67	22.22	27.78	33.33	_38.89	44.44	50.00	6.0
.I .2	5.65 5.74	11.30 11.48	16.94 17.22	22.59 22.96	28.24 28.70	33.89 34.44	39.54 40.19	45.19 45.93	50.83 51.67	.I .2
.3	5.83	11.43	17.50	23.33	29.17	35.00	40.83	46.67	52.50	.3
.4	5.93	11.85	17.78	23.70	29.63	35.56	41.48	47.41	53.33	.4
-5	6.02	12.04	18.06	24.07	30.09	36.11	42.13	48.15	54.17	- 5
.6	6.11	12.22	18.33	24.44	30.56	36.67	42.78	48.89	55.00	.6
.7	6.20	12.41	18.61	24.81	31.02	37.22	43.43	49.63	55.83	.7
.8 .9	6.30 6.39	12.59	18.89 19.17	25.19 25.56	31.48 31.94	37.78 38.33	44.07 44.72	50.37 51.11	56.67 57.50	.8 .9
7.0	6.48	12.96	19.44	25.93	32.41	38.89	45.37	51.85	58.33	7.0
.1	6.57	13.15	19.72	26.30	32.87	39.44	46.02	52.59	59.17	1.1
.2	6.67	13.33	20.00	26.67	33.33	40.00	46.67	53.33	60.00	.2
.3	6.76	13.52	20.28	27.04	33.80	40.56	47.31	54.07	60.83	.3
-4	6.85	13.70	20.56	27.41	34.26	41.11	47.96	54.81	61.67	-4
·5 .6	6.94 7.04	13.89	20.83	27.78 28.15	34.72 35.19	41.67 42.22	48.61 49.26	55.56 56.30	62.50 63.33	.5
.7	7.13	14.07	21.11	28.52	35.65	42.78	49.20	57.04	64.17	.7
.8	7.22	14.44	21.59	28.89	36.11	43.33	50.56	57.78	65.00	.8
.9	7.31	14.63	21.94	29.26	_36.57	43.89	51.20	58.52	65.83	.9
8.0	7.41	14.81	22.22	29.63	37.04	44.44	51.85	59.26	66.67	8.0
. 1	7.50	15.00	22.50	30.00	37.50	45.00	52.50	60.00	67.50	Ι.
.2	7.59 7.69	15.19	22.78	30.37	37.96	45.56 46.11	53.15	60.74 61.48	68.33 69.17	.2
.3	7.78	15.37 15.56	23.06	30.74	38.43 38.89	46.67	53.80 54.44	62.22	70.00	.3
.4 .5	7.87	15.74	23.51	31.48	39.35	47.22	55.09	62.96	70.83	·4 ·5
.6	7.96	15.93	23.89	31.85	39.81	47.78	55.74	63.70	71.67	.6
.7	8.06	16.11	24.17	32,22	40.28	48.33	56.39	64.44	72.50	.7
.8 .9	8.15 8.24	16.30 16.48	24.44	32.59 32.96	40.74 41.20	48.89	57.04 57.69	65.19 65.93	73.33	.8 .9
9.0	8.33	16.67	24.72	33.33	41.67	50.00	58.33	66.67	74.17	9.0
.1	8.43	16.85	25.28	33.70	42.13	50.56	58.98	67.41	75.83	J.U
.2	8.52	17.04	25.56	34.07	42.13	51.11	59.63	68.15	76.67	.2
.3	8.61	17.22	25.83	34.44	43.06	51.67	60.28	68.89	77.50	-3
.4	8.70	17.41	26.11	34.81	43.52	52.22	60.93	69.63	78.33	.4
·5	8.80	17.59	26.39	35.19	43.98	52.78	61.57	70.37	79.17	.5 .6
.6	8.89 8.98	17.78	26.67 26.94	35.56	44.44 44.91	53.33 53.89	62.22 62.87	71.11	80.00	.7
.7 .8	9.07	17.90	20.94	35 · 93 36 · 30	44.91	53.89	63.52	71.85	81.67	.8
.9	9.17	18.33	27.50	36.67	45.83	55.00	64.17	73.33	82.50	.9
10.0	9.26	18.52	27.78	37.04	46.30	55.56	64.81	74.07	83.33	10.0
										L

Y	I	2	3	4	5	6	7	8	9	Y/X
X										
10.1	9.35	18.70	28.06	37.41	46.76	56.11	65.46	74.81	84.17	10.1
.2	9.44 9.54	18.89 19.07	28.33 28.61	37.78 38.15	47.22 47.69	56.67 57.22	66.11 66.76	75.56 76.30	85.00 85.83	.2
.3	9.63	19.26	28.89	38.52	48.15	57.78	67.41	77.04	86.67	.4
-4	9.72	19.44	29.17	38.89	48.61	58.33	68.06	77.78	87.50	-5
.6	9.81	19.63	29.44	39.26	49.07	58.89	68.70	78.52	88.33	.6
.7	9.91	19.81	29.72	39.63	49.54	59.44	69.35	79.26	89.17	.7
.8	10.00	20.00	30.00	40.00	50.00	60.00	70.00	80.00	90.00	.8
.9	10.09	20.19	30.28	40.37	50.46	60.56	70.65	80.74	90.83	.9
11.0	10.19	20.37	30.56	40.74	50.93	61.11	71.30	81.48	91.67	11.0
.I .2	10.28	20.56	30.83	41.11	51.39 51.85	61.67 62.22	71.94 72.59	82.22 82.96	92.50 93.33	.I .2
.3	10.46	20.93	31.39	41.85	52.31	62.78	73.24	83.70	93.33	.3
.4	10.56	21.11	31.67	42.22	52.78	63.33	73.89	84.44	95.00	.4
.5	10.65	21.30	31.94	42.59	53.24	63.89	74.54	85.19	95.83	-5
.6	10.74	21.48	32.22	42.96	53.70	64.44	75.19	85.93	96.67	.6
.7	10.83	21.67	32.50	43.33	54.17	65.00	75.83	86.67	97.50	.7
.8	IO.93 II.02	21.85	32.78 33.06	43.70	54.63 55.09	65.56 66.11	76.48	87.41 88.15	98.33	.8
12.0	II.II	22.22			55.56	66.67	77.13	88.89	100.00	.9 12.0
	II.20	22.41	33.33 33.61	44.44	56.02	67.22	77.78	89.63	100.83	.1
.I .2	11.30	22.41	33.89	45.19	56.48	67.78	79.07	90.37	101.67	. 2
.3	11.39	22.78	34.17	45.56	56.94	68.33	79.72	91.11	102.50	-3
.4	11.48	22.96	34.44	45.93	57.41	68.89	80.37	91.85	103.33	-4
5	11.57	23.15	34.72	46.30	57.87	69.44	81.02	92.59	104.17	-5
.6	11.67	23.33	35.00	46.67	58.33	70.00	81.67	93.33	105.00	.6
.7 .8	11.76	23.52	35.28 35.56	47.04	58.80 59.26	70.56 71.11	82.31 82.96	94.07	105.83	.7
.9	II.94	23.70	35.83	47.4I 47.78	59.72	71.11	83.61	94.81 95.56	100.67	9.9
13.0	12.04	24.07	36.11	48.15	60.19	72.22	84.26	96.30	108.33	13.0
.1	12.13	24.26	36.39	48.52	60.65	72.78	84.91	97.04	109.17	.1
.2	12.22	24.44	36.67	48.89	61.11	73.33	85.56	97.78	110.00	.2
-3	12.31	24.63	36.94	49.26	61.57	73.89	86.20	98.52	110.83	.3
-4	12.41	24.81	37.22	49.63	62.04	74.44	86.85	99.26	111.67	-4
.5 .6	12.50	25.00 25.19	37.50 37.78	50.00	62.50 62.96	75.00 75.56	87.50 88.15	100.00	II2.50 II3.33	.6
.7	12.69	25.37	38.06	50.74	63.43	76.11	88.80	101.48	113.33	.7
.8	12.78	25.56	38.33	51.11	63.89	76.67	89.44	101.48	114.17	.8
.9	12.87	25.74	38.61	51.48	64.35	77.22	90.09	102.96	115.83	.9
14.0	12.96	25.93	38.89	51.85	64.81	77.78	90.74	103.70	116.67	14.0
.I	13.06	26.11	39.17	52.22	65.28	78.32	91.39	104.44	117.50	. І
.2	13.15	26.30	39 44	52.59	65.74	78.89	92.04	105.19	118.33	.2
-3	13.24	26.48	39.72	52.96	66.20	79.44	92.69	105.93	119.17	.3
.4 .5	13.33 13.43	26.67 26.85	40.00	53.33 53.70	66.67 67.13	80.00 80.56	93.33 93.98	106.67	120.00	-4
.6	13.43	27.04	40.56	54.07	67.59	81.11	93.98	107.41	121.67	.5 .6
.7	13.61	27.22	40.83	54.44	68.06	81.67	95.28	108.89	122.50	.7
.8	13.70	27.41	41.11	54.81	68.52	82.22	95.93	109.63	123.33	.8
.9	13.80	27.59	41.39	55.19	68.98	82.78	96.57	110.37	124.17	.9
15.0	13.89	27.78	41.67	55.56	69.44	83.33	97.22	III.II	125.00	15.0
	I									

Name	\ Y							ĺ			Y /
14.07	$X \setminus$	1	2	3	4	5	6	7	8	9	/X
1.3						"					15.1
14 14 26 28 52 42 78 57 04 71 30 85 56 99 81 114 07 128 33 14 13 14 14 14 18 129 17 15 15 14 13 13 14 14 15 15 14 14 15 15											.2
S			1	1			-				
6											.4
8											.6
8	.7	14.54	29.07	43.61	58.15	72.69	87.22	101.76	116.30	130.83	.7
16.0											.8
14.91		14.72	29.44	44.17	58.89	73.61			117.78	132.50	.9
15.00 30.00 45.00 60.00 75.00 90.00 105.00 120.00 135.00 3.5.00 3.15.09 30.19 45.28 60.37 75.46 90.56 105.65 120.74 135.83 3.3 3.3 30.37 45.56 60.74 75.93 91.11 106.30 121.48 136.67 3.5 15.28 30.56 45.83 61.11 76.39 91.67 106.94 122.22 137.50 6.6 15.37 30.74 46.11 61.48 76.85 92.22 107.59 122.96 138.33 6.6 7.3 1.5	16.0	14.81	29.63	44.44	59.26	74.07	88.89	103.70	118.52	133.33	16.0
3											1.
.4 15.19 30.37 45.56 60.74 75.93 91.11 106.30 121.48 136.67 2.2 137.50 .6 15.37 30.74 46.11 61.48 76.89 92.22 107.59 122.22 137.50 .8 15.36 30.93 46.39 61.85 77.31 92.78 108.24 123.70 139.17 .6 19.55 31.30 46.94 62.22 77.78 93.33 108.89 124.44 140.00 .9 15.55 31.30 46.94 62.59 78.24 93.89 109.54 125.19 140.83 17.0 15.74 31.48 47.22 62.96 78.70 94.44 110.19 125.93 141.67 14.83 .9 15.93 141.67 142.50 .1 .1 15.83 31.67 47.50 63.33 79.17 95.00 110.83 122.41 143.33 .2 15.93 141.67 142.50 .1 .1 .1 140.83 145.00 .1 .1 .1 .1 .1 .1 .1 .1 .1 .1 .1 .											.2
15. 28]		1	1	í
.6 15.37 30.74 46.11 61.48 76.85 92.22 107.59 122.96 138.33 .6 .7 15.46 30.93 46.39 61.85 77.31 92.78 108.24 123.70 139.17 .6 .8 15.56 31.30 46.94 62.29 77.78 93.33 108.89 124.44 140.08 .6 .9 15.65 31.30 46.94 62.59 78.70 94.44 110.19 125.93 141.67 142.50 .1 15.83 31.67 47.50 63.33 79.17 95.00 110.83 126.67 142.50 .2 15.93 31.85 47.78 63.70 79.63 95.56 111.48 127.41 143.33 .2 .3 16.02 32.41 48.66 64.07 80.09 96.11 112.13 128.89 145.50 .4 .5 16.20 32.41 48.61 64.81 81.02 97.22 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>-4</th></t<>											-4
.7 15.46 30.93 46.39 61.85 77.31 92.78 108.24 123.70 139.17 3.8 15.56 31.11 46.67 62.22 77.78 93.33 108.89 124.44 140.00 8.8 17.0 15.74 31.48 47.22 62.96 78.70 94.44 110.19 125.93 141.67 17.0 1 15.83 31.67 47.50 63.33 79.17 95.00 110.83 126.67 142.50 12.30 2 15.93 31.85 47.78 63.70 79.63 95.56 111.48 127.41 143.33 144.17 .3 3 16.02 32.41 48.66 64.97 80.09 96.11 112.13 128.89 145.50 5 16.20 32.41 48.61 64.81 81.02 97.22 113.43 129.63 145.83 .4 6 16.30 32.78 49.17 65.56 81.94 98.33 114.72											.6
.8 15.56 31.11 46.67 62.22 77.78 93.33 108.89 124.44 140.00 8.5 .9 15.65 31.30 46.94 62.29 78.24 93.89 109.54 125.19 140.80 .5 .1 15.83 31.67 47.50 63.33 79.17 95.00 110.83 126.67 142.50 .2 15.93 31.85 47.78 63.70 79.63 95.50 111.48 127.41 143.33 17.6 .3 16.02 32.41 48.66 64.97 80.09 96.11 112.13 128.89 145.00 .5 16.20 32.41 48.61 64.81 81.02 97.22 113.43 129.63 145.83 146.67 .7 16.39 32.78 49.17 65.56 81.94 98.33 114.72 131.11 147.50 27 .8 16.48 32.96 49.44 65.93 82.41 98.89 115.37	.7	15.46	30.03	46.30	61.85	77.31	92.78	108.24	123.70		.7
19											.8
.1 15.83 31.67 47.50 63.33 79.17 95.00 110.83 126.67 142.50 1.2 15.93 31.85 47.78 63.70 79.63 95.56 111.48 127.41 143.33 2.2 143.33 2.2 48.80 64.07 80.09 96.11 112.13 128.15 144.17 3.3 140.17 3.3 140.17 3.3 140.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 44.17 3.3 3.3 4.44 80.56 96.67 112.78 128.89 145.50 4.25 4.25 4.25 4.25 4.25 4.25 4.26 4.26 4.26 97.78 114.07 130.37 146.67 4.25 4.26 4.26 4.26 4.26 4.26 4.26 4.26 4.26 4.26 4.26	.9	15.65	31.30	46.94	62.59	78.24	93.89	109.54		140.83	.9
15.93 31.85 47.78 63.70 79.63 95.56 111.48 127.41 143.33 144.17	17.0	15.74	31.48	47.22	62.96	78.70	94 - 44	110.19	125.93	141.67	17.0
3											.r
.4 16.11 32.22 48.33 64.44 80.56 96.67 112.78 128.89 145.00 .4 .5 16.20 32.41 48.61 64.81 81.02 97.22 113.43 129.63 145.83 .5 .6 16.30 32.78 49.17 65.56 81.94 98.33 114.72 131.11 147.50 .6 .8 16.48 32.96 49.44 65.93 82.41 98.89 115.37 131.85 148.33 148.33 .9 .9 16.57 33.15 49.72 66.30 82.87 99.44 116.02 132.59 149.17 .9 .9 .16.67 33.33 150.00 .16.67 33.33 150.00 .16.67 33.33 150.00 .1 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>.2</th></td<>											.2
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16											-4
.7 16.39 32.78 49.17 65.56 81.94 98.33 114.72 131.11 147.50 .7 .8 16.48 32.96 49.44 65.93 82.41 98.89 115.37 131.85 148.33 .8 .9 16.57 33.15 49.72 66.30 82.87 99.44 116.02 132.59 149.17 .1 16.07 33.33 50.00 66.67 83.33 100.00 116.67 133.33 150.00 .1 16.76 33.52 50.28 67.04 83.80 105.56 117.31 134.07 150.83 .2 16.85 33.70 50.56 67.41 84.26 101.11 117.96 134.81 151.67 .3 16.94 33.89 50.83 67.78 84.72 101.67 118.61 135.56 152.50 .4 17.04 34.07 51.11 68.15 85.19 102.22 119.26 136.30 153.33 .4 .5 17.13 34.26 51.39 68.52 85.65 102.78 119.91 137.04 154.17 .6 17.22 34.44 51.67 68.89 86.11 103.33 120.56 137.78 155.00 .7 17.31 34.63 51.94 69.26 86.57 103.89 121.20 138.52 155.80 .8 17.41 34.81 52.22 69.63 87.04 104.44 121.85 139.26 156.67 .9 17.50 35.00 52.78 70.37 87.96 105.56 123.15 140.00 157.50 .1 17.69 35.37 53.06 70.74 88.43 106.11 138.00 .1 17.69 35.93 53.89 71.85 89.81 107.78 125.74 143.70 161.67 .5 18.66 36.11 54.17 72.22 90.28 108.33 126.39 144.44 162.50 .6 18.15 36.30 54.44 72.59 90.74 108.89 127.04 145.19 163.33 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.91 165.00 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.91 165.00 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.91 165.00 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00											.6
.8 16.48 32.96 49.44 65.93 82.41 98.89 115.37 131.85 148.33 .8 .9 16.57 33.15 49.72 66.30 82.87 99.44 116.02 132.59 149.17 18.0 18.0 16.67 33.33 50.00 66.67 83.83 100.00 116.67 133.33 150.08 .1 16.76 33.52 50.28 67.04 83.80 100.56 117.31 134.07 150.83 .2 16.85 33.70 50.56 67.41 84.26 101.11 117.96 134.81 151.67 .3 16.94 33.89 50.83 67.78 84.72 101.67 118.61 135.56 152.50 .3 .4 17.04 34.07 51.11 68.15 85.19 102.22 119.96 136.30 153.33 .4 .5 17.13 34.63 51.94 69.26 86.57 103.89 121.20 138.52 </th <th></th> <th></th> <th></th> <th></th> <th> - • </th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>					- •						
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$\begin{array}{c} \textbf{.1} \textbf{16.76} \textbf{33.52} \textbf{50.28} \textbf{67.04} \textbf{83.80} \textbf{100.56} \textbf{117.31} \textbf{134.07} \textbf{150.83} \\ \textbf{.2} \textbf{16.85} \textbf{33.70} \textbf{50.56} \textbf{67.41} \textbf{84.26} \textbf{101.11} \textbf{117.96} \textbf{134.81} \textbf{151.67} \\ \textbf{.3} \textbf{16.94} \textbf{33.89} \textbf{50.83} \textbf{67.78} \textbf{84.72} \textbf{101.67} \textbf{118.61} \textbf{135.56} \textbf{152.50} \\ \textbf{.4} \textbf{17.04} \textbf{34.07} \textbf{51.11} \textbf{68.15} \textbf{85.19} \textbf{102.22} \textbf{119.26} \textbf{136.30} \textbf{153.33} \\ \textbf{.5} \textbf{17.13} \textbf{34.26} \textbf{51.39} \textbf{68.52} \textbf{85.65} \textbf{102.78} \textbf{119.91} \textbf{137.04} \textbf{154.17} \\ \textbf{.6} \textbf{17.22} \textbf{34.44} \textbf{51.67} \textbf{68.89} \textbf{86.11} \textbf{103.33} \textbf{120.56} \textbf{137.78} \textbf{155.00} \\ \textbf{.7} \textbf{17.31} \textbf{34.63} \textbf{51.94} \textbf{69.26} \textbf{86.57} \textbf{103.89} \textbf{121.20} \textbf{138.52} \textbf{155.83} \\ \textbf{.8} \textbf{17.41} \textbf{34.81} \textbf{52.22} \textbf{69.63} \textbf{87.04} \textbf{104.44} \textbf{121.85} \textbf{139.26} \textbf{156.67} \\ \textbf{.9} \textbf{17.50} \textbf{35.00} \textbf{52.50} \textbf{70.00} \textbf{87.50} \textbf{105.00} \textbf{122.50} \textbf{140.00} \textbf{157.50} \\ \textbf{19.0} \textbf{17.59} \textbf{35.37} \textbf{35.06} \textbf{70.74} \textbf{88.43} \textbf{106.11} \textbf{123.80} \textbf{141.48} \textbf{159.17} \\ \textbf{.2} \textbf{17.78} \textbf{35.56} \textbf{53.33} \textbf{71.11} \textbf{88.89} \textbf{106.67} \textbf{124.44} \textbf{142.22} \textbf{160.00} \\ \textbf{.3} \textbf{17.87} \textbf{35.56} \textbf{35.30} \textbf{51.17.11} \textbf{89.33} \textbf{107.22} \textbf{125.09} \textbf{142.96} \textbf{160.83} \\ \textbf{.4} \textbf{17.96} \textbf{35.93} \textbf{53.89} \textbf{71.85} \textbf{89.81} \textbf{107.78} \textbf{125.74} \textbf{143.70} \textbf{161.67} \\ \textbf{.5} \textbf{18.66} \textbf{36.11} \textbf{54.17} \textbf{72.22} \textbf{90.28} \textbf{108.33} \textbf{126.39} \textbf{144.44} \textbf{162.50} \\ \textbf{.6} \textbf{18.15} \textbf{36.30} \textbf{54.44} \textbf{72.59} \textbf{90.74} \textbf{108.89} \textbf{127.04} \textbf{145.19} \textbf{163.33} \\ \textbf{.6} \textbf{.18.33} \textbf{36.67} \textbf{55.00} \textbf{73.33} \textbf{91.67} \textbf{110.00} \textbf{128.33} \textbf{146.67} \textbf{165.00} \\ \textbf{.8} \textbf{18.33} \textbf{36.67} \textbf{55.00} \textbf{73.33} \textbf{91.67} \textbf{110.00} \textbf{128.33} \textbf{146.67} \textbf{165.00} \\ \textbf{.8} \textbf{18.33} \textbf{36.67} \textbf{55.00} \textbf{73.33} \textbf{91.67} \textbf{110.00} \textbf{128.33} \textbf{146.67} \textbf{165.00} \\ \textbf{.8} \textbf{165.33} \textbf{36.67} 55$.9	16.57	33.15	49.72		82.87	99.44	116.02	132.59	149.17	.9
.2 16.85 33.70 50.56 67.41 84.26 101.11 117.96 134.81 151.67 .3 .3 16.94 33.89 50.83 67.78 84.72 101.67 118.61 135.56 152.50 .3 .4 17.04 34.07 51.11 68.15 85.19 102.22 119.26 136.30 153.33 .4 .5 17.13 34.26 51.39 68.52 85.65 102.78 119.91 137.04 154.17 .5 .6 17.22 34.44 51.67 68.89 86.11 103.33 120.56 137.78 155.00 .5 .7 17.31 34.63 51.94 69.26 86.57 103.89 121.20 138.52 155.83 .5 .8 17.41 34.81 52.22 69.63 87.04 104.44 121.85 139.26 155.69 .8 .9 17.50 35.97 52.50 70.07 87.96 <t< th=""><th>18.0</th><th>16.67</th><th>33.33</th><th>50.00</th><th>66.67</th><th>83.33</th><th>100.00</th><th>116.67</th><th>133.33</th><th>150.00</th><th>18.0</th></t<>	18.0	16.67	33.33	50.00	66.67	83.33	100.00	116.67	133.33	150.00	18.0
.3 16.94 33.89 50.83 67.78 84.72 101.67 118.61 135.56 152.50 .3 .4 17.04 34.07 51.11 68.15 85.19 102.22 119.26 136.30 153.33 .4 .5 17.13 34.26 51.39 68.52 85.65 102.78 119.91 137.04 154.17 .5 .6 17.22 34.44 51.67 68.89 86.11 103.33 120.56 137.04 154.17 .5 .8 17.41 34.63 51.94 69.26 86.57 103.89 121.20 138.52 155.83 156.67 .8 .9 17.50 35.00 52.50 70.00 87.50 105.00 122.50 140.00 157.50 180.67 19.0 17.59 35.19 52.78 70.37 87.96 105.56 123.15 140.04 158.33 19.0 17.50 157.50 19.0 17.83 35.65 53.33											.1
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.7 17.31 34.63 51.94 69.26 86.57 103.89 121.20 138.52 155.83 17.41 34.81 52.22 69.63 87.04 104.44 121.85 139.26 156.67 18.24 17.59 35.00 52.50 70.00 87.50 105.00 122.50 140.00 157.50 19.0 17.59 35.37 53.06 70.74 88.43 106.11 123.80 141.48 159.17 158.33 17.87 35.56 53.33 71.11 88.89 106.67 124.44 142.22 160.00 23.37 17.87 35.74 53.61 71.48 89.35 107.22 125.09 142.96 160.83 33.37 33.61 71.48 89.35 107.22 125.09 142.96 160.83 33.37 35.44 17.96 35.93 53.44 77.222 90.28 108.33 126.39 144.44 162.50 53.33 163.30 144.44 162.50 163.33 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.47 163.30 164.17 163.30 164.17 163.30 164.17 163.30 164.17 163.30 164.17 165.00	.6										.6
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19.0 17.59 35.19 52.78 70.37 87.96 105.56 123.15 140.74 158.33 19.0 .1 17.69 35.37 53.66 70.74 88.43 106.11 123.80 141.48 159.17 .1 .2 17.78 35.56 53.33 71.11 88.89 106.67 124.44 142.22 160.00 .2 .3 17.87 35.74 53.61 71.85 89.81 107.78 125.09 142.96 160.83 .3 .4 17.96 35.93 53.89 71.85 89.81 107.78 125.74 143.70 161.67 .5 .5 18.06 36.11 54.17 72.22 90.28 108.33 126.39 144.44 162.50 .5 .6 18.15 36.30 54.44 72.59 90.74 108.89 127.04 145.19 163.33 .6 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.93 164.17 .7 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8					1						.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$.9	17.50		52.50	70.00	87.50	105.00	122.50	140.00	157.50	.9
.2 17.78 35.56 53.33 71.11 88.89 106.67 124.44 142.22 160.00 .2 .3 17.87 35.74 53.61 71.48 89.35 107.22 125.09 142.96 160.83 .3 .4 17.96 35.93 53.89 71.85 89.81 107.78 125.74 143.70 161.67 .4 .5 18.06 36.11 54.17 72.22 90.28 108.33 126.39 144.44 162.50 .5 .6 18.15 36.30 54.44 72.59 90.74 108.89 127.04 145.19 163.33 .6 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.93 164.17 .7 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8	19.0	17.59	35.19	52.78	70.37	87.96	105.56	123.15	140.74	158.33	19.0
.3 17.87 35.74 53.61 71.48 89.35 107.22 125.09 142.96 160.83 .3 .4 17.96 35.93 53.89 71.85 89.81 107.78 125.74 143.70 161.67 .4 .5 18.66 36.11 54.17 72.22 90.28 108.33 126.39 144.44 162.50 .5 .6 18.15 36.30 54.44 72.59 90.74 108.89 127.04 145.19 163.33 36 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.93 164.17 .7 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8											ı.
.4 17.96 35.93 53.89 71.85 89.81 107.78 125.74 143.70 161.67 .4 .5 18.06 36.11 54.17 72.22 90.28 108.33 126.39 144.44 162.50 .5 .6 18.15 36.30 54.44 72.59 90.74 108.89 127.04 145.19 163.33 .6 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.93 164.17 .7 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8						-					.2
.5 18.06 36.11 54.17 72.22 90.28 108.33 126.39 144.44 162.50 .5 .6 18.15 36.30 54.44 72.59 90.74 108.89 127.04 145.19 163.33 .6 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.93 164.17 .7 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8										-	
.6 18.15 36.36 54.44 72.59 90.74 108.89 127.04 145.19 163.33 .6 .7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.93 164.17 .7 .8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8											-4
.7 18.24 36.48 54.72 72.96 91.20 109.44 127.69 145.93 164.17 .7 8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8	.6										.6
.8 18.33 36.67 55.00 73.33 91.67 110.00 128.33 146.67 165.00 .8			i				-				
											.8
	.9	18.43	36.85	55.28	73.70	92.13	110.56	128.98	147.41	165.83	.9
20.0 18.52 37.04 55.56 74.07 92.59 111.11 129.63 148.15 166.67 20.0	20.0	18.52	37.04	55.56	74.07	92.59	III.II	129.63	148.15	166.67	20.0

V 17					_					17 /
X	1	2	3	4	5	6	7	8	9	X = X
20.1	18.61	37.22	55.83	74.44	93.06	111.67	130.28	148.89	167.50	20.1
. 2	18.70	37.41	56.11	74.81	93.52	112.22	130.93	149.63	168.33	.2
.3	18.80	37.59	56.39	75.19	93.98	112.78	131.57	150.37	169.17	.3
	18.89	37.78	56.67	75.56	94.44	113.33	132.22	151.11	170.00	1
.4	18.98	37.76	56.94	75.93	94.41	113.89	132.22	151.85	170.83	-4
.5 .6	19.07	38.15	57.22	76.30	95.37	114.44	133.52	152.59	171.67	.5 .6
.7	19.17	38.33	57.50	76.67	95.83	115.00	134.17	153.33	172.50	.7
.8	19.26	38.52	57.78	77.04	96.30	115.56	134.81	154.07	173.33	.8
.9	19.35	38.70	58.06	77.4I	96.76	116.11	135.46	154.81	174.17	.9
21.0	19.44	38.89	58.33	77.78	97.22	116.67	136.11	155.56	175.00	21.0
. Ι	19.54	39.07	58.61	78.15	97.69	117.22	136.76	156.30	175.83	. 1
.2	19.63	39.26	58.89	78.52	98.15	117.78	137.41	157.04	176.67	.2
-3	19.72	39 - 44	59.17	78.89	98.61	118.33	138.06	157.78	177.50	.3
-4	19.81	39.63	59.44	79.26	99.07	118.89	138.70	158.52	178.33	.4
-5	19.91	39.81	59.72	79.63	99.54	119.44	139.35	159.26	179.17	.5
.6	20.00	40.00	60.00	80.00	100.00	120.00	140.00	160.00	180.00	.6
.7	20.09	40.19	60.28	80.37	100.46	120.56	140.65	160.74	180.83	.7
.8	20.19	40.19	60.56	80.74	100.40	121.11	141.30	161.48	181.67	.8
.9	20.19	40.56	60.83	81.11	101.39	121.67	141.94	162.22	182.50	.9
22.0			61.11	81.48	101.85	122.22	142.59	162.96		22.0
	20.37	40.74							183.33	1
.I	20.46	40.93	61.39	81.85	102.31	122.78	143.24	163.70	184.17	I.
.2	20.56	41.11	61.67	82.22	102.78	123.33	143.89	164.44	185.00	.2
.3	20.65	41.30	61.94	82.59	103.24	123.89	144.54	165.19	185.83	.3
-4	20.74	41.48	62.22	82.96	103.70	124.44	145.19	165.93	186.67	-4
- 5	20.83	41.67	62.50	83.33	104.17	125.00	145.83	166.67	187.50	-5
.6	20.93	41.85	62.78	83.70	104.63	125.56	146.48	167.41	188.33	.6
.7	21.02	42.04	63.06	84.07	105.09	126.11	147.13	168.15	189.17	.7
.8	21.11	42.22	63.33	84.44	105.56	126.67	147.78	168.89	190.00	.8
.9	21.20	42.41	63.61	84.81	106.02	127.22	148.43	169.63	190.83	.9
23.0	21.30	42.59	63.89	85.19	106.48	127.78	149.07	170.37	191.67	23.0
. 1	21.39	42.78	64.17	85.56	106.94	128.33	149.72	171.11	192.50	. г
.2	21.48	42.96	64.44	85.93	107.41	128.89	150.37	171.85	193.33	.2
.3	21.57	43.15	64.72	86.30	107.87	129.44	151.02	172.59	194.17	.3
.4	21.67	43.33	65.00	86.67	108.33	130.00	151.67	173.33	195.00	.4
.5	21.76	43.52	65.28	87.04	108.80	130.56	152.31	174.07	195.83	-5
.6	21.85	43.70	65.56	87.41	109.26	131.11	152.96	174.81	196.67	.6
.7			65.83		-	-				
.8	2I.94 22.04	43.89	66.11	87.78 88.15	109.72 110.19	131.67 132.22	153.61 154.26	175.56 176.30	197.50	.7 .8
.9	22.13	44.07	66.39	88.52	110.19	132.22	154.91	177.04	190.33	.9
24.0	22.22		66.67	88.89	111.11		155.56	177.78	200.00	24.0
		44.44				133.33				
Ι.	22.31	44.63	66.94	89.26	111.57	133.89	156.20	178.52	200.83	.1
.2	22.41	44.81	67.22	89.63	112.04	134.44	156.85	179.26	201.67	.2
3	22.50	45.00	67.50	90.00	112.50	135.00	157.50	180.00	202.50	-3
-4	22.59	45.19	67.78	90.37	112.96	135.56	158.15	180.74	203.33	.4
.5	22.69	45.37	68.06	90.74	113.43	136.11	158.80	181.48	204.17	.5
.6	22.78	45.56	68.33	91.11	113.89	136.67	159.44	182.22	205.00	.6
-7	22.87	45.74	68.61	91.48	114.35	137.22	160.09	182.96	205.83	.7
.8	22.96	45.93	68.89	91.85	114.81	137.78	160.74	183.70	206.67	.8
.9	23.06	46.11	69.17	92.22	115.28	138.33	161.39	184.44	207.50	.9
25.0	23.15	46.30	69.44	92.59	115.74	138.89	162.04	185.19	208.33	25.0

										11/ 2
X	I	2	3	4	5	6 .	7	8	9	Y X
25.1	23.24	46.48	69.72	92.96	116.20	139.44	162.69	185.93	209.17	25.1
.2	23.33	46.67	70.00	93 . 33	116.67	140.00	163.33	186.67	210.00	. 2
.3	23.43	46.85	70.28	93.70	117.13	140.56	163.98	187.41	210.83	.3
.4	23.52	47.04	70.56	94.07	117.59	141.11	164.63	188.15	211.67	.4
.5	23.61	47.22	70.83	94.44	118.06	141.67	165.28	188.89	212.50	-5
.6	23.70	47.41	71.11	94.81	118.52	142.22	165.93	189.63	213.33	.6
1	23.80			95.19	118.98	142.78	166.57	190.37	214.17	.7
.7 .8	23.80	47 · 59 47 · 78	71.39 71.67	95.19	119.44	143.33	160.37	191.11	214.17	.8
.9	23.98	47.96	71.99	95.93	119.44	143.89	167.87	191.85	215.83	.9
26.0		48.15	72.22	96.30			168.52	192.59	216.67	26.0
	24.07				120.37	144.44				i I
Ι.	24.17	48.33	72.50	96.67	120.83	145.00	169.17	193.33	217.50	. I
.2	24.26	48.52	72.78	97.04	121.30 121.76	145.56	169.81 170.46	194.07	218.33	.2
3	24.35	48.70	73.06	97.41				194.81	219.17	-3
.4	24.44	48.89	73.33	97.78	122.22	146.67	171.11	195.56	220.00	-4
.5	24.54	49.07	73.61	98.15	122.69	147.22	171.76	196.30	220.83	-5
.6	24.63	49.26	73.89	98.52	123.15	147.78	172.41	197.04	221.67	.6
.7	24.72	49.44	74.17	98.89	123.61	148.33	173.06	197.78	222.50	.7
.8	24.81	49.63	74.44	99.26	124.07	148.89	173.70	198.52	223.33	.8
.9	24.91	49.81	74.72	99.63	124.54	149.44	174.35	199.26	224.17	.9
27.0	25.00	50.00	75.00	100.00	125.00	150.00	175.00	200.00	225.00	27.0
. 1	25.09	50.19	75.28	100.37	125.46	150.56	175.65	200.74	225.83	.1
.2	25.19	50.37	75.56	100.74	125.93	151.11	176.30	201.48	226.67	.2
.3	25.28	50.5 6	75.83	101.11	126.39	151.67	176.94	202.22	227.50	-3
.4	25.37	50.74	76.11	101.48	126.85	152.22	177.59	202.96	228.33	.4
.5	25.46	50.93	76.39	101.85	127.31	152.78	178.24	203.70	229.17	-5
.6	25.56	51.11	76.67	102.22	127.78	153.33	178.89	204.44	230.00	.6
.7	25.65	51.30	76.94	102.59	128.24	153.89	179.54	205.19	230.83	.7
.8	25.74	51.48	77.22	102.96	128.70	154.44	180.19	205.93	231.67	.8
.9	25.83	51.67	77.50	103.33	129.17	155.00	180.83	206.67	232.50	.9
28.0	25.93	51.85	77.78	103.70	129.63	155.56	181.48	207.41	233.33	28.0
. 1	26.02	52.04	78.06	104.07	130.09	156.11	182.13	208.15	234.17	. 1
.2	26.11	52.22	78.33	104.44	130.56	156.67	182.78	208.89	235.00	.2
.3	26.20	52.41	78.61	104.81	131.02	157.22	183.43	209.63	235.83	.3
	26.30	52.59	78.89	105.19	131.48	157.78	184.07	210.37	236.67	.4
.4	26.30	52.78	79.17	105.19	131.46	158.33	184.72	211.11	237.50	-5
.5 .6	26.48	52.96	79.44	105.93	132.41	158.89	185.37	211.85	238.33	.6
				106.30	132.87		186.02	212.59	239.17	.7
.7 .8	26.57 26.67	53.15 53.33	79.72 80.00	106.67	132.87	159.44	186.67	213.33	240.00	.8
.9	26.76	53.52	80.28	107.04	133.80	160.56	187.31	214.07	240.83	.9
29.0	26.85	53.70	80.56	107.41	134.26	161.11	187.96	214.81	241.67	29.0
						161.67	188.61			1 1
. I . 2	26.94 27.04	53.89	80.83	107.78	134.72	162.22	189.26	215.56	242.50	. I . 2
.2	27.13	54.26	81.39	108.52	135.65	162.78	189.91	217.04	243.33	-3
-4	27.22	54.44	81.67	108.89	136.11	163.33 163.89	190.56	217.78 218.52	245.00	.4
.5 .6	27.3I 27.4I	54.63 54.81	81.94	109.20	130.57	164.44	191.20	219.26	245.63	.5 .6
							1	-		1 1
.7	27.50	55.00	82.50	110.00	137.50	165.00	192.50	220.00	247.50	.7
.8	27.59	55.19	82.78	110.37	137.96	165.56 166.11	193.15	220.74	248.33	.8
.9	27.69	55.37	83.06	110.74	138.43		193.80		249.17	.9
30.0	27.78	55.56	83.33	111.11	138.89	166.67	194.44	222.22	250.00	30.0
		1	1		r			1	,	

		-					-			** /
Y	1	2	3	4	5	6	7	8	9	$Y \setminus_X$
30.1	27.87	55.74	83.61	111.48	139.35	167.22	195.09	222.96	250.83	30.1
.2	27.96	55.93	83.89	111.85	139.81	167.78	195.74	223.70	251.67	.2
-3	28.06	56.11	84.17	112,22	140.28	168.33	196.39	224.44	252.50	.3
-4	28.15	56.30	84.44	112.59	140.74	168.89	197.04	225.19	253.33	-4
.5 .6	28.24 28.33	56.48 56.67	84.72 85.00	112.96	141.20	169.44 170.00	197.69	225.93 226.67	254.17	.5 .6
.0			-	113.33	141.07	170.00	198.33	220.07	255.00	٠٠ ا
.7	28.43	56.85	85.28	113.70	142.13	170.56	198.98	227.41	255.83	.7
.8	28.52	57.04	85.56	114.07		171.11	199.63	228.15	256.67	.8
.9	28.61	57.22	85.83	114.44	143.06	171.67	200.28	228.89	257.50	.9
31.0	28.70	57.41	86.11	114.81	143.52	172.22	200.93	229.63	258.33	31.0
Ι.	28.80	57.59	86.39	115.19	143.98	172.78	201.57	230.37	259.17	.1
.2	28.89	57.78	86.67	115.56	144.44	173.33	202.22	231.11	260.00	. 2
.3	28.98	57.96	86.94	115.93	144.91	173.89	202.87	231.85	260.83	.3
.4	29.07	58.15	87.22	116.30	145.37	174.44	203.52	232.59	261.67	.4
.5	29.07	58.33	87.50	116.67	145.83	175.00	203.32	232.39	262.50	.5
.6	29.26	58.52	87.78	117.04	146.30	175.56	204.81	234.07	263.33	.6
										1
.7 .8	29.35	58.70	88.06	117.41	146.76	176.11	205.46	234.81	264.17	.7
	29.44	58.89	88.33 88.61	117.78	147.22	176.67	206.11 206.76	235.56	265.00	
.9	29.54	59.07			147.69	177.22		236.30		.9
32.0	29.63	59.26	88.89	118.52	148.15	177.78	207.41	237.04	266.67	32.0
. 1	29.72	59 . 44	89.17	118.89	148.61	178.33	208.06	237.78	267.50	Ι.
.2	29.81	59.63	89.44	119.26	149.07	178.89	208.70	238.52	268.33	.2
.3	29.91	59.81	89.72	119.63	149.54	179.44	209.35	239.26	269.17	.3
.4	30.00	60.00	90.00	120.00	150.00	180.00	210.00	240.00	270.00	-4
- 5	30.09	60.19	90.28	120.37	150.46	180.56	210.65	240.74	270.83	-5
.6	30.19	60.37	90.56	120.74	150.93	181.11	211.30	241.48	271.67	.6
.7	30.28	60.56	90.83	121.11	151.39	181.67	211.94	242.22	272.50	.7
.8	30.37	60.74	91.11	121.48		182.22	212.59	242.96	273.33	8.
.9	30.46	60.93	91.39	121.85	152.31	182.78	213.24	243.70	274.17	9.
33.0	30.56	61.11	91.67	122.22	152.78	183.33	213.89	244.44	275.00	33.0
1										
.I	30.65	61.30	91.94	122.59	153.24	183.89 184.44	214.54	245.19	275.83	.I
.2	30.74 30.83	61.67	92.22	122.96	153.70 154.17	185.00	215.19	245.93 246.67	277.50	3
-3	1	i	1							1
-4	30.93	61.85	92.78	123.70		185.56	216.48	247.41	278.33	-4
-5	31.02	62.04	93.06	124.07	155.09	186.11	217.13	248.15	279.17	-5
.6	31.11	62,22	93.33	124.44		186.67	217.78	248.89	280.00	.6
.7	31.20	62.41	93.61	124.81	156.02	187.22	218.43	249.63	280.83	.7
. 8	31.30	62.59	93.89	125.19		187.78	219.07	250.37	281.67	.8
.9	31.39	62.78	94.17	125.56		188.33	219.72	251.11	282.50	.9
34.0	31.48	62.96	94.44	125.93	157.41	188.89	220.37	251.85	283.33	34.0
. т	31.57	63.15	94.72	126.30	157.87	189.44	221.02	252.59	284.17	. 1
.2	31.67	63.33	95.00	126.67	158.33	190.00	221.67	253.33	285.00	.2
.3	31.76	63.52	95.28	127.04	158.80	190.56	222.31	254.07	285.83	.3
.4	31.85	63.70	95.56	127.41	159.26	191.11	222.96	254.81	286.67	.4
-5	31.94	63.89	95.83	127.78		191.67	223.61	255.56	287.50	-5
.6	32.04	64.07	96.11	128.15	160.19	192.22	224.26	256.30	288.33	.6
.7	32.13	64.26	96.39	128.52	160.65	192.78	224.91	257.04	289.17	.7
.8	32.13	64.44	96.67	128.89		193.33	225.56	257.78	290.00	8
.9	32.31	64.63	96.94	129.26		193.89	226.20	258.52	290.83	.9
35.0	32.41	64.81	97.22	129.63		194.44	226.85	259.26	291.67	35.0
30.0	32.41	04.01	91.22	129.03	102.04	194.44	220.03	239.20	291.07	155.5

X	ı	2	3	4	5	6	7	8	9	Y X
35.1	32.50	65.00	97.50	130.00	162.50	195.00	227.50	260,00	292.50	35.1
.2	32.59	65.19	97.78	130.37	162.96	195.56	228.15	260.74	293.33	.2
.3	32.69	65.37	98.06	130.74	163.43	196.11	228.80	261.48	293.33	
		l	1 1				ĺ			-3
.4	32.78	65.56	98.33	131.11	163.89	196.67	229.44	262.22	295.00	-4
.5	32.87	65.74	98.61	131.48	164.35	197.22	230.09	262.96	295.83	.5
.6	32.96	65.93	98.89	131.85	164.81	197.78	230.74	263.70	296.67	.6
.7	33.06	66.11	99.17	132.22	165.28	198.33	231.39	264.44	297.50	.7
.8	33.15	66.30	99.44	132.59		198.89	232.04	265.19	298.33	.8
.9	33.24	66.48	99.72	132.96	166.20	199.44	232.69	265.93	299.17	.9
36.0	33.33	66.67	100.00	133.33	166.67	200.00	233.33	266.67	300.00	36.0
					<u>-</u>					
. 1	33.43	66.85	100.28	133.70	167.13	200.56	233.98	267.41	300.83	Ι.
.2	33.52	67.04	100.56	134.07	167.59	201.11	234.63	268.15	301.67	.2
.3	33.61	67.22	100.83	134.44	168.06	201.67	235.28	268.89	302.50	.3
.4	33.70	67.41	101.11	134.81	168.52	202.22	235.93	269.63	303.33	.4
.5	33.80	67.59	101.39	135.19	168.98	202.78	236.57	270.37	304.17	.5
.6	33.89	67.78	101.67	135.56	169.44	203.33	237.22	271.11	305.00	.6
.7	33.98	67.96	101.94	135.93	169.91	203.89	237.87	257 95		_
.8		68.15	101.94	135.93	170.37		237.07	271.85	305.83	.7 .8
.9	34.07		102.22	136.67	170.37	204.44		272.59	306.67	
	34.17	68.33				205.00	239.17	273.33	307.50	.9
37.0	34.26	68.52	102.78	137.04	171.30	205.56	239.81	274.07	308.33	37.0
. 1	34.35	68.70	103.06	137.41	171.76	206.11	240.46	274.81	309.17	. 1
.2	34.44	68.89	103.33	137.78	172.22	206.67	241.11	275.56	310.00	.2
.3	34.54	69.07	103.61	138.15	172.69	207.22	241.76	276.30	310.83	-3
-4	34.63	69.26	103.89	138.52	173.15	207.78	242.41	277.04	311.67	.4
-5	34.72	69.44	104.17	138.89	173.61	208.33	243.06	277.78	312.50	.5
.6	34.81	69.63	104.44	139.26	174.07	208.89	243.70	278.52	313.33	.6
7		69.81	'''							
.8	34.9I 35.00	70.00	104.72	139.63		209.44	244.35	279.26	314.17	.7 .8
.9		70.19		140.00			245.00	280.00	315.00	
	35.09		105.28	140.37	175.46	210.56	245.65	280.74	315.83	.9
38.0	35.19	70.37	105.56	140.74	175.93	211.11	246.30	281.48	316.67	38.0
.I	35.28	70.56	105.83	141.11	176.39	211.67	246.94	282.22	317.50	. 1
.2	35.37	70.74	106.11	141.48	176.85	212.22	247.59	282.96	318.33	.2
.3	35.46	70.93	106.39	141.85	177.31	212.78	248.24	283.70	319.17	.3
.4	35.56	71.11	106.67	142.22	177.78	213.33	248.89	284.44	320.00	.4
-5	35.65	71.30	106.94	142.59	178.24	213.89	249.54	285.19	320.83	.5
.6	35.74	71.48	107.22		178.70	214.44	250.19	285.93	321.67	.6
.7	1	1	1 1							
.8	35.83	71.67	107.50		179.17	215.00	250.83	286.67	322.50	.7
.9	35.93	71.85	107.78	143.70	179.63	215.56	251.48	287.41	323.33	.8
	36.02	72.04		144.07	180.09	216.11	252.13	288.15	324.17	.9
39.0	36.11	72.22	108.33	144.44	180.56	216.67	252.78	288.89	325.00	39.0
.I	36.20	72.41	108.61	144.81	181.02	217.22	253.43	289.63	325.83	.1
.2	36.30	72.59	108.89	145.19	181.48	217.78	254.07	290.37	326.67	.2
.3	36.39	72.78	109.17	145.56	181.94	218.33	254.72	291.11	327.50	.3
.4	36.48	72.96	109.44	145.93	182.41	218.89	255.37	291.85	328.33	.4
.5	36.57	73.15	109.72	146.30	182.87	219.44	256.02	292.59	329.17	.5
.6	36.67	73.33	110.00	146.67	183.33	220.00	256.67	293.33	330.00	.6
.7			1							1
.8	36.76	73.52	110.28	147.04	183.80	220.56	257.31	294.07	330.83	.7
.9	36.85	73.70	110.56	147.41	184.26	221.11	257.96	294.81	331.67	.8
	36.94	73.89	110.83	147.78	184.72	221.67	258.61	295.56	332.50	.9
40.0	37.04	74.07	III.II	148.15	185.19	222,22	259.26	296.30	333 - 33	40.0

TABLE XLI

Prismoidal Corrections to be subtracted from average end area volumes 100 feet long. $D-D_1=$ difference in total width; $C-C_1=$ difference in center height. Corrections in cubic yards.

0 0 01					_					D D /
$D-D_1$ $C-C_1$	I	2	3	4	5	6	7	8	9	$D-D_1$ $C-C_1$
.2	0.06	0.12	0.19	0.25	0.31	0.37	0.43	0.49	0.56	.2
.4	0.12	0.25	0.37	0.49	0.62	0.74	0.86	0.99	1.11	.4
.6	0.19	0.37	0.56	0.74	0.93	1.11	1.30	1.48	1.67	.6
.8	0.25	0.49	0.74	0.99	1.23	1.48	1.73	1.98	2.22	.8
I.0	0.23	0.62	0.93	1.23	1.54	1.43	2.16	2.47	2.78	I.0
.2	0.37	0.74	1.11	1.48	1.85	2.22	2.59	2.96		.2
			1	1					3.33	
-4	0.43	0.86	1.30	1.73	2.16	2.59	3.02	3.46	3.89	-4
.6	0.49	0.99	1.48	1.98	2.47	2.96	3.46	3.95	4.44	.6
.8	0.56	I.II	1.67	2.22	2.78	3.33	3.89	4.44	5.00	.8
2.0	0.62	1.23	1.85	2.47	3.09	3.70	4.32	4.94	5.56	2.0
.2	0.68	1.36	2.04	2.72	3.40	4.07	4.75	5.43	6.11	.2
.4	0.74	1.48	2.22	2.96	3.70	4.44	5.19	5.93	6.67	-4
.6	0.80	1.60	2.41	3.21	4.01	4.81	5.62	6.42	7.22	.6
.8	0.86	1.73	2.59	3.46	4.32	5.19	6.05	6.91	7.78	.8
3.0	0.93	1.85	2.78	3.70	4.63	5.56	6.48	7.41	8.33	3.0
.2	0.99	1.98	2.96	3.95	4.94	5.93	6.91	7.90	8.89	.2
	1.05	2.10	3.15	4.20	5.25	6.30	7.35	8.40	9.44	1
.4 .6	1.05	2.10	3.15	4.44	5.25	6.67	7.78	8.89	10.00	·4 .6
.8	1.17	2.35	3.52	4.44	5.86	7.04	8.21	9.38	10.56	.8
4.0	1.23	2.47	3.70	4.94	6.17	7.41	8.64	9.88	II.II	4.0
.2	1.30	2.59	3.89	5.19	6.48	7.78	9.07	10.37	11.67	.2
-4	1.36	2.72	4.07	5.43	6.79	8.15	9.51	10.86	12.22	-4
.6	1.42	2.84	4.26	5.68	7.10	8.52	9.94	11.36	12.78	.6
.8	1.48	2.96	4.44	5.93	7.41	8.89	10.37	11.85	13.33	.8
5.0	1.54	3.09	4.63	6.17	7.72	9.26	10.80	12.35	13.89	5.0
.2	1.60	3.21	4.81	6.42	8.02	9.63	11.23	12.84	14.44	.2
.4	1.67	3.33	5.00	6.67	8.33	10.00	11.67	13.33	15.00	-4
.6	1.73	3.46	5.19	6.91	8.64	10.37	12.10	13.83	15.56	.6
.8	1.79	3.58	5.37	7.16	8.95	10.74	12.53	14.32	16.11	.8
6.0	1.85	3.70	5.56	7.41	9.26	II.II	12.96	14.81	16.67	6.0
	_					11.48			17.22	l .
.2	1.91	3.83	5.74	7.65	9.57	1	13.40	15.31		.2
.4	1.98	3.95	5.93	7.90 8.15	9.88	11.85	13.83	16.30	17.78	-4
.6	2.04	4.07	6.11	_	10.19	12.22	14.26	-	18.33	.6
.8	2.10	4.20	6.30	8.40	10.49	12.59	14.69	16.79	18.89	.8
7.0	2.16	4.32	6.48	8.64	10.80	12.96	15.12	17.28	19.44	7.0
.2	2.22	4 - 44	6.67	8.89	11.11	13.33	15.56	17.78	20.00	.2
-4	2.28	4.57	6.85	9.14	11.42	13.70	15.99	18.27	20.56	-4
.6	2.35	4.69	7.04	9.38	11.73	14.07	16.42	18.77	21.11	.6
.8	2.41	4.81	7.22	9.63	12.04	14.44	16.85	19.26	21.67	.8
8.0	2.47	4.94	7.41	9.88	12.35	14.81	17.28	19.75	22.22	8.0
.2	2.53	5.06	7.59	IO. 12	12.65	15.19	17.72	20.25	22.78	.2
.4	2.59	5.19	7.78	10.37	12.96	15.56	18.15	20.74	23.33	.4
.6	2.65	5.31	7.96	10.62	13.27	15.93	18.58	21.23	23.89	.6
.8	2.72	5.43	8.15	10.86	13.58	16.30	19.01	21.73	24.44	.8
9.0	2.78	5.56	8.33	11.11	13.89	16.67	19.44	22.22	25.00	9.0
.2	2.84	5.68	8.52	11.36	14.20	17.04	19.88	22.72	25.56	.2
	2.90	5.80	8.70	11.60	14.51	17.41	20.31	23.21	26.11	l
.4 .6	2.90	1	8.89	11.85	14.81	17.41	20.31	23.70	26.67	.4 .6
.0 .8	3.02	5.93 6.05	9.07	12.10	15.12	18.15	21.17	24.20	27.22	.8
10.0										10.0
10.0	3.09	6.17	9.26	12.35	15.43	18.52	21.60	24.69	27.78	10.0

$D-D_1$ $C-C_1$	1	2	3	4	5	6	7	8	9	$D-D_1$
10.2	3. I5 3. 2I	6.30	9.44	12.59	15.74	18.89	22.04	25.19 25.68	28.33 28.89	10.2
.6	3.27	6.54	9.81	13.09	16.36	19.63	22.90	26.17	29.44	.6
.8 11.0	3.33	6.67 6.79	10.00	13.33 13.58	16.67 16.98	20.00	23.33 23.77	26.67 27.16	30.00 30.56	.8 0.11
.2	3.46	6.91	10.37	13.83	17.28	20.74	24.20	27.65 28.15	31.11	.2
.4 .6	3.52 3.58	7.04 7.16	10.74	14.32	17.90	21.48	25.06	28.64	31.67 32.22	.6
.8 12.0	3.64	7.28	10.93	14.57	18.21	21.85	25.49	29.14	32.78	.8 12 .0
. 2	3.77	7.53	11.30	15.06	18.83	22.59	26.36	30.12	33.89	. 2
.4 .6	3.83	7.65 7.78	11.48	15.31 15.56	19.14 19.44	22.96 23.33	26.79 27.22	30.62 31.11	34 · 44 35 · 00	.4 .6
.8	3.95	7.90	11.85	15.80	19.75	23.70	27.65	31.60	35.56	.8
13.0	4.0I 4.07	8.02 8.15	12.04 12.22	16.05 16.30	20.06	24.07 24.44	28.09 28.52	32.10 32.59	36.11 36.67	13.0
.4 .6	4.14 4.20	8.27 8.40	12.41 12.59	16.54 16.79	20.68	24.81 25.19	28.95 29.38	33.09 33.58	37.22	·4 .6
.8	4.26	8.52	12.59	17.04	21.30	25.56	29.30	34.07	37.78 38.33	.8
14.0	4.32	8.64	12.96	17.28	21.60	25.93	30.25	34.57	38.89	14.0
. 2 . 4	4.38 4.44	8.77 8.89	13.15	17.53 17.78	21.91 22.22	26.30 26.67	30.68 31.11	35.06 35.56	39 · 44 40 · 00	.2 .4
.6 .8	4.5I 4.57	9.01 9.14	13.52	18.02	22.53 22.84	27.04 27.41	31.54 31.98	36.05 36.54	40.56 41.11	.6 .8
15.0	4.63	9.26	13.89	18.52	23.15	27.78	32.41	37.04	41.67	15.0
.2 .4	4.69 4.75	9.38 9.51	14.07	18.77	23.46	28.15 28.52	32.84	37·53 38.02	42.22	.2
6	4.81	9.63	14.44	19.26	24.07	28.89	33.70	38.52	43.33	.6 .8
16.0	4.88	9.75	14.63	19.51	24.38	29.26	34.14	39.01	43.89	16.0
.2	5.00	10.00	15.00	20.00	25.00	30.00	35.00	40.00	45.00	.2
.4 .6	5.06 5.12	10.12 10.25	15.19 15.37	20.25 20.49	25.31 25.62	30.37 30.74	35.43 35.86	40.49 40.99	45.56 46.11	.4 .6
.8 17.0	5.19 5.25	10.37 10.49	15.56 15.74	20.74 20.99	25.93 26.23	31.11 31.48	36.30 36.73	41.48 41.98	46.67 47.22	.8 17.0
.2	5.31	10.62	15.93	21.23	26.54	31.85	37.16	42.47	47.78	.2
·4 .6	5.37 5.43	10.74 10.86	16.11 16.30	21.48 21.73	26.85 27.16	32.22 32.59	37.59 38.02	42.96 43.46	48.33 48.89	.4 .6
.8	5.49	10.99	16.48	21.98	27.47	32.96	38.46	43.95	49.44	.8
18.0 .2	5.56	11.11	16.67	22.22	27.78	33.33	38.89	44.44	50.∞ 50.56	18.0 .2
-4	5.68	11.36	17.04	22.72	28.40	34.07	39.75	45.43	51.11	.4
.6 .8	5.74 5.80	11.48	17.22 17.41	22.96 23.21	28.70 29.01	34.44 34.81	40.19	45.93 46.42	51.67 52.22	.6 .8
19.0 .2	5.86 5.93	11.73 11.85	17.59 17.78	23.46 23.70	29.32 29.63	35.19 35.56	41.05 41.48	46.91 47.41	52.78 53.33	19.0 .2
.4	5.99	11.05	17.96	23.70	29.03	35.50	41.40	47.41	53.89	.4
.6 .8	6.05	12.10 12.22	18.15 18.33	24.20 24.44	30.25 30.56	36.30 36.67	42.35 42.78	48.40 48.89	54.44 55.00	.6 .8
20.0	6.17	12.35	18.52	24.69	30.86	37.04	43.21	49.38	55.56	20.0

TABLE XLII. — Level Section Volumes 100 feet long. Roadbed 14 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	57 126 206 296 398 511 635 770 917 1074 1243 1422 1613 1815 2028 2252 2487	5 64 133 214 306 409 523 648 785 932 1090 1260 1441 1633 1836 2050 2275 2511	11 70 141 223 316 420 535 661 799 947 1107 1278 1459 1652 1857 2072 2298 2535	16 77 149 232 326 431 547 675 813 963 1123 1295 1478 1672 1878 2094 2321 2560	22 83 156 241 336 442 559 688 828 978 1140 1313 1497 1692 1899 2116 2345 2345	27 90 164 250 346 453 572 701 842 994 1157 1331 1516 1713 1920 2138 2368 2368	33 97 172 259 356 465 584 715 857 1010 1174 1349 1535 1733 1941 2161 2392 2633	39 104 181 268 366 476 597 729 872 1026 1191 1367 1555 1753 1963 2183 2415 2658	45 111 189 277 377 488 609 742 887 1042 1208 1385 1574 1774 1984 2206 2439 2683	51 119 197 287 387 499 622 1058 1225 1404 1593 1794 2006 2229 2463 2708	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16
18	2733 2991	2759 3017	2784 3044	2809 3070	2835 3097	2861 3124	2886 3151	2912 3178	2938 3205	2965 3232	18 19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3259 6556 10963	3539 6946 11465	3830 7348 11978	4131 7761 12502	4444 8185 13037	4769 8620 13583	5104 9067 1414 1	5450 9524 14709	5807 9993 1 52 89	6176 10472 25880	20 30 40

TABLE XLIII. — Level Section Volumes 100 feet long. Roadbed 16 feet. Slope $1\frac{1}{2}:1$.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 I 2	65 141	6 72 149	12 79 157	18 86 166	25 94 174	31 101 183	38 109 192	44 117 201	51 125 209	58 133 219	0 I 2
3 4 5	228 326 435 556	237 336 447 568	247 347 458 581	256 358 470 594	266 368 482 607	275 379 494 620	285 390 506 633	295 401 518 646	305 412 531 660	316 424 543 673	3 4 5 6
2 3 4 5 6 7 8 9	687 830 983	701 845 999	715 859 1015	729 875 1032	743 890 1048	757 905 1064	77I 92I 108I	786 936 1098	800 952 1114	815 967 1131	7 8 9
10 11 12 13	1148 1324 1511 1709	1165 1342 1530 1730	1182 1361 1550 1750	1200 1379 1569 1771	1217 1398 1589 1792	1235 1416 1609 1813	1252 1435 1629 1833	1270 1454 1649 1855	1288 1473 1669 1876	1306 1492 1689 1897	10 11 12 13
14 15 16	1919 2139 2370	1940 2162 2394	1962 2184 2418	1983 2207 2442	2005 2230 2466	2027 2253 2490	2049 2276 2515	2072 2300 2539	2094 2323 2564	2116 2347 2588	14 15 16
17 18 19	2613 2867 3131	2638 2893 3159	2663 2919 3186	2688 2945 3213	2713 2971 3241	2738 2998 3268	2764 3024 3296	2789 3051 3323	2815 3078 3351	2841 3105 3379	17 18 19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3407 6778 11259	3694 7176 11769	3993 7585 12289	4302 8006 12820	4622 8437 13363	4954 8880 13917	5296 9333 14481	5650 9798 15057	6015 10274 15644	6391 10761 16243	20 30 40

TABLE XLIV. — Level Section Volumes 100 feet long. Roadbed 20 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	a.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	80 170 272 385 509 644 791 948 1117 1296 1487 1689 1902 2126 2361 2607 2865	7 88 180 283 397 522 659 806 964 1134 1315 1507 1710 1924 2149 2385 2633 2891	15 97 190 294 409 535 673 821 981 1152 1334 1527 1731 1946 2172 2409 2658 2918	23 106 200 305 421 549 687 998 1169 1352 1546 2195 2435 2683 2944	31 115 210 316 433 562 702 852 1014 1187 1371 1566 1773 1990 2219 2458 2709 2971	38 124 220 327 446 575 716 868 1031 1205 1390 1587 1794 2012 2242 2483 2735 2998	46 133 230 339 458 589 731 1048 1223 1409 1607 1815 2035 2266 2508 2761	55 142 240 350 471 603 746 900 1065 1241 1429 1627 1837 2058 2289 2532 2786 3052	63 151 251 362 484 617 761 916 1082 1259 1448 1648 1858 2080 2313 2557 2812	71 161 262 373 496 630 776 630 1099 1278 1461 1668 1880 2103 2337 2582 2839 3106	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16
18 19	3133 3413	3161 3442	3188 3470	3216 3499	3244 3528	3272 3557	3300 3586	3328 3615	3079 3356 3645	3384 3674	17 18 19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3704 7222 11852	4006 7635 12376	4319 8059 12911	4643 8494 13457	4979 8941 14015	5324 9398 14583	5681 9867 15163	6050 10346 15754	6430 10837 16356	6820 11339 16969	20 30 40

TABLE XLV. — Level Section Volumes 100 feet long. Roadbed 20 feet. Slope 1 : 1.

				_							
Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		7	15	23	30	38	46	54	62	70	0
ī	78	86	94	103	111	114	128	137	145	154	ĭ
2	163	172	181	190	199	208	218	227	236	246	2
	256	265	275	285	295	305	315	325	335	345	
4	356	366	376	387	398	408	419	430	441	452	3 4 5 6
5	463	474	485	497	508	519	531	543	554	566	5
6	578	590	602	614	626	638	650	663	675	687	6
3 4 5 6 7 8 9	700	713	725	7.38	751	764	777	790	803	816	7 8
8	830	843	856	870	884	897	911	925	939	953	8
9	967	981	995	1009	1024	1038	1052	1067	1082	1096	9
	IIII	1126	1141	1156	1171	1186	1201	1217	1232	1247	10
11	1263	1279	1294	1310	1326	1342	1358	1374	1390	1406	11
12	1422	1439	1455	1471	1488	1505	1521	1538	1555	1572	12
13	1589	1606	1623	1640	1658	1675	1692	1710	1728	1745	13
14	1763	1781	1799	1817	1835	1853	1871	1889	1908	1926	14
15 16	1944	1963	1982	2000	2019	2038	2057	2076	2095	2114	15 16
10	2133	2153	2172	2191	2211	2231	2250	2270	2290	2310	
17	2330	2350	2370	2390	2410	2431	2451	2471	2492	2513	17
18	2533	2554	2575	2596	2617	2638	2659	2680	2702	2723	18
19	2744	2766	2788	2809	2831	2853	2875	2897	2919	2941	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
	2062	2780	2400	2662		126-					
20	2963	3189	3422	3663	3991	4167	4430	4700	4978	5263	20
30	5556 8889	5856	6163 9644	6478	6800	7130	7467	7811	8163	8522	30
40	0009	9263	9044	10033	10430	10833	11244	11663	12089	12522	40

TABLE XLVI. — Level Section Volumes 100 feet long. Roadbed 24 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		9	18	27	36	46	55	65	75	85	0
ĭ	94	105	115	125	135	146	156	167	178	189	ī
2	200	211	222	234	245	257	269	280	292	304	2
	317	329	341	354	366	379	392	405	418	431	
3 4 5 6	444	458	471	485	499	512	526	540	555	569	3 4 5 6
5	583	598	612	627	642	657	672	687	702	718	Ś
	733	749	765	780	796	812	829	845	861	878	6
7 8 9	894	911	928	945	962	979	996	1014	1031	1049	7 8
8	1067	1085	1102	II2I	1139	1157	1175	1194	1212	1231	8
9	1250	1269	1288	1307	1326	1346	1365	1385	1405	1425	9
10	1444	1465	1485	1505	1525	1546	1566	1587	1608	1629	10
11	1650	1671	1692	1714	1735	1757	1779	1800	1822	1845	11
12	1867	1889	1911	1934	1956	1979	2002	2025	2048	2071	12
13	2094	2118	2141	2165	2189	2213	2236	2261	2285	2309	13
14	2333	2358	2382	2407	2432	2457	2482	2507	2532	2558	14
15 16	2583	2609	2635	2661	2686	2713	2739	2765	2791	2818	15
10	2844	2871	2898	2925	2952	2979	3006	3034	3061	3089	16
17 18	3117	3145	3172	3201	3229	3257	3285	3314	3342	3371	17
	3400	3429	3458	3487	3516	3546	3575	3605	3635	3665	18
19	3694	3725	3755	3785	3815	3846	3876	3907	3938	3969	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.o	9.0	Center height
20	4000	4317	4644	4983	5333	5694	6067	6450	6844	7250	20
30	7667	8004	8533	8983	9444	9917	10.100	10894	11400	11917	30
40	12444	12983	13533	14094	14667	15250	15844	16450	17067	17694	40
		303	-0000	-4334	-4301	-32,70	-3544	45	-,507	-, -, 94	-10

TABLE XLVII. — Level Section Volumes 100 feet long. Roadbed 24 feet. Slope 1 : 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 13 14 15 16 17 18	93 193 300 415 537 667 804 1100 1259 1426 1600 1782 1970 2167 2370 2582 2800 3026	9 102 203 311 427 550 680 818 963 1116 1276 1443 1618 1800 1990 2187 2391 2603 2822	18 112 214 322 439 562 694 832 978 1131 1292 1466 1636 1819 2009 2207 2412 2625 2845	27 122 224 334 451 575 707 846 993 1147 1308 1477 1654 1837 2028 2227 2433 2646 2867 3095	36 132 235 345 463 588 721 861 1008 1163 1325 1495 1672 1856 2048 2247 2454 2668 2889 3118	45 142 245 356 475 601 734 875 1023 1179 1342 1512 1690 1875 2068 2475 2690 2912	55 152 256 368 487 614 748 890 1038 1195 1358 1530 1708 1894 2087 2288 2496 2712 2935 3165	64 162 267 380 500 627 762 904 1054 1211 1375 1547 1726 1913 2107 2308 2517 2734 2957 2734 2958	74 172 278 391 510 640 756 919 1069 1226 1392 1565 1745 1932 2127 2329 2756 2980	83 182 289 403 524 653 790 933 1084 1243 1409 1582 1763 1951 2147 2350 2560 2778 3003 3236	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center height	0.0	3049 1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3259 6000 9481	3500 6315 9870	3748 6637 10267	4004 6967 10670	4267 7304 11081	4537 7648 11500	4815 8000 11926	5100 8359 12359	5393 8726 12800	5692 9100 13248	20 30 40

TABLE XLVIII. — Level Section Volumes 100 feet long. Roadbed 26 feet. Slope $1\frac{1}{2}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
-		10	19	29	39	50	60	70	81	91	0
	102	113	124	135	146	157	168	180	191	203	ĭ
1 2	215	227	239	251	263	275	288	301	313	326	2
3		352	365	378	392	405	419	432	446	460	
	339	488	502	517	531	546	561	575	590	605	3
4	474 620	636	651	666	682	698	713	729	745	762	7
4 5 6	778	794	811	827	844	861	878	895	912	929	3 4 5 6
2	946	964	981	999	1017	1035	1053	1071	1089	1107	, ,
6	1126	1144	1163	1182	1201	1220	1239	1258	1278	1297	7 8 9
0	1317	1333	1356	1376	1396	1416	1436	1457	1477	1498	ŏ
7 8 9	1519	1539	1560	1581	1602	1624	1645	1666	1688	1710	10
11	1731	1753	1775	1798	1820	1842	1865	1887	1910	1933	11
12	1956	1979	2002	2025	2048	2072	2095	2119	2143	2167	12
13	2191	2215	2239	2263	2288	2312	2337	2362	2387	2412	13
	2437	2462	2488	2513	2539	2564	2590	2616	2642	2668	14
14	2694	2721	2747	2774	2800	2827	2854	2881	2908	2936	î
15 16	2963	2990	3018	3046	3073	3101	3129	3158	3186	3214	15 16
10	3243	3271	3300	3329	3358	3387	3416	3445	3474	3504	17
17 18	3533	3563	3593	3623	3653	3683	3713	3743	3774	3804	17 18
19	3835	3866	3897	3928	3959	3990	4022	4053	4085	4116	19
19	3033	3000	3097	3920	3939	3990	4022	4033	4003	4110	1 -3
Cente r height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
	47.0	4470	4805	5754	FFTT	5880	6259	6650	7052	7465	20
20	4148	4472	4807	5154	5511	10176	10667	11168	7052 11681	12205	
30	7889	8324	8770	9228	9696		16185			18057	30
40	12741	13287	13844	14413	14992	15583	10185	16798	17422	10057	40

TABLE XLIX. — Level Section Volumes 100 feet long. Roadbed 26 feet. Slope 1:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		10	19	29	39	49	59	69	79	90	0
ī	100	110	121	131	142	153	164	174	185	196	ī
2	207	219	230	241	252	264	275	287	299	310	2
	322	334	346	358	370	382	395	407	419	432	3
3	444	457	470	483	495	508	521	534	548	561	1 A
3 4 5 6	574	587	601	614	628	642	655	669	683	697	4 5 6
6	711	725	739	754	768	782	797	811	826	841	ĕ
	856	870	885	900	915	931	946	961	976	992	7
8	1007	1023	1039	1054	1070	1086	1102	1118	1134	1150	7 8
7 8 9	1167	1183	1199	1216	1232	1249	1266	1283	1299	1316	9
10	1333	1350	1368	1385	1402	1419	1437	1454	1472	1490	10
11	1507	1525	1543	1561	1579	1597	1615	1634	1652	1670	11
12	1689	1707	1726	1745	1764	1782	1801	1820	1839	1859	12
13	1878	1897	1916	1936	1955	1975	1995	2014	2034	2054	13
14	2074	2094	2114	2134	2155	2175	2195	2216	2236	2257	14
15	2278	2299	2319	2340	2361	2382	2404	2425	2446	2467	15 16
15 16	2489	2510	2532	2554	2575	2597	2619	2641	2663	2685	16
17 18	2707	2730	2752	2774	2797	2819	2842	2865	2888	2910	17
18	2933	2956	2979	3003	3026	3049	3072	3096	3119	3143	18
19	3167	3190	3214	3238	3262	3286	3310	3334	3359	3383	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20	2407	3656	2077	477.4	****	1700	5007	5300	5600	5907	20
20	3407 6222		3911 6874	4174	4444	4722	8267	8633	9007	9389	30
30		6544 10174	10578	7211 10989	7556	7907 11833	12267	12707	13156	13611	40
40	9778	10174	10578	10989	11407	11033	12207	12/0/	13150	13011	40

TABLE L. — Level Section Volumes 100 feet long. Roadbed 28 feet. Slope $1\frac{1}{2}:I$.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	109 230 361 504 656 822 998 1185 1383 1592 1812 2044 2287 2541 2806 3081 3368 3667	10 121 242 375 519 673 839 1016 1204 1403 1614 1835 2068 2312 2567 2833 3109 3397	21 132 255 389 534 690 856 1035 1224 1635 1858 2092 2337 2593 2860 3138 3427 3728	32 144 268 403 549 706 874 1053 1243 1443 1457 1881 2116 2362 2619 2887 3166 3456 3456 3758	42 156 281 417 564 722 891 1072 1263 1465 1679 1904 2140 2387 2645 2915 3195 3498	53 168 294 431 579 738 909 1090 1283 1486 1701 1927 2164 2413 2672 2942 3223 3516	64 180 307 445 595 755 926 1109 1303 1507 1723 1950 2189 2438 2698 2970 3252 3546 3851	75 192 320 460 610 772 944 1128 1322 1528 1745 1973 2213 2464 2725 2997 3281 3576	86 205 334 474 626 788 962 1147 1343 1549 1767 1997 2238 2489 2752 3025 3310 3606	98 217 348 489 642 805 980 1166 1363 1571 1790 2020 22515 2779 3053 3339 3636 3944	0 1 3 4 56 7 8 9 10 11 12 13 14 15 16 17 18
19	3976	4007	4039	4070	4102	4134	4166	4198	4231	4263	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	4296 8111 13037	4627 8554 13591	4970 9007 14156	5324 9472 14731	5689 9948 15318	6065 10435 15917	6451 10933 16526	6850 11443 17146	7259 11963 17778	7680 12494 18420	20 30 40

TABLE LI. — Level Section Volumes 100 feet long. Roadbed 28 feet. Slope 1:1

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 3 4 5 6 7 8 9 10 11 13 14 15 16 17 18	107 222 344 474 611 656 908 1067 1233 1407 1589 1778 1974 2178 2389 2607 2833 3067 3307	10 119 234 357 487 625 770 923 1083 1250 1425 1607 1797 1994 2199 2410 2630 2856 3090 3332	21 130 246 370 501 639 785 939 1267 1443 1626 1816 2014 2219 2432 2652 2879 3114 3356	31 141 258 383 514 654 800 954 1116 1285 1461 1645 1836 2034 2240 2454 2674 2903 3138	42 152 270 395 528 668 816 970 1132 1302 1479 1664 1855 2055 2261 2475 2697 2926 3406	53 164 282 408 542 682 831 1986 1149 1319 1497 1682 1875 2075 2282 2497 2719 2949 3186 3431	64 175 295 421 555 697 846 1002 1166 1337 1515 1701 1895 2095 2304 2519 2742 2972 3210 3455	74 167 307 434 569 711 861 1018 1182 1354 1534 1720 1914 2116 2325 2996 3234 3480	85 199 319 448 583 726 876 1034 1199 1372 1739 1934 2136 2346 2563 2788 3019 3259 3505	96 210 332 461 597 741 892 1050 1216 1390 1570 1954 2157 2367 2367 2585 2810 3043 3283 3530	0 1 2 3 4 5 6 7 8 9 10 11 12 14 15 16 17 18 19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	3556 6444 10074	3811 6774 10478	4074 7111 10889	4344 7456 11307	4622 7807 11733	4907 8167 12167	5200 8533 12607	5500 8907 13056	5807 9289 13511	6122 9678 13974	20 30 40

TABLE LII. — Level Section Volumes 100 feet long. Roadbed 30 feet. Slope 1½:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0	117	11 129	22 I4I	34 154	45 166	57	69	80	92 218	104	0
2	244	258	271	285	299	179 312	192 326	205 340	355	231 369	1 2
	383	398	412	427	442	457	472	487	502	518	1 1
3	533	549	565	580	596	612	629	645	661	678	3
7	694	711	728	745	762	779	796	814	831	849	2
3 4 5 6	867	884	902	920	939	957	975	994	1012	1031	6
	1050	1069	1088	1107	1126	1146	1165	1185	1205	1224	7
7 8 9	1244	1264	1285	1305	1325	1346	1366	1387	1408	1429	3 4 5 6 7 8 9
9	1450	1471	1492	1514	1535	1557	1579	1600	1622	1644	9
10	1667	1689	1711	1734	1756	1779	1802	1825	1848	1871	10
11	1894	1918	1941	1965	1981	2012	2036	2060	2085	2109	11
12	2133	2158	2182	2207	2232	2257	2282	2307	2332	2358	12
13	2383	2409	2435	2460	2486	2512	2539	2565	2591	2618	13
14	2644	2671	2698	2725	2752	2779	2806	2834	2861	2889	14
15 16	2917	2944	2972	3000	3029	3057	3085	3114	3142	3171	15 16
	3200	3229	3258	3287	3316	3346	3375	3405	3435	3464	
17	3494	3525	3555	3585	3615	3646	3676	3707	3738	3769	17
18	3800	3831	3862	3894	3925	3957	3989	4020	4052	4084	18
19	4117	4149	4181	4214	4246	4279	4312	4345	4378	4411	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20 30 40	4444 8333 13333	4783 8783 13894	5133 9244 14467	5494 9717 15050	5867 10200 15644	6250 10694 16250	6644 11200 16867	7050 11717 17494	7467 12244 18133	7894 12783 18783	20 30 40

TABLE LIII. — Level Section Volumes 100 feet long. Roadbed 30 feet. Slope 1:1.

											_
Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		11	22	34	45	56	68	80	91	103	0
ĭ	115	127	139	151	163	175	187	200	212	224	ĭ
2	237	250	262	275	288	301	314	327	340	353	2
3	367	380	393	407	421	434	448	462	476	490	3
ă	504	518	532	546	561	575	589	604	619	633	
4 5 6	648	663	678	693	708	723	738	754	769	784	4 5 6
ĕ	800	816	831	847	863	879	895	911	927	943	ĕ
7	959	976	992	1008	1025	1042	1058	1075	1092	1109	7
8	1126	1143	1160	1177	1195	1212	1229	1247	1265	1282	7 8
7 8 9	1300	1318	1336	1354	1372	1390	1408	1426	1445	1463	9
IŎ	1481	1500	1510	1537	1556	1575	1594	1613	1632	1651	ΙÓ
11	1670	1690	1709	1728	1748	1768	1787	1807	1827	1847	11
12	1867	1887	1907	1927	1947	1968	1988	2008	2029	2050	12
13	2070	2091	2112	2133	2154	2175	2196	2217	2239	2260	13
14	2281	2303	2325	2346	2368	2390	2412	2434	2456	2478	14
15 16	2500	2522	2545	2567	2589	2612	2635	2657	2680	2703	15
	2726	2749	2772	2795	2818	2842	2865	2888	2912	2936	16
17 18	2959	2983	3007	3031	3055	3079	3103	3127	3151	3176	17
	3200	3224	3249	3274	3298	3323	3348	3373	3399	3423	18
19	3448	3473	3499	3524	3549	3575	3601	3626	3652	3678	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20	3704	3967	4237	4515	4800	5093	5393	5700	6015	6337	20
30	6667	7004	7348	7700	8059	8426	8800	9181	9570	9967	30
40	10370	10781	11200	11626	12059	12500	12948	13404	13867	14337	40
40	10370	10/01		11320		12300	12340	-3404	-5507	-4337	40

TABLE LIV. — Level Section Volumes 100 feet long. Roadbed 32 feet. Slope $1\frac{1}{2}:1$.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0		12	24	36	48	61	73	86	98	III	0
1	124	137	150	163	177	190	204	218	231	245	ī
2	259	273	288	302	316	331	346	360	375	390	2
3 4 5 6	406	421	436	452	467	483	499	515	531	547	
4	563	579	596	612	629	646	663	680	697	714	3 4 5 6
5	731	749	767	784	802	820	838	856	874	893	5
6	911	930	948	967	986	1005	1024	1043	1063	1082	
7 8	1102	1122	1141	1161	1181	1201	1222	1242	1262	1283	7
8	1304	1324	1345	1366	1388	1409	1430	1452	1473	1495	7 8 9
9	1517	1539	1561	1583	1605	1627	1650	1672	1695	1718	
10	1741	1764	1787	1810	1833	1857	1881	1904	1928	1952	10
11	1976	2000	2024	2049	2073	2009	2122	2147	2172	2197	11
12	2222	2247	2273	2298	2324	2350	2375	2401	2427	2453	12
13	2480	2506	2532	2559	2586	2612	2639	2666	2694	2721	13
14	2748	2776	2803	2831	2859	2887	2915	2943	2971	2999	14
15 16	3028	3056	3085	3114	3143	3172	3201	3230	3259	3289	15 16
10	3319	3348	3378	3408	3438	3468	3498	3529	3559	3590	
17 18	3620	3651	3682	3713	3744	3775	3807	3888	3870	3902	17
	3933	3965	3997	4029	4062	4094	4126	4159	4192	4224	18
19	4257	4290	4324	4357	4390	4424	4457	4491	4525	4559	19
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	Center height
20	4593	4939	5296	5665	6044	6435	6837	7250	7674	8109	20
30	8556	9013	9482	9962	10452	10954	11467	11991	12526	13072	30
40	13630	14198	14778	15369	15970	16583	17207	17843	18489	19146	40
					-71	, ,		. 10			, ,

TABLE LV. — Level Section Volumes 100 feet long. Roadbed 32 feet. Slope 1:1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	o .9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	122 252 389 533 685 844 1011 1185 1367 1556 2167 2385 2611 2844 3085 3333 3389	12 135 265 403 548 701 861 1028 1203 1385 1575 1772 1976 2188 2407 2634 2868 3110 3359 3615	24 148 279 417 563 716 877 1045 1221 1404 1594 1997 2210 2430 2657 2892 3134 3384 3641	36 160 292 431 578 732 894 1063 1239 1423 1614 1812 2018 2231 2452 2680 2916 3159 3409 3667	48 173 306 446 593 748 910 1080 1257 1441 1633 2253 2253 2475 2704 2940 3184 3435 3693	60 186 319 460 608 764 927 1097 1460 1653 1853 2060 2275 2497 2727 2964 3208 3460 3719	72 199 333 475 624 780 944 1115 1293 1479 1672 1873 2081 2297 2520 2988 3233 3486 3746	85 212 347 489 639 796 960 1132 1311 1498 1692 21894 2103 2319 2543 2774 3012 3258 3511 3772	97 225 361 504 812 977 1150 1330 1517 1712 1914 2124 2341 2565 2797 3036 3283 3537 3799	110 239 375 519 670 828 994 1167 1348 1536 1732 2145 2363 2588 2831 3061 3308 3563 3563 3825	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center height	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0 ទ	9.0	Center height
20 30 40	3852 6889 10667	4122 7233 11085	4400 7585 11511	4685 7944 11944	4978 8311 12385	5278 8685 12833	5585 9067 13289	5900 9456 13752	6222 9852 14222	6552 10256 14700	20 30 40

TABLE LVI. — Level Section Volumes 100 feet long. Roadbed 20 feet. Slope $\frac{1}{4}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4	75 152 231 311 394	7 83 160 238 319 402	15 90 167 246 327 410	22 98 175 254 336 419	30 106 183 263 344 427	37 113 191 271 352 435	45 121 199 279 360 444	52 129 207 287 369 452	60 136 214 295 377 461	67 144 223. 303 385 469	0 1 2 3 4 5
2 3 4 5 6 7 8 9 10 11	478 564 652 742 833 927 1022	486 573 661 751 843 936 1032	495 581 670 760 852 946 1042	503 590 679 769 861 955	512 599 688 778 870 965 1061	521 608 696 787 880 974 1071	529 616 706 796 889 984 1080	538 625 714 806 899 993 1090	546 634 724 815 908 1003 1100	555 643 733 824 917 1013 1110	6 7 8 9 10 11
12 13 14 15 16 17	1119 1219 1319 1422 1527 1633	1129 1229 1330 1433 1537 1644	1139 1239 1340 1443 1548 1655	1149 1249 1350 1453 1559 1666	1159 1259 1360 1464 1569	1169 1269 1371 1474 1580 1687	1179 1279 1381 1485 1591 1698	1189 1289 1391 1495 1601 1709	1199 1299 1402 1506 1612 1720	1209 1309 1412 1516 1623 1731	13 14 15 16 17
Center height	0.0	1.0	2.0	3.0	4.0	1796 5.0	6.o	7.0	1830 8.o	9.0	Center height
20 30 40	1852 3056 4444	1964 3186 4593	2078 3319 4744	2194 3453 4897	2311 3589 5052	2431 3727 5208	2552 3867 5367	2675 4008 5527	2800 4152 5689	2927 4297 5853	20 30 40

TABLE LVII. — Level Section Volumes 100 feet long. Roadbed 24 feet. Slope $\frac{1}{4}$: 1.

Center height	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	Center height
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	90 181 275 370 468 567 668 770 875 981 1090 1200 1312 1426 1542 1659 1779 1900	9 99 191 284 380 477 577 678 781 886 992 1101 1211 1323 1437 1553 1671 1791	18 108 200 294 390 487 587 688 791 1003 1112 1222 1335 1449 1565 1683 1803	27 117 209 303 399 497 597 698 802 907 1014 1123 1233 1346 1460 1577 1695 1815	36 126 219 313 409 507 708 812 917 1025 1134 1245 1357 1472 1588 1707 1827	45 135 228 322 419 517 719 822 928 1035 1145 1256 1369 1484 1600 1719 1839	54 145 237 332 428 527 729 833 939 1046 1156 1267 1380 1495 1612 1731 1851	63 154 247 342 438 537 637 739 843 949 1057 1167 1278 1392 1507 1624 1743 1863 1986	72 163 256 351 448 547 750 854 1068 1178 1289 1403 1518 1636 1755 1876 1998	81 172 266 361 458 557 760 864 971 1079 1189 1301 1414 1530 1647 1767 1888	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18
Center height	0.0	1.0	2.0	3.0	4.0	2085 5.0	2098 6.0	7.0	8.o	9.0	Center height
20 30 40	2148 3500 5037	2275 3645 5201	2404 3793 5367	2534 3942 5534	2667 4093 5704	2801 4245 5875	2937 4400 6048	3075 4556 6223	3215 4715 6400	3356 4875 6579	20 30 40

TABLE LVIII. — MIDDLE ORDINATES FOR CURVING RAILS Ordinate given in inches

From Roberts' "Track Formulæ and Tables."

Degree of					Le	ngth of	rails in	n feet				
curve	10	12	14	16	18	20	22	24	26	28	30	33
0.5° 1° 1.5°	:::				 1 s	 1/8	1.8	 ½8 ½8	1.6 1.4	1/8 1/8 1/4	1/6 1/4 3/8	1/8 1/4 3/8
2° 2.5° 3°		 1/8	1/8 1/8 1/8	18 18	18 14 14	78 14 14 14	14 14 36	78 14 38 16	3,8 3,8 1,5	74 38 12 58	78 38 12 58	58 34 78
3.5° 4° 4.5°	 ½8 ½8	18 18 18	78 1,6 1,8 1,4	78 14 14 14	74 3/8 3/8	3/8 3/8 3/8 1/2	3/8 1/2 1/2	1.2 5.8 5.8	58 34 34	34 38 78	78 78 I	1 118 114
5° 5.5° 6°	1/8 1/8 1/8	1.6 1.4 1.4	14 14 14 38	3/8 3/8 3/8	38 12 14	1/2 5/8	5 % 3 4 3 4	34	78 I I158	I I ¹ / ₅ I ¹ / ₄	178 174 138	138 158 134
6.5° 7° 7.5°	18 18	14 14	3.8 3.8 3.8	16 16 16	1/2 5/8	3.4 3.4 3.4	7 ś 7 ś	I I Ils	11.6 11.4 13.8	136 112 112	1 ¹ / ₂ 1 ⁵ / ₈ 1 ³ / ₄	178 2 218
8° 8.5° 9°	1.4 1.4 1.4	1. ₄ 3. ₅ 3. ₈	3.8 3.8 1.2	1.2 58 58	3.4 3.4 3.4	78 78 78	I I ^{1.} 8 I ^{1.} 8	1^{1}_{4} 1^{1}_{4} 1^{3}_{8}	138 112 158	158 134 178	178 2 218	2 ¹ / ₄ 2 ³ / ₈ 2 ¹ / ₂
9 5° 10° 10.5°	74 74 14	3/8 3/8 3/8	1/2 1/2 5/8	5 % 5 %	34 78 78	I I I ¹ ś	1 ^{1,4} 1 ^{1,4} 1 ³ 8	138 112 158	134 134 178	2 2 2 ¹ /8	21/4 23/8 21/2	2 ³ 4 2 ⁷ 8
11° 11.5° 12°	1/4 3/8 3/8	38 12 12	58 58 58	3,4 3,4 3,4	I I I	115 114 114	138 1^{1}_{2} 1^{1}_{2}	1 ⁵ \$ 1 ³ 4 1 ⁷ 8	2 2 ¹ /8 2 ¹ /8	2 ¹ / ₄ 2 ³ / ₈ 2 ¹ / ₂	258 234 278	3½8 3½ 3½ 338
12.5° 13° 13.5°	3.8 3.8 3.8	1/2 1/2 1/2	58 58 34	78 78 1	11.5 11.8 11.4	138 138 112	158 158 134	2 2 2 ¹ /8	2 ¹ 4 2 ¹ 4 2 ³ 8	258 258 234	3 3 3 ¹ /8	3 ⁵ / ₈ 3 ⁷ / ₈
14° 14.5° 15°	3/8 3/8 3/8	1.6 5.6 5.6	3.4 3.4 3.4	I I I	114 114 114	1 ¹ / ₂ 1 ⁵ / ₈ 1 ⁵ / ₈	134 178 178	2 ¹ / ₄ 2 ¹ / ₄ 2 ¹ / ₄	2 ¹ / ₂ 2 ⁵ / ₈ 2 ⁵ / ₈	27/8 3 31/8	3 ¹ 4 3 ³ 8 3 ¹ 2	4 4½ 4½ 4½
15.5° 16°	3/8 3/8	5 §	76 78	118	138 138	15 g 15 g	2 2	2 ³ § 2 ³ §	27 8 27 8	3 ^{1,} 4 3 ^{1,} 4	358 334	438 458

TABLE LVIIIa. - GAGE ON CURVES

Degree of curve	Gage	Degree of curve	Gage
8° and under 9°-10° 11°-12° 13°-14°	4' 8½'' 4' 8½'' 4' 8¾'' 4' 8½"'	15°-16° 17°-18° 19°-20°	4' 9'' 4' 9½'' 4' 9¼''

CANTING THE TRACK

Using the gage for the base, if R = radius, S = speed in miles per hour and e is the difference in level of the two rails in feet,

$$e = \frac{4.708}{\sqrt{1 + 223.5 \frac{R^2}{S^4}}}$$

Using gage plus one rail head which the author recommends for use with the common track level,

$$e = \frac{4.9}{\sqrt{1 + 223.5 \frac{R^2}{S^4}}}$$

The corresponding approximate formulas are $e = \frac{0.3149 \ S^2}{R}$ and $e = \frac{0.3278 \ S^2}{R}$. In inches $E = 0.00066 \ S^2D$ and $E = 0.000686 \ S^2D$.

The formula of the American Railway Engineering Association for difference of level measured at the gage lines is

$$E = 0.00066 S^2 D$$
,

but the author recommends $E = 0.000686 S^2D$. Both formulas are tabulated in Tables LIX and LIXa.

TABLE LIX

Difference of level in inches of the two rails of a standard gage track on curves of various degrees for various speeds.

Formula: $E = 0.00066 S^2D$

(Nearest ½ inch)

Degree of					Sr	eed in	n mile	s per	hour					Degree of
curve	10	15	20	25	30	35	40	45	50	55	60	65	70	curve
1	=	1,6	1/4	3/8	5/8	34	11/8	138	15%	2	23/8	234	31/4	1
2	1/8	3/8	1,2	7/8	11/8	158	21/8	258	31/4	4	434	51/2	61/2	2
3	1/4	1,6	34	11/4	134	23/8	31/8	4	47/8	6	71/8	83/8	934	3
4	1/4	58	I	158	23/8	31/4	41/4	538	658	8	91/2			4
5 6	3,8	3/4	11/4	2	3	4	514	658	81/4					5 6
	3/8	I	158	21/2	31.6	47/8	61/4	8						
7	1,2	11/8	17/8	27/8	41/8	558	73/8							7 8
8	1/2	11/4	21.8	31/4	434	61/2	83/8							
9	5/8	13/8	23/8	334	538	71/4								9
10	34	11/2	258	41/8	578	81/8								10
11	3/4	134		$4\frac{1}{2}$	61/2	87/8								11
12	7/s	17/8	31/8	47/8	738									12
13	7∕8	2	33/8	53/8	734									13
14	Ι	21/8	358	534	838									14
15	I	21/4	37/8	61/4	87/8									15
16	1½	21/2	414	65%										16
17	$1\frac{1}{4}$	258	41/2	7										17
18	11/4	23/4	43/4	71/2										18
19	138	27/8	5	734										19
20	138	3	51/4	81/8										20

TABLE LIXa

From Formula $E = 0.000686 S^2D$ (Nearest $\frac{1}{16}$ inch)

Degree of					Spe	ed in	miles	per	hour					Degree of
curve	10	15	20	25	30	35	40	45	50	55	60	65	70	curve
0.5	1/16	1/16	1/8	3/16	5/16	7/16	9/16	11/16		11/16	114	17/16	111/16	0.5
	1/16	1/8	1/4	7/16	5/8	13/16	11/16		111/16	$2\frac{1}{16}$	21/2	27/8	33/8	I
	1/8	516	9/16	7/8	11/4	111/16	23/16		3716	41/8	415/16		634	2
	3/16	716	13/16	15/16	178	21/2	35/16		51/8	63/16	738	811/16		3
4	4	5/8	11/16			33/8	43/8		613/16					4
	3/8	3/4	13/8	21/8	31/16	4316	5716							5 6
	7/16	15/16	15/8	29/16	31 1/16	5.0	6916							
	1/2 9/16	1/16	115/16		45/16	513/16	75/8			• • •				7 8
	916 58	13/4 13/8	23/16 21/2	3 ³ / ₈ 3 ¹ ³ / ₁₆	47/8 51/2	69/16								9
	11/16	1916	23/4	41/4	61/8	71/2								10
	3/4	I11/16		474	634	i				• • •				11
	13/16	17/8	35/16	51/8	75/16					• • • •				12
		23/16						::	:::					14
	11/16	21/2		613/16				::						16
	11/4	234	415/16											18
20	13/8	31/16	57/16											20

TABLE LX

From Roberts' "Track Formulæ and Tables."

					_	_	_	-	_	-	_	_	-	-	-			_	_		_	_	_	_	_	
olts	No.	keg	102			148		153		153	153	153	225	225	225	225		225	225	225	247	247	247		247	247
Track bolts	3	Olze	1×434"	1×4¾"	78×4½"	78×4½"	78×4¾"	78×4½″	78×4½"	78×4½"	78×4½″	78×4½"	34×418"	34×418"	34×438"	34×418"	34×418"	34×438"	34×438"	34×418"	34×3½"	34×31/2"	34×3½"	34×3½"	34×3½"	3/4×31/2"
Wt. in	I pair	bars	99.5	99.2	87.0	87.0	74.0	74.0	I.89	1.89	63.1	63.1	58.5	58.5	54.0	54.6	37.8	34.0	35.6	32.4	32.4	34.0	34.0	28.9	27.2	25.5
		bars	34"	34"	34"	34"	34"			34"	34"	34,,	34,,	34"	34"	34,,	24,,	24"	54,,	24"	24"	24"	24"	24"		2.1″
	ck ts	Kgs.	0.399	0.366	0.275	0.252	997.0	0.244	0.266	0.244	0.266	0.244	0.181	991.0	0.181	0.181	0.121	0.121	0.121	0.121	0.110	0.110	0.110	0.110	O.IIO	0.110
f track	Track bolts	No.	40.68	37.29	40.68	37.29	40.68 0.266	37.29	40.68	37.29	40.68 0.266	37.29	40.68	37.29	40.68	40.68	27.12	27.12	27.12 0.121	27.12	27.12	27.12	27.12 0.110	27.12	27.12	27.12 0.110
r feet o	bars	Tons	0.301	0.276	0.263	0.241	0.224	0.205	0.206	0.144	0.191	0.180	0.177	0.162	0.163	0.165		0.163	0.108	0.101	0.101	0.103	0.103		0.082	0.077
Material per 100 linear feet of track	Angle bars	No. prs.			6.780	6.215	6.780	6.215											9	6.780	9	6.780	6.780		6.780	6.780
per ic	Spk.	Kgs.	0.64				0.64	0.65				0.65		0.65	0				0					0.64		0.64
terial	Ties	No.	60.0	9.09	60.0	9.09		9.09	0.09	9.09	0.09	9.09	0.09	9.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	0.09	60.09	0.09	0.09	0.09
Ma	Rail	Tons	3.274	3.274	2.976	2.976	2.678	2.678	2.530		2.381	2.38I	2.232	2.232	2.143	2.083		1.964	I.933	1.830	1.786	-		I.607	1.548	1.488
	ck ts	Kgs.	21.1	19.3	14.5	13.2	14.0	12.8	14.0	12.8	14.0	12.8	9.6	8.7	9.6	9.6	6.4	6.4	6.4	6.4	5.8	5.8	8.00	5.8	5.8	5.8
৸	Track bolts	No.	2148	8961	2148	8961	2148	1968	2148	1968	2148	8961	2148	1968	2148	2148	1432	1432	1432	1432	1432	1432	1432	1432	1432	1432
Material per mile of track	bars	Tons	15.90	14.57	13.90	12.74	11.83	10.83	10.88	9.93	10.08	9.24	9.35	8.57	8.63	8.73	6.04	5.43	5.69	5.18	5.18	5.43	5.43	4.62	4.35	4.08
er mile	Angle bars	No.	358								358	328	358		358	358			358	358		358	358	358	358	358
erial p	Spk.	Kgs.	33.8	34.I	33.8	34.I	33.8	34.I	33.8	34.1	33.8	34.1	33.8	34.1				38				33.8				
Mat	Ties	No.	3168	3200	3168	3200	3168	3200	3168	3200	3168	3200	3168	3200	3168	3168	3168	3168	3168	3168	3168	3168	3168	3168	3168	3168
	Rail	Tons	172.86	172.86	157.14	157.14	141.43	141.43	133.57	0.417 133.57	125.71	125	117.86	117.86	0.321 113.14	0.312 110.00	105.29	103.71		96.64			_	84.86		78.57
Wt.	rail	Tons	0.491	0.540	0.446	0.491	0.402	0.442	0.379	0.417	0.357	0.393	0.335 117	0.368	0.321	0.312	0.299	0.295	0.290	0.275	0.268	0.260	0.250	0.241	0.232	0.223
Lgth.	rail	Ft.	စ္က	33	30	33	30	33	30	33	30	33	30	33	30	30	30	30	30	30	30	30	30	30	30	30
One	lays	Lin. ft.	30.5	30.5	33.6	33.6	37.3	37.3	36.5	39.5	42.0	42.0	44.8	44.8	41.7	48.0	50.2	50.9	51.7				60.0	62.2	64.6	67.2
Wt.	yd.	Lbs.	OII	OII	100	100	8	96	85	85	8	8	75	75	72	70	29	99	65	6115	8	581/4	26	24	25	20

Note. — Data for angle bars and track bolts computed on basis of using 10 per cent of 24', 26' and 28' rails with 30' rails and 10 per cent of 24', 26', and 30' rails with 33' rails. The data computed on basis of using 18 ties per 30' rail and 20 ties per 33' rail. Spike 375 to keg of 200 pounds.

One ton = 2240 pounds.

(289)

TABLE LXI
Conversion of linear feet of 100 ft. wide right-of-way into acres
From Roberts' "Track Formulæ and Tables."

				Robert		c Formul					_	
Acres	Lin. R. of		A	cres	Lin. ft. R. of W.	Acres	Lin. R. of		Ac	eres		in. ft. . of W.
1.0	435			11.0	4791.6	21.0	914	7.6	31	0.1	1	13503.6
2.0	871.			12.0	5227.2	22.0		3.2	32	2.0		13939.2
3.0	1306.	- 1	-	13.0	5662.8	23.0	1001	8.8	33	3.0	. 1	4374.8
4.0	1742.			14.0	6098.4	24.0	1045			1.0		14810.4
5.0	2178.			15.0	6534.0	25.0	1089			5.0		15246.0
6.0	2613.	- 1		16.0	6969.6	26.0	1132			5.0		15681.6
7.0	3049			17.0	7405.2	27.0 28.0	1176			7.0		6117.2
8.o 9.o	3484			18.0	7840.8 8276.4	29.0	1219			3.0 9.0		16552.8 16988.4
10.0	4356			20.0	8712.0	30.0	1306	' '	1	0.0		17424.0
10.0	4330			20.0	0/12.0	30.0	1,300	0.0	41	3.0		17424.0
Acres	Lin. ft.	Acre	es	Lin. ft.	Acres	Lin. ft.	Acres	Lin.	ft.	Acı	res	Lin. ft.
	2.2			89.3		176.4		263	-5	Ι.		350.7
0.01	6.5	0.2	Ĭ	02.5	0.41	180.8	0.61	26-		0.	51	355 0
0.02	0.5	0.2	2	93.7	0.42	100.0	0.62	267	.9	0.8	32	355.0
0.02	10.9	3.2	-	98.0	1	185.1	0.02	272	.3	٠		359.4
0.03		0.2	3		0.43	-	0.63			0.8	83	
	15.2			102.4	1	189.5		276	.6		_	363.7
0.04	70.6	0.2	4	106.7	0.44	702 8	0.64	281		0.	84	368.I
0.05	19.6	0.2	=	106.7	0.45	193.8	0.65	201	.0	0.	8=	300.1
0.03	24.0	0.2	3	111.1	0.43	198.2	0.03	285	.3	*	0,5	372.4
0.06	·	0.26	6		0.46		0.66			0.	86	
	28.3			115.4	1	202.6		289	.7		_	376.8
0.07		0.2	7		0.47	206.9	0.67	294		0.	87	381.2
0.08	32.7	0.28	8	119.8	0.48	200.9	0.68	294		0.	88	301.2
0.00	37.0	0.2		124.1	1 0.40	211.3	0.00	298	3.4			385.5
0.09		0.29	9		0.49		0.69			0.5	89	
	41.4			128.5	'	215.6		302	.7			389.9
0.10		0.30	0		0.50	220.0	0.70	205		0.	90	394.2
0.11	45.7	0.3	т	132.9	0.51	220.0	0.71	307	.1	0.	от	394.2
0.11	50.1	J	-	137.2	1	224.3	".,"	311	.5	•	-	398.6
0.12	-	0.3	2		0.52		0.72			0.	92	
	54.5	١	_	141.6	1	228.7		315	.8	١.,		402.9
0.13	58.8	0.3	3	145.9	0.53	233.0	0.73	320	, ,	0.	93	407.3
0.14	30.0	0.3	4	145.9	0.54	233.0	0.74	ا	2	0.9	94	407.3
J.14	63.2		*	150.3	1 34	237.4	,-	324	-5		• •	411.6
0.15		0.3	5		0.55		0.75			0.9	95	
	67.5	١.,	_	154.6		241.8		328	.9	١ .	26	416.0
0.16	71.9	0.30	O	159.0	0.56	246.1	0.76	333	,	0.9	90	420.4
0.17	11.9	0.3	7	139.0	0.57	240.1	0.77	333		0.9	97	425.4
	76.2	"		163.4	1 "	250.5	''	337	.6			424.7
0.18		0.38	8	١. ١	0.58		0.78	1		0.	98	
	80.6	ا		167.7		254.8	. =0	341	.9	١.,	00	429.1
0.19	84.9	0.39	9	172.1	0.59	259.2	0.79	346	. 2	0.	99	433.4
0.20	04.9	0.40	0	1,2.1	0.60	239.2	0.80	540		1.4	00	
	89.3	"		176.4		263.5		350	-7	l		437.8
						1			_			

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TABLE LXII. - Drainage Areas

Sq. ft. opening = $C\sqrt[4]{(drainage area, in acres)^3}$ From Roberts' "Track Formulæ and Tables."

10 20 30	5.6 9.5 12.8	Sq. ft. open	ing required	
20 30	9.5		T.O.	
30		6.2	1.9	I.I
- 1	12.8		3.2	1.9
		8.5	4.3	2.6
• 40	15.9 18.8	10.6	5.3	3.2
50 60	21.5	12.5	6.3 7.2	3.8
	- 1	14.3	7.2 8.1	4.3
70 80	24.2 26.7	16.1 17.8	8.1 8.9	4.8 5.3
90	29.2	17.8	9.7	5.3 5.8
100	31.6	21.1	10.5	6.3
150	42.9	28.6	14.3	8.6
160	44.9	29.9	15.0	9.0
200	53.2	35.5	17.7	10.6
240	60.9	40.6	20.3	12.2
300	72.1	48.I	24.0	14.4
320	75.9	50.6	25.3	15.2
400	89.4	59.6	29.8	17.9
480	102.5	68.3	34.2	20.5
500	105.7	70.5	35.2	21.1
560	115.1	76.7	38.4	23.0
600	121.2	80.8	40.4	24.2
640	127.2	84.8	42.4	25.4
800	150.4	100.3	50.1	30. I
1000	177.8	118.5	59.3	35.6
2000	299.0	199.3	99.7	59.8
2500	353.5	235.7	117.8	70.7
3600	464.8	309.9	154.9	93.0
5000	594.6	396.4	198.2	118.9
6000 7000	681.7 765.3	454.5 510.2	227.2 255.1	136.3 153.1
		-		
8000 9000	845.9 924.4	563.9 616.3	282.0 308.1	169.2 184.9
10 000	1000.0	666.7	333.3	200.0

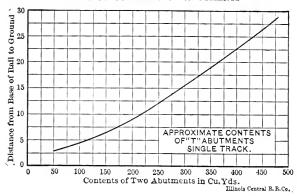
I. C. R.R. Co., 1906.

Extended, 1909, by S. S. R.

TABLE LXIII

From Roberts' "Track Formulæ and Tables."

CURVES OF CONTENTS OF ABUTMENTS



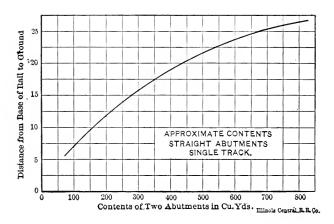


TABLE LXIV. — Cost Curves Timber Trestles From Roberts' "Track Formula and Tables"

Unit Prices.

Material in Place.

Caps	\$55.00 per M. Ft. B.M.
Stringers	55.00 per M. Ft. B.M.
Other material	43.00 per M. Ft. B.M.
Piles	o.37 per linear foot.
Untreated Material:	
Caps	\$42.00 per M. Ft. B.M.
Stringers	42.00 per M. Ft. B.M.
Other Material	30.00 per M. Ft. B.M.
Piles	0.24 per M. Ft. B.M.
Iron	0.05 per pound.

To the cost of the trestle obtained from the following curves by multiplying the cost per foot by the length, add for single track:

\$25.00 for two bulkheads in all cases.

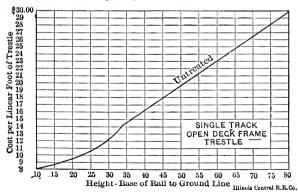
Creosoted Material:

\$50.00 for two bulkheads in all cases.

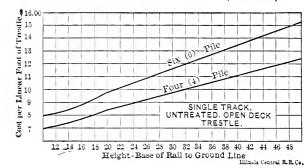
1.40 per linear foot for ties and ballast for ballast floors only.

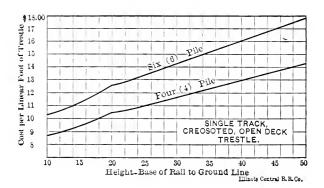
Creosoted open deck trestles have piles, caps and braces creosoted. Ballast floor trestles have all material creosoted.

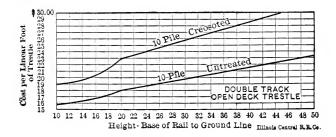
The cost per linear foot given by the following curves does *not* include longitudinal bracing. This should be figured separately for each trestle as the conditions at the opening may require.



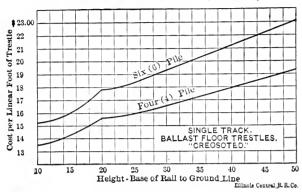












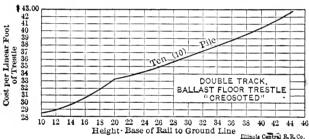


TABLE LXV. - PRELIMINARY CULVERT ESTIMATES AND BRIDGE WEIGHTS

Diam-		Iron pipe		Concrete arch									
eter, inches	Area, sq. ft.	Weight, lbs. per lin. ft.	Cu. yds. masonry, two ends	Dimen- sions, feet	Area, sq. ft.	Cu. yds. per ft. length	Cu. yds., two ends						
12 16 18 20 24 30 36 42	0.79 1.40 1.77 2.18 3.14 4.91 7.07 9.62	72.5 107.8 127.7 165.7 200.6 290.2 391.6 512.2	4.0 5.0 5.7 6.5 7.8 10.8 13.2 17.8	2× 2 3× 4 4× 6 6× 6 8× 8 10×10 12×12 15×15	3.5 10.9 22.0 30.4 54.4 85.4 123.3 193.2	0.57 1.06 1.63 3.10 3.99 5.57 6.89 8.81	8.0* 26.1* 60.9* 42.5† 76.2† 109.0† 168.4† 278.5†						

Square end walls.
 † Thirty-degree wing walls.

BRIDGE WEIGHTS*

W= weight of steel in pounds. l= span in feet for truss bridges and length overall for girder bridges.

Plate Girders:

i late of action	
Deck plate girder	$W = 12 l^2 + 150 l$
Through plate girder, iron floor system	$W = 12 l^2 + 500 l$
Through plate girder, large ties on shelf	
or flange angles	$W = 9\frac{1}{4}l^2 + 150l$
Through plate girder, solid iron floor	$W = 12 l^2 + 800 l$
Riveted Lattice Bridges:	
Deck bridge, cross-ties on top chord	$W = 7 l^2 + 200 l$
Through bridge, iron floor system	$W = 7 l^2 + 300 l$
Pin Connected Bridges:	
Deck span, cross-ties on top chord	$W = 5l^2 + 250l$

Through span, iron floor system $W = 7 l^2 + 650 l$ TABLE LXVI. — Preliminary Ballast Estimates

Deck span, iron floor system..... $W = 5 l^2 + 475 l$

Ties $6'' \times 8'' \times 8'$.

18 ties to a 33-ft. rail.

Tabular quantities are in cubic yards per mile.

Depth under tie		above tie at slope 2-1	top of ties	one level with s I ft. outside es I½-I
in inches	Single track	Double track	Single track	Double track
6 8 10	1400 1737 2095 2476	4159 4952 5767 6603	1965 2396 2845 3309	4418 5306 6210 7131

^{*} From "Modern Framed Structures" by Johnson, Bryan and Turneaure.

CHAPTER VI

TURNOUTS AND CROSSOVERS

Let F = frog angle.

S =switch angle.

f =toe length of frog from theoretic point.

T = heel spread of switch.

t = point thickness of switch rail.

t' = point thickness of actual frog point.

N = number of frog.

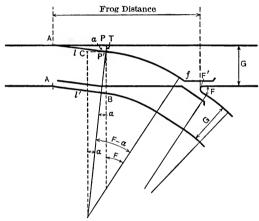


Fig. 26.

l = length of switch rail.

R = radius of turnout curve.

G = gage of track.

$$N = \frac{1}{2} \cot \frac{1}{2} F$$
, $\sin S = \frac{T - t}{I}$.

Frog distance = $I + [G - (T + f \sin F)] \cot \frac{1}{2} (F + S) + f \cos F + t'N$

$$R + \frac{1}{2}G = \frac{G - (T + f\sin F)}{2\sin\frac{1}{2}(F - S)\sin\frac{1}{2}(F + S)}$$

Values for F, R, frog distance, S, and other quantities for varying values of N and l are given in Tables XLVII and XLVIII, and for spring rail frogs in Table XLIX.

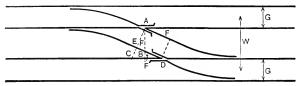


FIG. 27.

$$BD = (W - G) \cot F - \frac{G}{\sin F},$$

$$ED = \frac{W - G}{\sin F} - G \cot F.$$

Total length = $BD + 2 \times frog$ distance to theoretic point.

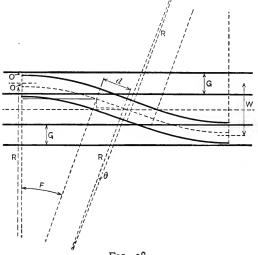


Fig. 28.

$$O = T - (R + \frac{1}{2}G) \text{ vers } S,$$

$$Vers (F + \theta) = \frac{\frac{W}{2} - d \sin F - O}{R},$$

$$\theta = (F + \theta) - F,$$

$$p = l - (R + \frac{1}{2}G)\sin S,$$

$$L = \text{length of crossover} = 2 \{R\sin (F + \theta) + d\cos F \mp p\}.$$

Distance between frogs = $L - 2 \times$ frog distance.

Length of connecting rail = $2 R \frac{\theta}{57.3}$.

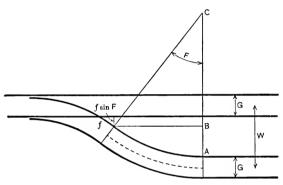


FIG. 29.

$$R = \frac{W - G - f' \sin F}{\text{vers } F} + \frac{1}{2}G.$$

Curve length is $R \frac{F}{57.3}$.

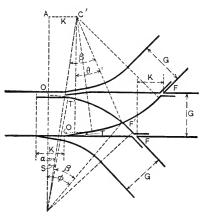


FIG. 30

K and the elements for both turnouts with equal frog angles F are known. To find F'' and the crotch frog distance.

$$O = T - (R + \frac{1}{2}G) \text{ vers } S,$$

$$AC = 2(R + O),$$

$$\frac{K}{AC} = \tan \alpha, \qquad CC' = \frac{K}{\sin \alpha} \quad \text{or} \quad \frac{AC}{\cos \alpha},$$

$$\frac{AC}{2(R + \frac{1}{2}G)} = \cos \beta, \qquad F'' = 2\beta,$$

$$\phi = \alpha + \beta,$$

$$\theta = \beta - \alpha$$

Crotch frog distance from first point is

$$L = (R + \frac{1}{2}G) (\sin \phi - \sin S) + l + \frac{N''}{32}.$$

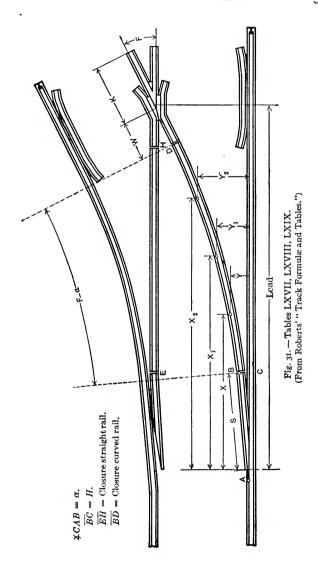


TABLE LXVII. — Properties of Frogs and Switches and Theoretical Switch Leads

In all cases gage is considered 4 ft. 8_2^1 in.

		Closure bevruce list	XIV	Feet	00 60	60.00	28.55	33.38	41.24	46.42	49.92	52.58	55.17	64.20	96.89	92.46	95.05	104.61	113.76	130.77
	s	Closure straight rail	XIII	Feet	88 00	00.33	28.19	33.11	41.02	46.22	49.74	52.40	55.oI	64.06	68.83	92.36	94.95	104.54	113.68	130.66
	Theoretical leads	Distance point to list and switch risil to theoretical to point of trog	XII	Peet	30 22	0.70	42.77	48.11	61.94	67.47	72.24	74.90	77.51	92.06	97.25	133.02	135.95	146.38	156.35	175.09
	Ţ	D = degree of lead curve	IX	Degrees	23 800	02.000	31.073	21.033	15.789	11.744	9.308	8.192	7.255	6.097	5.044	3.284	2.857	2.214	1.756	1.162
		R = radius of center line	×	Feet	ye ell	20.00	103.22	273.95	364.88	488.71	616.27	26.669	790.25	940.21	1136.34	1744.38	2005.98	2587.66	3262.98	4932.77
	Properties of switches for all switches Thickness of point $= 0.4$ " and heel distance $= H = 6.4$ "	dotiwe = a algna	XI	Degrees	2 605	109	2.002	2.605	1.736	1.736	1.736	1.736	1.736	1.302	1.302	0.868	998.0	0.868	0.868	0.868
-0.0	Properties of so for all switc Thickness of =0¼" and distance=H=	ntgnsl = 2 fortive to list	VIII	Ft. In.	,			0 11	9 91	9 91		9 9I		22 0	22 0	33 0	33 0	33 0	33 0	
		Spread at leed	VII	Feet	Y 22	900	1.20	1.10	1.15	1.09	1.11	1.05	1.05	1.05	10.1	0.99	8.1	86.0	0.97	0.97
	1.51	Spread at 500t	VI	Feet	0.70		0.71	00.00	0.63	0.59	0.67	0.63	0.60	0.54	0.53	0.51	0.50	0.49	.0.48	0.47
	ogs points o!	Total length	Λ	Ft. In.	8			o II	12 6	13 6	0 91	-	9 91	9 41	18 6	22 6	24 0	26 6	29 0	
	Properties of frogs mess of all frog poi	K = length theoretical point to heel	IV	Ft. In.	u	r 1		2 0	8	8	10 0	0 01	9 01	9 11	12 I	14 IO	0 91	17 8	19 4	
	Properties of frogs Thickness of all frog points 0½"	W = length theoretical point to toe	III	Ft. ln.	2 2		?	4	4 5	4		0 9	0	0 9	9		8	8 IO		11 4
	Th	F = frog	II	Degrees	14 250	107 11	11.421	9.527	8.171	7.153	6.360	920.9	5.725	5.205	4.772	3.818	3.580	3.182	2.864	2.387
		N = 100	I	202)		. 1	٥,	٥	7	×	6	6,6	OI	11	12	15	91	18	50	24

TABLE LXVIII. — PRACTICAL SWITCH LEADS In all cases gage is considered 4 ft. 8½ in.

		_			_	_		_	_	-	-	-	_	_	_	_	_	-	
	bevrue for curved rail	CIO	XXVIII		4	· 00	3	I-14.11 I-27		I-16.59 I-33		1-27.17 1-28		4		0 2-33		7 1-33	
			ľ		1-24	1-28	1-33	I-I	I-I	Ī	1-26	1-2	2-33	3-24	2-33	1-30	4-26	3-27	4-33
	tdgierts rot erus lier		XXVII					1-27	I-30	1-33	1.27	1-28	1-33	2-24	1-25.9	2-33	3-26	2-27 1-33	
	tdsients 101 91us	CIP	xx		1-23.60	1-27.68	1-32.73	1-13.89	1-16.40	1-16.41	1-25.82	1-27	1-32.85	1-23.88	2-33	1-29.90	1-25.93	1-26.92	1-32.89
	to a distance act- distance of switch distribution of the foot foot foot	en	XXVI	Feet	37.94	42.47	47.98	62.10	67.98	72.28	75.71	77.93	94.31	100.80	133.28	137.57	146.51	157.42	177.22
	= distance act- point of switch point of the gonl to throg	en	XXV	Feet	37.77	42.26	47.73	61.81	67.65	16.17	75.32	77.51	93.85	100.30	132.66	136.90	145.76	156.59	176.22
	- tangent adja- gori lo sot ot tn	$_{^{J}\!L}^{J}$	XXIV	Feet	9.0	0.82	99.0	0.19	8.0	0.57	0.0	0.0	0.0	0.0	0.0	0.0	1.08	8.0	8.0
l leads	= tangent adja- fist daiwe of tail	eso L	XXIII	Feet	1.03	0.0	8	0.0	0.30	8.0	92.0	0.0	2.99	5.33	8.0	1.56	8.0	0.44	2.43
Practical leads	arter rved I as	Y_2	XXII	Feet	2.79	2.62	2.72	2.74	2.91	2.75	2.83	2.85	2.87	2.91	2.82	2.87	2.86	2.93	3.8
	Rectangular coördinates to the quarter and center points on gage side of curved rail, referred to point of switch rail as origin	Y_1	XXI	Feet	1.67	19.1	1.74	1.71	1.78	1.76	1.82	1.84	1.84	06.1	1.78	1.82	1.82	I.88	1.97
	dinates to on gage si point of sw origin	I	xx	Feet	0.97	0.95	I.0I	0.97	1.02	1.02	1.06	1.06	1.08	1.15	10.1	1.04	1.04	1.08	1.27
	coördin oints or od to poi	X_2	XIX	Feet	29.75	31.27	35.15	47.11	51.45	53.19	56.37	57.81	72.19	77.28	100.41	105.35	IIO. IO	118.59	132.59
	tectangular coördinates nd center points on gage rail, referred to point of origin	X_1	XVIII	Feet	23.44	24.54	27.13	36.93	39.91	40.98	43.35	44.05	56.47	60.65	77.95	91.76	84.46	90.21	100.21
	Rect and rail	x	XVII	Feet	17.74	17.78	19.07	26.72	28.37	28.75	30.31	30.28	40.74	43.99	55.49	58.16	58.73	61.84	67.82
	$O_1 = \text{degree of}$ lead curve	,	XVI	Degrees	53.707	33.333	21.718	15.875	11.774	9.478	8.246	7.255	6.213	5.216	3.284	2.883	2.242	1.759	1.173
	$R_1 = \text{radius of}$ center line		XV	Feet	110.69	174.34	265.39	362.08	487.48	605.18		790.25	922.65	1098.73	1744.38	1993.24	2546.31	3257.26	4886.16
	gorl = V rədmun		I		4	S	9	7	∞	6	3/ ₁ 6	õ	II	12	15	91	81	9	24

TABLE LXIX. — TABLE OF SWITCH LEADS FOR SPRING FROGS

	Frog	ber,	9	7	∞	6	5/16	OI	12	15
		quired		0	10	9	4	4	7 2-15	,
	ds	Rails required	30	27 2-10	2-30 2-15	2-26	30 2-24	3 2-27	72-27	13 4-27
red	ıl lea	~	2-30	2-27		2-27	2–30	2-33	2–30	2-33
conside	Practical leads	Degree of curve	24.150°	16.750°	12.600°	9.533°	8.583°	7.500°	5.083°	3.033°
frog not		Length in feet	47.00	56.00	67.00	73.00	77.50	80.50	97.00	114.50
point of	Theoretical leads	Degree of curve, D	24.083° 24.583°	16.283° 16.750° 17.133°	12.100° 12.533°	9.467°	8.333° 8.450°	7.383°	4.867° 4.933°	2.950° 3.033°
Thickness of switch rail at point and bluntness of point of frog not considered	Theoret leads	Length in feet,	46.89	52.61 56.02 60.55	61.73	72.48	75.3I 77.84	78.07	91.81 94.67	109.91
nnd blun		G.C.	4' 8!\2" 4' 8!\2"	4' 8\5'' 4' 8\5'' 4' 8\5''	4' 8!2" 4' 8!2"	4' 81,2"	4' 8½" 4' 8½"	4' 8'\2"	4' 8'5"	4' 8!2" 4' 8!2"
t point a	Switch	angle, a	2.388° I.990°	2.388° 1.990° 1.592°	I.990° I.592°	I.592°	1.592° 1.448°	1.592° 1.448°	I.448° I.326°	1.326° 1.194°
h rail a	Heel die.	tance,	2, 2,	ณ์ณ์	2, 2,	2,,	2,'2	2,"	2, 2,	5″,
of switc	Length	switch rail, S	10' 0"	10' 0'' 12' 0'' 15' 0''	12' 0''	15, 0,,	15, 0"	. 16' 6"	16' 6" 18' 0"	18' o'' 20' o''
ckness		point to heel, K	8, 0,,	8, 0,,	% 0,/	8, 0,,	8, 0,,	% 0,%	% o,,	8' 0"
Thi	Dis-	point to toe, W	7, 0,,	1,0 ,1	1,0 ,1	7, 0,,	7, 0,,	7, 0,,	1,0,1	7, 0,,
	Frog	angle,	9.533°	8.167°	7.150°	6.367°	6.033°	5.733°	4.767°	3.817°
	Frog	ber,	9	7	œ	6	5/6	01	12	15

From Roberts' "Track Formulæ and Tables."

CHAPTER VII

AZIMUTH, LATITUDE, AND TIME

Meridian Determinations. 1. By an Observation on Polaris at Elongation. — Find the time of elongation from Table LXXI. Just before the time of elongation set the transit over a point and with the alidade clamped turn the telescope on the star, clamp the limb and follow the star with the slow motion till it seems to stop traveling east or west as the case may be. Plunge the telescope and range out a stake in line. If the observer is quick he may transit the telescope and take a second observation with the telescope reversed before the star moves in azimuth appreciably. Compute the azimuth of the star at elongation from the formula

$$Sin Z = \frac{\sin pole distance}{\cos latitude}.$$

The pole distance is found in Table LXX. The latitude may be taken to the nearest minute from a good map or determined as in the next article. Next morning set again over the transit point and from the established line set off Z and range out the meridian.

2. By an Observation on Polaris at Any Time. — This is not so good as the preceding method but is often more convenient and sufficiently precise for practically all field purposes.

Set the transit over a point and at any instant set the intersection of the wires on the star by clamps and slow motions. Range out a line in the azimuth plane of the star. Compute the azimuth of this line from the equation

$$\sin \frac{1}{2}Z = \pm \sqrt{\frac{\sin (s-a)\sin (s-l)}{\sin a\sin l}},$$

in which $s = \frac{1}{2}(d + a + l)$, d being the pole distance, a the co-altitude, and l the co-latitude.

Since there are two equal azimuth angles — one east, the other west — for any given altitude, and four positions of the star that will give the same Z angle — two east and two west of the meridian — the observer must know from the observed motion of the star in which quadrant of its apparent revolution the star is, or he may know from the

times of observation and culmination, the latter taken from Table LXXI.

3. By Equal Altitudes of a Star. — In the southern hemisphere or elsewhere when not convenient to use Polaris, use equal altitudes of any star that may be observed on both sides of the meridian at reasonable altitudes of between 20° and 40°.

Select a star; set up the instrument over a fixed point; clamp one horizontal motion, and with the other and the vertical motion of the telescope bring the intersection of the wires approximately on the star: clamp both motions; set the vertical circle to read a whole minute or 0.01° such that the star is approaching the horizontal wire: follow with the azimuth motion so that when the star is on the horizontal wire it shall be also on the vertical wire, i.e., at the intersection of the wires. Plunge the telescope and range out a stake some distance ahead. Repeat once or twice at intervals of from ten to twenty minutes and range out other points, numbering the points 1, 2, 3, etc. Set the vertical circle to read the last measured altitude and wait till the star again reaches it when an exact setting is made and a stake ranged out; set at the next altitude and repeat the operation until as many stakes are set on one side of the meridian as on the other, numbering them 3, 2, 1. The extra stakes are for checks on the work. In the morning bisect the angles 1-instrument-1, 2-instrument-2, etc., and set points which should coincide but may not. If they do not coincide set a point to average them unless there is enough variation to indicate an error. To average them select the most east or west of the middle points as an origin and measure the distance to each of the other middle points, add and divide by the number of middle points. The result is the distance of the average point from the origin. Use this and the instrument point to define the meridian. The times should be at least from one and one-half to two hours either side of the meridian. reaching culmination early in the night should be chosen. Approximate north and south will be known by the needle or the daytime position of the sun.

4. By a Transit Observation on the Sun. — Measure the altitude of the sun and its azimuth from any fixed line at the same instant; substitute the altitude, the latitude of the place determined from a good map to the nearest minute or by one of the methods of the next article, and the declination of the sun (explained later) in the formula,

$$\sin \frac{1}{2}Z = \pm \sqrt{\frac{\sin (s' - \phi) \sin (s' - h)}{\cos \phi \cos h}},$$

in which Z is the azimuth of the sun measured from the meridian, ϕ is the latitude, h is the altitude, and $s' = \frac{1}{2} (90 - \delta + \phi + h)$, δ being the declination taken with its proper sign, + when north and - when south. The difference between Z and the observed azimuth from the fixed line gives the azimuth of that line from which the meridian may be run out.

To make the observation, set the transit over a point at least one and one-half hours before or after noon and as long after sunrise or before sunset, and use any fixed distant point for zero azimuth. Use a piece of colored or smoked glass in the eyepiece cap or before the object glass, and bring the cross wires tangent to the sun's disc, approximately by hand motion of the alidade and telescope and clamps and precisely by both slow motions together; read the vertical circle and the azimuth. Subtract the refraction correction of Table LXX for the measured altitude from the vertical circle reading.

If the horizontal wire has been made tangent to the lower limb (edge) of the sun, add the sun's semi-diameter, 16^m or 0.26667°, to the corrected vertical circle reading; if the upper limb has been observed subtract the semi-diameter. The result is the correct altitude of the sun at the instant of observation. The sun's semi-diameter is not exactly 16^m but varies during the year and may be had from the Nautical Almanac mentioned later if greater precision is desired.

The measured azimuth from the reference line is increased or diminished according as the edge nearest or farthest from the reference line is observed, by $16' \times \sec h$ or $0.27^{\circ} \sec h$. If the observer is satisfied to quarter the sun's image with the cross wires no semi-diameter correction is required either for altitude or azimuth.

Explanation of Astronomical Terms. — Celestial bodies are located on the celestial sphere by coördinates corresponding to latitude and longitude of the terrestrial sphere. The celestial equator is a circle cut from the celestial sphere by the terrestrial equatorial plane extended, and angular distances north or south of the celestial equator are called declinations, corresponding to terrestrial latitude. An arbitrary meridian of the celestial sphere is chosen as the reference for what is called right ascension, corresponding to longitude. Right ascension is not used in the methods of this chapter.

The declination of the sun changes constantly. The Nautical Almanac or American Ephemeris, published by the Government annually, gives the hourly change. Several instrument makers distribute gratis in pocket form reprints of that part of the Nautical Almanac relating to the sun and useful to surveyors. Every surveyor should have one of these reprints.

To determine the declination at a given place and hour on a given day the approximate Greenwich time of the observation must be known. In North America if standard time is carried by the observer, he will know what meridian time he carries and hence how many hours slow he is of Greenwich time; Eastern time is 5 hours, Central time 6 hours, Mountain time 7 hours, and Pacific time 8 hours slow of Greenwich time. The Almanac gives the coördinates of the sun for Greenwich apparent and mean noon, and some reprints give the coördinates for one and some for the other.

Noon. — The sun does not appear to move at a uniform rate around the earth. Apparent noon is the instant the sun appears to cross the meridian. Mean noon is the instant that an imaginary sun, moving at a uniform rate and making the same number of revolutions in a year as the real sun, appears to cross the meridian. Mean time is time according to the mean sun and is what is carried by clocks and watches. The difference between apparent and mean time is called the equation of time and is found in the Nautical Almanac and reprints. It is sometimes to be added and sometimes subtracted to convert one time into the other. The sign to be used is given with the equation.

Assuming standard time at any place where central time is used, 9 o'clock in the morning, being 3 hours before noon, would be (6-3) hours = 3 hours after noon at Greenwich, and the declination of the table for a given day must be corrected for 3 hours change. In the table — means south and + north. If the change is marked — the sun is going south, and north or + declination is decreasing, while south or — declination is increasing.

If local mean time is carried by the observer he must know his approximate longitude and must convert this into time, 15° to the hour, to find the difference between Greenwich and local time. In either case if his reprint gives the position of the sun for apparent noon, he must apply the equation of time to his mean time to find the local or standard apparent time.

The positions of heavenly bodies are figured from the center of the earth. With a body as near as the sun this gives rise to a correction to altitudes measured at the surface known as the correction for parallax. It is but a few seconds and is neglected in this discussion. The methods of this chapter are such as are suited to field instruments reading to minutes or 0.01 of a degree and many refinements necessary in astronomical work are omitted.

Latitude. 1. By Polaris. — The altitude of the north pole equals the latitude of the place of observation. Measure the altitude of Polaris

at upper or lower culmination, subtract the refraction correction found in Table LXX. Add or subtract the pole distance of the star as found in Table LXX, according as lower or upper culmination is observed. The result is the latitude.

TABLE LXX. — POLAR DISTANCE OF POLARIS
For January 1 of years named

1915	1918	1921	1924	1927	1930	1933	1936	1939	1942
1.149°	1.133°	1.118°	I.102°	1.087°	1.071°	1.056°	1.041°	1.026°	1.011°

Sin of azimuth at elongation = $\frac{\sin \text{ polar distance}}{\cos \text{ine latitude}}$.

Latitude = altitude of Polaris at culmination \pm polar distance - refraction correction given below.

Latitude or altitude	Correction	Latitude or altitude	Correction
20° 30° 40°	0.043° 0.027°	50° 60°	0.013° 0.009°

To observe, set up a little before the time of culmination found in Table LXXI; set the horizontal wire on the star and follow with the slow motions till the star's motion seems to be wholly in azimuth and not at all in altitude. Read the vertical angle.

2. By a Noon Observation of the Sun.— Measure the altitude of the sun when at its highest point; subtract the refraction correction of Table LXX for the altitude found; subtract the sun's declination if north or add if south; the result is the co-latitude.

To observe set up the transit a little before noon; set the horizontal wire on the upper or lower limb (edge) of the sun's disc and keep it there as the sun rises and until it has ceased to rise and its motion seems to be wholly in azimuth; read the vertical circle very carefully and subtract or add the sun's semi-diameter according as the upper or lower limb was observed. Colored or smoked glass must be used, preferably in the eyepiece cap rather than before the object glass, but either may answer. The sun's semi-diameter is an average of 16 minutes or

0.26667°. It varies during the year and may be had from the Nautical Almanac or makers' reprint (see previous article) if desired to greater precision.

TABLE LXXI*

Approximate local mean times (counting from noon 24 hours) of the elongations and culminations of polaris in the year 1915 for latitude 40° N.; longitude $6^{\rm H}$ W. from Greenwich.

Date	East elongation		West elongation		Upper culmination		Lower culmination	
Jan. 1	h. o 23 22 21 20 20 18 17 16 16 14 13 12 12 10 10 8 7 6	m, 52.1 53.0 45.9 50.6 55.4 00.2 53.3 58.1 55.3 00.4 53.8 58.9 56.3 01.5 55.0 00.1 53.5 58.6 55.8	h. 12 11 10 9 8 7 6 5 4 3 2 1 0 23 22 21 20 19 18	m. 42.1 46.8 39.7 44.2 49.2 54.0 47.1 51.9 49.1 51.2 47.6 52.7 50.1 51.5 48.6 45.8	h. 6 5 4 3 3 2 2 1 0 23 22 21 20 19 18 17 16 15 14 13 12	m. 47.18 51.8 44.7 49.4 54.2 59.0 52.1 43.1 50.3 55.4 48.8 53.9 51.3 56.5 50.0 55.1 48.5 53.6	h. 18 17 16 15 14 13 12 11 10 9 8 7 6 5 4 3 2 1	m. 45.2 49.9 42.8 47.5 52.3 50.2 55.0 52.2 57.3 50.7 55.8 53.2 58.4 51.9 50.4 55.5 52.7
15	6	00.8	17	50.8	11	55.8	23	53.9
Nov. 1	4 3	54.0 58.9	16 15	44.0 48.9	9	49.0 53.9	22 2I	47.I 52.0
Dec. 1	2 2	55.8 00.6	14 13	45.8 50.6	8 7	50.8 55.6	20 19	48.9 53.7

^{*} From data furnished by the U.S. Coast and Geodetic Survey.

Approximate Determination of Time. 1. To Find the Error of a Watch. — The observation for azimuth on the sun may be utilized. The instant of the observation should be noted on the watch. Then

$$\sin t = \frac{\sin Z \cos h}{\cos \delta},$$

in which t is the hour angle in degrees before or after apparent local noon. Reduce t to hours by dividing by 15 and find the apparent local time; apply the equation of time for the day from the Nautical Almanac, and the result is mean local time. The longitude of the place must in general be had from a map, if possible to the nearest minute. The difference between local longitude and the standard meridian whose time is carried reduced to time is applied to the determined mean local time to get the mean standard time. The difference between this and the observed time of the observation is the error of the watch. If the watch carries local time, longitude is needed only to compute change in declination and need not be so precisely determined.

To refer to any calendar day other than the first and fifteenth of each month, subtract 3.94^m for every day between it and the preceding tabular day, or add 3.94^m for every day between it and the succeeding tabular day.

To find the times for the tabular dates after 1915, to the tabular value add 1.36^m for each year after 1915 less 3.9^m for each leap year. In any leap year deduction for that year is not made until March 1.

To find the time of western elongation for Jan. 18, 1919:

For January 15, 1915, western elongation, tabular time is 11^h 46.8^m. 1919 – 1915 = 4; $4 \times 1.36 = 5.4$. One leap year has intervened, and, therefore, $5.4 - 3.9 = 1.5^m$ to be added. 11^h 46.8^m + 1.5^m = 11^h 48.3^m for January 15, 1919. For January 18 subtract 38 – 15 = $3 \times 3 \times 3.94^m = 11.8^m$ getting 11^h 36.5^m.

To refer to any other than the tabular latitude between the limits of 25° and 50° north add to the time of west elongation 0.13^m for every degree south of latitude 40°, and subtract from the time of west elongation 0.18^m for every degree north of 40°. Reverse these signs for corrections to the times of east elongation. For latitudes as high as 60° diminish the times of west elongation and increase the times of east elongation by 0.23^m for every degree north of latitude 40°.

To refer to other longitudes, add 0.16^m for each hour east of 6 hours and subtract 0.16^m for each hour west of 6 hours.

TABLE LXXII

Length of o.or° of latitude and o.or° of longitude to the nearest

Length of o.o1° of latitude and o.o1° of longitude to the nearest whole foot

Latitude	Length o.or° latitude	Length o.or° longitude	Latitude	Length o.or° latitude	Length o.or° longitude
•					
1	3628	3652	31	3637	3133
2	3628	3650	32	3638	3100
3	3628	3647	33	3638	3066
	3628	3643	34	3639	3031
=	3628	3638	35	3640	2995
4 5 6	3628	3632	36	3641	2958
	3628	3625	37	3641	2920
7 8	3628	3617	37	3641	2882
9	3628	3608	39	3642	2842
10	3629	-	40	3643	2802
11	3629	3597 3586	41	3643	2761
11	3629 3629	3573	41	3644	2719
					2675
13	3629	3559	43	3645 3646	2075 2632
14	3630	3545	44		2587
15	3630	3529	45	3646	
16	3631	3512	46	3647	2542
17	3631	3494	47	3647	2495
18	3631	3475	48	3648	2449
19	3631	3455	49	3649	2401
20	3632	3433	50	3649	2353
21	3632	3411	51	3650	2303
22	3633	3388	52	3650	2254
23	3633	3364	53	3651	2203
24	3634	3338	54	3652	2152
25	3634	3312	55	3652	2099
26	3635	3285	56	3653	2047
27	3635	3256	57	3653	1994
28	3635	3227	58	3654	1940
29	3636	3197	59	3655	1886
30	3637	3166	60	3655	1831

TABLE LXXIII. — Convergence of Meridians

Latitude	Angular convergence per mile, degrees	Distance for convergence of o.oi°, feet	Latitude	Angular convergence per mile, degrees	Distance for convergence of o.or°, feet
۰			•		
1	0.000	209,240	31	0.000	6084
2	.001	104,588	32	.009	5851
3	.001	69,690	33	.009	5629
4	.001	52,231	34	.010	5420
5	100.	41,747	35	.010	5222
5 6	.002	34,750	36	.010	5032
7	.002	29,747	37	.011	4852
8	,002	26,002	38	.011	4681
9	.002	23,062	39	.012	4516
10	.003	20,715	40	.012	4359
11	.003	18,792	41	.013	4208
12	.003	17,185	42	.013	4062
13	.003	15,823	43	.013	3922
14.	.004	14,651	44	.014	3788
15	.004	13,634	45	.014	3658
16	.004	12,740	46	.015	3533
17	.004	11,950	47	.015	3412
18	.005	11,244	48	.016	3295
19	.005	10,611	49	.017	3181
20	.005	10,039	50	.017	3071
21	.006	9,518	51	.018	2964
22	.006	9,044	52	.018	2860
23	.006	8,609	53	.019	2758
24	.006	8,208	54	.020	2660
25	.007	7,837	55	.021	2563
26	.007	7,493	56	.021	2469
27	.007	7,173	57	.022	2377
28	.008	6,874	58	.023	2288
29	.008	6,594	59	.024	2200
30	.008	6,331	60	.025	2114

CHAPTER VIII

TABLES FOR METRIC CURVES

METRIC curves are used in Latin-American countries. The "degree" is the angle subtended by a chord of 20 meters. Practically all usually tabulated curve functions may be converted from feet values in tables for curves used in the United States to meter values for metric curves by dividing by five.

The more commonly used functions have been tabulated in the three following tables. The tabular values are in meters.

TABLE LXXIV. — RADII, TANGENT OFFSETS AND MIDDLE ORDINATES FOR METRIC CURVES

Degree = angle subtended by chord of 20 meters

			iigic o						
		Logarithm,		Mid.	Deg.,		Logarithm,		Mid.
D	R	log R	off., t	ord., m	D	R	$\log R$	off., t	ord., m
0.0		∞	.000	.000	10.0	114.74	2.05970	1.743	. 437
.2	5729.57	3.75812	.035	.009	.2	112.49	2.05113	1.778	- 445
.4	2864.80	3.45709	.070	.017	.4 .6	110.34	2.04272	1.813	· 454
.6	1909.87	3.28100	. 105	.026		108.26	2.03447	1.847	. 463
.8	1432.41	3.15607	. 140	.035	.8 11.0	106.26	2.02637	1 882	.472
I.O	1145.93	3.05916	.175	.044	.2	104.33	2.01843	1.917	. 480
.2	954.95	2.97998	. 209	Į.			_	1.952	.489
.4 .6	818.53 716.22	2.91304	.244	.061	.4 .6	100.68 98.95	2.00296 1.99544	1.986	. 498
.8	636.65	2.85505 2.80390	.279	.079	.8	98.95	1.98804	2.056	.507 .515
2.0	572.99	2.75814	.349	.087	12.0	95.67	1.98077	2.001	. 524
					.2		1.97361		
.2 .4	520.90 477.50	2.71676 2.67897	.384	.096	.4	94.11	1.96658	2.125	.533 .542
.6	440.77	2.64422	.454	.113	.6	91.13	1.95966	2.100	.550
.8	409.30	2.61204	.489	.122	.8	89.71	1.95285	2.229	.559
3.0	382.02	2.58208	.524	.131	13.0	88.34	1.93203	2.229	. 568
.2	358.15	2.55406	.558	. 140	.2	87.00	1.93954	2.299	.577
.4	337.08	2.52774	.593	.148	.4	85.71	1.93304	2.333	.585
.6	318.36	2.50292	.628	. 157	.6	84.46	1.93563	2.368	.594
.8	301.61	2.47945	.663	.166	.8	83.24	1.92032	2.403	.603
4.0	286.54	2.45718	.698	. 175	14.0	82.06	1.91411	2.437	.612
.2	272.90	2.43600	-733	. 183	.2	80.91	1.90798	2.472	.620
.4	260.50	2.41581	.768	. 192	.4	79.79	1.90193	2.507	.629
.6	249.18	2.39651	.803	.201	.6	78.70	1.89598	2.541	. 638
.8	238.80	2.37804	.838	, 209	. 8	77.64	1.89010	2.576	. 647
5.0	229.26	2.36032	.872	.218	15.0	76.61	1.88430	2.611	.655
.2	220.44	2.34330	. 907	.227	.2	75.61	1.87858	2.645	. 664
-4	212.29	2.32692	.942	.236	.4	74.63	1.87294	2.680	.673
.6	204.71	2.31114	.977	.244	.6	73.68	1.86737	2.714	.682
.8	197.66	2.29591	1.012	.253	.8	72.76	1.86187	2.749	. 690
6.0	191.07	2.28120	I.047	. 262	16.0	71.85	1.85644	2.783	. 699
.2	184.92	2.26697	1.082	.271	.2	70.97	1.85109	2.818	.708
-4	179.14	2.25320	1.116	.279	.4	70.11	1.84579	2.853	.717
.6	173.72	2.23985	1.151	.288	.6	69.27	1.84056	2.887	.726
.8	168.62	2.22690	1.186	.297	.8	68.45	1.83540	2.922	.734
7.0	163.80	2.21432 2.20211	1.221	.306	17.0	67.65 66.87	1.83030 1.82526	2.956	.743
.2	159.26			.314	.2			2.991	.752
.4 .6	154.96 150.89	2.19022 2.17866	1.291 1.325	.323	.4 .6	66.11 65.37	1.82027	3.025	.761 .769
.0 .8	147.03	2.17800	1.325	.332	.8	64.64	1.81048	3.000	.709
8.0	143.36	2.15642	1.395	-349	18.0	63.92	1.80567	3.129	.787
							1.80091		
.2 .4	139.87 136.54	2.14571 2.13526	1.430 1.465	.358	.2 .4	63.23 62.55	1.79620	3.163	.796 .805
.4 .6	130.54	2.13520	1.500	.307	.6	61.88	1.79155	3.198	.813
.8	130.35	2.11510	1.534	.384	.8	61.23	1.78694	3.267	.822
9.0	127.45	2.10536	1.569	.393	19.0	60.59	1.78239	3.301	.831
.2	124.69	2.09583	1.604	.402	.2	59.96	1.77789	3.335	.840
.4	122.04	2.08651	1.639	.410	-4	59.35	1.77343	3.370	.849
.6	119.51	2.07739	1.674	.419	.6	58.75	1.76902	3.404	.857
.8	117.07	2.06846	1.708	. 428	.8	58.16	1.76465	3.439	.866
10.0	114.74	2.05970	1.743	. 437	20.0	57 - 59	1.76033	3.473	.875

TABLE LXXV. - METRIC CURVES

Degree	Actual arc,	Long chords									
of curve	one station	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of curve		
0.2	20.000 m.	40.00	60.00	80.00	100.00	120.00	139.99	159.99	0.2		
-4	.000	0.00	0.00	0.00	0.00	119.99	9.98	9.98	.4		
.6	.000	0.00	0.00	79.99	99.99	9.98	9.97	9.95	.6		
.8 1.0	.000	10.00	0.00	9.99	9.98	9.97	9.95	9.92	.8		
.2	.000	0.00	59.99 9.99	79.99 9.98	99.97	9.92	9.88	9.82	1.0		
.4	.000	0.00	9.99	9.97	9.94	9.90	9.83	9.75	.4		
.6	.001	0.00	9.98	9.96	9.92	9.86	9.78	9.67	.6		
.8	.001	0.00	9.98	9.95	9.90	9.83	9.72	9.59	.8		
2.0	20.00I	39.99	59.97	79.94	99.88	119.78	139.66	159.49	2.0		
. 2	.001	9.99	9.97	9.93	9.85	9.74	9.59	9.38	.2		
-4	.001	9.99	9.96	9.91	9.82	9.69	9.51	9.26	-4		
.6	.002	9.99	9.96	9.90	9.80	9.64	9.42	9.14	.6		
.8 3.0	,002 20,002	9.99	9.95	9.88 79.86	9.76	9.58 119.52	9.33	9.00	.8 3.0		
.2	.003	9.98	9.94	9.84	9.69	9.45	9.13	8.69	.2		
.4	.003	9.98	9.93	9.82	9.65	9.39	9.02	8.53	.4		
.6	.003	9.98	9.92	9.80	9.60	9.31	8.90	8.35	.6		
.8	.004	9.98	9.91	9.78	9.56	9.23	8.77	8.16	.8		
4.0	20.004	39.98	59.90	79.76	99.51	119.15	138.64	157.96	4.0		
.2	.004	9.97	9.89	9.73	9.46	9.06	8.50	7.75	.2		
.4 .6	.005	9.97	9.88	9.71	9.41	8.97	8.36	7.54	.4 .6		
.8	.006	9.97	9.86	9.65	9.30	8.78	8.04	7.07	.8		
5.0	20.006	39.96	59.85	79.62	99.24	118.67	137.88	156.82	5.0		
. 2	.007	9.96	9.84	9.59	9.18	8.56	7.71	6.56	.2		
-4	.007	9.96	9.82	9.56	9.12	8.45	7.52	6.29	-4		
.6	.008	9.95	9.81	9.52	9.05	8.34	7.34	6.02	.6		
.8 6.0	.009	9.95	9.80	9.49	8.98	8.21	7.15	5.73	.8		
	20.009	39.94	59.78	79.45	98.91	118.09	136.95	155.43	6.0		
.2	.010	9.94	9.77 9.75	9.41	8.83 8.76	7.96	6.74	5.12	.2		
.6	.011	9.93	9.74	9.34	8.68	7.69	6.31	4.48	.6		
.8	.012	9.93	9.72	9.30	8.60	7.55	6.09	4.15	.8		
7.0	20.012	39.92	59.70	79.26	98.51	117.40	135.86	153.80	7.0		
.2	.013	9.92	9.69	9.21	8.43	7.25	5.62	3.45	. 2		
.4 .6	.014	9.92	9.67	9.17	8.34	7.10	5.37	3.08	.4		
.8	.015	9.91	9.65	9.12	8.25	6.94	5.12 4.87	2.7I 2.32	.6 .8		
8.0	20.016	39.90	59.61	79.03	98.06	116.62	134.60	151.94	8.0		
.2	.017	9.90	9.59	8.98	7.96	6.45	4.33	1.53	.2		
-4	.018	9.89	9.57	8.93	7.86	6.27	4.06	1.12	.4		
.6	.019	9.89	9.55	8.88	7.76	6.09	3.77	0.70	.6		
.8	.020	9.88	9.53	8.83	7.66	5.91	3.49	0.27	.8		
9.0	20.021	39.88 9.87	59.51	78.77 8.72	97.55	115.73	133.19	9.38	9.0		
.4	.022	9.87	9.49	8.66	7.44	5.54	2.59	8.93			
.6	.022	9.86	9.40	8.60	7.33	5.15	2.50	8.46	.4 .6		
.8	.024	9.85	9.42	8.55	7.10	4.94	1.95	7.99	.8		
10 0	20.025	39.85	59 39	78.48	96.98	114.74	131.62	147.50	10.0		
Degree	Actual arc	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree		

TABLE LXXV. — (Continued)

D	A -4 - 1								
Degree of	Actual arc, one			Lo	ng chor	ds			Degree of
curve	station	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	curve
10.0	20.025 m.	39.85	59.39	78.48	96.98	114.74	131.62	147.50	10.0
.2	.026	9.84	9.37	8.42	6.86	4.53	1.29	7.01	.2
.4	.027	9.84	9.34	8.36	6.74	4.31	0.95	6.51	.4
.6	.029	9.83	9.32	8.30	6.61	4.10	0.61	6.00	.6
.8	.030	9.82	9.29	8.23	6.48	3.87	0.25	5.48	.8
11.0	20.03I .032	39.82 9.81	59.27 9.24	78.17 8.10	96.35 6.22	113.65	129.90	144.95	11.0
	.032	9.80	9.24	8.03	6.08	3.42	9.54	4.42	.2
.4 .6	.033	9.80	9.21	7.97	5.95	3.19 2.95	9.17 8.80	3.87	.4 .6
.8	.035	9.79	9.15	7.90	5.81	2.71	8.42	2.76	.8
12.0	20.037	39.78	59.13	77.82	95.67	112.47	128.03	142.19	12.0
.2	.038	9.77	9.10	7.75	5.52	2.21	7.64	1.61	.2
.4	.039	9.77	9.07	7.68	5.38	1.96	7.24	1.03	.4
.6	.040	9.76	9.04	7.60	5.23	1.71	6.84	0.43	.6
.8	.042	9.75	9.01	7.53	5.08	1.45	6.43	139.83	.8
13.0	20.043	39.74	58.98	77 - 45	94.93	111.18	126.01	139.22	13.0
. 2	.044	9.73	8.94	7.37	4.77	0.92	5.59	8.60	.2
.4	.046	9.73	8.91	7.29	4.61	0.65	5.17	7.98	.4
.6 .8	.047 .048	9.72 9.71	8.88 8.85	7.21	4.45	0.37	4.73	7.34	.6 .8
14.0				7.13		0.09	4.30	6.70	1
	20.050	39.70	58.81	77.05	94.13	109.81	123.86	136.05	14.0
.2	.051	9.69	8.78 8.74	6.96	3.96 3.80	9.53	3.41	5.40	.2
.4 .6	.053	9.68	8.71	6.79	3.63	9.23 8.95	2.95	4.73 4.06	.4
.8	.056	9.67	8.67	6.70	3.45	8.65	2.03	3.38	.8
15.0	20.057	39.66	58.64	76.61	93.28	108.35	121.56	132.70	15.0
. 2	.059	9.65	8.60	6.52	3.10	8.04	1.09	2.00	.2
.4	.060	9.64	8.56	6.43	2.92	7.74	0.61	1.30	.4
.6	.062	9.63	8.53	6.34	2.74	7.43	0.12	0.60	.6
.8	.064	9.62	8.49	6.25	2.56	7.11	119.63	129.88	.8
16.0	20.065	39.61	58.45	76.15	92.37	106.79	119.14	129.16	16.0
. 2	. 067	9.60	8.41	6.06	2.18	6.48	8.64	8.44	.2
.4	.068	9.59	8.37	5.96	1.99	6.15	8.13	7.70	-4
.6	.070	9.58	8.33	5.86	1.80	5.82	7.62	6.96	.6
.8 17.0	.072 20.074	9.57 39.56	8.29 58.25	5.76 75.66	1.61 91.41	5.49	7.11	6.21	.8 17.0
.2	.075	9.55	8.21	5.56	1.22	4.82	6.06	4.70	.2
.4	.077	9.54	8.17	5.46	1.01	4.47	5.53	3.93	.4
.6	.079	9.53	8.13	5.36	0.81	4.13	5.00	3.16	.6
.8	.081	9.52	8.08	5.25	0.61	3.78	4.46	2.38	.8
18.0	20.082	39.51	58.04	75.15	90.40	103.43	113.91	121.59	18.0
.2	. 084	9.50	8.00	5.04	0.19	3.08	3.36	0.80	.2
-4	.086	9.48	7.95	4.93	89.98	2.72	2.81	0.00	.4
.6	.088	9.47	7.91	4.83	9.77	2.36	2.26	119.20	.6
8	.090	9.46	7.87	4.71	9.56	1.99	1.69	8.39	.8
19.0	20.092	39·45 9·44	57.82 7.78	74.60	89.34 9.12	1.26	0.56	6.76	19.0 .2
.4	.094	9.44	7.73	4.49	8.90	0.88	109.98	5.93	
.6	.098	9.43	7.68	4.30	8.68	0.51	9.40	5.93	.4 .6
.8	.100	9.40	7.64	4.15	8.46	0.13	8.82	4.27	.8
20.0	20.102	39.39	57.59	74.03	88.23	99.74	108.23	113.43	20.0
Degree	Actual arc	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

TABLE LXXVI. - METRIC CURVES

Degree			l l	Aiddle or	dinates				Degree
of curve	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of curve
0.2	.009	.035	.079	.140	.218	.314	.428	.558	0.2
-4	.017	.070	.157	.279	. 436	.628	.855	1.117	-4
.6	.026	.105	. 236	.419	. 654	.942	1.283	1.675	.6
.8	.035	.140	.314	.558	.873	1.256	1.710	2.233	.8
1.0	.044	.175	.393	.698	1.091	1.570	2.137	2.791	1.0
.2	.052	.209	.471	.838	1.309	1.884	2.565	3.349	.2
-4	.061	.244	.550	.977	1.527	2.198	2.992	3.907	-4
.6 .8	.070	. 279	.624	1.117	1.745	2.512	3.418	4.464	.6
	.079	.314	. 707	1.256	1.963	2.825	3.845	5.020	.8
2.0	. 087	349	.785	1.396	2.180	3.139	4.271	5.576	2.0
.2	.096	.384	.864	1.535	2.398	3.452	4.697	6.132	.2
.4 .6	.105	.419	.942	1.675	2.616	3.765	5.122	6.687	-4
	.113	454	1.021	1.814	2.833	4.078	5.548	7.241	.6
.8 3.0	.122	.489	1.099	1.953	3.051	4.391	5.973	7.795	.8
.2	. 131 . 140	.524	1.178	2.093	3.268	4.703 5.015	6.397	8.348	3.0
.4	.148	.593	_	2.371	3.703	5.327	7.244	-	1
.6	.157	.628	I.335 I.413	2.510	3.920	5.639	7.667	9.451	.4 .6
.8	. 166	.663	1.491	2.650	4.136	5.950	8.090	10.551	.8
4.0	. 175	. 698	1.570	2.789	4.353	6.262	8.511	11.100	4.0
.2	.183	.733	1.648	2.928	4.570	6.572	8.933	11.647	.2
.4	.192	.768	1.726	3.067	4.786	6.883	9.353	12.194	.4
.6	.201	.803	1.805	3.205	5.002	7.193	9.773	12.739	.6
.8	. 209	.838	1.883	3.344	5.218	7.502	10.192	13.283	.8
5.0	.218	.872	1.961	3.483	5 - 434	7.812	10.611	13.826	5.0
. 2	.227	.907	2.040	3.622	5.650	8.121	11.028	14.367	.2
-4	. 236	.942	2.118	3.760	5.865	8.429	11.445	14.907	.4
.6	. 244	.977	2.196	3.899	6.081	8.737	11.862	15.446	.6
.8	. 253	1.012	2.274	4.037	6.296	9.045	12.277	15.983	.8
6.0	. 262	I.047	2.352	4.175	6.511	9.352	12.691	16.519	6.0
.2	. 271	1.082	2.431	4.314	6.725	9.658	13.104	17.053	.2
-4	. 279	1.116	2.509	4.452	6.940	9.965	13.517	17.586	-4
.6	. 288	1.151	2.587	4.590	7.154	10.270	13.929	18.117	.6
.8	. 297	1.186	2,665	4.728	7.368	10.575	14.339	18.646	.8
7.0	. 306	1.221	2.743	4.866	7.581	10.880	14.749	19.174	7.0
.2	.314	1.256	2.821	5.003	7.795	11.184	15.157	19.700	.2
.4 .6	.323	1.291 1.325	2.899	5.141	8.008	11.487	15.565 15.971	20.223	.4 .6
.8	.332	1.325	3.055	5.416	8.433	12.092	16.376	21.265	.8
8.0	-349	1.395	3.133	5.553	8.645	12.394	16.780	21.783	8.0
.2	.358	1.430	3.211	5.691	8.857	12.695	17.183	22.299	.2
.4	.367	1.430	3.288	5.828	9.069	12.095	17.183	22.299	.4
.6	.375	1.500	3.366	5.965	9.280	13.294	17.985	23.325	.6
.8	.384	1.534	3.444	6.101	9.491	13.594	18.384	23.834	.8
9.0	.393	1.569	3.522	6.238	9.702	13.892	18.782	24.342	9.0
.2	. 402	1.604	3.599	6.375	9.912	14.189	19.178	24.847	. 2
-4	.410	1.639	3.677	6.511	10.122	14.486	19.573	25.350	.4
.6	.419	1.674	3.754	6.647	10.332	14.782	19.967	25.850	.6
.8	. 428	1.708	3.832	6.784	10.541	15.078	20.359	26.348	.8
10.0	. 437	1.743	3.910	6.919	10.750	15.372	20.750	26.843	10.0
Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

TABLE LXXVI. — (Continued)

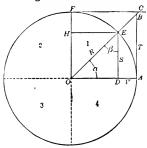
D				Middle or	dinates				Degree
Degree of curve	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	of curve
10.0	· 437	I.743	3.910	6.919	10.750	15.372	20.750	26.843	10.0
		1.778	3.987	7.055	10.958	15.666	21.139	27.336	.2
.2	. 445 . 454	1.778	4.065	7.191	11.167	15.959	21.527	27.827	-4
.6	. 463	1.847	4.142	7.327	11.374	16.251	21.913	28.315	.6
.8	.472	1.882	4.219	7.462	11.582	16.542	22.298	28.800	.8
11.0	. 480	1.917	4.297	7.597	11.789	16.832	22.681	29.282	11.0
.2	.489	1.952	4.374	7.732	11.995	17.122	23.063	29.762	.2
-4	. 498	1.986	4.451	7.867	12.201	17.410	23.443	30.239	.4 .6
.6 .8	.507	2.021	4.539 4.605	8.002 8.137	12.407 12.612	17.698 17.985	23.821 24.198	30.714 31.185	.8
	.515	2.056				18.271		31.654	12.0
12.0	.524	2.091	4.682	8.271	12.817		24.573	32.119	.2
.2 .4	.533	2.125 2.160	4.759 4.836	8.405 8.539	13.021 13.225	18.556 18.840	24.946 25.317	32.119	.4
.6	.550	2.195	4.913	8.673	13.429	19.123	25.687	33.041	.6
.8	.559	2.229	4.990	8.807	13.632	19.405	26.055	33.498	.8
13.0	.568	2.264	5.067	8.940	13.834	19.686	26.421	33.951	13.0
.2	.577	2.299	5.144	9.074	14.036	19.966	26.785	34.402	.2
.4	. 585	2.333	5.220	9.207	14.238	20.245	27.147	34.849	.4
.6	.594	2.368	5.297	9.339	14.439	20.523	27.507	35.292	.6
.8	.603	2.403	5.374	9.472	14.639	20.800	27.866	35.733	.8
14.0	.612	2.437	5.450	9.605	14.839	21.076	28.222	36.171	14.0
.2	.620	2.472	5.527	9.737	15.039	21.351	28.576	36.604 37.035	.2
.4 .6	.629 .638	2.507 2.54I	5.603 5.679	9.870	15.238 15.437	21.897	28.929 29.279	37.462	.4 .6
.8	.647	2.576	5.756	10.133	15.634	22.169	29.628	37.886	.8
15.0	.655	2.570	5.832	10.133	15.832	22.439	29.974	38.306	15.0
.2	.664	2.645	5.908	10.395	16.028	22.709	30.318	38.723	.2
.4	.673	2.680	5.984	10.526	16.225	22.977	30.660	39.137	.4
.6	.682	2.704	6.060	10.657	16.421	23.244	31.000	39.546	.6
.8	. 690	2.749	6.136	10.788	16.616	23.509	31.338	39.952	.8
16.0	. 699	2.783	6.212	10.918	16.810	23.774	31.673	40.355	16.0
.2	.708	2.818	6.288	11.048	17.005	24.037	32.007	40.753	.2
.4 .6	.717	2.853 2.887	6.364	11.178	17.198	24.299 24.560	32.338 32.667	41.148 41.540	.4 .6
.8	.726			-	17.583	24.820	32.993	41.927	.8
17.0	.734 .743	2.922 2.956	6.515 6.591	11.437 11.566	17.774	25.078	32.993	42.311	17.0
.2	.752	2.991	6.666	11.696	17.966	25.335	33.639	42.691	.2
-4	.761	3.025	6.741	11.824	18.156	25.591	33.959	43.067	.4
.6	.769	3.060	6.817	11.953	18.346	25.846	34.276	43 - 439	.6
.8	.778	3.094	6.892	12.081	18.534	26.099	34.591	43.807	.8
18.0	787	3.129	6.967	12.208	18.723	26.351	34.903	44.171	18.0
.2	.796	3.163	7.043	12.336	18.911	26.601	35.213	44.531	.2
.4 .6	.805	3.198	7.117	12.464	19.098	26.850 27.098	35.521 35.826	44.887	.4 .6
	.813	3.232	7.193	12.593	19.285		36.129	45.239	.8
.8 19.0	.822 .831	3.266 3.301	7.267	12.717	19.470	27.345 27.590	36.129	45.587 45.931	19.0
.2	.840	3.335	7.417	12.971	19.840	27.833	36.727	46.271	.2
-4	.849	3.370	7.492	13.097	20.024	28.076	37.022	46.606	.4
.6	.857	3.404	7.566	13.222	20.207	28.316	37.314	46.938	.6
.8	.866	3 · 439	7.641	13.348	20.389	28.556	37.604	47.265	.8
20.0	.875	3.473	7.715	13.473	20.571	28.794	37.892	47.588	20.0
Degree	ı Sta.	2 Sta.	3 Sta.	4 Sta.	5 Sta.	6 Sta.	7 Sta.	8 Sta.	Degree

CHAPTER IX

MISCELLANEOUS TABLES

TABLE LXXVII. - TRIGONOMETRIC FORMULAS, CIRCULAR MEASURE, ETC.

Trigonometric Functions and Formulas. Solution of Triangles



1. $ED = R \sin \alpha$. $OD = R \cos \alpha$. 2.

3. $DA = R \operatorname{versin} \alpha$.

 $HF = R \operatorname{coversin} \alpha$.

By definition, if R = 1,

 $ED = sine \alpha$. $OD = cosine \alpha$.

 $DA = \text{versed sine } \alpha$.

 $HF = \text{coversed sine } \alpha.$

 $BA = \text{tangent } \alpha$.

 $FC = \text{cotangent } \alpha.$ $OB = \text{secant } \alpha.$

 $OC = \operatorname{cosecant} \alpha$.

If R is other than I, it follows from the above definitions and the proportionality of similar figures, that

5. $BA = R \tan \alpha$.

6. $FC = R \cot \alpha$.

7. $OB = R \sec \alpha$.

 $OC = R \csc \alpha$.

from which also in any right triangle of angles α and β , if o be the side opposite the angle α , a the side adjacent thereto, and h the hypotenuse,

9.
$$\sin \alpha = \frac{o}{h} = \cos \beta$$
.

13.
$$\sec \alpha = \frac{h}{a} = \csc \beta$$
.

10.
$$\cos \alpha = \frac{a}{h} = \sin \beta$$
.

14.
$$\csc \alpha = \frac{h}{o} = \sec \beta$$
.

11.
$$\tan \alpha = \frac{o}{a} = \cot \beta$$
.

15.
$$\operatorname{vers} \alpha = \frac{h-a}{h} = \operatorname{covers} \beta.$$

12.
$$\cot \alpha = \frac{a}{o} = \tan \beta$$
.

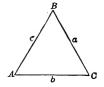
16. covers
$$\alpha = \frac{h-o}{h} = \text{vers } \beta$$
.

Hence.

17.
$$\begin{cases} o = h \sin \alpha = h \cos \beta. \\ h = \frac{o}{\sin \alpha} = \frac{o}{\cos \beta}. \end{cases}$$
 18.

18.
$$\begin{cases} a = h \cos \alpha = h \sin \beta. \\ h = \frac{a}{\cos \alpha} = \frac{a}{\sin \beta}. \end{cases}$$

19.
$$\begin{cases} o = a \tan \alpha = a \cot \beta. \\ a = \frac{o}{\tan \alpha} = \frac{o}{\cot \beta}. \end{cases}$$
22.
$$\begin{cases} h = o \csc \alpha = o \sec \beta. \\ o = \frac{h}{\csc \alpha} = \frac{h}{\sec \beta}. \end{cases}$$
20.
$$\begin{cases} a = o \cot \alpha = o \tan \beta. \\ o = \frac{a}{\cot \alpha} = \frac{a}{\tan \beta}. \end{cases}$$
23.
$$o = \sqrt{h^2 - a^2} = \sqrt{(h + a)(h - a)}. \end{cases}$$
24.
$$a = \sqrt{h^2 - o^2} = \sqrt{(h + o)(h - o)}. \end{cases}$$
25.
$$h = a \sec \alpha = a \csc \beta.$$
26.
$$A = \frac{o}{a} = \frac{o}{a}. \end{cases}$$
26.
$$A = \frac{o}{a} = \frac{o}{a}. \end{cases}$$



Oblique triangles may be solved by some one of the following formulas:

Given	Sought	Formulas
27. A, B, a,	C, b, c,	$C = 180^{\circ} - (A+B), b = \frac{a}{\sin A} \sin B,$
28. A, a, b,	B, C, c,	$c = \frac{a}{\sin A} \sin (A + B).$ $\sin B = \frac{\sin A}{a} b, C = 180^{\circ} - (A + B),$ $c = \frac{a}{\sin A} \sin C.$
29. Ċ, a, b,	$\frac{1}{2}(A+B),$	$\frac{1}{2}(A + B) = 90^{\circ} - \frac{1}{2}C.$
30. C, a, b,	$\frac{1}{2}(A-B),$	$\tan \frac{1}{2} (A - B) = \frac{a - b}{a + b} \tan \frac{1}{2} (A + B).$
31. C, a, b,	A, B,	$\begin{cases} A = \frac{1}{2}(A + B) + \frac{1}{2}(A - B); \\ B = \frac{1}{2}(A + B) - \frac{1}{2}(A - B). \end{cases}$ $c = (a + b) \frac{\cos \frac{1}{2}(A + B)}{\cos \frac{1}{2}(A - B)}$
32. C, a, b,	с,	$c = (a+b)\frac{\cos\frac{1}{2}(A+B)}{\cos\frac{1}{2}(A-B)}$ $\sin\frac{1}{2}(A+B)$
33. <i>C</i> , <i>a</i> , <i>b</i> , 34. <i>a</i> , <i>b</i> , <i>c</i> ,	Area, A ,	$= (a - b) \frac{\sin \frac{1}{2} (A + B)}{\sin \frac{1}{2} (A - B)}.$ Area = $\frac{1}{2} ab \sin C$. If $s = \frac{1}{2} (a + b + c)$,
		$\sin \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{bc}},$ $\cos \frac{1}{2}A = \sqrt{\frac{s(s-a)}{bc}},$
		$\tan \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{s(s-a)}},$
		$\sin A = \frac{2\sqrt{(s-a)(s-b)(s-c)}}{bc},$
		$\operatorname{vers} A = \frac{2(s-b)(s-c)}{bc}.$
35. a, b, c,	Area,	Area = $\sqrt{s(s-a)(s-b)(s-c)}$.
36. A, B, C, a,	Area,	Area $= \frac{a^2 \sin B \sin C}{2 \sin A}.$

From the definitions of the trigonometric functions, the geometrical properties of right triangles and in some cases algebraic transformations, it may be shown that if A is any angle and B any other angle,

37.
$$\sin^2 A + \cos^2 A = 1$$
.

38.
$$\sin A = \frac{I}{\csc A} = \sqrt{I - \cos^2 A} = \tan A \cos A$$

= $2 \sin \frac{1}{2} A \cos \frac{1}{2} A = \text{vers } A \cot \frac{1}{2} A$
= $\sqrt{\frac{1}{2} \text{vers } 2 A} = \sqrt{\frac{1}{2} (I - \cos 2 A)}$.

39.
$$\cos A = \frac{I}{\sec A} = \sqrt{I - \sin^2 A} = \cot A \sin A$$

= $I - \text{vers } A = 2 \cos^2 \frac{1}{2} A - I = I - 2 \sin^2 \frac{1}{2} A$
= $\cos^2 \frac{1}{2} A - \sin^2 \frac{1}{2} A = \sqrt{\frac{1}{2} + \frac{1}{2} \cos 2 A}$.

40.
$$\tan A = \frac{\sin A}{\cos A} = \frac{1}{\cot A} = \sqrt{\sec^2 A - 1}$$

$$= \sqrt{\frac{1}{\cos^2 A} - 1} = \frac{\sqrt{1 - \cos^2 A}}{\cos A} = \frac{\sin 2A}{1 + \cos 2A}$$

$$= \frac{1 - \cos 2A}{\sin 2A} = \frac{\text{vers } 2A}{\sin 2A} = \cot \frac{1}{2}A \text{ (sec } A - 1).$$

41. cot
$$A = \frac{\cos A}{\sin A} = \frac{1}{\tan A} = \sqrt{\csc^2 A - 1}$$

= $\frac{\sin 2A}{1 - \cos 2A} = \frac{\sin 2A}{\text{vers } 2A} = \frac{1 + \cos 2A}{\sin 2A} = \frac{\tan \frac{1}{2}A}{\sec A - 1}$

42. vers
$$A = I - \cos A = \sin A \tan \frac{1}{2} A = 2 \sin^2 \frac{1}{2} A = \cos A (\sec A - I)$$
.

43.
$$\sin (A \pm B) = \sin A \cos B \pm \sin B \cos A$$
.

44.
$$\cos (A \pm B) = \cos A \cos B \mp \sin A \sin B$$
.

45.
$$\sin \frac{1}{2}A = \sqrt{\frac{1 - \cos A}{2}} = \sqrt{\frac{\text{vers } A}{2}}$$
.

46.
$$\sin 2A = 2 \sin A \cos A$$
.

$$47. \cos \frac{1}{2}A = \sqrt{\frac{1+\cos A}{2}}.$$

48.
$$\cos 2A = 2\cos^2 A - I = \cos^2 A - \sin^2 A = I - 2\sin^2 A$$
.

49.
$$\tan \frac{1}{2} A = \frac{\tan A}{1 + \sec A} = \csc A - \cot A = \frac{1 - \cos A}{\sin A} = \sqrt{\frac{1 - \cos A}{1 + \cos A}}$$

50.
$$\tan 2A = \frac{2 \tan A}{1 - \tan^2 A}$$
.

51.
$$\cot \frac{1}{2}A = \frac{\sin A}{\text{vers }A} = \frac{1 + \cos A}{\sin A} = \frac{1}{\cos \cot A}$$

52.
$$\cot 2A = \frac{\cot^2 A - 1}{2 \cot A}$$

53.
$$\operatorname{vers} \frac{1}{2} A = \frac{\frac{1}{2} \operatorname{vers} A}{1 + \sqrt{1 - \frac{1}{2} \operatorname{vers} A}} = \frac{1 - \cos A}{2 + \sqrt{2 (1 + \cos A)}}$$

54. $vers 2A = 2 sin^2 A$

55. $\sin A + \sin B = 2 \sin \frac{1}{2} (A + B) \cos \frac{1}{2} (A - B)$.

56. $\sin A - \sin B = 2 \cos \frac{1}{2} (A + B) \sin \frac{1}{2} (A - B)$.

57. $\cos A + \cos B = 2 \cos \frac{1}{2} (A + B) \cos \frac{1}{2} (A - B)$.

58. $\cos B - \cos A = 2 \sin \frac{1}{2} (A + B) \sin \frac{1}{2} (A - B)$.

59. $\sin^2 A - \sin^2 B = \cos^2 B - \cos^2 A = \sin (A + B) \sin (A - B)$.

60. $\cos^2 A - \sin^2 B = \cos (A + B) \cos (A - B)$.

61. $\tan A + \tan B = \frac{\sin (A + B)}{\cos A \cos B}$

62. $\tan A - \tan B = \frac{\sin (A - B)}{\cos A \cos B}$

LENGTH OF CIRCULAR ARCS TO RADIUS I

Deg.	Length	Deg.	Length	Deg.	Length	Deg.	Length	Deg.	Length
10 20 30 40	0.1745329 0.3490659 0.5235988 0.6981317	60 70	o.8726646 I.0471976 I.2217305 I.3962634	100	1.5707963 1.7453293 1.9198622 2.0943951	140 150	2.2689280 2.4434610 2.6179939 2.7925268	180 190	2.9670597 3.1415927 3.3161256 3.4906585

$$\pi = 3.14159$$

 $\log \pi = 0.497150$

Degrees in arc of length equal to radius, 57.295780. Degrees in arc of length equal to π , 180.

Circumference = 2 mr = 260°

Circumference = $2 \pi r$ = 360 Area = πr^2 .

If l = length of circular arc
d = number of degrees in same
r = radius of same
c = chord of same
m = middle ordinate

$$d = \frac{l}{r} \cdot \frac{180^{\circ}}{\pi} = \frac{l}{r} \cdot 57.3^{\circ} \text{ approx.}$$

$$r = \frac{l}{d} \cdot \frac{180^{\circ}}{\pi} = \frac{l}{d} \cdot 57.3^{\circ} \text{ approx.}$$

$$l = \frac{d}{180} \pi r = \frac{d}{57.3^{\circ}} r \text{ approx.}$$
Area of sector = $\frac{1}{2} lr$.
Area of sector = $\frac{d}{360} \pi r^2$.
Approx. area of segment = $\frac{2}{3} cm$.

$$\frac{1}{\pi} = 0.31831.$$

Volume of sphere = $\frac{4}{3}\pi r^3$.

Square feet in I acre = 43,560.

Cubic feet in I cubic meter = 35.3145.

TABLE LXXVIII. — STADIA FUNCTIONS
Differences of elevation for 100 feet rod reading

Deg.	0	I	2	3	4	5	6 '	7	8	9	Deg.
.00 .05 .1	0.00 0.09 0.17 0.26	1.74 1.83 1.92 2.01	3.49 3.57 3.66 3.75	5.23 5.31 5.40 5.49	6.96 7.05 7.13 7.22	8.68 8.77 8.85 8.94	10.40 10.48 10.57	12.10 12.18 12.26 12.35	13.78 13.87 13.95 14.03	15.45 15.53 15.62	.00 .05 .1
.2 .25	0.35 0.42 0.52	2.09 2.18 2.27	3.84 3.92 4.01	5.57 5.66 5.75	7.30 7.39 7.48	9.03 9.11 9.20	10.74 10.82	12.43 12.52 12.60	14.12 14.20 14.28	15.78 15.87 15.95	.2 .25 .3
.35 .4	0.61	2.36 2.44	4.10 4.18	5.83 5.92	7.56 7.65	9.28 9.37	10.99	12.69 12.77	14.37 14.45	16.03 16.11	-35 -4
.45	0.79	2.53	4.27	6.01	7.73	9.46	11.16	12.86	14.54	16.20	.45
.5	0.87	2.62	4.36	6.09	7.82	9.54	11.25	12.94	14.62	16.28	.5
.55	0.96	2.70	4.44	6.18	7.91	9.63	11.33	13.03	14.70	16.36	.55
.6	I.05	2.79	4.53	6.27	7.99	9.71	11.42	13.11	14.79	16.44	.6
.65	I.13	2.88	4.62	6.35	8.08	9.80	11.50	13.19	14.87	16.52	.65
.7	I.22	2.97	4.71	6.44	8.17	9.88	11.59	13.28	14.95	16.61	.7
.75	1.31	3.05	4.79	6.53	8.25	9.97	11.67	13.36	15.04	16.69	.75
.8	1.40	3.14	4.88	6.61	8.34	10.05	11.76	13.45	15.12	16.77	.8
.85	1.48	3.23	4.97	6.70	8.42	10.14	11.84	13.53	15.20	16.86	.85
.9	1.57	3.3I	5.05	6.79	8.51	10.22	11.93	13.61	15.28	16.94	.9
.95	1.66	3.40	5.14	6.87	8.60	10.31	12.01	13.70	15.37	17.02	.95
1.00	1.74	3.49	5.23	6.96	8.68	10.40	12.10	13.78	15.45	17.10	1.00

Corrections to rod readings for horizontal distance

Rod	o°	1°	2°	3°	4°	5°	6°	7°	8°	9°	Rođ
100 200 300 400 500 600 700 800 900	0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.1 0.1 0.2 0.2 0.2 0.2 0.3	0.I 0.2 0.4 0.5 0.6 0.7 0.8 I.0 I.1	0.3 0.5 0.8 1.1 1.4 1.6 1.9 2.2 2.4 2.7	0.5 1.0 1.5 2.0 2.5 2.9 3.4 3.9 4.4 4.9	0.8 1.5 2.3 3.0 3.8 4.6 5.3 6.1 6.8 7.6	1.1 2.2 3.3 4.4 5.5 6.5 7.6 8.7 9.8 10.9	1.5 3.0 4.5 6.0 7.5 8.9 10.4 11.9 13.4	1.9 3.9 5.8 7.8 9.7 11.6 13.6 15.5 17.5	2.5 4.9 7.4 9.8 12.3 14.7 17.2 19.6 22.1 24.5	100 200 300 400 500 600 700 800 900

TABLE LXXVIII. — (Continued)

Deg.	10	II	12	13	14	15	16	17	18	19	Deg.
.00 .05 .1 .15 .2 .25 .3 .35 .4 .45 .5 .55 .6	17.10 17.18 17.26 17.35 17.43 17.51 17.59 17.67 17.76 17.84 17.92 18.00 18.08 18.16 18.24	19.70 19.78	20.34 20.42 20.50 20.58 20.66 20.73 20.81 20.89 20.97 21.05 21.15 21.21 21.21 21.21 21.21	21.92 22.00 22.08 22.15 22.23 22.31 22.39 22.47 22.54 22.62 22.70 22.78 22.85 22.93 23.01	23.47 23.55 23.63 23.70 23.78 23.86 23.93 24.01 24.09 24.16 24.24 24.32 24.39 24.47 24.55	25.00 25.08 25.15 25.23 25.30 25.38 25.45 25.53 25.68 25.75 25.83 25.90 25.98 26.05	26.50 26.57 26.64 26.72 26.79 26.87 26.94 27.01 27.09 27.16 27.23 27.31 27.38 27.45 27.52	27.96 28.03 28.10 28.18 28.25 28.32 28.39 28.46 28.54 28.61 28.68 28.75 28.89 28.96	29.39 29.46 29.53 29.60 29.67 29.74 29.81 29.88 29.95 30.02 30.06 30.23 30.30 30.37	30.78 30.85 30.92 30.99 31.06 31.13 31.26 31.33 31.40 31.47 31.53 31.60 31.74	.00 .05 .1 .15 .2 .25 .3 .35 .4 .45 .5 .55 .6 .65
.75 .8 .85 .9 .95	18.33 18.41 18.49 18.57 18.65 18.73	20.02 20.10 20.18 20.26	21.53 21.60 21.68 21.76 21.84 21.92		24.62 24.70 24.77 24.85 24.92 25.00	26.13 26.20 26.27 26.35 26.42 26.50	27.60 27.67 27.74 27.81 27.89 27.96	29.04 29.11 29.18 29.25 29.32 29.39	30.44 30.51 30.58 30.65 30.71 30.78	31.80 31.87 31.94 32.01 32.07 32.14	.75 .8 .85 .9 .95

Corrections to rod readings for horizontal distance

Rod	10°	110	12°	13°	14°	15°	16°	17°	18°	19°	Rođ
100 200 300 400 500 600 700 800 900	3.0 6.0 9.1 12.1 15.1 18.1 21.1 24.2 27.2 30.2	3.6 7.3 10.9 14.6 18.2 21.8 25.5 29.1 32.8 36.4	4.3 8.6 13.0 17.3 21.6 25.9 30.2 34.6 38.9 43.2	5.1 10.1 15.2 20.2 25.3 30.4 35.4 40.5 45.5 50.6	5.9 11.7 17.6 23.4 29.3 35.1 41.0 46.8 52.7 58.5	6.7 13.4 20.1 26.8 33.5 40.2 46.9 53.6 60.3 67.0	7.6 15.2 22.8 30.4 38.0 45.6 53.2 60.8 68.4	8.5 17.1 25.6 34.2 42.7 51.3 59.8 68.4 76.9 85.5	9.5 19.1 28.6 38.2 47.7 57.3 66.8 76.4 85.9 95.5	10.6 21.2 31.8 42.4 53.0 63.6 74.2 84.8 95.4	100 200 300 400 500 600 700 800 900

TABLE LXXVIII. — (Continued)

Deg.	20	21	22	23	24	25	26	27	28	29	Deg.
.00 .05 .1	32.14 32.21 32.27 32.34	33.46 33.52 33.59 33.65	34.73 34.80 34.86 34.92	35.97 36.03 36.09 36.15	37.16 37.22 37.27	38.30 38.36 38.41 38.47	39.40 39.45 39.51 39.56	40.45 40.50 40.55 40.60	41.45 41.50 41.55 41.60	42.40 42.45 42.49 42.54	.00 .05 .1
.2 .25 .3 .35	32.41 32.47 32.54 32.61	33.72 33.78 33.84 33.91	34.98 35.05 35.11 35.17	36.21 36.27 36.33 36.39	37 · 39 37 · 45 37 · 51 37 · 56	38.53 38.58 38.64 38.69	39.61 39.67 39.72 39.77	40.66 40.71 40.76 40.81	41.65 41.69 41.74 41.79	42.59 42.63 42.68 42.72	.2 .25 .3 .35
.4 .45 .5 .55	32.67 32.74 32.80 32.87	33.97 34.04 34.10 34.16	35.23 35.29 35.36 35.42	36.45 36.51 36.57 36.63	37.62 37.68 37.74 37.79	38.75 38.80 38.86 38.91	39.83 39.88 39.93 39.98	40.86 40.91 40.96 41.01	41.84 41.89 41.93 41.98	42.77 42.81 42.86 42.90	.4 .45 .5 .55
.6 .65 .7	32.93 33.00 33.07 33.13	34.23 34.29 34.35 34.42	35.48 35.54 35.60 35.66	36.69 36.75 36.80 36.86	37.85 37.91 37.96 38.02	38.97 39.02 39.08 39.13	40.04 40.09 40.14 40.19	41.06 41.11 41.16 41.21	42.03 42.08 42.12 42.17	42.95 42.99 43.04 43.08	.6 .65 .7
.8 .85 .9 .95	33.20 33.26 33.33 33.39	34.48 34.54 34.61 34.67	35.72 35.78 35.85 35.91	36.92 36.98 37.04 37.10	38.08 38.13 38.19 38.25	39.18 39.24 39.29 39.35	40.24 40.30 40.35 40.40	41.26 41.31 41.35 41.40	42.22 42.26 42.31 42.36	43.13 43.17 43.21 43.26	.8 .85 .9
I.00	33.46	34.73	35.97	37.16	38.30	39.40	40.45	41.45	42.40	43.30	1.00

Corrections to rod readings for horizontal distance

Rod	20°	21°	22°	23°	24°	25°	26°	27°	28°	29°	Rod
100 200 300 400 500 600 700 800 900	11.7 23.4 35.1 46.8 58.5 70.2 81.9 93.6 105.3 117.0	12.8 25.7 38.5 51.4 64.2 77.0 89.9 102.7 115.6	14.0 28.1 42.1 56.1 70.2 84.2 98.2 112.2 126.3 140.3	15.3 30.5 45.8 61.1 76.4 91.6 106.9 122.2 137.4	16.5 33.1 49.6 66.2 82.7 99.2 115.8 132.3 148.9 165.4	17.9 35.7 53.6 71.4 89.3 107.2 125.0 142.9 160.7 178.6	19.2 38.4 57.7 76.9 96.1 115.3 134.5 153.8 173.0	20.6 41.2 61.8 82.4 103.1 123.7 144.3 164.9 185.5	22.0 44.1 66.1 88.2 110.2 132.2 154.3 176.3 198.4	23.5 47.0 70.5 94.0 117.5 141.0 164.5 188.0 211.5	100 200 300 400 500 600 700 800 900

TABLE LXXIX. - BAROMETRIC ELEVATIONS

Giving altitudes above arbitrary sea level (barometer reading 30 inches) for various barometer readings B.

To determine difference of elevation of two points having barometer readings B and B_1 , take from the table the altitudes corresponding to B and B_1 , and correct their difference by Table LXXX. The corrected difference is the quantity required.

В	A	Diff. for o.oı	В	A	Diff. for c.or	В	A	Diff. for 0.01
Inches II.0 II.1 II.2 II.3 II.4 II.5 II.6 II.7 II.8 II.9 I2.0 I2.1 I2.2 I2.3 I2.4 I2.5 I2.6 I2.7 I2.8 I2.9 I3.0 I3.1 I3.2 I3.3 I3.4 I3.5 I3.6 I3.7 I3.8 I3.9 I3.6	Feet 27,336 27,090 26,846 26,364 26,364 26,126 25,890 25,656 25,424 25,194 24,956 24,740 24,516 24,294 24,073 23,854 23,637 22,785 22,576 22,368 21,757 21,358 21,160 20,962 20,765	Feet -24.6 24.4 24.2 24.0 23.8 23.6 23.4 23.2 23.0 22.8 22.6 22.4 22.2 22.1 21.9 21.7 21.6 21.4 21.2 21.0 20.8 20.6 20.4 21.9 21.9 21.7 21.6 21.4 21.2 21.0 20.9 20.8 20.6 20.4 20.1 20.0 19.9 19.8 19.8 -19.7	Inches 14.0 14.1 14.2 14.3 14.4 14.5 14.6 14.7 14.8 14.9 15.0 15.1 15.2 15.3 15.4 15.5 15.6 15.7 15.8 16.0 16.1 16.2 16.3 16.4 16.5 16.6 16.7 16.8 16.9 17.0	Feet 20,765 20,570 20,377 20,186 19,997 19,899 19,623 19,437 19,252 19,068 18,765 18,368 17,795 18,346 17,1643 17,176,43 17,176,43 17,176,43 17,176,43 17,176,17 16,958 16,789 16,621 16,454 16,288 16,124 15,961 15,798 15,661 15,476	Feet -19.5 19.3 19.1 18.9 18.8 18.6 18.5 18.4 18.2 18.1 17.6 17.5 17.4 17.3 17.2 16.9 16.8 16.6 16.4 16.3 16.3 16.3 16.2 -16.0	Inches 17.0 17.1 17.2 17.3 17.4 17.5 17.6 17.7 17.8 17.9 18.0 18.1 18.2 18.3 18.4 18.5 18.6 18.7 18.8 19.0 19.1 19.2 19.3 19.4 19.5 19.6	Feet 15.476 15.316 15.157 14.999 14.842 14.686 14.531 14.377 14.223 14.070 13.918 13.767 13.617 13.468 13.319 12.733 12.589 12.445 12.302 12.160 12.018 11.877 11.598 11.459 11.459 11.321 11.1845	Feet -16.0 15.9 15.8 15.7 15.6 15.5 15.4 15.3 15.2 15.1 15.0 14.9 14.7 14.6 14.6 14.4 14.4 14.4 14.4 14.4 14.1 14.0 13.9 13.8 13.7 -13.7

Taken from Appendix 10, "U.S. Coast and Geodetic Survey Report" for 1881.

TABLE LXXIX. — (Continued)

Inches	В	A	Diff.	В	A	Diff. for o.or	В	A	Diff. for 0.01
23.0 7,239 11.8 26.7 3,175 10.2 30.4 361 9.0 23.1 7,121 11.8 26.8 3,073 10.2 30.5 451 8.9 23.2 7,004 11.7 26.9 2,972 10.1 30.6 540 8.9 23.3 6,887 11.7 27.0 2,871 10.1 30.7 629 8.9 23.4 6,770 11.6 27.2 2,670 10.0 30.9 805 8.8 23.5 6,654 11.6 27.2 2,670 10.0 30.9 805 8.8 23.6 6,538 -11.5 27.3 2,570 -10.0 31.0 -893	20.0 20.1 20.2 20.3 20.4 20.5 20.6 20.7 20.8 20.9 21.0 21.1 21.2 21.3 21.4 21.5 21.6 21.7 21.8 21.9 22.0 22.1 22.2 22.3 22.4 22.5 22.6 22.7 22.8 22.9 23.0 23.1 23.2 23.3 23.4 23.5 23.6 23.7 23.8 23.9 23.0 23.1 23.2 23.3 23.4 23.5 23.6 23.7 23.8 23.9 23.0 23.1 23.2 23.3 23.4 23.5 23.6 23.7 23.8 23.9 23.0 23.1 23.2 23.3 23.4 23.5 23.6 23.7 23.8 23.9 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.1 23.0 23.0 23.0 23.1 23.0	11,047 10,911 10,776 10,642 10,508 10,375 10,242 10,110 9,979 9,848 9,718 9,589 9,460 9,332 9,204 8,677 8,257 8,204 8,082 7,960 7,838 7,717 7,597 7,477 7,359 7,121 7,004 6,887 6,770 6,654	Feet -13.6 13.5 13.4 13.4 13.3 13.3 13.2 13.1 13.1 13.0 12.9 12.9 12.8 12.8 12.8 12.1 12.0 12.0 12.0 12.0 11.9 11.9 11.9 11.1 11.0 11.6 11.6	23.7 23.8 23.9 24.0 24.1 24.2 24.3 24.4 24.5 24.6 24.7 24.8 24.9 25.0 25.1 25.2 25.3 25.4 25.5 25.6 25.7 25.8 25.9 26.0 26.1 26.2 26.3 26.4 26.5 26.3 26.4 26.5 26.6 27.7 26.8 26.9 27.0 27.1 27.2	6,423 6,308 6.194 6,080 5,967 5,854 5,741 5,629 5,518 5,407 4,968 4,859 4,751 4,643 4,521 4,643 4,215 4,125 4,100 4,004 3,899 3,794 3,690 3,786 3,483 3,380 3,277 3,175 3,073 2,972 2,877 2,670	Feet -11.5 11.4 11.3 11.3 11.3 11.3 11.1 11.1 11.1	27.4 27.5 27.6 27.7 27.8 27.9 28.0 28.1 28.2 28.3 28.4 28.5 28.6 28.7 29.0 29.1 29.2 29.3 29.4 29.5 29.7 29.8 29.0 30.1 30.2 30.3 30.4 30.5 30.6 30.7 30.8	2,470 2,371 2,272 2,173 2,075 1,975 1,980 1,783 1,686 1,589 1,493 1,397 1,302 1,207 1,112 1,018 924 830 643 550 458 366 274 182 91 90 —91 181 271 361 451 549 669 717 805	Feet -9.9 9.9 9.8 9.8 9.7 9.7 9.7 9.6 9.5 9.5 9.5 9.2 9.4 9.4 9.4 9.3 9.2 9.2 9.1 9.1 9.0 9.0 9.0 8.9 8.8 8.8

TABLE LXXX. — Correction Coefficient for Temperature AND Hygrometric Conditions

This correction is used when no hygrometric observations have been made. To the difference in altitude found in Table LXXIX for the given barometer readings is added algebraically the product of that difference and the correction below given, according to the formula, diff. alt. = (diff. by Table LXXIX) (r + c).

Sum O. T. ¹	Corr. coeff.	Sum O. T.	Corr. Coeff.	Sum O. T.	Corr. coeff.
0° 10 20 30 40 50	-0.1024 -0.0915 -0.0806 -0.0698 -0.0592 -0.0486 -0.0380	70° 80 90 100 110 120	-0.0273 -0.0166 -0.0058 +0.0049 +0.0156 +0.0262 +0.0368	140° 150 160 170 180	+0.0471 +0.0575 +0.0677 +0.0779 +0.0879

¹ Computed from Tables I and IV, Appendix 10, "U.S. Coast Survey Report" for 1881.

TABLE LXXXI.¹—Volume in cubic feet per second discharging over a thin plate weir one foot in length without end contractions² according to Francis' Formula $Q = _{3.33} L\sqrt{H^3}$.

Hand		Head		Used		Hand		Uand	
Head, H, in	Cu. ft.	Head, H, in	Cu. ft.	Head, H , in	Cu. ft.	Head, H, in	Cu. ft.	Head,	Cu. ft.
ft.	per sec.	ft.	per sec.	ft.	per sec.	ft.	per sec.	ft.	per sec.
.01	0.003	.51	1.213	I.OI	3.380	1.51	6.179	2.0I	9.489
.02	0.000	.52	1.249	I.02	3.430	1.52	6.240	2.02	9.560
.03	0.017	-53	1.285	1.03	3.481	1.53	6.302	2.03	9.631
.04	0.027	.54	1.321	1.04	3.532	I.54	6.364	2.04	9.703
.05	0.037	.55	1.358	1.05	3.583	1.55	6.426	2.05	9.774
.06	0.049	.56	1.395	1.06	3.634	1.56	6.488	2.06	9.846
.07	0.062	.57	1.433	1.07	3.686	1.57	6.551	2.07	9.917
.08	0.075	. 58	1.471	1.08	3.737	1.58	6.613	2.08	9.989
.09	0.090	.59	1.500	1.09	3.790	1.59	6.676	2.09	10.062
.10	0.105	.60	1.548	1.10	3.842	1.60	6.739	2.10	10.134
.11	0.121	.61	1.586	1.11	3.894	1.61	6.803	2.11	10.206
.12	0.138	.62	1.626	1.12	3.947	1.62	6.866	2.12	10.279
.13	0.156	.63	1.665	1.13	4.000	1.63	6.930	2.13	10.352
.14	0.174	.64	1.705	1.14	4.053	1.64	6.994	2.14	10.425
.15	0.193	.65	1.745	1.15	4.107	1.65	7.058	2.15	10.498
.16	0.213	.66	1.786	1.16	4.160	1.66	7.122	2.16	10.571
.17	0.233	.67	1.826	1.17	4.214	1.67	7.187	2.17	10.645
.18	0.254	.68	1.867	1.18	4.268	1.68	7.251	2.18	10.718
.19	0.276	.69	1.909	1.19	4.323	1.69	7.316	2.19	10.792
.20	0.298	.70	1.950	I.20	4.377	1.70	7.381	2.20	10.866
.21	0.320	.71	1.992	I.2I	4.432	1.71	7.446	2.21	10.940
.22	0.344	.72	2.034	I.22	4.487	I.72	7.512	2.22	11.015
.23	0.367	.73	2.077	1.23	4.543	1.73	7.577	2.23	11.089
.24	0.392	.74	2.120	I.24	4.598	1.74	7.643	2.24	11.164
.25	0.416	.75	2.163	I.25	4.654	1.75	7.709	2.25	11.239
.26	0.441	.76	2.206	1.26	4.710	1.76	7.775	2.26	11.314
.27	0.467	.77	2.250	1.27	4.766	1.77	7.842	2.27	11.389
. 28	0.493	. 78	2.294	1.28	4.822	1.78	7.908	2.28	11.464
.29	0.520	.79	2.338	1.29	4.879	1.79	7.975	2.29	11.540
.30	0.547	.80	2.383	1.30	4.936	1.80	8.042	2.30	11.615
.31	0.575	.81	2.428	1.31	4.993	1.81	8.109	2.31	11.691
.32	0.603	.82	2.473	1.32	5.050	1.82	8.176	2.32	11.767
+33	0.631	.83	2.518	1.33	5.108	1.83	8.244	2.33	11.843
-34	0.660	.84	2.564	I.34	5.165	1.84	8.311	2.34	11.920
.35	0.690	.85	2.610	1.35	5.223	1.85	8.379	2.35	11.996
.36	0.719	.86	2.656	1.36	5.281	1.86	8.447	2.36	12.073
.37	0.749	.87	2.702	I.37	5.340	1.87	8.515	2.37	12.150
.38	0.780	.88	2.749	1.38	5.398	1.88	8.584	2.38	12.227
-39	0.811	.89	2.796	1.39	5 - 457	1.89	8.652	2.39	12.304
.40	0.842	.90	2.843	I.40	5.516	1.90	8.721	2.40	12.381
.41	0.874	.91	2.891	1.41	5.575	1.91	8.790	2.41	12.459
.42	0.906	.92	2.939	I.42	5.635	1.92	8.859	2.42	12.536
.43	0.939	.93	2.987	I.43	5.694	1.93	8.929	2.43	12.614
-44	0.972	.94	3.035	I.44	5.754	1.94	8.998	2.44	12.692
.45 .46	1.005	.95	3.083	1.45	5.814	1.95	9.068	2.45	12.770
.40	I.039 I.073	.96	3.132	1.46	5.875	1.96	9.138	2.46 2.47	12.848
.48	1.1073	.97 .98	3.181	1.47	5.935	1.97	9.208	2.47	13.005
.49	1.107	.90	3.231	1.48	5.996	1.98	9.278 9.348		13.005
.50	1.142	1.00		1.49	6.057 6.118	1.99 2.00	9.346	2.49 2.50	13.163
.,,,		1.00	3.330	1.50	0.118	2.00	9.419	2.30	13.103

¹ From Trautwine's Engineers' Pocketbook.

² The table values are not seriously in error when there are end contractions provided L is at least 10 H. The original formula was limited to heads, H, between ½ foot and 2 feet. The tabular values are probably not seriously in error for the range given. For any weir of length L feet multiply the tabular values by L.

TABLE LXXXII Feet to Meters

	0	1	2	3	4	5	6	7	8	9
Feet	Meters	Meters	Meters	Meters	Meters	Meters	Meters	Meters	Meters	Meters
0			0.610		1,219	7 504	1.829	2.134	2.438	2.742
	0.000	0.305		0.914 3.962	4.267		4.877	5.182	5.486	2.743
10	3.048	3.353						-		5.791
20	6.036	6.401	6.706	7.010	7.315		7.925	8.229		8.839
30	9.144	9.449	9.753	10.058	10.363	10.668	10.972	11.277	11.582	11.887
40	12.192	12.496	12.801	13.106	13.411	13.716	14.020	14.325	14.630	14.935
50	15.239	15.544	15.849	16.154	16.459	16.763	17.068	17.373	17.678	17.983
60	18,287	18.592	18.897	19.202	19.507	19.811	20.116	20.421	20.726	21.031
70	21.335		21.945			22.859	23.164	23.469	23.774	24.079
80	24.383	1		25.298			26.212	26.517		27.126
90	27.431	27.736				28.955	29.260	29.565	29.870	30.174
100	30.479		31.089		31.698	32.003	32.308	32.613		

Meters to Feet

	0	ı	2	3	4	5	6	7	8	9
Meters	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet	Feet
0	0.00	3.28	6.56	9.84	13.12	16.40	19.69	22.97	26.25	29.53
10	32.81	36.09	39.37	42.65	45.93	49.21	52.49	55.78	59.06	62.34
20	65.62	68.90	72.18	75.46	78.74	82.02	85.30	88.58	91.87	95.15
30	98.43	101.71	104.99	108.27	111.55	114.83	118.11	121.39	124.67	127.96
40	131.24	134.52	137.80	141.08	144.36	147.64	150.92	154.20	157.48	160.76
50	164.04	167.33	170.61	173.89	177.17	180.45	183.73	187.01	190.29	193.57
60	196.85	200.13	203.42	206.70	209.98	213.26	216.54	219.82	223.10	226.38
70	229.66	232.94	236.22	239.51	242.79	246.07	249.35	252.63	255.91	259.19
8o	262.47	265.75	269.03	272.31	275.60	278.88	282.16	285.44	288.72	292.00
90	295.28	298.56	391.84	305.12	308.40	311.69	314.97	318.25	321.53	324.81
100	328.09	331.37	334.65	337.93	341.21	344 - 49	347.78	351.06	354 - 34	357.62

¹ statute mile = 1.6093 kilometers.

¹ kilometer = 0.6214 statute mile.

CHAPTER X

ADJUSTMENT OF INSTRUMENTS

The Transit. — The adjustments in order are:

- I. Axis of plate bubbles perpendicular to vertical axis of instrument.
- II. Line of sight perpendicular to and presumably coincident with horizontal axis of telescope.
 - 1. Parallax.
 - 2. Vertical wire perpendicular to horizontal axis of telescope.
 - 3. Intersection of wires to axis of telescope.
 - 4. Objective slide coincident with axis of telescope.
 - 5. Line of sight perpendicular to horizontal axis of telescope.
 - 6. Eyepiece to center.
 - III. Horizontal axis of telescope truly horizontal (Standard).
 - IV. Axis of telescope bubble parallel to line of sight.
 - V. Error of vernier of vertical circle.

To test for and make the adjustments:

- I. Set up; turn the alidade through 180°; if the plate bubbles depart from the centers of their tubes, bring them halfway back with the adjusting pin, and relevel. Repeat test and adjustment until complete.
- II. I. Carefully focus the eyepiece on the wires until they are sharp and there is no apparent motion over an object sighted as the eye is moved a little sidewise or up and down.
- 2. Sight a minute distant point and note whether the vertical wire remains on the point as the telescope is slightly revolved on its horizontal axis. If not, loosen two adjacent capstan screws carrying the wire ring, and turn the ring slightly until by further trial the adjustment is complete.
- 3. Construct a pair of Y standards of wood, as two notches cut in opposite sides of a box, that will support the telescope near the two ends after it has been removed from the standards. Remove the telescope and place it in the Y's; direct the line of sight to any minute distant point and revolve the telescope in the Y's 180°; notice if the intersection of the wires remains on the point; if not, bring the wires halfway back to the point by opposite capstan screws, moving first

one set and then the other. Repeat the test and adjustment until complete. This adjustment is not often made but should be made if careful leveling is to be done with the transit.

- 4. Not all object slides are adjustable. If the slide may be adjusted, its adjustment may be tested by making a test for 3 on a very near object; if an error appears, the slide may be moved by moving the ring carrying it. The ring is often concealed by a band around the telescope. After adjusting the slide a test should be made again for 3, and both tests and adjustments repeated until complete.
- 5. Set up; sight a minute distant point, or set a pin some 200 to 400 feet away; transit the telescope and find a distant point in the line of sight or set a pin some 200 to 400 feet away; revolve in azimuth and sight the first point; transit and see whether the line of sight falls on the second point; if not, move the vertical wire one-fourth the apparent distance toward the second point; repeat the test and adjustment until complete. The same first point may be retained but new second points must be found or set for each test.
- 6. If the wires seem to be to one side of the field of view, the eyepiece is not centered. This need not cause error in work. To correct the condition, if the eyepiece is adjustable, move the ring carrying it between the eye end and the wire ring until the wires appear to be in the center of the field.
- III. (a) Hang a plumb line from a high point not far from the transit, turn the line of sight on the line near its top and plunge the telescope downward, noting if the intersection of the wires follows the line; if not, raise or lower one end of the horizontal axis until the required condition is met.
- (b) Sight a nearby high point, say, on a building, plunge the telescope and set a point near the level of the instrument or lower; reverse in azimuth, transit, and sight the high point; plunge again and note whether the line of sight cuts the first lower point set; if not, raise or lower one end of the horizontal axis until the required condition is met. A new lower point will be needed for each test.
 - IV. Adjust as described for the Y level, II I (b).
- V. After making IV, with the transit carefully leveled, bring the telescope bubble to the center of its tube and note the reading of the vertical arc vernier. If it is not zero, either move the vernier till it does read zero or note the error as an index error to be applied to all vertical angle readings. Care must be taken to note whether the error is such as to diminish or increase angles of elevation; angles of depression will be affected in the opposite way.

The Y Level. - The adjustments are:

- I. Line of sight coincident with axis of telescope.
 - 1. Parallax.
 - 2. Horizontal wire perpendicular to vertical axis of instrument.
 - 3. Intersection of wires to axis of telescope.
 - 4. Objective slide coincident with axis of telescope.
 - 5. Evepiece to center.
- II. Bubble axis parallel to line of sight.
 - I. Vertical adjustment.
 - 2. Lateral adjustment.
- III. Y adjustment bubble axis perpendicular to vertical axis of level.

To Make the Adjustment:

- I. I. Set up; focus the eyepiece on the wires until they appear sharp and there is no apparent motion over the field as the eye is moved a little sidewise or vertically.
- 2. Sight a distant point near one end of the horizontal wire; turn the telescope a little on the vertical axis and note if the point remains covered by the wire from one end to the other; if not, loosen two adjacent screws carrying the wire ring and turn the ring until by trial the required condition is met.
- 3. Loosen the clips over the Y's and sight a distant point, clamping the azimuth motion; revolve the telescope in the Y's upside down, and note whether the intersection of the wires remains on the point; if not, move the wire ring first sidewise and then vertically about half the apparent error until the intersection of the wires will remain on a point through a complete revolution of the telescope.
- 4. If the object slide is adjustable, perform the same test on a very near point and adjust the object slide. The ring carrying the object slide when it is adjustable is likely to be concealed beneath a band around the telescope between the object focusing screw and the wire adjusting screws.
- 5. When the instrument is adjusted the wires may appear to be out of the center of the field of view; if so, the eyepiece is out of center and may be centered by moving the ring between the eye end and the wire ring until the wires appear to center the field.
- II. I (a) Set up carefully, loosen the clips over the Y's, remove the telescope and replace it end for end; if the bubble does not return to the center of the tube bring it halfway back by the bubble adjusting screws, relevel, and test and adjust again, until the required condition is met. A better method is the following:

- (b) Set up midway between two stakes about 200 feet apart; read a rod on the two stakes and get their difference of elevation; set up beyond one of the stakes about $\frac{1}{10}$ the distance between them; read the rod on the near stake, apply the difference in level and add a correction for curvature, = 0.001 ft. for 220 feet, for a trial reading on the distant stake; read the rod on the distant stake and if the reading is not the same as the trial reading, move the target up or down $\frac{1}{10}$ of the apparent error according as the instrument is pointing low or high; set the line of sight on the target and bring the bubble to the center by its adjusting screws. Without moving the instrument make another complete test on near and far rod and continue until the required condition is met. If the level is set outside one stake one-fourth of the distance between the stakes the apparent error will be multiplied by $\frac{5}{4}$ instead of $\frac{1}{10}$, and similarly for other proportions.
- 2. With the level set up and the clips loose, turn the telescope a little in the Y's and note whether the bubble remains centered; if not, adjust it by the lateral adjusting screws at one end until it will so remain when the telescope is turned from side to side.
- III. Set up and level with particular care over one set of leveling screws; turn on the vertical axis 180° and note whether the bubble remains in the center of the tube; if not, bring it halfway back by raising or lowering one Y by the capstan nuts through which its stem passes; relevel and repeat until the required condition is met.

The Dumpy Level. - The adjustments are:

- I. Bubble axis perpendicular to vertical axis of level.
- II. Line of sight parallel to bubble axis.
 - 1. Parallax.
 - 2. Horizontal wire perpendicular to vertical axis of instrument.
 - 3. Line of sight.

The adjustments are made as follows:

- I. Set up with telescope leveled with particular care over one set of screws; reverse in azimuth and note whether the bubble remains in the center of its tube; if not, bring it halfway back by the bubble adjusting screws; relevel and repeat until the condition is met.
 - II. I and 2 are made as for the Y level.
- 3 is made as for Y level II I (b), adjusting the wires to the bubble rather than the bubble to the wires; i.e., centering the bubble and moving the horizontal wire to the computed correct reading on the distant rod.

CHAPTER XI

SEXAGESIMAL TRIGONOMETRIC FUNCTIONS

TABLE LXXXIII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS FOR EACH MINUTE OF ARC

To interpolate when the angles are less than 3° , the quantities S and T as found in the 5th and 6th columns of the first three pages are used as follows:

Log sine
$$\alpha = \text{Log } \alpha' - S$$
,
Log tangent $\alpha = \text{Log } \alpha' - T$,
Log $\alpha' = \text{Log sine } \alpha + S = \text{Log tangent } \alpha + T$.

For cosine and cotangent of angles near 90° use the sine and tangent of the complements.

0°

	_	_								
′	_′_	L Sin	d	S	Т	L Tan	c d	L Cot	L Cos	1
0	0						-		0.00 000	60
I	I	6.46 373	30103	3.53 627	3.53 627	6.46 373	30103	3.53 627	0.00 000	59
2	2	6.76 476 6.94 085	17609	3.53 627 3.53 627	3.53 627 3.53 627	6.76 476 6.94 085	17609	3.23 524 3.05 915	0.00 000	58
3 4	3 4	7.06 579	12494	3.53 627	3.53 627	7.06 579	12494	2.93 421	0.00 000	57 56
5 6	5	7.16 270	9691 7918	3.53 627	3.53 627	7.16 270	9691 7918	2.83 730	0.00 000	55
6		7.24 188	6694	3.53 627	3.53 627	7.24 188	6694	2.75 812	0.00 000	54
7 8	7 8	7.30 882	5800	3.53 627	3.53 627	7.30 882	5800	2.69 118	0.00 000	53
9	9	7.36 682 7.41 797	5115	3.53 627 3.53 627	3.53 627 3.53 627	7.36 682	5115	2.63 318	0.00 000	52 51
IO	10	7.46 373	4576	3.53 627	3.53 627	7.46 373	4576	2.53 627	0.00 000	50
II	II	7.50 512	4139	3.53 627	3.53 627	7.50 512	4139	2.49 488	0.00 000	49
12	I 2	7.54 291	3779 3476	3.53 627	3.53 627	7.54 291	3779 3476	2.45 709	0.00 000	48
13	13	7.57 767	3218	3.53 627	3.53 627	7.57 767	3219	2.42 233	0.00 000	47
14	14 15	7.60 985 7.63 982	2997	3.53 628 3.53 628	3.53 627 3.53 627	7.60 986 7.63 982	2996	2.39 014	0.00 000	46
15 16	16	7.66 784	2802	3.53 628	3.53 627	7.66 785	2803	2.33 215	0.00 000	45
17	17	7.69 417	2633	3.53 628	3.53 627	7.69 418	2633 2482	2.30 582	9.99 999	43
18	18	7.71 900	2483 2348	3.53 628	3.53 627	7.71 900	2348	2.28 100	9.99 999	42
19	19	7.74 248	2227	3.53 628	3.53 627	7.74 248	2228	2.25 752	9.99 999	41
20	20	7.76 475	2119	3.53 628	3.53 627	7.76 476	2119	2.23 524	9.99 999	40
2 I	21	7.78 594	2021	3.53 628	3.53 627	7.78 595	2020	2.21 405	9.99 999	39
22 23	22 23	7.80 615	1930	3.53 628 3.53 628	3.53 627	7.80 615	1931	2.19 385	9.99 999	38
24	24	7.84 393	1848	3.53 628	3.53 627	7.84 394	1848	2.15 606	9.99 999	36
25	25	7.86 166	1773 1704	3.53 628	3.53 627	7.86 167	1773 1704	2.13 833	9.99 999	35
26	26	7.87 870	1639	3.53 628	3.53 627	7.87 871	1639	2.12 129	9.99 999	34
27 28	27 28	7.89 509 7.91 088	1579	3.53 628 3.53 628	3.53 626 3.53 626	7.89 510	1579	2.10 490	9.99 999	33
29	29	7.91 688	1524	3.53 628	3.53 626	7.92 613	1524	2.07 387	9.99 998	31
30	30	7.94 084	1472	3.53 628	3.53 626	7.94 086	1473	2.05 914	9.99 998	30
31	31	7.95 508	1424	3.53 628	3.53 626	7.95 510	1424	2.04 490	9.99 998	29
32	32	7.96 887	1379 1336	3.53 628	3.53 626	7.96 889	1379 1336	2.03 111	9.99 998	28
33	33	7.98 223	1297	3.53 628	3.53 626	7.98 225	1297	2.01 775	9.99 998	27
34	34	7.99 520 8.00 779	1259	3.53 628 3.53 628	3.53 626	7.99 522 8.00 781	1259	1.99 219	9.99 998 9.99 998	26 25
35 36	35 36	8.02 002	1223	3.53 628	3.53 626	8.02 004	1223	1.97 996	9.99 998	24
37	37	8.03 192	1190	3.53 628	3.53 626	8.03 194	1190	1.96 806	9.99 997	23
38	38	8.04 350	1158	3.53 628	3.53 626	8.04 353	1159	1.95 647	9.99 997	22
39	39	8.05 478	1100	3.53 628	3.53 626	8.05 481	1100	1.94 519	9.99 997	21
40	40	8.06 578	1072	3.53 628	3.53 625	8.06 581	1072	1.93 419	9.99 997	20
41	41	8.07 650	1046	3.53 628	3.53 625	8.07 653	1047	1.92 347	9.99 997	18
42	42	8.08 696 8.09 718	1022	3.53 628 3.53 629	3.53 625 3.53 625	8.08 700	1022	1.91 300	9.99 997	17
44	44	8.10 717	999	3.53 629	3.53 625	8.10 720	998	1.89 280	9.99 996	16
45	45	8.11 693	976 954	3.53 629	3.53 625	8.11 696	976	1.88 304	9.99 996	15
46	46	8.12 647	934	3.53 629	3.53 625	8.12 651	934	1.87 349	9.99 996	14
47 48	47 48	8.13 581 8.14 495	914	3.53 629	3.53 625	8.13 585	915	1.86 415	9.99 996	13
49	49	8.15 391	896	3.53 629	3.53 624	8.15 395	895 878	1.84 605	9.99 996	11
50	50	8.16 268	877 860	3.53 629	3.53 624	8.16 273	860	1.83 727	9.99 995	10
51	51	8.17 128		3.53 629	3.53 624	8.17 133		1.82 867	9.99 995	9
52	52	8.17 971	843 827	3.53 629	3.53 624	8.17 976	843 828	1.82 024	9.99 995	8
53	53	8.18 798	812	3.53 629	3.53 624	8.18 804	812	1.81 196	9.99 995	7
54 55	54 55	8.19 610	797	3.53 629	3.53 624 3.53 624	8.19 616	797	1.80 384	9.99 995	5
56	56	8.21 189	782	3.53 629	3.53 624	8 21 195	782	1.78 805	9.99 994	4
57	57	8.21 958	769 755	3.53 629	3.53 623	8.21 964	769	1.78 036	9.99 994	3
58	58	8.22 713	743	3.53 629	3.53 623	8.22 720	742	1.77 280	9.99 994	2
59 60	59 60	8.23 456	730	3.53 630	3.53 623	8.23 462	730	1.76 538	9.99 994	0 1
00	-00	8.24 186		3.53 630	3.53 623	8.24 192		1.75 808	9.99 993	I
		L Cos	d			L Cot	c d	L Tan	L Sin	′

90° (338) **89°**

60 61 62 63 64 65 66 67 68 69 70 71 72	0 1 2 3 4 5 6 7 8 9 10	8.24 186 8.24 903 8.25 609 8.26 304 8.26 988 8.27 661 8.28 324 8.28 977 8.29 621 8.30 255	717 706 695 684 673 663 653	3.53 630 3.53 630 3.53 630 3.53 630 3.53 630 3.53 630	3.53 623 3.53 623 3.53 623 3.53 623	8.24 192 8.24 910	718	L Cot 1.75 808 1.75 090	9.99 993	60
61 62 63 64 65 66 67 68 69 70	1 2 3 4 5 6 7 8 9 10	8.24 903 8.25 609 8.26 304 8.26 988 8.27 661 8.28 324 8.28 977 8.29 621 8.30 255	706 695 684 673 663 653	3.53 630 3.53 630 3.53 630 3.53 630 3.53 630	3.53 623 3.53 623	8.24910	l ' . I			
62 63 64 65 66 67 68 69 70	2 3 4 5 6 7 8 9 10	8.25 609 8.26 304 8.26 988 8.27 661 8.28 324 8.28 977 8.29 621 8.30 255	695 684 673 663 653	3.53 630 3.53 630 3.53 630 3.53 630	3.53 623				9.99 993	59
64 65 66 67 68 69 70	4 5 6 7 8 9 10	8.26 988 8.27 661 8.28 324 8.28 977 8.29 621 8.30 255	684 673 663 653	3.53 630	3.53 623	8.25 616	706 696	1.74 384	9.99 993	58
65 66 67 68 69 70	5 6 7 8 9 10	8.27 661 8.28 324 8.28 977 8.29 621 8.30 255	673 663 653	3.53 630		8.26 312	684	1.73 688	9.99 993	57
66 67 68 69 70	7 8 9 10	8.28 324 8.28 977 8.29 621 8.30 255	663 653	3.33 030	3.53 622 3.53 622	8.26 996 8.27 669	673	1.73 004	9.99 992	56 55
67 68 69 70 71	7 8 9 10	8.28 977 8.29 621 8.30 255		3.53 630	3.53 622	8.28 332	663	1.71 668	9.99 992	54
68 69 70 71	9 10 11	8.29 621 8.30 255		3.53 630	3.53 622	8.28 986	654	1.71 014	9.99 992	53
70 71	10		644	3.53 630	3.53 622	8.29 629	643 634	1.70 371	9.99 992	52
7 I	11		624	3.53 630	3.53 622	8.30 263	625	1.69 737	9.99 991	51
		8.30 879	616	3.53 630	3.53 621	8.30 888	617	1.69 112	9.99 991	50
		8.31 495	608	3.53 630 3.53 631	3.53 621 3.53 621	8.31 505 8.32 112	607	1.68 495 1.67 888	9.99 991	49 48
73	13	8.32 103 8.32 702	599	3.53 631	3.53 621	8.32 711	599	1.67 289	9.99 990	47
74	14	8.33 292	590	3.53 631	3.53 621	8.33 302	591	1.66 698	9.99 990	46
75	15	8.33 875	583	3.53 631	3.53 620	8.33 886	584	1.66 114	9.99 990	45
76	16	8.34 450	575 568	3.53 631	3.53 620	8.34 461	575 568	1.65 539	9.99 989	44
77	17	8.35 o 18 8.35 5 78	560	3.53 631 3.53 631	3.53 620 3.53 620	8.35 029 8.35 590	561	1.64 971 1.64 410	9.99 989 9.99 989	43
79	19	8.36 131	553	3.53 631	3.53 620	8.36 143	553	1.63 857	9.99 989	42 41
80	20	8.36 678	547	3.53 631	3.53 620	8.36 689	546	1.63 311	9.99 988	40
81	21	8.37 217	539	3.53 631	3.53 619	8.37 229	540	1.62 771	9.99 988	39
82	22	8.37 750	533	3.53 632	3.53 619	8.37 762	533	1.62 238	9.99 988	38
83	23	8.38 276	526	3.53 632	3.53 619	8.38 289	527 520	1.61 711	9.99 987	37
84	24	8.38 796	514	3.53 632	3.53 619	8.38 809	514	1.61 191	9.99 987	36
85 86	25 26	8.39 310	508	3.53 632 3.53 632	3.53 619 3.53 618	8.39 323 8.39 832	509	1.60 677	9.99 987 9.99 986	35 34
87	27	8.40 320	502	3.53 632	3.53 618	8.40 334	502	1.59 666	9.99 986	33
88	28	8.40 816	496	3.53 632	3.53 618	8.40 830	496	1.59 170	9.99 986	32
89	29	8.41 307	491 485	3.53 632	3.53 618	8.41 321	491 486	1.58 679	9.99 985	31
90	30	8.41 792	480	3.53 632	3.53 617	8.41 807	480	1.58 193	9.99 985	30
91	31	8.42 272	474	3.53 632	3.53 617	8.42 287	475	1.57 713	9.99 985	29
92 93	32	8.42 746 8.43 216	474	3.53 633 3.53 633	3 53 617 3.53 617	8.42 762 8.43 232	470	1.57 238 1.56 768	9.99 984 9.99 984	28 27
93	33	8.43 680	464	3.53 633	3.53 617	8.43 696	464	1.56 304	9.99 984	26
95	35	8.44 139	459	3.53 633	3.53 616	8.44 156	460	1.55 844	9.99 983	25
96	36	8.44 594	455	3.53 633	3.53 616	8.44 611	455 450	1.55 389	9.99 983	24
97	37	8.45 044	450	3.53 633	3.53 616	8.45 061	446	1.54 939	9.99 983	23
98 99	38 39	8.45 489 8.45 930	441	3.53 633 3.53 633	3.53 616 3.53 615	8.45 507	441	1.54 493 1.54 052	9.99 982	22 21
100	40	8.46 366	436	3.53 634	3.53 615	8.46 385	437	1.53 615	9.99 982	20
101	41	8.46 799	433	3.53 634	3.53 615	8.46 817	432	1.53 183	9.99 981	19
102	41	8.47 226	427	3.53 634	3.53 615	8.47 245	428	1.52 755	9.99 981	18
103	43	8.47 650	424	3.53 634	3.53 614	8.47 669	424	1.52 331	9.99 981	17
104	44	8.48 069	419 416	3.53 634	3.53 614	8.48 089	420	1.51 911	9.99 980	16
105	45 46	8.48 485 8.48 896	411	3.53 634	3.53 614	8.48 505 8.48 917	412	1.51 495 1.51 083	9.99 980 9.99 979	15 14
100	47	8.49 304	408	3.53 634	3.53 614	8.49 325	408	1.50 675	9.99 979	13
108	48	8.49 708	404	3.53 635	3.53 613	8.49 729	404	1.50 271	9.99 979	12
109	49	8.50 108	400 396	3.53 635	3.53 613	8.50 130	401 397	1.49 870	9.99 978	11
110	50	8.50 504	393	3.53 635	3.53 613	8.50 527	393	1.49 473	9.99 978	10
III	51	8.50 897	393	3.53 635	3.53 612	8.50 920	393	1.49 080	9.99 977	9 8
112	52	8.51 287 8.51 673	386	3.53 635	3.53 612	8.51 310	386	1.48 690 1.48 304	9.99 977 9.99 977	8 7
113	53 54	8.52 055	382	3.53 635	3.53 612	8.51 696	383	1.47 921	9.99 977	6
115	55	8.52 434	379	3.53 635	3.53 611	8.52 459	380	1.47 541	9.99 976	5
116	56	8.52 810	376	3.53 636	3.53 611	8.52 835	376	1.47 165	9.99 975	4
117	57	8.53 183	373	3.53 636	3.53 611	8.53 208	373	1.46 792	9.99 975	3
118	58 59	8.53 552 8.53 919	367	3.53 636	3.53 610	8.53 578 8.53 945	367	1.46 422	9.99 974	2
120	60	8.54 282	363	3.53 636	3.53 610	8.54 308	363	1.45 692	9.99 974	ō
		L Cos	d	333 34		L Cot	c d	L Tan	L Sin	,

′	'	L Sin	d	S	Т	L Tan	c d	L Cot	L Cos	
I 20	0	8.54 282	260	3.53 636	3.53 610	8.54 308	267	1.45 692	9.99 974	60
121	1	8.54 642	360	3.53 636	3.53 609	8.54 669	361	1.45 331	9.99 973	59 58
122	2	8.54 999	357 355	3.53 637	3.53 609	8.55 027	358 355	1.44 9 73 1.44 6 18	9.99 973 9.99 972	
123	3 4	8.55 354 8.55 705	351	3.53 637 3.53 637	3.53 609	8.55 734	352	1.44 266	9.99 972	57 56
125	5 6	8.56 054	349	3.53 637	3.53 608	8.56 083	349	1.43 917	9.99 971	55
126		8.56 400	346 343	3.53 637	3.53 608	8.56 429	346 344	1.43 571	9.99 971	54
127	7 8	8.56 743 8.57 084	341	3.53 637 3.53 637	3.53 608 3.53 607	8.56 773	341	1.43 227 1.42 886	9.99 970	53 52
129	او	8.57 421	337	3.53 638	3.53 607	8.57 452	338	1.42 548	9.99 969	51 51
130	10	8.57 757	336	3.53 638	3.53 607	8.57 788	336	1.42 212	9.99 969	50
131	11	8.58 089	332	3.53 638	3.53 606	8.58 121	333	1.41 879	9.99 968	49 48
132	12	8.58 419	330 328	3.53 638	3.53 606	8.58 451	330	1.41 549	9.99 968	48
133	13	8.58 747 8.59 072	325	3.53 638	3.53 606	8.59 105	326	1.41 221	9.99 967	47 46
135	15	8.59 395	323	3.53 639	3.53 605	8.59 428	323	1.40 572	9.99 967	45
136	16	8.59 715	320 318	3.53 639	3.53 605	8.59 749	321	1.40 251	9.99 966	44
137	17	8.60 033	316	3.53 639	3.53 604	8.60 068	316	1.39 932	9.99 966	43
138 139	19	8.60 349 8.60 662	313	3.53 639 3.53 639	3.53 604 3.53 604	8.60 384 8.60 698	314	1.39 616	9.99 965	42 41
140	20	8.60 973	311	3.53 639	3.53 603	8.61 009	311	1.38 991	9.99 964	40
141	21	8.61 282	309	3.53 640	3.53 603	8.61 319	310	1.38 681	9.99 963	39
142	22	8.61 589	307	3.53 640	3.53 603	8.61 626	307	1.38 374	9.99 963	38
143	23	8.61 894	305 302	3.53 640	3.53 602	8.61 931	303	1.38 069	9.99 962	37
144	24 25	8.62 196 8.62 497	301	3.53 640	3.53 602 3.53 602	8.62 234 8.62 535	301	1.37 766	9.99 962	36
146	26	8.62 795	298	3.53 640	3.53 601	8.62 834	299	1.37 166	9.99 961	34
147	27	8.63 091	296	3.53 641	3.53 601	8.63 131	297	1.36 869	9.99 960	33
148 149	28 29	8.63 385	294 293	3.53 641	3.53 601	8.63 426	293	1.36 574	9.99 960	32 31
150	30	8.63 678	290	3.53 641	3.53 600	8.64 009	291	1.35 991	9.99 959	30
151	31	8.64 256	288	3.53 641	3.53 600	8.64 298	289	1.35 702	9.99 958	29
152	32	8.64 543	287	3.53 641	3.53 599 3.53 599	8.64 585	287	1.35 415	9.99 958	28
153	33	8.64 827	284 283	3.53 642	3.53 599	8.64 870	285	1.35 130	9.99 957	27
154	34	8.65 110	281	3.53 642	3.53 598	8.65 154	281	1.34 846	9.99 956	26
155 156	35 36	8.65 391 8.65 670	279	3.53 642 3.53 642	3.53 598 3.53 598	8.65 435 8.65 715	280	1.34 565	9.99 956	25
157	37	8.65 947	277	3.53 642	3.53 597	8.65 993	278	1.34 007	9.99 955	23
158	38	8.66 223	276	3.53 643	3.53 597	8.66 269	276	1.33 731	9.99 954	22
159	39	8.66 497	274 272	3.53 643	3.53 596	8.66 543	273	1.33 457	9.99 954	21
160	40	8.66 769	270	3.53 643	3.53 596	8.66 816	271	1.33 184	9.99 953	20
161 162	4I 42	8.67 039 8.67 30 8	269	3.53 643	3.53 596	8.67 o87 8.67 356	269	1.32 913	9.99 952	19
163	43	8.67 575	267	3.53 644	3.53 595	8.67 624	268	1.32 376	9.99 951	17
164	44	8.67 841	266	3.53 644	3.53 594	8.67 890	266	1.32 110	9.99 951	16
165 166	45 46	8.68 104 8.68 367	263	3.53 644	3.53 594	8.68 154 8.68 417	263	1.31 846	9.99 950	15
167	47	8.68 627	260	3.53 644	3.53 594 3.53 593	8.68 678	261	1.31 303	9.99 949	13
168	48	8.68 886	259	3.53 645	3.53 593	8.68 938	260	1.31 062	9.99 948	I 2
169	49	8.69 144	258 256	3.53 645	3.53 592	8.69 196	258	1.30 804	9.99 948	II
170	50	8.69 400	254	3.53 645	3.53 592	8.69 453	255	1.30 547	9.99 947	10
171	51	8.69 654	253	3.53 645	3.53 592	8.69 708	254	1.30 292	9.99 946	8
172 173	52 53	8.69 907 8.70 159	252	3.53 646 3.53 646	3.53 591	8.69 962	252	1.30 038	9.99 946	7
174	54	8.70 409	250	3.53 646	3.53 590	8.70 465	251	1.29 535	9.99 944	6
175	5.5	8.70658	249 247	3.53 646	3.53 590	8.70714	249 248	1.29 286	9.99 944	5
176 177	56	8.70 905 8.71 151	246	3.53 646	3.53 589	8.70 962	246	1.29 038	9.99 943	3
178	57 58	8.71 395	244	3.53 647	3.53 589 3.53 589	8.71 453	245	1.28 547	9.99 942	2
179	59	8.71 638	243	3.53 647	3.53 588	8.71 697	244	1.28 303	9.99 941	1
180	60	8.71 880	242	3.53 647	3.53 588	8.71 940	243	1.28 060	9.99 940	0
	1	L Cos	d			L Cot	c d	L Tan	L Sin	'

_	8-												
Ľ	L Sin	d	L Tan	c d	L Cot	L Cos	_				PP		
0	8.71 880	240	8.71 940	241	1.28 060	9.99 940	60		241	239	237	236	234
1	8.72 120	239	8 72 181	239	1.27 819	9.99 940	59	I	24.I	23.9	23.7	23.6	23.4
2	8.72 359	238	8.72 420	239	1.27 580	9.99 939	58	3	48.2 72.3	47.8	47.4 71.1	47.2 70.8	46.8 70.2
3	8.72 597	237	8.72 659	237	1.27 341	9.99 938	57	4	96.4	95.6	94.8	94.4	93.6
4	8.72 834	235	8.72 896	236	1.27 104	9.99 938	56	5	120.5	119.5	118.5	118.0	117.0
5	8.73 069	234	8.73 132	234	1.26 868	9.99 937 9.99 936	55 54	6	144.6	143.4	142.2	141.6	140.4
Ů	8.73 303	232	8.73 366	234				7 8	168.7	167.3	165.9	165.2 188.8	163.8
8	8.73 535	232	8.73 600 8.73 832	232	1.26 400	9.99 936 9.99 935	53 52	9	216.9	191.2 215.1	189.6 213.3	212.4	187.2
9	8.73 767 8.73 997	230	8.74 063	231	I 25 937	9.99 933	51	7					
1		229		229				Ι.	232	231	229	227	226
10	8.74 226		8.74 292		1.25 708	9.99 934	50	1 2	23.2 46.4	23.I 46.2	22.9 45.8	22.7	22.6 45.2
11	8 74 454	228	8.74 521	229	1.25 479	9.99 933	49	3	69.6	69.3	68.7	45.4 68.1	67.8
I 2	8 74 454 8.74 680	226 226	8 74 748	227	1.25 252	9.99 932	48	4	92.8	92.4	91.6	90.8	90.4
13	8.74 906	224	8.74 974	226	1.25 026	9.99 932	47	5	116.0	115.5	114.5	113.5	113.0
14	8 75 130		8.75 199	- 1	1.24 801	9.99 931	46	6	139.2 162.4	138.6 161.7	137.4 160.3	136.2	135.6 158.2
15	8.75 353	223	8.75 423	224	1.24 577	9.99 930	45	7 8	185.6	184.8	183.2	181.6	180.8
1,6	8 75 575	220	8.75 645	222	1.24 355	9.99 929	44	9	208.8	207.9	206.1	204.3	203.4
17	8.75 795	220	8.75 867	220	1.24 133	9.99 929	43		224		220		
18	8.76 o15 8.76 234	219	8.76 o87 8.76 306	219	1.23 913	9.99 928	42	,		222	22.0	219	217
1		217		219	1.23 694		Ι΄.	2	22.4 44.8	22.2 44.4	22.0 44.0	43.8	21.7 43.4
20	8.76 451	1 ** /	8.76 525	219	1.23 475	9.99 926	40	3	67.2	66.6	66.0	65.7	65.I
21	8 26 662	216	9 =6 = 12	217		9.99 926	39	4	89.6	88.8	88.0	87.6	86.8
21	8.76 667 8.76 883	216	8.76 742 8.76 958	216	1.23 258	9.99 920	38	5	112.0	111.0	110.0	109.5	108.5
2.3	8.77 097	214	8.77 173	215	1.22 827	9.99 924	37	6	134.4	133.2	132.0 154.0	131.4	130.2 151.9
24	8.77 310	213		214	1.22 613	9.99 923	36	8	179.2	155.4	176.0	175.2	173.6
25	8.77 522	212	8.77 387 8.77 600	213	1.22 400	9.99 923	35	9	201.6	199.8	198.0	197 I	195.3
26	8.77 733	211	8.77 811	211	1.22 189	9.99 922	34	1	216	214	213	211	209
27	8.77 943		8.78 022		1.21 978	9.99 921	33	۱.					
28	8.77 943 8.78 152	209	8.78 232	210	1.21 768	9.99 920	32	1 2	43.2	42.8	42.6	2I.I 42.2	20.9 41.8
29	8.78 360	Į.	8.78 441	209	1.21 559	9.99 920	31	3	64.8	64.2	63.9	63.3	62.7
30	8.78 568	208	8.78 649	208	1.21 351	9.99 919	30	4	86.4	85.6	85.2	84.4	83.6
		206		206	1.21 331		١.	5	108.0	107.0	106.5 127.8	105.5	104.5 125.4
31	8.78 774 8.78 979	205	8.78 855	206	1.21 145	9.99 918	29		151.2	149.8	149.1	147.7	146.3
32	8.79 183	204	8.79 o61 8.79 266	205	1.20 939	9.99 917	27	8	172.8	171.2	170.4	168.8	167.2
	8.79 386	203		204	I	1	26	9	194.4	192.6	191.7	189.9	188.1
34 35	8.79 588	202	8.79 470 8.79 673	203	1.20 530	9.99 916	25	1	206	206	203	201	199
36	8.79 789	201	8.79 875	202	1.20 125	9.99 914	2.4	l ı	20.8	20.6	20.3	20.1	10.0
37	8.79 990	201	8.80 076	201	1	9.99 913	23	2	41.6	41.2	40.6	40.2	39.8
38	8.80 189	199	8.80 277	201	1.19 924	9.99 913	22	3	62.4	61.8	60.9	60.3	59.7
39	8.80 388	199	8.80 476	199	1.19 524	9.99 912	21	4	83.2	82.4	81.2	80.4 100.5	79.6
40	8.80 585	197	8.80 674	198		9.99 911	20	6	104.0	103.0	121.8	120.6	99.5 119.4
1.		197		198	1,19 326		1		145.6	144.2	142.1	140.7	139.3
41	8.80 782	196	8.80 872	196	1.19 128	9.99 910	19	8	166.4	164.8	162.4	8.001	159.2
42	8.80 978 8.81 173	195	8.81 o68 8.81 264	196	1.18 932	9.99 909	18	9	187.2	185.4	182.7	180.9	179.1
		194		195	1		1 '		198	196	194	192	190
44 45	8.81 367 8.81 560	193	8.81 459 8.81 653	194	1.18 541	9.99 908	16	1	19.8	19.6	19.4	19.2	19.0
46	8.81 752	192	8.81 846	193	1.18 154	9.99 907	14	2	39.6	39.2 58.8	38.8	38.4	38.0
47	8.81 944	192	8.82 038	192	1.17 962	9.99 905	13	3 4	79.2	58.8 78.4	58.2 77.6	57.6 76.8	57.0 76.0
48	8.82 134	190	8.82 230	192	1-17 770	9.99 903	12		99.0	98.0	97.0	96.0	95.0
49	8.82 324	190	8.82 420	190	1-17 580	9.99 904	11	5	118.8	117.6	116.4	115.2	114.0
50	8.82 513	189	8.82 610	190	1.17 390	9.99 903	10	8	138.6	137.2 156.8	135.8	134.4	133.0
		188		180			·l	l °	158.4	176.4	155.2 174.6	153.6	152.0 171.Q
51	8.82 701	187	8.82 799	188	1.17 201	9.99 902	8	′					
52 53	8.82 888 8.83 075	187	8.82 987 8.83 175	188	1.17 013	9.99 900	1 7	١.	188	186	184	182	181
		186		186			6	1 2	18.8 37.6	18.6 37.2	18.4 36.8	18.2 36.4	18.1 36.2
54 55	8.83 261 8.83 446	185	8.83 361 8.83 547	186	1.16 639	9.99 899 9.99 898	5	3	56.4	55.8	55.2	54.6	54.3
56	8.83 630	184	8.83 732	185	1.16 268	9.99 898	1 4	4	75.2	74-4	73.6	72.8	72.4
57	8.83 813	183	8.83 916	184	1.16 084	9.99 897		5	94.0	93.0	92.0	91.0	90.5
58	8.83 996	183	8.84 100	184	1.15 900	9.99 896	3 2	6	112.8	111.6	110.4	109.2	108.6 126.7
59	8.84 177	181	8.84 282	182	1.15 718	9.99 895	1	8	150.4	148.8	147.2	145.6	144.8
60	8.84 358	181	8.84 464	182	1.15 536	9.99 894	0	9		167.4	165.6	163.8	162.9
	L Cos	d	L Cot	c d	L Tan	L Sin	 	-			PP		
	,	, ~	1 - 550	100			1						

	4°												
′	L Sin	d	L Tan	c d	L Cot	L Cos					PP		
0	8.84 358	181	8.84 464	182	1.15 536	9.99 894	60		182	181	180	179	178
1	8.84 539	179	8.84 646	180	1-15 354	9.99 893	59	1 2	18.2 36.4	18.1 36.2	18.0 36.0	17.9	17.8
3	8.84 718 8.84 897	179	8.84 826 8.85 006	180	1.15 174	9.99 892 9.99 891	58 57	3	54.6	54.3	30.0 54.0	35.8 53.7	35.6 53.4
4	8.85 075	178	8.85 185	179	1 14 815	0.00 801	56	4	72.8	72.4 90.5	72.0	71.6 89.5	71.2
5 6	8.85 252 8.85 429	177	8.85 363 8.85 540	177	1.14 637	9.99 890 9.99 889	55 54	6	109.2	108.6	108.0	107.4	89.0 106.8
7	8.85 605	176	8.85 717	177	1 14 283	9.99 888	53	7 8	127.4	126.7	126.0 144.0	125.3	124.6
8	8.85 780	175	8.85 893	176 176	1.14 107	9.99 887	52	9	163.8	162.9	162.0	161.1	160.2
9	8.85 955	173	8.86 069	174	1.13 931	9.99 886	51		177	176	175	174	178
10	8.86 128		8.86 243		1.13 757	9.99 885	50	1	17.7	17.6	17.5	17.4	17.3
11	8.86 301	173	8.86 417	174	1.13 583	9.99 884	49	3	35.4 53.1	35.2 52.8	35.0 52.5	34.8	34.6 51-9
I 2 I 3	8.86 474 8.86 645	171	8.86 591 8.86 763	172	1.13 409	9.99 883 9.99 882	48 47	4	70.8 88.5	70.4 88.0	70.0	69.6	51.9 69.2
14	8.86 816	171	8.86 935	172	1.13 065	9.99 881	46	6	106.2	105.6	87.5 105.0	87.0	86.5 103.8
15	8.86 987	171 160	8.87 106	171	1.12 894	9.99 880	45	7 8	123.9	123.2	122.5	121.8	12I-I
16	8.87 156	169	8.87 277	170	1.12 723	9.99 879	44	9	141.6	140.8 158.4	140.0 157.5	139.2 156 6	138.4
17	8.87 325 8.87 494	169	8.87 447 8.87 616	169	1.12 553	9.99 879 9.99 878	43 42		172	171	170	169	166
19	8.87 661	167	8.87 785	169	1.12 215	9.99 877	41	1	17.2	17.1	17.0	16.9	16.8
20	8.87 829	168	8.87 953	168	1.12 047	9.99 876	40	3	34.4 51 6	34.2 51.3	34.0 51.0	33.8 50.7	33.6 50.4
21	8.87 995	166	8.88 120	167	1.11 880	9.99 875	39	4	68.8	68.4	68.o	67.6	67.2
22	8.88 161	166 165	8.88 287	167 166	1.11 713	9.99 874	38	5	86.0	85.5	85.0	84.5	84.0
23	8.88 3 26	164	8.88 453	165	1.11 547	9.99 873	37	7	120.4	119.7	119.0	118.3	117.6
24 25	8.88 490 8.88 654	164	8.88 618 8.88 783	165	1.11 382	9.99 872	36 35	8	137.6	136.8	136.0 153.0	135.2 152.1	134.4
26	8.88 817	163	8.88 948	163	1.11 052	9.99 870	34	1	167	166	165	164	163
27	8.88 980	162	8.89 111	163	1.10 889	9.99 869	33	1	16.7	16.6	16.5	16.4	16.3
28	8.89 142 8.89 304	162	8.89 274 8.89 437	163	1.10 726	9.99 868 9.99 867	32 31	2	33-4	33.2	33.0	32.8	32.6
30	8.89 464	160	8.89 598	161	1.10 402	9.99 866	30	3 4	50.1	49.8 66.4	49.5 66.0	49.2 65.6	48.9 65.2
		161		162		l		5	83.5	83.0	82.5	82.0	81.5
31 32	8.89 625 8.89 784	159	8.89 760 8.89 920	160	1.10 240	9.99 865	29 28	7	116.9	99.6 116.2	99. o 115.5	98.4 114.8	97.8 114.1
33	8.89 943	159	8.90 080	160	1.09 920	9.99 863	27	8	133.6	132.8	132.0	131.2	130.4
34	8.90 102	158	8.90 240	159	1.09 760	9.99 862	26	,					
35 36	8.90 260 8.90 417	157	8.90 399 8.90 557	158	1.09 601	9.99 861 9.99 860	25	,	162	16.1	160	159 15.9	158 15.8
37	8.90 574	157	8.90 715	158	1.09 285	9.99 859	23	2	32.4	32.2	32.0	31.8	31.6
38	8.90 730 8.90 885	155	8.90 872 8.91 0 29	157	1.09 128	9.99 858	2 2 2 I	3	48.6 64.8	48.3 64.4	48.0 64.0	47.7 63.6	47.4 63.2
39		155		156	1.08 971	9.99 857		5	81.0	80.5	80.0	79.5	79.0
40	8.91 040	155	8.91 185	155	1.08 815	9.99 856	20	6 7	97-2 113.4	96.6 112.7	96.0 112.0	95.4 111.3	94.8 110.6
41	8.91 195	154	8.91 340	155	1.08 660	9.99 855	19	8	129.0	128.8	128.0	127.2	126.4
42 43	8.91 349 8.91 502	153	8.91 495 8.91 650	155	1.08 505	9.99 854 9.99 853	17	9	145.8	144.9	144.0	143.1	142.2
44	8.91 655	153	8.91 803	153	1.08 197	9.99 852	16	,	157 15.7	156 15.6	155 15.5	154 15.4	153 15.3
45 46	8.91 807 8.91 959	152	8.91 957 8.92 110	153	1.08 043	9.99 851	15	2	31.4	31.2	31.0	30.8	30.6
47	8.92 110	151	8.92 262	152	1.07 890	9.99 848	13	3	47 t 62.8	46.8 62.4	46.5 62.0	46.2 61.6	45.9
48	8.92 261	151	8.92 414	152 151	1.07 586	9.99 847	12	5	78.5	78.0	77-5	77.0	76.5
49	8.92 411	150	8.92 565	151	1.07 435	9.99 846	11	6 7	94.2	93.6 109.2	93. 0 108.5	92.4 107.8	91. 8 107.1
50	8.92 561	149	8.92 716	150	1.07 284	9.99 845	10	8	125.6	124.8	124.0	123.2	122.4
51	8.92 710 8.92 859	149	8.92 866	150	1.07 134	9.99 844 9.99 843	8	"	152	151	150	149	143
52 53	8.93 007	148	8.93 0 16 8.93 165	149	1.06 984	9.99 842	7	1	15.2	15.1	15.0	14.9	14.8
54	8.93 154	147	8.93 313	148	1.06 687	9.99 841	6	2	30.4	30.2	30.0	29.8	29.6
55 56	8.93 301 8.93 448	147	8.93 462 8.93 609	147	1.06 538	9.99 840	5	3 4	45.6 60.8	45.3 60.4	45.0 60.0	44.7 59.6	44·4 59.2
5.7	8.93 594	146	8.93 756	147	1.06 244	9.99 838	3	5	76.0	75.5	75.0	74.5 89.4	74.0 88.8
58	8.93 740 8.93 885	146	8.93 903	147	1.06 097	9.99 837	2	7	91.2 106.4	90.6 105.7	105.0	104.3	103.6
59		145	8.94 049	146	1.05 951	9.99 836	1	8	121.6	120.8	120.0	119.2 134.1	118.4 133.2
60	8.94 030	_	8.94 195		1.05 805	9.99 834	0	_		.55.7	-05	.04.4	
	L Cos	d	L Cot	c d	L Tan	L Sin	'				PΡ		
							ego						

94°

	5 °						174						
	L Sin	d	L Tan	c d	L Cot	L Cos				РΙ	P		
0	8.94 030	144	8.94 195	145	1.05 805	9.99 834	60		147	146	145	144	
1	8.94 174	143	8.94 340	1.45	1.05 660	9.99 833	59	1 2	14.7	14.6	14.5	14.4 28.8	
3	8.94 317 8.94 461	144	8.94 485 8.94 630	145	1.05 515	9.99 832 9.99 831	58 57	3	29.4 44.1	29.2 43.8	29.0 43.5	43.2	
4	8.94 603	1.42	8.94 773	143	1.05 227	9.99 830	56	4	58.8	58.4	58.0	57.6	
5	8.94 746	143	8.94 917	144	1.05 083	9.99 829	55	5	73.5 88.2	73.0 87.6	72.5	72.0 86.4	
ő	8.94 887	141	8.95 060	143	1.04 940	9.99 828	54	7	102.0	102.2	87.0 101.5	100.8	
7 8	8.95 029	141	8.95 202	142	1.04 798	9.99 827	53	8	117.6	116.8	116.0	115.2	
	8.95 170	140	8.95 344 8.95 486	142	1.04 656	9.99 825	52	9	132.3	131.4	130.5	129.6	
9	8.95 310	140	0.95 400	141	1.04 514	9.99 824	51		143	142	141	140	
10	8.95 450	1	8.95 627	'	1.04 373	9.99 823	50	1	14.3	14.2	14.1	14.0	
111	8.95 589	139	8.95 767	140	1.04 233	9.99 822	49	3	28.6 42.9	28.4 42.6	28.2 42.3	28.0 42.0	
12	8.95 728	139	8.95 908	141	1.04 092	9.99 821	48	4	57.2	56.8	56.4	56.0	
13	8.95 867	138	8.96 047	140	1.03 953	9.99 820	47	5 6	71.5 85.8	71.0	70.5	70.0	
14	8.96 005	138	8.96 187	138	1.03 813	9.99 819	46		100.1	85.2 99.4	84.6 98.7	84.0 98.0	
16	8.96 143 8.96 280	137	8.96 325 8.96 464	139	1.03 675	9.99 817	45	7 8	114.4	113.6	112.8	112.0	
	1 1	137	8.96 602	138			44	9	128.7	127.8	126.9	1 26.0	
17	8.96 417 8.96 553	136	8.96 739	137	1.03 398	9.99 815	43		139	138	137	136	
19	8.96 689	136	8.96 877	138	1.03 123	9.99 813	41	1	13.9	13.8	13.7	13.6	
20	8 06 9 2 -	136	8 07 01-	136			1	2	27.8	27.6	27.4	27.2	
40	8.96 825	135	8.97 013	137	1.02 987	9.99 812	40	3	41.7 55.6	41.4 55.2	41.1 54.8	40.8	
21	8.96 960	135	8.97 150	135	1.02 850	9.99 810	39	5	69.5	55.2 69.0	68.5	54.4 68.0	
22	8.97 095	134	8.97 285	136	1.02 715	9.99 809	38	6	83.4	82.8	82.2	81.6	
23	8.97 229	134	8.97 421	135	1.02 579	9.99 808	37	7 8	97.3	96.6	95.9	95.2	
24	8.97 363	133	8.97 556 8.97 691	135	1.02 444	9.99 807	36	°	111.2 125.1	110.4	109.6	108.8	
26	8.97 496 8.97 629	133	8.97 825	134	1.02 175	9.99 804	35	'					
27	8.97 762	133	8.97 959	134	1.02 041	9.99 803			135	134	133	132	
28	8.97 894	132	8.98 092	133	1.01 908	9.99 802	33	1 2	13.5	13.4 26.8	13.3 26.6	13.2 26.4	
29	8.98 026	-	8.98 225	133	1.01 775	9.99 801	31	3	40.5	40.2	39.9	39.6	
30	8.98 157	131	8.98 358	133	1.01 642	9.99 800	30	4	54.0	53.6	53.2	52.8	
		131		132			l	5	67.5 81.0	67.0 80.4	66.5 79.8	66.0 79.2	
31 32	8.98 288 8.98 419	131	8.98 490 8.98 622	132	1.01 510	9.99 798 9.99 797	29	7	94.5	93.8	93.1	92.4	
33	8.98 549	130	8.98 753	131	1.01 247	9.99 796	27	8	108.0	107.2	106.4	105.6	
34	8.98 679	130	8.98 884	131	1.01 116	9.99 795	26	9	121.5	1 20.6	119.7	118.8	
35	8.98 808	I 29	8.99 015	131	1.00 985	9.99 793	25		131	130	129	128	
36	8.98 937	129	8.99 145	130	1.00 855	9.99 792	2.4	1	13.1	13.0	12.9	12.8	
37	8.99 066	128	8.99 275	130	1.00 725	9.99 791	23	3	26.2 39.3	26.0 39.0	25.8 38.7	25.6 38.4	
38	8.99 194	128	8.99 405	129	1.00 595	9.99 790	22	4	52.4	52.0	51.6	51.2	
39	8.99 322	1 28	8.99 534	128	1.00 466	9.99 788	21	5	65.5	65.0	64.5	64.0	
40	8.99 450		8.99 662		1.00 338	9.99 787	20	6	78.6	78.0	77.4	76.8 89.6	
41	8.99 577	127	8 99 791	129	1.00 200	9.99 786	10	7 8	91.7	91.0 104.0	90.3	102.4	
42	8.99 704	127	8.99 919	128	1.00 081	9.99 785	18	9	117.9	117.0	116.1	115.2	
43	8 99 830	126	9.00 046	128	0.99 954	9.99 783	17		127	126	125	124	
44	8.99 956	126	9.00 174	127	0.99 826	. 9.99 782	16	1	12.7	12.6	12.5	12.4	
45 46	9.00 082	125	9.00 301	126	0.99 699	9.99 781	15	2	25.4	25.2	25.0	24.8	
		125		126	0 99 573	9.99 780	14	3	38.1 50.8	37.8 50.4	37.5 50.0	37.2 49.6	
47 48	9.00 332 9.00 456	124	9.00 553	126	0.99 447	9.99 778 9.99 777	13	4 5	63.5	63.0	62.5	62.0	
49	9.00 581	125	9.00 805	126	0.99 195	9.99 776	11	6	76.2	75.6 88.2	75.0	74.4	
50	9.00 704	123	9.00 930	125	0 99 070		10	7 8	88.9	88.2 100.8	87.5	86.8 99.2	
		12.1		125	-,,,,,,	9-99 775	1"	9	114.3	113.4	112.5	111.6	
51 52	9.00 828	123	9.01 055	124	0.98 945	9.99 773	9		123	122	121	120	
53	9.01 074	123	9.01 303	I 24	0.98 697	9.99 772 9.99 771	7	1	12.3	12.2	12.1	12.0	
54	9.01 196	122	9.01 427	I 2.4	0 98 573	9.99 769	6	2	24.6	24.4	24.2	24.0	
55	9.01 318	122	9.01 550	I 23 I 23	0.98 450	9.99 768	5	3	36.9	36.6 48.8	36.3 48.4	36.0 48.0	
56	9.01 440	121	9.01 673	123	0.98 327	9.99 767	4	4 5	49.2	61.0	40.4 60.5	48.0 60.0	
57	9.01 561	121	9.01 796	123	0.98 204	9.99 765	3	5	61.5 73.8 86.1	73.2	72.6	72.0	
58 59	9.01 682	121	9.01 918	122	0.98 082	9.99 764	2	7 8	86.1	85.4	84.7	84.0	
		120	9.02 040	I 2 2	0.97 960	9.99 763	1	9	98.4 110.7	97.6 109.8	96.8 108.9	96.0 108.0	
60	9.01 923		9.02 162		0.97 838	9.99 761	0						
L	L Cos	d	L Cot	c d	L Tan	L Sin	'			PF	•		

 95°

	6° 173°												
1	L Sin	d	L Tan	c d	L Cot	L Cos				PF)		
0	9.01 923	120	9.02 162	121	0.97 838	9.99 761	60						
I 2	9.02 043	120	9.02 283	121	0.97 717	9.99 760	59 58						
3	9.02 283	120	9.02 525	121	0.97 475	9.99 757	57		121	120	119	118	
4	9.02 402	119	9.02 645	I 20 I 2 I	0.97 355	9.99 756	56	2	12.I 24.2	12.0	11.9 23.8	11.8 23.6	
5	9.02 520	110	9.02 766	119	0.97 234	9.99 755 9.99 753	55 54	3	36.3	36.0	35.7	35.4	
	9.02 757	118	9.03 005	120	0.96 995	9.99 752	53	4	48.4 60.5	48.0 60.0	47.6	47.2	
7 8	9.02 874	117	9.03 124	119	0.96 876	9.99 751	52	5	72.6	72.0	59.5 71.4	59.0 70.8	
. 9	9.02 992	117	9.03 2.12	119	0.96 758	9.99 749	51	7 8	84.7	84.0	83.3	82.6	
10	9.03 109	117	9.03 361	118	0.96 639	9.99 748	50	9	96.8	96.0 108.0	95.2 107.1	94.4 106.2	
II I2	9.03 226	116	9.03 479 9.03 5 97	118	0.96 403	9.99 747	48	,	,		,		
13	9.03 458	116	9.03 714	117	0.96 286	9.99 744	47						
14	9.03 574	116	9.03 832	116	0.96 168	9.99 742 9.99 741	46 45		117	116	115	114	
15 16	9.03 690	115	9.03 940	117	0.95 935	9.99 740	43	I 2	11.7 23.4	11.6 23.2	23.0	11.4	
17	9.03 920	115	9.04 181	116	0.95 819	9.99 738	43	3	35.I	34.8	34.5	34.2	
18	9.04 034	111	9.04 297	116	0.95 703	9.99 737 9.99 736	42 41	4	46.8	46.4 58.0	46.0 57.5	45.6	
19 20	9.04 149	113	9.04 413	115	0.95 557	9.99 734	40	5	70.2	69.6	69.0	57.0 68.4 79.8	
21	9.04 376	114	9.04 523	115	0.95 357	9.99 733	39	7 8	81.9	81.2	80.5	79.8	
22	9.04 490	114	9.04 758	115	0.95 242	9.99 731	38	9	93.6	92.8	92.0 103.5	91.2 102.6	
23	9.04 603	112	9.04 873	114	0.95 127	9.99 730	37		5-0		0-0		
24 25	9.04715	113	9.04 987	114	0.95 013	9.99 728	36		440	440		440	
26	9.04 940	II2	9.05 214	113	0.94 786	9.99 726	34		113	112	111	110	
27	9.05 052	II2	9.05 328	II3	0.94 672	9.99 724	33	1 2	11.3 22.6	11.2 22.4	22.2	22.0	
28	9.05 164	III	9.05 441	II2	0.94 559	9.99 721	31	3	33.9	33.6	33.3	33.0	
30	9.05 386	III	9.05 666	113	0.94 334	9.99 720	30	4	45.2 56.5	44.8 56.0	44.4	44.0	
31	9.05 497	III	9.05 778	112	0.94 222	9.99 718	29	5	67.8	67.2	55.5 66.6	55.0 66.0	
32	9.05 607	110	9.05 890	112	0.94110	9.99 717	28	7 8	79.1	78.4	77.7 88.8	77.0 88.0	
33	9.05 717	110	9.06 002	III	0.93 998	9.99 716	27	9	90.4	89.6	99.9	99.0	
35	9.05 937	110	9.06 224	III	0.93 776	9.99713	25	_			.,,	,,	
36	9.06 046	109	9.06 335	110	0.93 665	9.99 711	2.4	ŀ	100	400	405	400	
37 38	9.06 155	109	9.06 445 9.06 556	III	0.93 555	9.99 710	23		109	108	107	106	
39	9.06 372	108	9.06 666	110	0.93 334	9.99 707	2 I	1 2	10.9	10.8 21.6	10.7	10.6	
40	9.06 481	108	9.06 775	110	0.93 225	9.99 705	30	3	32.7	32.4	32.1	31.8	
41	9.06 589	107	9.06 885	100	0.93 115	9.99 704	19	4 5	43.6 54.5	43.2 54.0	42.8 53.5	42.4 53.0	
42 43	9.06 696	108	9.06 994	109	0.93 006	9.99 702	18	6	65.4	64.8	64.2	63.6	
44	9.06 911	107	9.07 211	108	0.92 789	9.99 699	16	8	76.3 87.2	75.6 86.4	74.9 85.6	74.2 84.8	
45	9.07 018	107	9.07 320	109	0.92 680	9.99 698	15	9	98.I	97.2	96.3	95.4	
46 47	9.07 124	107	9.07 428	108	0.92 572	9.99 696	14	ľ	-				
48	9.07 337	106	9.07 6.43	107	0.92 357	9.99 693	I 2		105	4	04	103	
49	9.07 442	105	9.07 751	108	0.92 249	9.99 692	11		105				
50	9.07 548	105	9.07 858	106	0.92 142	9.99 690	10		10.5		0.4	10.3 20.6	
51 52	9.07 653 9.07 758	105	9.07 964	107	0.92 036	9.99 689	8		31.5	31	.2	30.9	
53	9.07 863	105	9.08 177	106	0.91 823	9.99 686	7		4 42.0		.6 !.0	41.2 51.5	
54	9.07 968	105	9.08 283	106	0.91 717	9.99 684	6		63.0	62	.4	61.8	
55 56	9.08 072	104	9.08 389	106	0.91 611	9.99 683	5 4		73.5	72	2.8	72.I 82.4	
57	9.08 280	104	9.08 600	105	0.91 400	9.99 680	3		94.5		3.6	92.7	
58	9.08 383	103	9.08 705	105	0.91 295	9.99 678	2						
59 60	9.08 486	103	9.08 810	101	0.91 190	9.99 677	0						
1				-		L Sin	1	-		PI			
	L Cos	a	L Cot	c d	L Tan	LSIN	Ľ			Г			

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	7°						72				
7	L Sin	d	L Tan	c d	L Cot	L Cos				PP	
0	9.08 589	700	9.08 914	705	0.91 086	9.99 675	60				
1	9.08 692	103	9.09019	105	0.90 981	9.99 674	59				
2	9.08 795	103	9.09 123	104	0.90 877	9.99672	58		105	104	103
3	9.08 897	102	9.09 227	103	0.90 773	9.99 670	57	1	10.5	10.4	10.3
4	9.08 999	102	9.09 330	104	0.90 566	9.99 667	56 55	2	21.0	20.8	20.6
5 6	9.09 202	101	9.09 537	103	0.90 463	9.99 666	54	3	31.5	31.2 41.6	30.9
7	9.09 304	102	9.09 640	103	0.90 360	9.99 664	53	4 5	42.0 52.5	52.0	41.2 51.5
8	9.09 405	IOI	9.09 742	102	0.90 258	9.99 663	52	6	63.0	62.4	61.8
9	9.09 506	100	9.09 845	103	0.90 155	9.99 661	51	7 8	73.5	72.8	72.I
10	9.09 606	101	9.09 947	102	0.90 053	9.99 659	50	9	84.0 94.5	83.2 93.6	82.4 92.7
II	9.09 707	100	9.10 049	101	0.89 951	9.99 658	49 48	9	94.3	93.0	92.7
12 13	9.09 807	100	9.10 150 9.10 252	102	0.89 748	9.99 655	47				
14	9.10 006	99	9.10 353	101	0.89 647	9.99 653	46		102	101	99
15	9.10 106	100	9.10 454	101	0.89 546	9.99 651	45	1	10.2	10.1	9.9
16	9.10 205	99	9.10 555	IOI	0.89 445	9.99 650	44	2	20.4	20.2	19.8
17	9.10 304	98	9.10656	100	0.89 344	9.99 648	43	3	30.6	30.3	29.7
18 19	9.10 402 9.10 501	99	9.10 756 9.10 856	100	0.89 244	9.99 647	42 41	4 5	40.8	40.4 50.5	39.6 49.5
20	9.10 501	98	9.10 956	100	0.89 044	9.99 643	40	6	61.2	60.6	59.4
21	9.10 599	98	9.11 056	100	0.88 944	9.99 642	39	7 8	71.4	70.7	69.3
22	9.10 097	98	9.11 155	99	0.88 845	9.99 640	38	8	81.6	80.8 90.9	79.2 89.1
23	9.10 893	98	9.11 254	99	0.88 746	9.99 638	37	9	91.0	90.9	09.1
24	9.10 990	97	9.11 353	99	0.88 647	9.99 637	36				
25	9.11087	97 97	9.11 452	99 99	0.88 548	9.99 635	35		98	97	96
26	9.11 184	97	9.11 551	98	0.88 449	9.99 633	34	1	9.8	9.7	9.6
27 28	9.11 281 9.11 377	96	9.11 649	98	0.88 253	9.99 630	33	2	19.6	19.4	19.2
29	9.11 474	97	9.11 845	98	0.88 155	9.99 629	31	3	29.4	29.1	28.8
30	9.11 570	96	9.11 943	98	0.88 057	9.99 627	30	5	39.2 49.0	38.8 48.5	38.4 48.0
31	9.11 666	96	9.12 040	97	0.87 960	9.99 625	29	6	58.8	58.2	57.6
32	9.11761	95 96	9.12138	98	0.87 862	9.99 624	28	7 8	68.6	67.9	67.2
33	9.11 857	95	9.12 235	97 97	0.87 765	9.99 622	27	8 9	78.4 88.2	77.6	76.8 86.4
34	9.11 952 9.12 047	95	9.12 332 9.12 428	96	0.87 668	9.99 620 9.99 618	26 25	9	00.2	87.3	00.4
35	9.12 047	95	9.12 525	97	0.87 475	9.99 617	24				
37	9.12 236	94	9.12 621	96	0.87 379	9.99 615	23		95	94	93
38	9.12 331	95	9.12 717	96 96	0.87 283	9.99613	22	1	9.5	9.4	9.3
39	9.12 425	94 94	9.12 813	96	0.87 187	9.99 612	21	2	19.0	18.8	18.6
40	9.12 519	93	9.12 909	95	0.87 091	9.99 610	20	3	28.5	28.2	27.9
41	9.12612	94	9.13 004	95	0.86 996	9.99 608	19	4	38.0 47.5	37.6 47.0	37.2 46.5
43	9.12 706	93	9.13 099	95	0.86 901	9.99 607	18	5	57.0	56.4	55.8
43	9.12 /99	93	9.13 289	95	0.86 711	9.99 603	16	7 8	66.5	65.8	65.1
45	9.12 985	93	9.13 384	95	0.86616	9.99 601	15		76.0	75.2	74.4
46	9.13 078	93	9.13 478	94 95	0.86 522	9.99 600	14	9	85.5	84.6	83.7
47	9.13 171	93	9.13 573	93	0.86 427	9.99 598	13	1			
48 49	9.13 263 9.13 355	92	9.13 667 9.13 761	94	0.86 333	9.99 596	11		92	91	90
50	9.13 447	92	9.13 751	93	0.86 146	9.99 593	10	l ,	9.2	9.1	9.0
51	9.13 539	92	9.13 948	94	0.86 052	9.99 591	9	2	18.4	18.2	18.0
52	9.13 539	91	9.13 940	93	0.85 959	9.99 589	8	3	27.6	27.3	27.0
53	9.13 722	92	9.14 134	93	0.85 866	9.99 588	7	4	36.8	36.4	36.0
54	9.13 813	91	9.14 227	93	0.85 773	9.99 586	6	5 6	46.0 55.2	45.5 54.6	45.0 54.0
55	9.13 904	90	9.14 320	93	0.85 680	9.99 584	5	7	64.4	63.7	63.0
56	9.13 994	91	9.14 412	92	0.85 588	9.99 582	4 3	8	73.6	72.8	72.0
57 58	9.14 175	90	9.14 504	93	0.85 403	9.99 579	2	9	82.8	81.9	81.0
59	9.14 266	91	9.14 688	91	0.85 312	9.99 577	ī				
60	9.14356	90	9.14780	92	0.85 220	9.99 575	0				
	L Cos	d	L Cot	c d	L Tan	L Sin	,			PP	

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1 9.144 35 90 9.14 963 90 14 963 90 14 963 90 14 963 90 14 963 90 15 154 90 9.15 154 9.15	′	L Sin	d	L Tan	c d	L Cot	L Cos			F	P	
1 0.14.415 0.9 0.14.872 0.14.873 0.15.873 0.99.574 59 0.16.1673 0.16.1			80		92			l · ·				
2 91.4 35.0 91.5 14.5 90.9 15.1 4.5 90.9 15.1 4.5 90.9 15.1 4.5 90.9 15.1 4.5 90.9 15.1 4.5 90.9 15.1 4.5 90.9 15.1 4.5 90.9 15.1 4.5 90.9 15.1 90.0 90.8 88.9 91.5 37.7 91.1 98.9 91.5 38.9 91.5 37.7 91.1 98.9 91.5 38.9			_			0.85 128		59				
4 9.11 71 70 9.15 71 70 9.16 71 70 70 70 70 70 70 70		9.14 535	89		91	0.84 9.16				92	91	90
6 0,14 801 80 91,5 327 91 92,5 72,0 73,3 32,0 36						0.84855						
7 0.14.980	5	9.14803				0.84 764						
S			89							36.8	36.1	
19 0.15 245 88 9.15 688 9.15 688 9.15 688 9.15 688 9.15 688 9.15 688 9.15 688 9.15 777 9.15 596 88 9.15 596 89 0.84 123 9.99 554 47 9.15 596 87 9.15 596 89 0.84 123 9.99 554 47 9.15 596 89 0.16 135 89 0.83 368 9.99 550 49 9.15 596 89 0.16 135 89 0.83 368 9.99 550 49 9.15 596 89 0.84 123 9.99 550 49 9.15 596 89 0.84 123 9.99 550 40 9.15 596 89 0.83 368 9.99 550 44 9.15 596 89 0.16 135 89 0.83 368 9.99 550 44 9.15 596 89 0.16 135 89 0.83 368 9.99 550 44 9.15 596 89 0.16 518 89 0.83 368 9.99 550 44 9.15 596 89 0.16 518 89 0.83 368 9.99 550 44 9.15 596 89 0.16 518 89 0.83 368 9.99 550 44 9.15 596 44 9.15 596 80 0.83 368 9.99 550 44 9.15 596 44	8	9.15 069				0.84 492		52		46.0	45.5	45.0
10	-	9.15 157		9.15 598			9.99 559			55.2	54.0	54.0
11 0.15 33 34 35 37 37 30 39 530 49 30 30 30 30 30 30 30 3			88							73.6	72.8	72.0
13 9.15 506			88	9.15 777	-	0.84 223			9	82.8	81.9	81.0
1.4 0.15 596 87 9.16 046 89 0.83 951 9.99 548 45 17 9.15 857 87 9.16 924 88 0.83 876 9.99 548 45 17 9.15 857 87 9.16 924 88 0.83 876 9.99 548 45 17 9.15 857 87 9.16 924 88 0.83 888 9.99 548 45 17 8.9 8.8 8.8 17.6 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.6 17.8 17.8 17.6 17.8 17.8 17.6 17.8 17.8 17.6 17.8 17.8 17.8 17.8 17.6 17.8						0.84 044			1			
1	_	9.15 596		9.16 046		0.83 954	9.99 550			89		88
17 9.15 877 87 9.16 312 88 9.99 543 43 326.7 26.4 4 9.16			87		89					I 8.9		8.8
18 9,15,944 86 9,16,939 86 9,16,16,16 87 9,16,16,16 87 9,16,16,17 88 0,83,121 9,99,541 41 4 35.6 35.2 20,16,16 9,16,16 87 9,16,16 88 0,83,123 9,99,531 40 6 5,34 43.5 35.6 35.2 21.8 44.9 44.9 16,16 35.3 36.8 9,16,17 88 0,83,313 9,99,533 40 6 5,34 43.2 44.9 17.2 70.4 9,17,14 86 9,16,17 88 0,83,243 9,99,333 37 9 80.1 70.2 9,17,2 29 9,16,646 85 9,17,103 85 9,17,103 85 9,17,103 87 0,82,810 9,99,333 37 29 9,16,866 85 9,17,439 84 9,17,439 85 9,17,439 86 9,17,439 87 0,82,234 9,99,333 37 18 87 8.6 8.5 30 9,17,239 84 9,17,702 86 0,82,234 9,99,333			87		88				1			
19	18	9.15 944		9.16 401		0.83 599			ĺ			
20						0.83 511			l			44.0
21								ı		6 53.4		52.8
23						0.83 335				8 71.2		
24				9.16 841		0.83 159	9.99 533					
26	24	9.16 460				0.83 072						
10	25	9.16 545	86							87	86	85
28 9.16 850 85 9.17 2363 87 0.82 530 9.09 522 31 3 26.1 25.8 25.5 30 9.17 975 84 9.17 450 85 9.17 536 86 0.82 237 9.99 521 31 3 26.1 25.8 25.5 31 9.17 905 84 9.17 7536 86 0.82 378 9.99 517 28 49.17 17 536 86 0.82 2464 9.99 517 28 7 60.9 60.2 59.5 34 9.17 307 84 9.17 918 86 0.82 240 9.99 517 28 7 60.9 60.2 59.5 35 9.17 343 84 9.17 918 86 0.82 240 9.99 517 28 36 9.17 558 84 9.17 988 85 0.82 266 9.99 517 28 36 9.17 558 84 9.17 988 85 0.82 260 9.99 511 28 37 9.17 558 83 9.18 8136 85 0.81 819 9.99 517 28 38 9.17 641 83 9.18 366 85 0.81 819 9.99 507 23 41 9.17 807 83 9.18 306 85 9.18 306 85 9.18 306 85 42 9.17 973 82 9.18 307 85<					87				,			
29 9.16 886 85 9.17 363 85 9.17 363 85 9.17 365 86 9.25 86 9.25 86 9.25 87 9.25 87 9.25 87 9.25 87 9.25 87 9.25 9.25 87 9.25 9.2		9.16801			87	0.82 723		32			17.2	
Solution			84	9.17 363		0.82 637	9.99 522	31				
31 9,17053 84 9,177039 85 0.82 279 9,99 515 27 86 0.9 60.2 59.5 86 0.82 201 9,99 515 27 87 84 9,179 80 85 0.82 201 9,99 515 27 87 84 9,179 80 85 0.82 201 9,99 515 27 87 80 80 80 80 80 80 80 80 80 80 80 80 80								1.				
33 0.17 223 84 0.17 708 86 0.82 292 0.99 513 26 0.82 203 0.99 513 25 0.99 513 25 0.87 0.99 513 25 0.87 0.99 513 25 0.87 0.99 513 25 0.87 0.99 513 25 0.87 0.99 513 25 0.87 0.82 205 0.99 513 25 0.87 0.99 513 25 0.87 0.87 0.99 513 25 0.87 0.87 0.99 513 25 27 27 27 27 27 27 27		9.17 055		9.17 536	86	0.82 464			6	52.2	51.6	51.0
34		9.17 139	84		86				7 8			59.5
36 0.17 474 84 84 84 85 9.17 965 85 9.18 0.51 85 9.19 0.51 85 9.19 0.51 85 9.19 0.51 85 9.19 0.51 85 9.19 0.51 85 9.19 0.55 85 9.10 0.55 85 9.10 0.55 85 9.1		9.17 307						26		78.3		
37 0.17 558 84 0.18 051 85 0.81 804 0.99 507 22 23 84 83 0.91 7041 83 0.91 7724 83 0.91 8021 85 0.81 804 0.99 505 22 21 16.8 16.6 0.81 604 0.99 409 0.81 604 0.99 505 0.81 604 0.99 505 0.81 604 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.99 409 0.91 805 0.91 805 0.99 409 0.91 805			83									
38 9.17 641 83 9.18 136 85 0.81 864 9.99 505 22 1 1 8.4 8.3 40 9.17 807 83 9.18 306 85 0.81 797 9.99 503 21 1 8.4 8.3 41 9.17 807 83 9.18 306 85 0.81 609 9.99 499 10 4 3.36 3.3.2 24.9 9.99 497 18 5 4.2 9.17 807 8.3 9.18 8175 8.5 0.81 609 9.99 497 18 5 4.2 0.4 1.5 4.0 81 537 4.0 81 537 4.0 81 537 9.99 499 17 7 8.8.8 8.1 4.0 81 356 9.99 499 17 7 8.8.8 8.1 4.0 81 356 9.99 499 17 7 8.8.8 8.1 4.0 81 356 9.99 499 17 7 8.8.8 8.1 4.0 81 356 9.99 499 17 7 8.8.8 8.1 9.99 481 9.99 499 17 7 8.8.8 8.1 9.8 9.18 13 9.8 9.18 13	•		84		86					0.4		0.9
10 10 10 10 10 10 10 10	38	9.17 641		9.18 136	85	0.81 864		22				
1	39		83		85			1		2 16.8		
1					85			1		3 25.2		24.9
43 9.18 655 82 44 9.18 637 44 9.18 637 45 9.18 65 85 85 85 85 85 85 8			83	9.18 391								
44 9.18 137 45 9.18 137 45 9.18 137 45 9.18 137 45 9.18 137 45 9.18 137 45 9.18 137 45 9.18 137 47 9.18 138			82		85					6 50.4		49.8
46 9.18 302 82 9.18 979 47 9.18 812 84 0.81 104 9.99 488 13 86 9.18 870 81 9.19 9.19 1.46 83 0.80 688 9.99 485 12 9.18 979 81 9.19 9.19 9.19 870 82 9.18 979 81 9.19 9.19 9.19 870 82 9.19 9.19 9.19 9.19 870 82 9.19 9.19 9.19 9.19 9.19 9.19 9.19 9.1	44	9.18 137		9.18644	84	0.81 356	9.99 494			7 58.8		58.1
47	45 46	9.18 220			84	0.81 272						
48 9.18 465 82 9.18 979 83 0.80 937 9.99 484 11 82 81 80 9.19 632 81 9.19 146 9.18 979 81 9.19 312 83 0.80 937 9.99 484 11 1 1 8.2 8.1 8.0 9.19 632 81 9.19 146 9.19 312 83 0.80 937 9.99 485 9.19 633 81 9.19 312 83 0.80 608 9.19 643 82 9.19 644 19		9.18 383			84							
Section Sect	48	9.18 465		9.18 979	83	0.81 021	9.99 486	12		00	04	00
St 9.18 072 51 9.18 072 52 9.18 790 52 9.18 790 53 9.18 871 54 9.19 9.32 53 9.19 9.33 55 9.19 0.33 50 9.19 1.33 56 9.19 1.33 58 9.19 561 82 83 9.19 561 83					83			1				
51 9.18 790 81 9.19 229 0.80 6771 9.99 478 8 3 24.6 24.3 24.0 52 9.18 790 81 9.19 312 83 0.80 688 9.99 478 4 32.8 32.4 32.0 54 9.18 952 81 9.19 478 83 0.80 605 9.99 476 7 4 32.8 32.4 32.0 55 9.19 0333 81 9.19 561 83 0.80 439 9.99 477 6 6 49.2 48.6 48.0 57 9.19 193 80 9.19 643 82 0.80 357 9.99 470 4 8 65.6 64.8 64.0 59 9.19 3353 80 9.19 889 82 0.80 275 9.99 462 2 60 9.19 433 80 9.19 971 82 0.80 279 9.99 462 1 L Cos d L Cot c d L Tan L Sin r r P P			8 r									
33		9.18 709	8 r		8.3			8		24.6		24.0
S4 9.18 952 S1 9.19 478 S3 0.80 522 0.99 471 S5 S5 9.19 033 S1 9.19 478 S2 0.80 439 9.99 472 S5 S6.00 S6 9.19 13 S6 S6 9.19 643 S2 0.80 377 9.99 470 S7 S7.4 S6.7 S6.00 S6 9.19 273 S6 9.19 857 S7 9.99 468 S7 9.99 468 S7 9.99 469 S7 S7 S7 S7 S7 S7 S7 S		9.18 871		9.19 395	83				4			32.0
Solution Solution	54			9.19478					5		48.6	48.0
57 9.19 19 80 9.19 725 82 0.80 273 9.99 468 2 0.80 273 9.99 466 2 0.80 273 80 9.19 353 80 9.19 353 80 9.19 353 80 9.19 353 80 9.19 353 80 9.19 353 80 9.19 889 82 0.80 211 9.99 462 1 0.80 229 9.99 462 0 0.80 229 9.99 462 0 0.80 229 0.80 229 0.80			80		82				7	57.4	56.7	56.0
S8 9.19 273 80 9.19 807 82 0.80 103 9.99 466 2 1 1 1 1 1 1 1 1 1	57				82					05.6	72.6	
Social S	58	9.19 273		9.19 807		0.80 193	9.99 466	2	9	13.0	12.0	, 2.0
L Cos d L Cot cd L Tan L Sin / PP									1			
L COST d L COC Cu L Tan L Com	60			-							D D	
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	L Sin	d	L Tan	c d	L Cot	L Cos				PΡ	
_		<u>u</u>		- u			60			- F	
0	9.19 433	80	9.19 971	82	0.80 029	9.99 462		1			
1 2	9.19 513	79	9.20 053	8 r	0.79 947	9.99 460	59 58				
3	9.19 672	80	9.20 216	82	0.79 784	9.99 456	57	1			
4	9.19751	79	9.20 297	81 81	0.79 703	9.99 454	56	1	82	81	80
5	9.19830	79 79	9.20 378	81	0.79 622	9.99 452	55	1	8.2	8.1	8.0
6	9.19 909 9.19 988	79	9.20 459	81	0.79 541	9.99 450	54 53	2	16.4	16.2	16.0
7	9.19 988	79	9.20 540	81	0.79 379	9.99 446	52	3 4	24.6 32.8	24.3 32.4	24.0 32.0
9	9.20 145	78	9.20 701	80 81	0.79 299	9.99 444	51	5	41.0	40.5	40.0
10	9.20 223	78	9.20 782	80	0.79 218	9.99 442	50	6	49.2	48.6	48.0
11	9.20 302	79	9.20 862	80	0.79 138	9.99 440	49	7 8	57.4 65.6	56.7 64.8	56.0 64.0
12	9.20 380	78 78	9.20 942	80	0.79 058	9.99 438	48	9	73.8	72.9	72.0
13 14	9.20 458	77	9.21 022 9.21 102	80	0.78 978	9.99 436	47 46				
15	9.20 535	78	9.21 182	80	0.78 818	9.99 432	45	1			
16	9.20 691	78	9.21 261	79 80	0.78 739	9.99 429	44				
17	9.20 768	77 77	9.21 341	79	0.78 659	9.99 427	43	l			
18	9.20 845	77	9.21 420	79	0.78 580	9.99 425 9.99 423	42 41	l	79	78	77
20	9.20 922	77		79	0.78 422	9.99 421	40	1 1	7.9	7.8	7.7
		77	9.21 578	79				2	15.8	15.6	15.4
2 I 2 2	9.21 076 9.21 153	77	9.21 657	79	0.78 343	9.99 419	39 38	3	23.7	23.4	23.1
23	9.21 229	76	9.21 814	78	0.78 186	9.99 415	37	4 5	39.5	31.2 39.0	30.8 38.5
24	9.21 306	77	9.21 893	79 78	0.78 107	9.99 413	36	6	47.4	46.8	46.2
25	9.21 382	76 76	9.21 971	78	0.78 029	9.99 411	35	7 8	55-3	54.6	53.9
26 27	9.21 458	76	9.22 049	78	0.77 951	9.99 409	34	8	63.2 71.1	62.4 70.2	61.6 69.3
28	9.21 534	76	9.22 127	78	0.77 795	9.99 407	32	9'	/ 1.1	,0.2	09.3
29	9.21 685	75	9.22 283	78 78	0.77 717	9.99 402	31				
30	9.21 761	76	9.22 361		0.77 639	9.99 400	30	1			
31	9.21 836	75	9.22 438	77 78	0.77 562	9.99 398	29				
32	9.21 912	76 75	9.22 516	77	0.77 484	9.99 396	28	1	76	75	74
33	9.21 987	75	9.22 593	77	0.77 407	9.99 394	27	1 1	7.6	7.5	7.4
34	9.22 002	75	9.22 747	77	0.77 253	9.99 392	25	2	15.2	15.0	14.8
36	9.22 211	74	9.22 824	77	0.77 176	9.99 388	24	3	22.8	22.5	22.2
37	9.22 286	75	9.22 901	77 76	0.77 099	9.99 385	23	4	30.4 38.0	30.0	29.6
38	9.22 361	75 74	9.22 977	77	0.77 023	9.99 383	22 21	5 6	45.6	37.5 45.0	37.0 44.4
39 40	9.22 435	74	9.23 054	76	0.76 870	9.99 379	20	7 8	53.2	52.5	51.8
1 1	9.22 509	74	9.23 130	76	0.76 794	9.99 379	10		60.8	60.0	59.2
41 42	9.22 503	74	9.23 283	77	0.76 717	9.99 377	18	9	68.4	67.5	66.6
43	9.22 731	74	9.23 359	76	0.76 641	9.99 372	17				
44	9.22 805	74	9.23 435	76 75	0.76 565	9.99 370	16	l			
45	9.22 878	73 74	9.23 510	76	0.76 490	9.99 368	15	1			
46 47	9.22 952 9.23 0 25	73	9.23 560	75	0.76 339	9.99 364	13		70	20	774
48	9.23 023	73	9.23 737	76	0.76 263	9.99 362	12	Ι.	73	72	71
49	9.23 171	73	9.23 812	75 75	0.76 188	9.99 359	11	2	7.3 14.6	7.2	7.I 14.2
50	9.23 244	73 73	9.23 887	75	0.76 113	9.99 357	10	3	21.0	14.4 21.6	21.3
51	9.23 317	-	9.23 962		0.76 038	9.99 355	9	4	29.2	28.8	28.4
52	9.23 390	73 72	9.24 037 9.24 II2	75 75	0.75 963	9.99 353	8 7	5 6	36.5	36.0	35·5 42.6
53	9.23 462	73	9.24 112	74	0.75 814	9.99 351	6		43.8 51.1	43.2 50.4	49.7
55	9.23 507	72	9.24 261	75	0.75 739	9.99 346	5	7 8	58.4	57.6	56.8
56	9.23 679	72	9.24 335	74	0.75 665	9.99 344	4	9	65.7	64.8	63.9
57	9.23 752	73 71	9.24 410	75 74	0.75 590	9.99 342	3	l			
58 59	9.23 823	72	9.24 484	74	0.75 516	9.99 340	2 I	1			
60	9.23 967	72	9.24 538	74	0.75 368	9.99 337	0	1			
۳		<u> </u>					1			PP	
	L Cos	d	L Cot	c d	L Tan	L Sin	60			77	

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	L Sin	_d_	L Tan	cd	L Cot	L Cos	<u>d</u>	_	PP
0	9.23 967	72	9.24 632	74	0.75 368	9.99 335	2	60	
I	9.24 039	71	9.24 706	73	0.75 294	9.99 333	2	59	
3	9.24 110 9.24 181	7 I	9.24 779 9.24 853	74	0.75 22I 0.75 I47	9.99 331 9.99 328	3	58 57	
4	9.24 253	72	9.24 926	73	0.75 074	9.99 326	2	56	74 73 72
5	9.24 324	7I 7I	9.25 000	74 73	0.75 000	9.99 324	2 2	55	17 17
6	9.24 395	71	9.25 073	73	0.74 927	9.99 322	3	54	1 7.4 7.3 7.2 2 14.8 14.6 14.4
7 8	9.24 536	70	9.25 219	73	0.74 781	9.99 319	2	53 52	3 22.2 21.9 21.6
9	9.24 607	71 70	9.25 292	73	0.74 708	9.99 315	2	51	4 29.6 29.2 28.8 5 37.0 36.5 36.0
10	9.24 677	71	9.25 365	72	0.74 635	9.99 313	3	50	6 44.4 43.8 43.2
11	9.24 748	70	9.25 437	73	0.74 563	9.99 310	2	49	7 51.8 51.1 50.4
12 13	9.24 818 9.24 888	70	9.25 510	72	0.74 490	9.99 308	2	48 47	8 59.2 58.4 57.6 9 66.6 65.7 64.8
14	9.24 958	70	9.25 655	73	0.74 345	9.99 304	2	46	3., 54.5
15	9.25 028	70 70	9.25 727	7 2 7 2	0.74 273	9.99 301	3	45	
16 17	9.25 098	70	9.25 799	72	0.74 201	9.99 299	2	44	
18	9.25 237	69	9.25 943	72	0.74 129	9.99 297	3	43	74 70 00
19	9.25 307	70 69	9.26 015	72 71	0.73 985	9.99 292	2	41	71 70 69
20	9.25 376	69	9.26 086	72	0.73 914	9.99 290	2	40	1 7.1 7.0 6.9 2 14.2 14.0 13.8
2 I	9.25 445	69	9.26 158	71	0.73 842	9.99 288	3	39	3 21.3 21.0 20.7
22	9.25 514 9.25 583	69	9.26 229	72	0.73 771	9.99 285	2	38	4 28.4 28.0 27.6
24	9.25 652	69	9.26 372	71	0.73 628	9.99 281	2	36	5 35.5 35.0 34.5 6 42.6 42.0 41.4
25	9.25 721	69 69	9.26 443	7 I 7 I	0.73 557	9.99 278	3	35	7 49.7 49.0 48.3
26 27	9.25 790	68	9.26 514	71	0.73 486	9.99 276	2	34	8 56.8 56.0 55.2 9 63.9 63.0 62.1
28	9.25 858	69	9.26 655	70	0.73 415	9.99 274	3	33	9 03.9 03.0 02.1
29	9.25 995	68 68	9.26 726	7I 7I	0.73 274	9.99 269	2 2	31	
30	9.26 063	68	9.26 797	70	0.73 203	9.99 267	3	30	
31	9.26 131	68	9.26 867	70	0.73 133	9.99 264	2	29	
32	9.26 199	68	9.26 937 9.27 008	71	0.73 063	9.99 262	2	28	68 67 66
34	9.26 335	68	9.27 078	70	0.72 992	9.99 257	3	26	I 6.8 6.7 6.6
35	9.26 403	68 67	9.27 148	70 70	0.72852	9.99 255	3	25	2 13.6 13.4 13.2 3 20.4 20.1 19.8
36	9.26 470	68	9.27 218	70	0.72 782	9.99 252	2	24	4 27.2 26.8 26.4
37 38	9.26 538	67	9.27 288	69	0.72 712	9.99 250	2	23	5 34.0 33.5 33.0 6 40.8 40.2 39.6
39	9.26 672	67 67	9.27 427	70 69	0.72 573	9.99 245	3	2 I	7 47.6 46.9 46.2
40	9.26739	67	9.27 496	70	0.72 504	9.99 243	2	20	8 54.4 53.6 52.8
41	9.26 806	67	9.27 566	69	0.72 434	9.99 241	3	19	9 61.2 60.3 59.4
42	9.26 873	67	9.27 635	69	0.72 365	9.99 238	2	18	
44	9.27 940	67	9.27 773	69	0.72 227	9.99 233	3	16	
45	9.27 073	66	9.27 842	69	0.72 158	9.99 231	2 2	15	
46	9.27 140	66	9.27 911	69	0.72 089	9.99 229	3	14	65 3
47 48	9.27 206	67	9.27 980 9.28 049	69	0.72 020	9.99 226	2	13	1 6.5 0.3
49	9.27 339	66 66	9.28 117	68	0.71 883	9.99 221	3	II	2 13.0 0.6 3 19.5 0.9
50	9.27 405	66	9.28 186	68	0.71814	9.99 219	2	10	3 19.5 0.9 4 26.0 1.2
51	9.27 471	66	9.28 254	69	0.71 746	9.99 217	2	9	5 32.5 1.5
52 53	9.27 537 9.27 602	65	9.28 323 9.28 391	68	0.71 677	9.99 214	3 2	8 7	
54	9.27 668	66	9.28 459	68	0.71 541	9.99 212	3	6	8 52.0 2.4
55	9.27 734	66	9.28 527	68 68	0.71 473	9.99 207	2	5	9 58.5 2.7
56	9.27 799	65	9.28 595	67	0.71 405	9.99 204	3 2	4	
57 58	9.27 864	66	9.28 662 9.28 730	68	0.71 338	9.99 202	2	3 2	
59	9.27 995	65	9.28 798	68	0.71 202	9.99 197	3	ī	
60	9.28 060	65	9.28 865	07	0.71 135	9.99 195		0	
L	L Cos	d	L Cot	c d	L Tan	L Sin	d	,	PP

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	11°							68°	
7	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.28 060	65	9.28 865	68	0.71 135	9.99 195		60	
1	9.28 125	65	9.28 933	67	0.71 067	9.99 192	3	59	
2	9.28 190 9.28 254	64	9.29 000	67	0.71 000	9.99 190 9.99 187	3	58 57	
3 4	9.28 319	65	9.29 134	67	0.70 866	9.99 185	2	56	68 67 66
5	9.28 384	65	9.29 201	67	0.70 799	9.99 182	3	55	1 6.8 6.7 6.6
6	9.28 448	64 64	9.29 268	67 67	0.70 732	9.99 180	3	54	2 13.6 13.4 13.2
7 8	9.28 512 9.28 577	65	9.29 335 9.29 402	67	0.70 665	9.99 177 9.99 175	2	53 52	3 20.4 20.I 19.8 4 27.2 26.8 26.4
9	9.28 641	64	9.29 468	66	0.70 532	9.99 172	3	51	4 27.2 26.8 26.4 5 34.0 33.5 33.0
10	9.28 705	64	9.29 535	67 66	0.70 465	9.99 170	2	50	6 40.8 40.2 39.6
11	9.28 769	64 64	9.29 601	67	0.70 399	9.99 167	3	49	7 47.6 46.9 46.2 8 54.4 53.6 52.8
12	9.28 833 9.28 896	63	9.29 668	66	0.70 332	9.99 165 9.99 162	3	48	9 61.2 60.3 59.4
13	9.28 960	64	9.29 734	66	0.70 200	9.99 160	2	46	
15	9.29 024	64	9.29 866	66	0.70 134	9.99 157	3	45	
16	9.29 087	63 63	9.29 932	66 66	0.70 068	9.99 155	3	44	İ
17 18	9.29 150	64	9.29 998 9.30 064	66	0.70 002	9.99 I 52 9.99 I 50	2	43	
19	9.29 214 9.29 277	63	9.30 130	66	0.69 870	9.99 147	3	42 41	65 64 63
20	9.29 340	63	9.30 195	65	0.69 805	9.99 145	2	40	i 6.5 6.4 6.3
21	9.29 403	63	9.30 261	66	0.69 739	9.99 142	3	39	2 13.0 12.8 12.6 3 19.5 19.2 18.9
22	9.29 466	63 63	9.30 326	65 65	0.69 674	9.99 140	3	38	4 26.0 25.6 25.2
23	9.29 529	62	9.30 391	66	0.69 609	9.99 137	2	37	5 32.5 32.0 31.5
24 25	9.29 591 9.29 654	63	9.30 457 9.30 522	65	0.69 543	9.99 135 9.99 132	3	36 35	6 39.0 38.4 37.8 7 45.5 44.8 44.1
26	9.29 716	62	9.30 587	65	0.69 413	9.99 130	2	34	8 52.0 51.2 50.4
27	9.29 779	63 62	9.30 652	65 65	0.69 348	9.99 127	3	33	9 58.5 57.6 56.7
28 29	9.29 841	62	9.30 717	65	0.69 283	9.99 I24 9.99 I22	2	32 31	
30	9.29 966	63	9.30 846	64	0.69 154	9.99119	3	30	
31	9.30 028	62	9.30 911	65	0.69 089	9.99 117	2	29	
32	9.30 090	62	9.30 975	64	0.69 025	9.99 114	3	28	
33	9.30 151	61 62	9.31 040	65 64	0.68 960	9.99 112	3	27	62 61 60
34	9.30 213	62	9.31 104	64	0.68 896	9.99 109	3	26 25	1 6.2 6.1 6.0 2 12.4 12.2 12.0
35 36	9.30 275	61	9.31 233	65	0.68 767	9.99 104	2	24	3 18.6 18.3 18.0
37	9.30 398	62 61	9.31 297	64	0.68 703	9.99 101	3	23	4 24.8 24.4 24.0
38	9.30 459	62	9.31 361	64	0.68 639	9.99 099	3	22 21	5 31.0 30.5 30.0 6 37.2 36.6 36.0
39 40	9.30 521	61	9.31 425	64	0.68 575	9.99 096	3	20	7 43.4 42.7 42.0
41	9.30 502	61	9.31 489	63	0.68 448	9.99 093	2	19	
42	9.30 704	61	9.31 616	64	0.68 384	9.99 088	3	18	9 55.8 54.9 54.0
43	9.30 765	61 61	9.31 679	63 64	0.68 321	9.99 086	3	17	
44	9.30 826	61	9.31 743 9.31 806	63	0.68 257	9.99 083 9.99 080	3	16 15	
45 46	9.30 007	60	9.31 870	64	0.68 130	9.99 078	2	14	
47	9.31 008	61	9.31 933	63	0.68 067	9.99 075	3	13	59 3
48	9.31 068	60 61	9.31 996	63 63	0.68 004	9.99 072	3	12	1 5.9 0.3
49 50	9.31 129	60	9.32 059	63	0.67 941	9.99 070	3	10	2 11.8 0.6
51	9.31 189	6 1	9.32 122	63	0.67 878	9.99 064	3	9	3 17.7 0.9 4 23.6 1.2
52	9.31 310	60	9.32 248	63	0.67 752	9.99 062	2	8	
53	9.31 370	60 60	9.32 311	63 62	0.67 689	9.99 059	3	7	6 35.4 1.8
54	9.31 430	60	9.32 373	63	0.67 627	9.99 056	2	6	7 4I.3 2.I 8 47.2 2.4
55 56	9.31 490	59	9.32 436	62	0.67 564	9.99 054	3	5	9 53.1 2.7
57	9.31 609	60	9.32 561	63	0.67 439	9.99 048	3	3	1
58	9.31 669	60 59	9.32 623	62	0.67 377	9.99 046	3	2	
59 60	9.31 728	60	9.32 685	62	0.67 315	9.99 043	3	0	1
			9.32 747		0.67 253	9.99 040		1	
	L Cos	d	L Cot	cd	L Tan	L Sin	d	<u> </u>	PP

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12° 167°

1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP	
0	9.31 788	59	9.32 747	63	0.67 253	9.99 040	2	60		_
1	9.31 847	60	9.32810	62	0.67 190	9.99 038	3	59	1	
2	9.31 907	59	9.32 872	61	0.67 128	9.99 035	3	58 57		1
3	9.32 025	59	9.32 933	62	0.67 005	9.99 032	2	56	63 62 61	
5 6	9.32 084	59	9.33 057	62	0.66 943	9.99 027	3	55	I 6.3 6.2 6.1	1
	9.32 143	59 59	9.33 119	61	0.66 881	9.99 024	3	54	2 12.6 12.4 12.2	Į
7 8	9.32 202 9.32 261	59	9.33 180	62	0.66 820	9.99 022	3	53	3 18.9 18.6 18.3 4 25.2 24.8 24.4	1
9	9.32 319	58	9.33 303	61	0.66 697	9.99019	3	52 51	4 25.2 24.8 24.4 5 31.5 31.0 30.5	
10	9.32 378	59	9.33 365	62 61	0.66 635	9.99 013	3	50	6 37.8 37.2 36.6	ı
11	9.32 437	59	9.33 426	61	0.66 574	9.99 011	2	49	7 44.I 43.4 42.7 8 50.4 49.6 48.8	1
I 2	9.32 495	58 58	9.33 487	61	0.66 513	9.99 008	3	48	9 56.7 55.8 54.9	1
13	9.32 553	59	9.33 548	6 I	0.66 391	9.99 003	3	47 46		1
15	9.32 670	58	9.33 670	6 r	0.66 330	9.99 000	2	45		
16	9.32 728	58 58	9.33 731	61	0.66 269	9.98 997	3	44		1
17	9.32 786 9.32 844	58	9.33 792 9.33 853	61	0.66 208	9.98 994	3	43		
10	9.32 902	58	9.33 913	60	0.66 087	9.98 989	2	42 4I	60 59	
20	9.32 960	58	9.33 974	61	0.66 026	9.98 986	3	40	I 6.0 5.9 2 12.0 11.8	
21	9.33 018	58	9.34 034	60	0.65 966	9.98 983	3	39	3 18.0 17.7	1
22	9.33 075	57 58	9.34 095	61 60	0.65 905	9.98 980	3	38	4 24.0 23.6	١
23	9.33 133 9.33 190	57	9.34 155	60	0.65 845	9.98 978	3	37	5 30.0 29.5 6 36.0 35.4	1
24 25	9.33 248	58	9.34 276	61	0.65 724	9.98 972	3	36		ı
26	9.33 305	57 57	9.34 336	60	0.65 664	9.98 969	3 2	34	8 48.0 47.2	1
27	9.33 362	58	9.34 396	60	0.65 604	9.98 967	3	33	9 54.0 53.1	-
28 29	9.33 420	57	9.34 456 9.34 516	60	0.65 544	9.98 961	3	32 31		1
30	9.33 534	57	9.34 576	60	0.65 424	9.98 958	3	30		
31	9.33 591	57	9.34 635	59	0.65 365	9.98 955	3	29		
32	9.33 647	56 57	9.34 695	60	0.65 305	9.98 953	3	28	58 57	
33	9.33 704	57	9.34 755	59	0.65 245	9.98 950 9.98 947	3	27 26	1 5.8 5.7	
34 35	9.33 761 9.33 818	57	9.34 814	60	0.65 126	9.98 947	3	25	2 11.6 11.4	ı
36	9.33 874	56 57	9-34 933	59 59	0.65 067	9.98 941	3	24	3 17.4 17.1	
37	9.33 931	56	9.34 992	59	0.65 008	9.98 938 9.98 936	3	23	4 23.2 22.8 5 29.0 28.5	
38 39	9.33 987 9.34 043	56	9.35 051	60	0.64 949	9.98 933	3	2 2 2 I	6 34.8 34.2	
40	9.34 100	57	9.35 170	59	0.64 830	9.98 930	3	20	7 40.6 39.9	1
41	9.34 156	56	9.35 229	59	0.64 771	9.98 927	3	19	8 46.4 45.6 9 52.2 51.3	-
12	9.34 212	56 56	9.35 288	59 59	0.64712	9.98 924	3	18		1
43	9.34 268	56	9.35 347	58	0.64 653	9.98 921	2	17		1
44 45	9.34 324 9.34 380	56	9.35 405	59	0.64 536	9.98 919	3	15		1
46	9.34 436	56 55	9.35 523	59 58	0.64 477	9.98 913	3	14		1
47	9.34 491	56	9.35 581	59	0.64 419	9.98 910	3	13	56 55 3	-
48 49	9.34 547 9.34 602	55	9.35 640	58	0.64 360	9.98 907	3	I2	1 5.6 5.5 0.3	
50	9.34 658	56	9.35 757	59	0.64 243	9.98 901	3	10	2 11.2 11.0 0.6 3 16.8 16.5 0.9	1
51	9.34 713	55	9.35 815	58	0.64 185	9.98 898	3	9	4 22.4 22.0 I.2	
52	9.34 769	56 55	9.35 873	58 58	0.64 127	9.98 896	3	8	5 28.0 27.5 1.5	
53	9.34 824 9.34 879	55	9.35 931	58	0.64 069	9.98 893	3	7 6		
54 55	9.34 934	55	9.35 989	58	0.63 953	9.98 887	3	5	8 44.8 44.0 2.4	-
56	9.34 989	55	9.36 105	58 58	0.63 895	9.98 884	3	4	9 50.4 49.5 2.7	
57	9.35 044	55 55	9.36 163	58	0.63 837	9.98 881	3	3	l	
58 59	9.35 099	55	9.36 221	58	0.63 779	9.98 878 9.98 875	3	2 I		
60	9.35 209	55	9.36 336	57	0.63 664	9.98 872	3	0		
	L Cos	d	L Cot	c d	L Tan	L Sin	d	7	PP	-

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13° 166°

	1 6:	٦	1 Tan	ام ما	I Cct	I Car						эр	
	L Sin	d	L Tan	c d	L Cot	L Cos	_d	-				- P	
0	9.35 209	54	9.36 336	58	0.63 664	9.98 872	3	60					
I 2	9.35 263 9.35 318	55	9.36 394	58	0.63 606	9.98 867	2	59 58					
3	9.35 373	55	9.36 509	57	0.63 491	9.98 864	3	57					
4	9.35 427	54 54	9.36 566	57	0.63 434	9.98 861	3	56		ŧ	i8	57	56
5	9.35 481 9.35 536	55	9.36 624 9.36 681	57	0.63 376	9.98 858	3	55 54	1		5.8	5.7	5.6
7	9.35 590	54	9.36 738	57	0.63 262	9.98 852	3	53	3		1.6 7.4	11.4 17.1	11.2 16.8
8	9.35 644	54	9.36 795	57 57	0.63 205	9.98 849	3	52	4		3.2	22.8	22.4
9	9.35 698	54 54	9.36 852	57	0.63 148	9.98 846	3	51	5		9.0	28.5	28.0
10	9.35 752	54	9.36 909	57	0.63 091	9.98 843	3	50			4.8 5.6	34.2 39.9	33.6 39.2
II I2	9.35 806 9.35 860	54	9.36 966 9.37 0 23	57	0.63 034	9.98 840 9.98 837	3	49 48	7 8	4	5.4	45.6	44.8
13	9.35 914	54	9.37 080	57	0.62 920	9.98 834	3	47	9	1 5	2.2	51.3	50.4
14	9.35 968	54	9.37 137	57 56	0.62 863	9.98831	3	46					
15 16	9.36 022 9.36 075	54 53	9.37 193 9.37 250	57	0.62 807	9.98 828 9.98 825	3	45					
17	9.36 129	54	9.37 306	56	0.62 694	9.98 822	3	44					
18	9.36 182	53	9.37 363	57 56	0.62 637	9.98819	3	42		,	5	54	53
19	9.36 236	54 53	9.37 419	57	0.62 581	9.98816	3	41	1		5.5	5.4	5.3
20	9.36 289	53	9.37 476	56	0.62 524	9.98 813	3	40	2		1.0	10.8	10.6
2I 22	9.36 342 9.36 395	53	9.37 532 9.37 588	56	0.62 468	9.98 810 9.98 807	3	39 38	3		5.5	16.2	15.9
23	9.36 449	54	9.37 644	56	0.62 356	9.98 804	3	37	4	1	2.0 7.5	21.6	21.2 26.5
24	9.36 502	53	9.37 700	56	0.62 300	9.98801	3	36	5 6		3.0	32.4	31.8
25 26	9.36 555 9.36 608	53 53	9.37 756 9.37 812	56	0.62 244	9.98 798 9.98 795	3	35	7 8		3.5	37.8	37.I
27	9.36 660	52	9.37 868	56	0.62 132	9.98 793	3	34	9		1.0).5	43.2 48.6	42.4 47.7
28	9.36 713	53	9.37 924	56	0.62 076	9.98 789	3	32	,	1 7.	,.,	4-10	77.7
29	9.36 766	53 53	9.37 980	56 55	0.62 020	9.98 786	3	31					
30	9.36 819	52	9.38 035	56	0.61 965	9.98 783	3	30					
31 32	9.36 871 9.36 924	53	9.38 o91 9.38 147	56	0.61 909 0.61 853	9.98 780 9.98 777	3	29 28					
33	9.36 976	52	9.38 202	55	0.61 798	9.98 774	3	27			52		i1
34	9.37 028	52	9.38 257	55	0.61 743	9.98 771	3	26		Ī	5.2		5.1
35 36	9.37 081	53 52	9.38 313 9.38 368	56 55	o.61 687 o.61 632	9.98 768	3	25		3	10.4		5.3
37	9.37 I33 9.37 I85	52	9.38 423	55	0.61 577	9.98 765 9.98 762	3	24		4	20.8		0.4
38	9.37 237	52	9.38 479	56	0.61 521	9.98 759	3	22		5	26.0	2	5.5
39	9.37 289	52 52	9.38 534	55 55	0.61 466	9.98 756	3	21			31.2 36.4		o.6 5.7
40	9.37 341	52	9.38 589	55	0.61 411	9.98 753	3	20		7 8	41.6	40	o.8
4I 42	9.37 393	52	9.38 644 9.38 699	55	0.61 356	9.98 750	4	19		9	46.8	4.5	5.9
43	9.37 445	52	9.38 754	55	0.61 361	9.98 740	3	17					
44	9.37 549	52	9.38 808	54	0.61 192	9.98 740	3	16					
45 46	9.37 600 9.37 652	51 52	9.38 863	55 55	0.61 137	9.98 737	3	15					
47	9.37 703	51	9.38 972	54	0.61 082	9.98 734 9.98 731	3	14			4		3
48	9.37 755	52	9.39 027	55	0.60 973	9.98 728	3	12		I	0.4		0.3
49	9.37 806	51 52	9.39 082	55 54	0.60 918	9.98 725	3	11		2	0.8		0.6
50	9.37 858	51	9.39 136	54	0.60 864	9.98 722	3	10		3	1.2		0.9
51 52	9.37 909 9.37 960	51	9.39 190	55	o.60 810 o.60 755	9.98 719 9.98 715	4	8		4	1.6		1.2
53	9.37 900	51	9.39 245	54	0.60 755	9.98 713	3	7		5 6	2.4	1	1.8
54	9.38 062	51	9.39 353	54	0.60 647	9.98 709	3	6		7 8	2.8		2.1
55	9.38 113	51 51	9.39 407	54 54	0.60 593	9.98 706	3	5		9	3.2		2.4
56 57	9.38 164	51	9.39 461	54	o.6o 539 o.6o 485	9.98 703	3	4 3		_	. 5.4	•	
58	9.38 266	51	9.39 569	54	0.60 431	9.98 697	3	2					
59	9.38 317	51 51	9.39 623	54 54	0.60 377	9.98 694	3	I					
60	9.38 368		9.39 677		0.60 323	9.98 690		0					
	L Cos	d	L Cot	c d	L Tan	L Sin	d	'			P	Р	

14° 165°

_	14	_						00	
1	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.38 368		9.39 677	54	0.60 323	9.98 690	2	60	
1	9.38 418	50	9.39 731	54	0.60 269	9.98 687	3	59	
3	9.38 469	50	9.39 785 9.39 838	53	0.60 215	9.98 684	3	58 57	
4	9.38 579	51	9.39 892	54	0.60 108	9.98 678	3	56	54 53
5 6	9.38 620	50 50	9.39 945	53 54	0.60 055	9.98 675	3 4	55	1 5.4 5.3
	9.38 670	51	9.39 999	53	0.60 001	9.98 671	3	54	2 10.8 10.6
7 8	9.38 771	50	9.40 106	54	0.59 894	9.98 665	3	52	3 16.2 15.9 4 21.6 21.2
9	9.38 821	50 50	9.40 159	53	0.59 841	9.98 662	3	51	5 27.0 26.5
10	9.38871	50	9.40 212	53 54	0.59 788	9.98 659	3	50	
11	9.38 921	50	9.40 266	53	0.59 734	9.98 656	4	49	8 43.2 42.4
I 2 I 3	9.38 971	50	9.40 319	53	0.59 681	9.98 652	3	48	9 48.6 47.7
14	9.39 071	50	9.40 425	53	0.59 575	9.98 646	3	46	
15	9.39 121	50 49	9.40 478	53 53	0.59 522	9.98 643	3	45	
16 17	9.39 170	50	9.40 531	53	0.59 469	9.98 640	4	44 43	
18	9.39 270	50	9.40 636	52	0.59 364	9.98 633	3	42	52 51 50
19	9.39 319	49 50	9.40 689	53 53	0.59 311	9.98 630	3	41	
20	9.39 369	49	9.40 742	53	0.59 258	9.98 627	4	40	I 5.2 5.1 5.0 2 10.4 10.2 10.0
21	9.39 418	49	9.40 795	52	0.59 205	9.98 623	3	39	3 15.6 15.3 15.0
22	9.39 467 9.39 517	50	9.40 047	53	0.59 153	9.98 617	3	38	4 20.8 20.4 20.0 5 26.0 25.5 25.0
24	9.39 566	49	9.40 952	52	0.59 048	9.98614	3	36	5 26.0 25.5 25.0 6 31.2 30.6 30.0
25	9.39 615	49 49	9.41 005	53 52	0.58 995	9.98 610	4	35	7 36.4 35.7 35.0 8 41.6 40.8 40.0
26 27	9.39 664	49	9.41 057	52	0.58 943	9.98 6 07 9.98 6 0 4	3	34	8 41.6 40.8 40.0 9 46.8 45.9 45.0
28	0.30 762	49	9.41 161	52	0.58 839	9.98 601	3	32	, , , , , , , ,
29	9.39 811	49 49	9.41 214	53 52	0.58 786	9.98 597	4	31	
30	9.39 860	49	9.41 266	52	0.58 734	9.98 594	3	30	
31 32	9.39 909	49	9.41 318	52	0.58 682	9.98 591 9.98 588	3	29 28	
33	9.40 006	48	9.41 422	52	0.58 578	9.98 584	4	27	49 48 47
34	9.40 055	49 48	9.41 474	52 52	0.58 526	9.98 581	3	26	1 4.9 4.8 4.7
35 36	9.40 103	49	9.41 526	52	0.58 474	9.98 578	4	25 24	2 9.8 9.6 9.4 3 14.7 14.4 14.1
37	9.40 200	48	9.41 629	51	0.58 371	9.98 571	3	23	4 19.6 19.2 18.8
38	9.40 249	49	9.41 681	52 52	0.58 319	9.98 568	3	22	5 24.5 24.0 23.5 6 29.4 28.8 28.2
39	9.40 297	49	9.41 733	51	0.58 267	9.98 565	4	21	7 34.3 33.6 32.9
40	9.40 346	48	9.41 784	52	0.58 216	9.98 561	3	20	8 39.2 38.4 37.6
41 42	9.40 394	48	9.41 836	51	0.58 164	9.98 558	3	19	9 44.1 43.2 42.3
43	9.40 490	48 48	9.41 939	52 51	0.58 061	9.98 551	4	17	
44	9.40 538	18	9.41 990	51	0.58 010	9.98 548	3	16	
45 46	9.40 586	.18	9.42 041	52	0.57 959	9.98 545 9.98 541	4	15	
47	9.40 682	48	9.42 144	51	0.57 856	9.98 538	3	13	4 3
48	9.40 730	48 48	9.42 195	51 51	0.57 805	9.98 535 9.98 531	3	I2	1 0.4 0.3
49 50	9.40 778	47	9.42 246	51	0.57 754	9.98 528	3	10	2 0.8 0.6
51	9.40 873	48	9.42 297	51	0.57 652	9.98 525	3	9	3 1.2 0.9 4 1.6 1.2
52	9.40 921	48	9.42 340	51	0.57 601	9.98 521	4	8	5 2.0 1.5
53	9.40 968	47 48	9.42 450	51 51	0.57 550	9.98 518	3	7	
54 55	9.41 016	47	9.42 50I 9.42 552	51	0.57 499	9.98 515	4	5	8 3.2 2.4
56	9.41 111	48	9.42 603	51	0.57 397	9.98 508	3	4	9 3.6 2.7
57	9.41 158	47 47	9.42 653	50	0.57 347	9.98 505	3	3	
58 59	9.41 205 9.41 252	47	9.42 704	51	0.57 296	9.98 501	3	2 I	
60	9.41 300	48	9.42 805	50	0.57 195	9.98 494	4	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	•	PP

_	19							04					
1	L Sin	d	L Tan	c d	L Cot	L Cos	d				P	Р	
0	9.41 300		9.42 805		0.57 195	9.98 494		60					
1	9.41 347	47	9.42 856	51	0.57 144	9.98 491	3	59					
2	9.41 394	47	9.42 906	50 51	0.57 094	9.98 488	3	58					
3	9.41 441	47	9.42 957	50	0.57 043	9.98 484	3	57			1	50 49	
4	9.41 488	47	9.43 007	50	0.56 993	9.98 481	4	56					
5 6	9.41 582	47	9.43 108	51	0.56 892	9.98 474	3	55 54	1 2		5. I 5. 2	5.0 4.9 10.0 9.8	
7	9.41 628	46	9.43 158	50	0.56842	9.98 471	3	53	3		5.3	15.0 14.7	
8	9.41 675	47	9.43 208	50	0.56 792	9.98 467	4	52	4		0.4	20.0 19.6	
9	9.41722	47	9.43 258	50	0.56 742	9.98 464	3	51	5		.5	25.0 24.5	
10	9.41 768		9.43 308	-	0.56 692	9.98 460	4	50	6		0.6	30.0 29.4	
11	9.41 815	47	9.43 358	50	0.56 642	9.98 457	3	49	7 8	35	5.7	35.0 34.3 40.0 39.2	
I 2	9.41 861	46	9.43 408	50 50	0.56 592	9.98 453	4	48	9		.9	45.0 44.1	
13	9.41 908	46	9.43 458	50	0.56 542	9.98 450	3	47					
14 15	9.41 954	47	9.43 508	50	0.56 492	9.98 447	4	46					
16	9.42 047	46	9.43 558 9.43 607	49	0.56 393	9.98 443	3	45 44					
17	9.42 093	46	9.43 657	50	0.56 343	9.98 436	4	43					
18	9.42 140	47	9.43 707	50	0.56 293	9.98 433	3	42		4	8	47 46	
19	9.42 186	46 46	9.43 756	49 50	0.56 244	9.98 429	4	41	1		8		
20	9.42 232	46	9.43 8 0 6		0.56 194	9.98 426	3	40	2		6	4.7 4.6 9.4 9.2	
21	9.42 278	46	9.43 855	49	0.56 145	9.98 422	4	39	3	14		14.1 13.8	
22	9.42 324	46	9.43 905	50 49	0.56 095	9.98 419	3	38	4	19		18.8 18.4	
23	9.42 370	46	9-43 954	50	0.56 046	9.98 415	3	37	5	2.4		23.5 23.0	
24 25	9.42 416	45	9.44 004	49	0.55 996	9.98 412	3	36	6	28 33		28.2 27.6 32.9 32.2	
26	9.42 507	46	9.44 053 9.44 102	49	0.55 947 0.55 898	9.98 405	4	35	7 8	38	.4	37.6 36.8	
27	9.42 553	46	9.44 151	49	0.55 849	9.98 402	3	33	9	43		42.3 41.4	
28	9.42 599	46	9.44 201	50	0.55 799	9.98 398	4	32					
29	9.42 644	45 46	9.44 250	49 49	0.55750	9.98 395	3	31					
30	9.42 690	45	9.44 299	49	0.55 701	9.98 391		30					
31	9.42 735		9.44 348		0.55 652	9.98 388	3	29					
32	9.42 781	46 45	9-44 397	49 49	0.55 603	9.98 384	4	28			45	44	
33	9.42 826	46	9.44 446	49	0.55 554	9.98 381	4	27		I	4.5		
34	9.42 917	45	9.44 495 9.44 544	49	0.55 505	9.98 377 9.98 373	4	26 25		2	9.0		
36	9.42 962	45	9.44 592	48	0.55 408	9.98 370	3	24		3	13.5	13.2	
37	9.43 008	46	9.44 641	49	0.55 359	9.98 366	4	23		4	18.0		
38	9.43 053	45	9.44 690	49 48	0.55 310	9.98 363	3	22		5	22.5		
39	9.43 098	45 45	9.44 738	49	0.55 262	9.98 359	4	21			31.5		
40	9.43 143	45	9.44 787	49	0.55 213	9.98 356	4	20		8	36.0	35.2	
41	9.43 188		9.44 836	48	0.55 164	9.98 352		19		9	40.5	39.6	
42	9.43 233	45 45	9.44 884	49	0.55 116	9.98 349	3	18					
43	9.43 278	45	9.44 933	48	0.55 067	9.98 345	3	17					
44 45	9.43 323	44	9.44 981	48	0.55 019	9.98 342 9.98 338	4	15					
46	9.43 412	45	9.45 078	49	0.54 922	9.98 334	4	1.4					
47	9.43 457	45	9.45 126	48	0.54874	9.98 331	3	13			4	3	
48	9.43 502	45	9.45 174	48 48	0.54 826	9.98 327	4	12		I	0.4	0.3	
49	9.43 546	44 45	9.45 222	49	0.54 778	9.98 324	3 4	II		2	0.8	0.6	
50	9.43 591	44	9.45 271	48	0.54 729	9.98 320	3	10		3	1.2	0.9	
51	9.43 635	45	9.45 319	48	0.54 681	9.98 317	4	9		4	1.6	I.2 I.5	
52 53	9.43 680	45	9.45 367	48	0.54 633	9.98 313	4	8		5 6	2.4	1.8	
54	9.43 724	45	9.45 415	48	0.54 585	9.98 309	3	7		7	2.8	2.1	
55	9.43 709	44	9.45 463 9.45 511	48	0.54 537	9.98 300	4	5		8	3.2	2.4	
56	9.43 857	44	9.45 559	48	0.54 441	9.98 299	3	4		9	3.6	2.7	
57	9.43 901	44	9.45 606	47	0.54 394	9.98 295	4	3					
58	9.43 946	45 44	9.45 654	48 48	0.54 346	9.98 291	4	2					
59 60	9.43 990	44	9.45 702	48	0.54 298	9.98 288	4	0					
100	9.44 034		9.45 750	_	0.54 250	9.98 284		-					-
	L Cos	d	L Cot	c d	L Tan	L Sin	d	_′_			٢	P	

105° (353) **74°**

	1 Cir	4	I Ton	0.4	1 Co+	I Con	٨		PP
	L Sin	_d	L Tan	c d	L Cot	L Cos	_d	0	
0	9 44 034	44	9.45 750	47	0.54 205	9.98 284	3	60	
1 2	9.44 078	44	9.45 797	48	0.54 203	9.98 277	4	59 58	
3	9.44 166	44	9.45 892	47 48	0.54 108	9.98 273	4	57	
4	9.44 210	44	9.45 940	47	0.54 060	9.98 270	3	56	48 47 46
5	9.44 253 9.44 297	44	9.45 987	48	0.54 013	9.98 266	4	55 54	I 4.8 4.7 4.6
7	9.44 341	44	9.46 082	47	0.53 918	9.98 259	3	53	2 9.6 9.4 9.2 3 14.4 14.1 13.8
8	9.44 385	44	9.46 130	48	0.53 870	9.98 255	4	52	4 19.2 18.8 18.4
9	9.44 428	43 44	9.46 177	47 47	0.53 823	9.98 251	4	51	5 24.0 23.5 23.0
10	9.44 472	44	9.46 224	47	0.53 776	9.98 248	4	50	6 28.8 28.2 27.6 7 33.6 32.9 32.2
II	9.44 516	43	9.46 271	48	0.53 729	9.98 244	4	49 48	8 38.4 37.6 36.8
12 13	9.44 559	43	9.46 319	47	0.53 681	9.98 237	3	47	9 43.2 42.3 41.4
14	9.44 646	44	9.46 413	47	0.53 587	9.98 233	4	46	
15	9.44 689	43	9.46 460	47 47	0.53 540	9.98 229	4	45	
16	9.44 733	44 43	9.46 507	47	0.53 493	9.98 226	4	44	
17 18	9.44 776	43	9.46 554 9.46 601	47	0.53 446	9.98 222	4	43	
19	9.44 862	43	9.46 648	47	0.53 352	9.98 215	3	41	45 44 43
20	9.44 905	43	9.46 694	46	0.53 306	9.98 211	4	40	I 4.5 4.4 4.3
21	9.44 948	43	9.46 741	47	0.53 259	9.98 207	4	39	2 9.0 8.8 8.6 3 13.5 13.2 12.9
22	9.44 992	44 43	9.46 788	47 47	0.53 212	9.98 204	3	38	4 18.0 17.6 17.2
23 24	9.45 035	43	9.46 835	46	0.53 165	9.98 200	4	37 36	5 22.5 22.0 21.5
25	9.45 077	43	9.46 928	47	0.53 119	9.98 190	4	35	6 27.0 26.4 25.8 7 31.5 30.8 30.1
26	9.45 163	43	9.46 975	47	0.53 025	9.98 189	3	34	8 36.0 35.2 34.4
27	9.45 206	43	9.47 021	46 47	0.52 979	9.98 185	4	33	9 40.5 39.6 38.7
28 29	9.45 249	43	9.47 068	46	0.52 932	9.98 181	4	32 31	
30	9.45 334	42	9.47 160	46	0.52 840	9.98 174	3	30	
31	9.45 377	43	9.47 207	47	0.52 793	9.98 174	4	29	
32	9.45 419	42	9.47 253	46	0.52 747	9.98 166	4	28	40 44
33	9.45 462	43 42	9.47 299	46 47	0.52 701	9.98 162	4 3	27	42 41
34	9.45 504	43	9.47 346	46	0.52 654	9.98 159 9.98 155	4	26	I 4.2 4.1 2 8.4 8.2
35 36	9-45 547 9-45 589	42	9.47 392 9.47 438	46	0.52 562	9.98 151	4	24	3 12.6 12.3
37	9.45 632	43	9.47 484	46	0.52 516	9.98 147	4	2.3	4 16.8 16.4
38	9.45 674	42 42	9.47 530	46 46	0.52 470	9.98 144	3	22	5 21.0 20.5 6 25.2 24.6
39 40	9.45 716	42	9.47 576	46	0.52 424	9.98 140	4	21	7 29.4 28.7
	9.45 758	43	9.47 622	46	0.52 378	9.98 136	4	1	8 33.6 32.8
41 42	9.45 801 9.45 843	42	9.47 668	46	0.52 332	9.98 132	3	18	9 37.8 36.9
43	9.45 885	42	9.47 760	46	0.52 240	9.98 125	4	17	
44	9.45 927	42 42	9.47 806	46 46	0.52 194	9.98 121	4	16	
45 46	9.45 969	42	9.47 852 9.47 897	45	0.52 148	9.98 117	4	15	
47	9.46 053	42	9.47 943	46	0.52 057	9.98 110	3	13	1 .
48	9.46 095	42	9.47 989	46	0.52 011	9.98 106	4	I 2	4 3
49	9.46 136	4I 42	9.48 035	46 45	0.51 965	9.98 102	4	II	1 0.4 0.3 2 0.8 0.6
50	9.46 178	42	9.48 080	46	0.51 920	9.98 098	4	10	3 1.2 0.9
51	9.46 220	42	9.48 126	45	0.51 874	9.98 094	4	9 8	4 1.6 1.2
52 53	9.46 262 9.46 303	41	9.48 171	46	0.51 829	9.98 090	3	°	5 2.0 I.5 6 2.4 I.8
54	9.46 345	42	9.48 262	45	0.51 738	9.98 083	4	6	7 2.8 2.1
55	9.46 386	4I 42	9.48 307	45	0.51 693	9.98 079	4	5	8 3.2 2.4
56	9.46 428	42 41	9.48 353	46 45	0.51 647	9.98 075	4	4	9 3.6 2.7
57 58	9.46 469 9.46 511	42	9.48 398	45	0.51 602	9.98 071	4	3 2	
59	9.46 552	4 I	9.48 489	46	0.51 557	9.98 063	4	I	
60	9.46 594	42	9.48 534	45	0.51 466	9.98 060	3	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP

1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.46 594		9.48 534		0.51 466	9.98 060		60	
1	9.46 635	41	9.48 579	45	0.51 421	9.98 056	4	59	
2	9.46 676	4I 4I	9.48 624	45 45	0.51 376	9.98 052	4	58	
3	9.46 717	41	9.48 669	45	0.51 331	9.98 048	4	57	
4	9.46 758	42	9.48 714 9.48 759	45	0.51 286	9.98 044 9.98 040	4	56	
5	9.46 841	4 I	9.48 804	45	0.51 196	9.98 036	4	55 54	
7	9.46 882	41	9.48 849	45	0.51 151	9.98 032	4	53	
7 8	9.46 923	41	9.48 894	45	0.51 106	9.98 029	3	52	45 44 43
9	9.46 964	4I 4I	9.48 939	45 45	0.51 061	9.98 025	4	51	I 4.5 4.4 4.3
10	9.47 005	40	9.48 984	45	0.51 016	9.98 021	4	50	2 9.0 8.8 8.6
11	9.47 045	41	9.49 029		0.50971	9.98 017		49	3 13.5 13.2 12.9
12	9.47 086	41	9.49 073	44 45	0.50 927	9.98 013	4	48	4 18.0 17.6 17.2
13	9.47 127 9.47 168	41	9.49 118	45	0.50 882	9.98 009	4	47	5 22.5 22.0 21.5 6 27.0 26.4 25.8
14	9.47 209	41	9.49 163	44	0.50837	9.98 001	4	46 45	7 31.5 30.8 30.1
16	9.47 249	40	9.49 252	45	0.50 748	9.97 997	4	44	7 31.5 30.8 30.1 8 36.0 35.2 34.4
17	9.47 290	41	9.49 296	44	0.50 704	9.97 993	4	43	9 40.5 39.6 38.7
18	9.47 330	40 41	9.49 341	45 44	0.50 659	9.97 989	4	42	
19	9.47 371	40	9.49 385	45	0.50 615	9.97 986	3 4	41	
20	9.47 411	41	9.49 430	44	0.50 570	9.97 982	4	40	
21	9.47 452	40	9.49 474	45	0.50 526	9.97 978	4	39	
22	9.47 492	41	9.49 519	44	0.50 481	9.97 974	4	38	
23	9·47 533 9·47 573	40	9.49 563	44	0.50 437	9.97 970	4	37 36	
25	9.47 613	40	9.49 652	45	0.50 348	9.97 962	4	35	42 41 40
26	9.47 654	41	9.49 696	44	0.50 304	9.97 958	4	34	
27	9.47 694	40	9.49 740	44	0.50 260	9.97 954	4	33	1 4.2 4.1 4.0 2 8.4 8.2 8.0
28	9.47 734	40 40	9.49 784	44 44	0.50 216	9.97 950	4	32	3 12.6 12.3 12.0
29	9.47 774	40	9.49 828	44	0.50 172	9.97 946	4	31	4 16.8 16.4 16.0
30	9.47 814	40	9.49 872	44	0.50 128	9.97 942	4	30	5 21.0 20.5 20.0 6 25.2 24.6 24.0
31	9.47 854	40	9.49 916	44	0.50 084	9.97 938	4	29	
32	9.47 894	40	9.49 960	44	0.50 040	9.97 934	4	28 27	8 33.6 32.8 32.0
34	9.47 934	40	9.50 048	44	0.49 952	9.97 930	4	26	9 37.8 36.9 36.0
35	9.48 014	40	9.50 092	44	0.49 908	9.97 922	4	25	
36	9.48 054	40	9.50 136	44	0.49 864	9.97 918	4	24	
37	9.48 094	40	9.50 180	44	0.49820	9.97 914	4	23	
38	9.48 133	39 40	9.50 223	43 44	0.49 777	9.97 910	4	22	
39	9.48 173	40	9.50 267	44	0.49 733	9.97 906	4	21	
40	9.48 213	39	9.50 311	44	0.49 689	9.97 902	4	20	
41	9.48 252	40	9.50 355	43	0.49 645	9.97 898 9.97 894	4	19	39 5 4 3
42	9.48 332	40	9.50 398 9.50 442	44	0.49 602	9.97 890	4	17	
44	9.48 371	39	9.50 485	43	0.49 515	9.97 886	4	16	1 3.9 0.5 0.4 0.3 2 7.8 1.0 0.8 0.6
45	9.48 411	40	9.50 529	44	0.49 471	9.97 882	4	15	3 11.7 1.5 1.2 0.9
46	9.48 450	39 40	9.50 572	43	0.49 428	9.97 878	4	14	4 15.6 2.0 1.6 1.2
47	9.48 490	39	9.50 616	44	0.49 384	9.97 874	4	13	5 19.5 2.5 2.0 1.5 6 23.4 3.0 2.4 1.8
48 49	9.48 529 9.48 568	39	9.50 659	43	0.49 341	9.97 870 9.97 866	4	12	6 23.4 3.0 2.4 I.8 7 27.3 3.5 2.8 2.I
50	9.48 607	39	9.50 703	43	0.49 297	9.97 861	5	10	8 31.2 4.0 3.2 2.4
		40		43	0.49 254		4		9 35.1 4.5 3.6 2.7
51 52	9.48 647 9.48 686	39	9.50 789	44	0.49 211	9.97 857	4	8	
53	9.48 725	39	9.50 876	43	0.49 107	9.97 849	4	7	i e
54	9.48 764	39	9.50 919	43	0.49 081	9.97 845	4	6	1
55	9.48 803	39	9.50 962	43	0.49 038	9.97 841	4	5	
56	9.48 842	39	9.51 005	43	0.48 995	9.97 837	4	4	l
57 58	9.48 881	39	9.51 048	44	0.48 952	9.97 833	4	3	
59	9.48 920	39	9.51 092	43	0.48 908	9.97 829 9.97 825	4	2 I	1
60	9.48 998	39	9.51 178	43	0.48 822	9.97 821	4	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	,	PP

107° (355) **72°**

1	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
6	9.48 998	<u>u</u>	9.51 178		0.48 822	9.97 821	<u> </u>	60	
ı	9.49 937	39	9.51 221	43	0.48 779	9.97 821	4	59	
2	9.49 076	39	9.51 264	43	0.48 736	9.97 812	5	58	
3	9.49 115	39 38	9.51 306	42	0.48 694	9.97 808	4	57	
4 5	9.49 153	39	9.51 349 9.51 392	43	0.48 651	9.97 804	4	56	
6	9.49 192	39	9.51 435	43	0.48 565	9.97 796	4	55	
7	9.49 269	38	9.51 478	43	0.48 522	9.97 792	4	53	
8	9.49 308	39 39	9.51 520	42	0.48 480	9.97 788	4	52	43 42 41
10	9.49 347	38	9.51 563	43	0.48 394	9.97 784	5	51 50	1 4.3 4.2 4.1
11	9.49 424	39	9.51 648	42	0.48 352	9.97 779	4	49	2 8.6 8.4 8.2 3 12.9 12.6 12.3
I 2	9.49 462	38	9.51 691	43	0.48 309	9.97 771	4	48	4 17.2 16.8 16.4
13	9.49 500	38 39	9.51 734	43	0.48 266	9.97 767	4	47	5 21.5 21.0 20.5
14 15	9.49 539 9.49 577	38	9.51 776	43	0.48 224	9.97 763	4	46	6 25.8 25.2 24.6 7 30.1 29.4 28.7
16	9.49 615	38	9.51 861	42	0.48 139	9.97 754	5	45	8 34.4 33.6 32.8
17	9.49654	39	9.51 903	42	0.48 097	9.97 750	4	43	9 38.7 37.8 36.9
18	9.49 692	38 38	9.51 946 9.51 988	43	0.48 054	9.97 746	4	42	
20	9.49 730	38	9.51 988	43	0.48 012	9.97 742	4	41 40	
21	9.49 708	38	9.52 073	42	0.47 927	9.97 734	4	39	
22	9.49 844	38	9.52 115	42	0.47 885	9.97 729	5	38	
23	9.49 882	38 38	9.52 157	42	0.47 843	9.97 725	4	37	
24 25	9.49 920	38	9.52 200	42	0.47 800	9.97721	4	36	
26	9.49 936	38	9.52 284	42	0.47 716	9.97 717	4	35	39 38 37
27	9.50 034	38	9.52 326	42	0.47 674	9.97 708	5	33	1 3.9 3.8 3.7
28 29	9.50 072	38 38	9.52 368	42 42	0.47 632	9.97 704	4	32	2 7.8 7.6 7.4
30	9.50 110	38	9.52 410	42	0.47 590	9.97 700	4	31 30	3 II.7 II.4 II.I 4 I5.6 I5.2 I4.8
31	9.50 185	37	9.52 494	42	0.47 548	9.97 691	5	29	4 15.6 15.2 14.8 5 19.5 19.0 18.5
32	9.50 223	38	9.52 536	42	0.47 464	9.97 687	4	28	6 23.4 22.8 22.2
33	9.50 261	38	9.52 578	42	0.47 422	9.97 683	4	27	7 27.3 26.6 25.9 8 31.2 30.4 29.6
34	9.50 298	37 38	9.52 620	42 41	0.47 380	9.97 679	4 5	26	9 35.1 34.2 33.3
35 36	9.50 336 9.50 374	38	9.52 703	42	0.47 339 0.47 297	9.97 674	4	25 24	
37	9.50 411	37	9.52 745	42	0.47 255	9.97 666	4	23	
38	9.50 449	38 37	9.52 787	42 42	0.47 213	9.97 662	4 5	22	
39 40	9.50 486	37	9.52 829	42 4I	0.47 171	9.97 657	4	21	
	9.50 523	38	9.52 870	42	0.47 130	9.97 653	4	20	
4I 42	9.50 561 9.50 598	37	9.52 912	41	0.47 088	9.97 649 9.97 645	4	18	
43	9.50 635	37	9.52 995	42	0.47 005	9.97 640	5	17	
44	9.50 673	38 37	9.53 037	42 41	0.46 963	9.97 636	4	16	36 5 4
45	9.50 710	37	9.53 078 9.53 120	42	0.46 922	9.97 632	4	15 14	I 3.6 0.5 0.4 2 7.2 I.O 0.8
47	9.50 784	37	9.53 161	41	0.46 839	9.97 623	5	13	2 7.2 I.O 0.8 3 IO.8 I.5 I.2
48	9.50 821	37 37	9.53 202	4I 42	0.46 798	9.97 619	4	I 2	4 14.4 2.0 1.6
49 50	9.50 858	38	9.53 244	41 41	0.46 756	9.97 615	5	11	5 18.0 2.5 2.0 6 21.6 3.0 2.4
1	9.50 896	37	9.53 285	42	0.46 715	9.97 610	4	10	7 25.2 3.5 2.8
51 52	9.50 933	37	9.53 327 9.53 368	41	0.46 673	9.97 606	4	8	8 28.8 4.0 3.2
53	9.51 007	37	9.53 409	41	0.46 591	9.97 597	5	7	9 32.4 4.5 3.6
54	9.51 043	36 37	9.53 450	4I 42	0.46 550	9.97 593	4	6	
55	9.51 080	37	9.53 492 9.53 533	41 41	0.46 508	9.97 589 9.97 584	5	5 4	
57	9.51 154	37	9.53 574	41	0.46 426	9.97 580	4	3	
58	9.51 191	37 36	9.53 615	41	0.46 385	9.97 576	4 5	2	
59 60	9.51 227	37	9.53 656	4I 4I	0.46 344	9.97 571	4	I	
00	9.51 264 L Cos		9.53 697 L Cot	cd	0.46 303 L Tan	9.97 567 L Sin		0	PP
	L 008	u	L 000	c u	⊾ ran	L 3111	u		FF

19° 160°

1	L Sin	d	L Tan	c d	L Cot	L Cos	d	Π	PP
0	9.51 264		9.53 697	4.7	0.46 303	9.97 567	<u> </u>	60	
1	9.51 301	37	9.53 738	41	0.46 262	9.97 563	5	59	
2	9.51 338	37 36	9.53 779 9.53 820	4I 4I	0.46 221	9.97 558	4	58	
3	9.51 3/4	37	9.53 861	41	0.46 139	9.97 550	4	56	
5	9.51 447	36	9.53 902	41	0.46 098	9.97 545	5	55	
6	9.51 484	37 36	9.53 943	4I 4I	0.46 057	9.97 541	5	54	
7 8	9.51 520	37	9.53 984 9.54 025	41	0.46 016	9.97 536 9.97 532	4	53	41 40 39
9	9.51 593	36	9.54 065	40	0.45 935	9.97 528	4	51	
10	9.51 629	36	9.54 106	41	0.45 894	9.97 523	5	50	1 4.I 4.0 3.9 2 8.2 8.0 7.8
11	9.51 666	37 36	9.54 147	4I 40	0.45 853	9.97 519	4	49	3 12.3 12.0 11.7
12	9.51 702	36	9.54 187	41	0.45 813	9.97 515	4 5	48	4 10.4 10.0 15.0
13 14	9.51 738	36	9.54 228	41	0.45 772	9.97 506	4	47 46	
15	9.51811	37	9.54 309	40	0.45 691	9.97 501	5	45	7 28.7 28.0 27.3
16	9.51 847	36 36	9.54 350	41 40	0.45 650	9.97 497	5	44	8 32.8 32.0 31.2 9 36.9 36.0 35.1
17 18	9.51 883	36	9.54 390	41	0.45 610	9.97 492 9.97 488	4	43	9 30.9 30.0 33.1
19	9.51 955	36	9.54 431 9.54 471	40	0.45 529	9.97 484	4	42 41	
30	9.51 991	36	9.54 512	41	0.45 488	9.97 479	5	40	1
21	9.52 027	36	9.54 552	40	0.45 448	9.97 475	4	39	1
22	9.52 063	36 36	9-54 593	4I 40	0.45 407	9.97 470	5 4	38	1
23	9.52 099	36	9.54 633	40	0.45 367	9.97 466 9.97 461	5	37	
24 25	9.52 135 9.52 171	36	9.54 673	41	0.45 327 0.45 286	9.97 457	4	36	
26	9.52 207	36	9.54 754	40 40	0.45 246	9.97 453	4	34	37 36 35
27 28	9.52 242	35 36	9.54 794	41	0.45 206	9.97 448	5 4	33	I 3.7 3.6 3.5 2 7.4 7.2 7.0
28 29	9.52 278	36	9.54 835 9.54 875	40	0.45 165	9.97 444 9.97 439	5	32 31	2 7.4 7.2 7.0 3 11.1 10.8 10.5
30	9.52 350	36	9.54 915	40	0.45 085	9.97 435	4	30	4 14.8 14.4 14.0
31	9.52 385	35	9.54 955	40	0.45 045	9.97 430	5	29	5 18.5 18.0 17.5 6 22.2 21.6 21.0
32	9.52 421	36	9-54 995	40	0.45 005	9.97 426	4	28	
33	9.52 456	35 36	9.55 035	40 40	0.44 965	9.97 421	5 4	27	8 29.6 28.8 28.0
34 35	9.52 492 9.52 527	35	9.55 075 9.55 115	40	0.44 925 0.44 885	9.97 417 9.97 412	5	26 25	9 33.3 32.4 31.5
36	9.52 563	36	9.55 155	40	0.44 845	9.97 408	4	24	
37	9.52 598	35 36	9.55 195	40 40	0.44 805	9.97 403	5	23	
38 39	9.52 634 9.52 669	35	9.55 235 9.55 275	40	0.44 705	9.97 399 9.97 394	5	22 21	ĺ
40	9.52 705	36	9.55 315	40	0.44 685	9.97 394	4	20	ļ
41	9.52 740	35	9.55 355	40	0.44 645	9.97 385	5	19	
42		35	9.55 395	40	0.44 605	9.97 381	4	18	
43	9.52 775 9.52 811	36 35	9.55 434	39 40	0.44 566	9.97 376	5	17	34 5 4
44 45	9.52 846 9.52 881	35	9.55 474	40	0.44 526	9.97 372 9.97 367	5	16	1 3.4 0.5 0.4
46	9.52 916	35	9.55 554	40	0.44 446	9.97 363	4	14	2 6.8 1.0 0.8
47	9.52 951	35	9.55 593	39	0.44 407	9.97 358	5	13	3 10.2 1.5 1.2 4 13.6 2.0 1.6
48 49	9.52 986	35 35	9.55 633	40 40	0.44 367	9.97 353	5	12	5 17.0 2.5 2.0
50	9.53 021	35	9.55 673	39	0.44 327	9.97 349	5	11 10	6 20.4 3.0 2.4 7 23.8 3.5 2.8
51	9.53 050	36	9.55 712	40	0.44 248	9.97 344	4	9	7 23.8 3.5 2.8 8 27.2 4.0 3.2
52	9.53 126	34	9.55 752	39	0.44 240	9.97 340	5	8	9 30.6 4.5 3.6
53	9.53 161	35	9.55831	40	0.44 169	9.97 331	4	7	1
54	9.53 196	35 35	9.55 870	39 40	0.44 130	9.97 326	5 4	6	1
55 56	9.53 231 9.53 266	35	9.55 910	39	0.44 090 0.44 05 I	9.97 322	5	5	
57	9.53 301	35	9.55 989	40	0.44 011	9.97 312	5	3	
58	9.53 336	35	9.56 028	39 39	0.43 972	9.97 308	4	2	
59	9.53 370	34 35	9.56 067	40	0.43 933	9.97 303	5 4	I	
60	9.53 405	_	9.56 107	_	0.43 893	9.97 299		,	
	L Cos	đ	L Cot	c d	L Tan	L Sin	d		PP

109° (357) **70°**

r	L Sin	d	L Tan	c d	L Cot	L Cos	d				PΡ	
0	9.53 405	35	9.56 107	20	0.43 893	9.97 299		60				
1	9.53 440	35	9.56 146	39 39	0.43 854	9.97 294	5	59				
3	9.53 475 9.53 509	34	9.56 185	39	0.43 815	9.97 289 9.97 285	5 4	58 57				
4	9.53 544	35	9.56 264	40	0.43 736	9.97 280	5	56				
5	9.53 578	34	9.56 303	39 39	0.43 697	9.97 276	4	55				
	9.53 613	35 34	9.56 342	39	0.43 658	9.97 271	5 5	54				
7 8	9.53 647 9.53 682	35	9.56 381	39	0.43 619	9.97 266 9.97 262	4	53 52		40	00	00
9	9.53 716	34	9.56 459	39	0.43 541	9.97 257	5	51	_	40	39	38
10	9.53 751	35	9.56 498	39	0.43 502	9.97 252	5	50	1 2	4.0 8.0	3.9 7.8	3.8 7.6
11	9.53 785	34	9.56 537	39 39	0.43 463	9.97 248	4	49	3	12.0	11.7	11.4
12	9.53 819	35	9.56 576 9.56 615	39	0.43 424	9.97 243 9.97 238	5	48	4	16.0	15.6	15.2
13 14	9.53 888	34	9.56 654	39	0.43 385	9.97 234	4	47 46	5 6	24.0	19.5 23.4	19.0
15	9.53 922	34	9.56 693	39	0.43 307	9.97 234	5	45	7 8	28.0	27.3	26.6
16	9.53 957	35 34	9.56 732	39	0.43 268	9.97 224	5	44	8	32.0	31.2	30.4
17	9.53 991 9.54 025	34	9.56 771	39	0.43 229	9.97 220	5	43	9	36.0	35.1	34.2
19	9.54 025	34	9.56 849	39	0.43 190	9.97 215	5	42 41				
20	9.54 093	34	9.56 887	38	0.43 113	9.97 206	4	40				
2 I	9.54 127	34	9.56 926	39	0.43 074	9.97 201	5	39				
22	9.54 161	34 34	9.56 965	39 39	0.43 035	9.97 196	5	38				
23	9.54 195	34	9.57 004	38	0.42 996	9.97 192	4 5	37				
24 25	9.54 229	34	9.57 0.12 9.57 081	39	0.42 958	9.97 187	5	36				
26	9.54 297	34 34	9.57 120	39	0.42 880	9.97 178	4	34		37	35	34
27	9.54 331	34	9.57 158	38 39	0.42842	9.97 173	5	33	1	3.7	3.5	3.4 6.8
28 29	9.54 365 9.54 399	34	9.57 197 9.57 235	38	0.42 803	9.97 168	5	32 31	3	7-4 II.I	7.0 10.5	10.2
30	9.54 433	34	9.57 274	39	0.42 705	9.97 159	4	30	4	1.4.8	14.0	13.6
31	9.54 466	33	9.57 312	38	0.42 688	9.97 154	5	20	5	18.5	17.5	17.0
32	9.54 500	34	9.57 351	39	0.42 649	9.97 149	5	28	6 7	22.2	21.0 24.5	20.4
33	9.54 534	34 33	9.57 389	38 39	0.42 611	9.97 145	5	27	8	29.6	28.0	27.2
34 35	9.54 567 9.54 601	34	9.57 428	38	0.42 572	9.97 140	5	26	9	33.3	31.5	30.6
36	9.54 635	34	9.57 466	38	0.42 534	9.97 I35 9.97 I30	5	25 24				
37	9.54 668	33 34	9.57 543	39	0.42 457	9.97 126	4	23				
38	9.54 702	33	9.57 581	38 38	0.42 419	9.97 121	5	22				
39 40	9.54 735	34	9.57 619	39	0.42 381	9.97 116	5	21 20				
41	9.54 769	33	9.57 658	38	0.42 342	9.97 111	4					
41	9.54 836	34	9.57 090	38	0.42 304 0.42 266	9.97 107 9.97 102	5	19				
43	9.54 869	33 34	9.57 772	38	0.42 228	9.97 097	5	17		33	5	4
44	9.54 903	33	9.57 810	38 39	0.42 190	9.97 092	5 5	16	1	3.3	0.5	0.4
45 46	9.54 936	33	9.57 849 9.57 887	38	0.42 151	9.97 0 87 9.97 0 83	4	15	2	6.6	1.0	0.8
47	9.55 003	34 33	9.57 925	38	0.42 075	9.97 078	5	13	3 4	9.9	1.5 2.0	1.2 1.6
48	9.55 036	33	9.57 963	38 38	0.42 037	9.97 073	5	12	5 6	16.5	2.5	2.0
49 50	9.55 069	33	9.58 001	38	0.41 999	9.97 068	5 5	II		19.8	3.0	2.4
1	9.55 102	34	9.58 039	38	0.41 961	9.97 063	4	10	7 8	23.I 26.4	3·5 4.0	2.8 3.2
51 52	9.55 136	33	9.58 077	38	0.41 923	9.97 059	5	8	9	29.7	4.5	3.6
53	9.55 202	33 33	9.58 153	38	0.41 847	9.97 049	5	7				
54	9.55 235	33	9.58 191	38 38	0.41 809	9.97 044	5	6				
55 56	9.55 268 9.55 301	33	9.58 229 9.58 267	38	0.41 771	9.97 0 39 9.97 0 35	4	5 4				
57	9.55 334	33	9.58 304	37	0.41 696	9.97 030	5	3				
58	9.55 367	33	9.58 342	38 38	0.41 658	9.97 025	5	2				
59 60	9.55 400	33	9.58 380	38	0.41 620	9.97 020	5	I				
1	9.55 433 L Cos	_	9.58 418		0.41 582	9.97 OI5		•) p	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	'				

21° 158°

		-			1.0	1.0	-		
Ľ	L Sin	d	L Tan	c d	L Cot	L Cos	_d	_	PP
0	9.55 433	33	9.58 418	37	0.41 582	9.97 015	5	60	
I	9.55 466	33	9.58 455	38	0.41 545	9.97 010	5	59 58	
3	9.55 499 9.55 532	33	9.58 493 9.58 531	38	0.41 507	9.97 005 9.97 001	4	57	
4	9.55 564	32	9.58 569	38	0.41 431	9.96 996	5	56	
5	9.55 597	33	9.58 606	37 38	0.41 394	9.96 991	5	55	
6	9.55 630	33 33	9.58 644	37	0.41 356	9.96 986	5	54	1
7 8	9.55 663 9.55 695	32	9.58 681 9.58 719	38	0.41 319	9.96 981 9.96 976	5	53	66
ğ	9.55 728	33	9.58 757	38	0.41 243	9.96 971	5	51	38 37 36
10	9.55 761	33	9.58 794	37	0.41 206	9.96 966	5	50	1 3.8 3.7 3.6
11	9.55 793	32	9.58832	38	0.41 168	9.96 962	4	49	2 7.6 7.4 7.2 3 11.4 11.1 10.8
12	9.55 826	33 32	9.58 869	37 38	0.41 131	9.96 957	5	48	4 15.2 14.8 14.4
13	9.55 858 9.55 891	33	9.58 907 9.58 944	37	0.41 093	9.96 952	5	47	5 19.0 18.5 18.0
15	9.55 923	32	9.58 981	37	0.41 030	9.96 947	5	45	6 22.8 22.2 21.6 7 26.6 25.9 25.2
16	9.55 956	33	9.59 019	38	0.40 981	9.96 937	5	44	7 26.6 25.9 25.2 8 30.4 29.6 28.8
17	9.55 988	32 33	9.59 056	37 38	0.40 944	9.96 932	5	43	9 34.2 33.3 32.4
18	9.56 021	32	9.59 0 94 9.59 1 31	37	o.40 906 o.40 869	9.96 927 9.96 922	5	42 41	
20	9.56 085	32	9.59 168	37	0.40 832	9.96 917	5	40	
21	9.56 118	33	9.59 205	37	0.40 795	9.96 917	5	39	
22	9.56 150	32	9.59 243	38	0.40 757	9.96 907	5	38	1
23	9.56 182	32 33	9.59 280	37 37	0.40 720	9.96 903	4 5	37	1
24	9.56 215	32	9.59 317	37	0.40 683	9.96 898 9.96 893	5	36	
25 26	9.56 247 9.56 279	32	9.59 354 9.59 391	37	0.40 609	9.96 888	5	35	33 32 31
27	9.56 311	32	9.59 429	38	0.40 571	9.96 883	5	33	
28	9.56 343	32	9.59 466	37 37	0.40 534	9.96 878	5 5	32	1 3.3 3.2 3.1 2 6.6 6.4 6.2
29	9.56 375	33	9.59 503	37	0.40 497	9.96 873	5	31	3 9.9 9.6 9.3
30	9.56 408	32	9.59 540	37	0.40 460	9.96 868	5	30	4 13.2 12.8 12.4 5 16.5 16.0 15.5
31 32	9.56 440 9.56 472	32	9.59 577 9.59 614	37	0.40 423	9.96 863 9.96 858	5	29 28	5 16.5 16.0 15.5 6 19.8 19.2 18.6
33	9.56 504	32	9.59 651	37	0.40 349	9.96 853	5	27	7 23.1 22.4 21.7
34	9.56 536	32	9.59 688	37	0.40 31 2	9.96 848	5	26	8 26.4 25.6 24.8 9 29.7 28.8 27.9
35	9.56 568	32 31	9.59 725	37 37	0.40 275	9.96 843	5 5	25	9 29.7 20.0 27.9
36 37	9.56 599 9.56 631	32	9.59 762 9.59 799	37	0.40 238	9.96 838 9.96 833	5	24 23	
38	9.56 663	32	9.59 835	36	0.40 165	9.96 828	5	22	l
39	9.56 695	32 32	9.59872	37	0.40 128	9.96 823	5 5	2 I	
40	9.56 727	32	9.59 909	37	0.40 091	9.96818	5	20	
41	9.56 759	31	9.59 946	37	0.40 054	9.96813	5	19	1
42 43	9.56 790 9.56 822	32	9.59 983 9.60 01 9	36	0.40 017	9.96 8o8 9.96 8o3	5	18	
44	9.56 854	32	9.60 056	37	0.39 944	9.96 798	5	16	6 5 4
45	9.56 886	32	9.60 093	37	0.39 907	9.96 793	5	15	1 0.6 0.5 0.4
46	9.56 917	31 32	9.60 130	37 36	0.39870	9.96 788	5	14	2 I.2 I.0 0.8 3 I.8 I.5 I.2
47 48	9.56 949 9.56 980	3 I	9.60 166	37	0.39 834	9.96 783	5	13	3 1.8 1.5 1.2 4 2.4 2.0 1.6
49	9.57 012	32	9.60 240	37	0.39 760	9.96 772	6	11	5 3.0 2.5 2.0
50	9.57 044	32	9.60 276	36	0.39 724	9.96 767	5	10	6 3.6 3.0 2.4 7 4.2 3.5 2.8
51	9.57 075	31	9.60 313	37	0.39 687	9.96 762	5	9	8 4.8 4.0 3.2
52	9.57 107	32 31	9.60 349	36 37	0.39651	9.96 757	5	8	9 5.4 4.5 3.6
53	9.57 138	31	9.60 386	36	0.39 614	9.96 752 9.96 747	5	7 6	1
54 55	9.57 201	32	9.60 422	37	0.39 578	9.96 747	5	5	1
56	9.57 232	31 32	9.60 495	36	0.39 505	9.96 737	5	4	
57	9.57 264	31 31	9.60 532	37 36	0.39 468	9.96 732	5	3	1
58 59	9.57 295 9.57 326	31	9.60 568	37	0.39 432	9.96 727 9.96 722	5	2 I	
60	9.57 358	32	9.60 641	36	0.39 359	9.96 717	5	0	1
	L Cos		L Cot	c d	L Tan	L Sin	d	Ť	PP
	L 005	u	- 001	o u	L I all	L 3111	u		F_

111° (359) **68°**

'	L Sin	d	L Tan	cd	L Cot	L Cos	d		PP
0	9.57 358		9.60 641		0.39 359	9.96 717		60	
1	9.57 389	31	9.60 677	36	0.39 323	9.96711	6	59	
2	9.57 420	3I 3I	9.60 714	37 36	0.39 286	9.96 706	5 5	58	
3	9.57 451	31	9.60 750	36	0.39 250	9.96 701	5	57	
5	9.57 482	32	9.60 823	37	0.39 177	9.96 691	5	56 55	
6	9.57 545	31	9.60 859	36	0.39 141	9.96 686	5	54	
7	9.57 576	3I 3I	9.60 895	36 36	0.39 105	9.96 681	5	53	
8	9.57 607 9.57 638	31	9.60 931	36	0.39 069	9.96 676	5 6	52	37 36 35
10	9.57 669	31	9.61 004	37	0.38 996	9.96 665	5	51 50	I 3.7 3.6 3.5 2 7.4 7.2 7.0
11	9.57 700	31	9.61 040	36	0.38 960	9.96 660	5	1 1	2 7.4 7.2 7.0 3 II.I IO.8 IO.5
12	9.57 73I	31	9.61 076	36	0.38 900	9.96 655	5	49 48	4 14.8 14.4 14.0
13	9.57 762	31	9.61 112	36	0.38 888	9.96 650	5	47	5 18.5 18.0 17.5 6 22.2 21.6 21.0
14	9.57 793	31 31	9.61 148	36 36	0.38852	9.96 645	5	46	
15 16	9.57 824 9.57 855	31	9.61 184	36	0.38 816	9.96 640	5	45	7 25.9 25.2 24.5 8 29.6 28.8 28.0
17	9.57 885	30	9.61 256	36	0.38 744	9.96 629	5	44 43	9 33.3 32.4 31.5
18	9.57 916	31	9.61 292	36	0.38 708	9.96 624	5	12	
19	9.57 947	31 31	9.61 328	36 36	0.38 672	9.96 619	5	41	
20	9.57 978	30	9.61 364	36	0.38 636	9.96 614	6	40	
21	9.58 008	31	9.61 400	36	0.38 600	9.96 608	5	39	
22	9.58 o39 9.58 o70	3 I	9.61 436 9.61 472	36	0.38 564	9.96 6 0 3 9.96 598	5	38	
24	9.58 101	31	9.61 508	36	0.38 492	9.96 593	5	37	
25	9.58 131	30	9.61 544	36	0.38 456	9.96 588	5 6	35	32 31 30
26	9.58 162	31 30	9.61 579	35 36	0.38 421	9.96 582	5	34	
27 28	9.58 192 9.58 223	31	9.61 615	36	0.38 385	9.96 577 9.96 572	5	33	I 3.2 3.I 3.0 2 6.4 6.2 6.0
29	9.58 253	30	9.61 687	36	0.38 313	9.96 567	5	32 31	3 9.6 9.3 9.0
30	9.58 284	31	9.61 722	35	0.38 278	9.96 562	5	30	4 12.8 12.4 12.0
31	9.58 314	30	9.61 758	36	0.38 242	9.96 556	6	20	5 16.0 15.5 15.0 6 19.2 18.6 18.0
32	9.58 345	3I 30	9.61 794	36 36	0.38 206	9.96 551	5 5	28	7 22.4 21.7 21.0
33	9.58 375	31	9.61 830	35	0.38 170	9.96 546	5	27	
34	9.58 406	30	9.61 865	36	0.38 099	9.96 541	6	26 25	9 28.8 27.9 27.0
36	9.58 467	31	9.61 936	35	0.38 064	9.96 530	5	24	
37	9.58 497	30	9.61 972	36 36	0.38 028	9.96 525	5	23	
38	9.58 527	30	9.62 008	35	0.37 992	9.96 520	5 6	22	
40	9.58 588	31	9.62 079	36	0.37 921	9.96 509	5	21	
4I	9.58 618	30	9.62 114	35	0.37 886	9.96 504	5	1	
42	9.58 648	30	9.62 150	36	0.37 850	9.96 498	6	18	
43	9.58 678	30 31	9.62 185	35 36	0.37815	9.96 493	5 5	17	29 6 5
44	9.58 709	30	9.62 221	35	0.37 779	9.96 488		16	1 2.9 0.6 0.5
45 46	9.58 739 9.58 769	30	9.62 256	36	0.37 744	9.96 483	5	15	2 5.8 1.2 1.0
47	9.58 799	30	9.62 327	35	0.37 673	9.96 472	5	14	
48	9.58 829	30	9.62 362	35 36	0.37 638	9.96 467	5 6	12	
49	9.58 859	30	9.62 398	35	0.37 602	9.96 461	5	11	6 17.4 3.6 3.0
50	9.58 889	30	9.62 433	35	0.37 567	9.96 456	5	10	7 20.3 4.2 3.5 8 23.2 4.8 4.0
51	9.58 919	30	9.62 468	36	0.37 532	9.96 451	6	9	9 26.1 5.4 4.5
52 53	9.58 979	30	9.62 539	35	0.37 461	9.96 445	5	8 7	
54	9.59 009	30	9.62 574	35	0.37 426	9.96 435	5	6	
55	9.59 039	30	9.62 609	35 36	0.37 391	9.96 429	6	5	
56	9.59 069	29	9.62 645	35	0.37 355	9.96 424	5	4	
57 58	9.59 098	30	9.62 715	35	0.37 320	9.96 413	6	3 2	
59	9.59 158	30	9.62 750	35	0.37 250	9.96 408	5	1	
60	9.59 188	30	9.62 785	35	0.37 215	9.96 403	5	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	′_	PP

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	23							56	
′	L Sin	d	L Tan	c d	L Cot	L Cos	d	П	PP
0	9.59 188	30	9.62 785	25	0.37 215	9.96 403	6	60	
1	9.59 218	29	9.62 820	35	0.37 180	9.96 397	5	59	ļ
3	9.59 247 9.59 277	30	9.62 855	35	0.37 145	9.96 392		58	
4	9.59 307	30	9.62 926	36	0.37 074	9.96 381	5 6	56	,
5	9.59 336	29	9.62 961	35	0.37 039	9.96 376	5 6	55	
6	9.59 366	30	9.62 996	35 35	0.37 004	9.96 370	5	54	
7 8	9.59 396 9.59 425	29	9.63 031	35	0.36 969	9.96 365	5	53 52	36 35 34
9	9.59 455	30	9.63 101	35	0.36 899	9.96 354		51	I 3.6 3.5 3.4 2 7.2 7.0 6.8
10	9.59 484	29	9.63 135	34	0.36 865	9.96 349	5 6	50	
11	9.59 514	30 20	9.63 170	35	0.36 830	9.96 343		49	3 10.8 10.5 10.2 4 14.4 14.0 13.6
12	9.59 543	30	9.63 205	35 35	0.36 795	9.96 338	5	48	5 18.0 17.5 17.0
13	9.59 573	29	9.63 240	35	0.36 760	9.96 333	ő	47 46	6 21.6 21.0 20.4 7 25.2 24.5 23.8
15	9.59 632	30	9.63 310	35	0.36 690	9.96 322	5 6	45	7 25.2 24.5 23.8 8 28.8 28.0 27.2
16	9.59 661	29 29	9.63 345	35 34	0.36 655	9.96 316	5	44	9 32.4 31.5 30.6
17 18	9.59 690	30	9.63 379	35	0.36 621	9.96 311	6	43	
19	9.59 720 9.59 749	29	9.63 414	35	0.36 586	9.96 305	5	42 41	
20	9.59 778	29	9.63 484	35	0.36 516	9.96 294	6	40	
21	9.59 808	30	9.63 519	35	0.36 481	9.96 289	5	39	
22	9.59837	29 29	9.63 553	34 35	0.36 447	9.96 284	5 6	38	
23	9.59 866	29	9.63 588	35	0.36 412	9.96 278	5	37	
24 25	9.59 895	29	9.63 623	34	0.36 377	9.96 273	6	36 35	30 29 28
26	9.59 954	30	9.63 692	35	0.36 308	9.96 262	5 6	34	I 3.0 2.9 2.8
27	9.59 983	29 29	9.63 726	34	0.36 274	9.96 256	1	33	2 6.0 5.8 5.6
28 29	9.60 012	29	9.63 761	35 35	0.36 239	9.96 251	5	32	3 9.0 8.7 8.4
30	9.60 070	29	9.63 796	34	0.36 170	9.96 245	5	31 30	4 12.0 11.6 11.2 5 15.0 14.5 14.0
31	9.60 099	29	9.63 865	35	0.36 135	9.96 234	6	29	5 15.0 14.5 14.0 6 18.0 17.4 16.8
32	9.60 128	29	9.63 899	34	0.36 101	9.96 234	5	28	7 21.0 20.3 19.6 8 24.0 23.2 22.4
33	9.60 157	29 29	9.63 934	35	0.36 066	9.96 223	6 5	27	8 24.0 23.2 22.4 9 27.0 26.1 25.2
34	9.60 186	29	9.63 968	35	0.36 032	9.96 218	6	26	9 -1.10 2012 2312
35 36	9.60 213	29	9.64 037	34	0.35 997 0.35 963	9.96 212	5	25	
37	9.60 273	29	9.64 072	35	0.35 928	9.96 201	6	23	
38	9.60 302	29 29	9.64 106	34	0.35 894	9.96 196	5	22	
39 40	9.60 331	28	9.64 140	35	0.35 860	9.96 190	5	21	
	9.60 359	29	9.64 175	34	0.35 825	9.96 185	6	20	
4I 42	9.60 388	29	9.64 209	34	0.35 791	9.96 179 9.96 174	5 6	19	
43	9.60 446	29 28	9.64 278	35	0.35722	9.96 168	6	17	6 5
44	9.60 474	20	9.64 312	34	0.35 688	9.96 162		16	1 0.6 0.5 2 1.2 1.0
45 46	9.60 503 9.60 532	29	9.64 346 9.64 381	35	0.35 654	9.96 157 9.96 151	5	15	3 1.8 1.5
47	9.60 561	29	9.64 415	34	0.35 585	9.96 146	5	13	4 2.4 2.0
48	9.60 589	28 29	9.64 449	34	0.35 551	9.96 140	6	I 2	5 3.0 2.5 6 3.6 3.0
49	9.60 618	28	9.64 483	34	0.35 517	9.96 135	5	II	7 4.2 3.5
50	9.60 646	29	9.64 517	35	0.35 483	9.96 129	6	10	
51 52	9.60 675	29	9.64 552 9.64 586	34	0.35 448	9.96 123 9.96 118	5	8	9 5.4 4.5
53	9.60 732	28	9.64 620	34	0.35 380	9.96 112		7	
54	9.60 761	29 28	9.64 654	34	0.35 346	9.96 107	5	6	
55 56	9.60 789	29	9.64 688	34	0.35 312	9.96 101 9.96 095	6	5	
57	9.60 846	28	9.64 756	34	0.35 278	9.96 090	5	4 3	
58	9.60 875	29 28	9.64 790	34	0.35 210	9.96 084	6	2	
59	9.60 903	28 28	9.64 824	34	0.35 176	9.96 079	5 6	1	
60	9.60 931		9.64 858	-	0.35 142	9.96 073		<u>0</u>	
Ш	L Cos	d	L Cot	cd	L Tan	L Sin	d		PP

113° (361) 66°

7	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.60 931	29	9.64 858	2.4	0.35 142	9.96 073	6	60	
1	9.60 960	28	9.64 892	34	0.35 108	9.96 067		59	
2	9.60 988	28	9.64 926	34 34	0.35 074	9.96 062	5 6	58	
3	9.61 016	29	9.64 960	34	0.35 040	9.96 056	6	56	
	9.61 073	28	9.65 028	34	0.34 972	9.96 045	5	55	
5 6	9.61 101	28 28	9.65 062	34 34	0.34 938	9.96 039	6 5	54	
7 8	9.61 129	20	9.65 096	34	0.34 904	9.96 034	6	53	34 33
9	9.61 158 9.61 186	28	9.65 164	34	0.34 870	9.96 0 28 9.96 0 22	6	52 51	I 3.4 3.3
10	9.61 214	28	9.65 197	33	0.34 803	9.96 017	5	50	2 6.8 6.6
II	9.61 242	28	9.65 231	34	0.34 769	9.96 011	6	49	3 10.2 9.9
12	9.61 270	28 28	9.65 265	34	0.34 735	9.96 005	6	48	4 13.6 13.2 5 17.0 16.5
13	9.61 298	28	9.65 299	34 34	0.34 701	9.96 000	5	47	5 17.0 16.5 6 20.4 19.8
14	9.61 326	28	9.65 333	33	0.34 667	9.95 994	6	46	7 23.8 23.1
15 16	9.61 354 9.61 382	28	9.65 400	34	0.34 600	9.95 982	6	45	8 27.2 26.4 9 30.6 29.7
17	9.61 411	29	9.65 434	34	0.34 566	9.95 977	5	43	9 30.0 29.7
18	9.61 438	27 28	9.65 467	33	0.34 533	9.95 971	6	42	
19	9.61 466	28	9.65 501	34	0.34 499	9.95 965	5	41	
20	9.61 494	28	9.65 535	33	0.34 465	9.95 960	6	40	
2I 22	9.61 522	28	9.65 568	34	0.34 432	9.95 954 9.95 948	6	39 38	
23	9.61 578	28	9.65 636	34	0.34 398	9.95 942	6	37	
24	9.61 606	28	9.65 669	33	0.34 331	9.95 937	5	36	
25	9.61 634	28 28	9.65 703	34	0.34 297	9.95 931	6	35	29 28 27
26	9.61 662	27	9.65 736	33 34	0.34 264	9.95 925	. 5	34	1 2.9 2.8 2.7
27 28	9.61 689 9.61 717	28	9.65 770	33	0.34 230	9.95 920 9.95 914	6	33	2 5.8 5.6 5.4
29	9.61 745	28	9.65 837	34	0.34 163	9.95 908	6	31	3 8.7 8.4 8.1
30	9.61 773	28	9.65 870	33	0.34 130	9.95 902	6	30	4 11.6 11.2 10.8 5 14.5 14.0 13.5
31	9.61 800	27	9.65 904	34	0.34 096	9.95 897	5	29	5 14.5 14.0 13.5 6 17.4 16.8 16.2
32	9.61 828	28 28	9.65 937	33 34	0.34 063	9.95 891	6	28	7 20.3 19.6 18.9 8 23.2 22.4 21.6
33	9.61 856 9.61 883	27	9.65 971	33	0.34 029	9.95 885	6	27	
34 35	9.61 911	28	9.66 00 4	34	0.33 996	9.95 873	6	26	9 20.1 25.2 24.3
36	9.61 939	28	9.66 071	33	0.33 929	9.95 868	5	24	
37	9.61 966	27 28	9.66 104	33	0.33 896	9.95 862	6	23	
38	9.61 994	27	9.66 138 9.66 171	34 33	0.33 862	9.95 856	6	22 21	
39 40	9.62 021	28	9.66 204	33	0.33 829	9.95 850	6	20	
	9.62 076	27	9.66 238	34	0.33 762	9.95 839	5	10	
4I 42	9.62 104	28	9.66 271	33	0.33 702	9.95 833	6	18	
43	9.62 131	27 28	9.66 304	33	0.33 696	9.95 827	6	17	6 5
44	9.62 159	27	9.66 337	33 34	0.33 663	9.95 821	6	16	1 0.6 0.5
45 46	9.62 186 9.62 214	28	9.66 371 9.66 404	33	0.33 629	9.95 815 9.95 810	5	15	2 1.2 1.0
47	9.62 241	27	9.66 437	33	0.33 563	9.95 804		13	3 1.8 1.5
48	9.62 268	27 28	9.66 470	33	0.33 530	9.95 798	6	12	4 2.4 2.0 5 3.0 2.5
49	9.62 296	27	9.66 503	33	0.33 497	9.95 792	6	II	6 3.6 3.0
50	9.62 323	27	9.66 537	33	0.33 463	9.95 786	6	10	7 4.2 3.5
51	9.62 350	27	9.66 570	33	0.33 430	9.95 780	5	8	8 4.8 4.0 9 5.4 4.5
52 53	9.62 377	28	9.66 6o3 9.66 636	33	0.33 397	9.95 775 9.95 769	6	7	9134 43
54	9.62 432	27	9.66 669	33	0.33 331	9.95 763	6	6	
55	9.62 459	27	9.66 702	33	0.33 298	9.95 757	6	5	
56	9.62 486	27 27	9.66 735	33	0.33 265	9.95 751	6	4	
57 58	9.62 513 9.62 541	28	9.66 768	33	0.33 232	9.95 745 9.95 739	6	3 2	
59	9.62 568	27	9.66 834	33	0.33 166	9.95 733	6	I	
60	9.62 595	27	9.66 867	33	0.33 133	9.95 728	5	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	'	PP

114° (362) **65**°

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Ľ	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.62 595	27	9.66 867	33	0.33 133	9.95 728	6	60	
1	9.62 622	27	9.66 900	33	0.33 100	9.95 722	6	59	
3	9.62 649	27	9.66 933	33	0.33 067	9.95 716	6	58 57	
4	9.62 703	27	9.66 999	33	0.33 001	9.95 704	6	56	
5	9.62 730	27	9.67 032	33	0.32 968	9.95 698	6	55	
6	9.62 757	27 27	9.67 065	33	0.32 935	9.95 692	6	54	
7 8	9.62 784	27	9.67 098	33	0.32 902	9.95 686	6	53	
9	9.62 811	27	9.67 131	32	0.32 869	9.95 680 9.95 674	6	52 51	33 32
10	9.62 865	27	9.67 196	33	0.32 804	9.95 668	6	50	
11	9.62 892	27	9.67 229	33	0.32 771	9.95 663	5	49	1 3.3 3.2 2 6.6 6.4
12	9.62 918	26	9.67 262	33	0.32 738	9.95 657	6	48	3 9.9 9.6
13	9.62 945	27 27	9.67 295	33	0.32 705	9.95 651	6	47	4 13.2 12.8
14	9.62 972	27	9.67 327	33	0.32 673	9.95 645	6	46	5 16.5 16.0 6 19.8 19.2
15 16	9.62 999 9.63 0 26	27	9.67 360	33	0.32 640	9.95 639	6	45	
17	9.63 052	26	9.67 426	33	0.32 574	9.95 627	6	43	8 26.4 25.6
18	9.63 079	27	9.67 458	32	0.32 542	9.95 621	6	42	9 29.7 28.8
19	9.63 106	27 27	9.67 491	33 33	0.32 509	9.95 615	6	41	
20	9.63 133	26	9.67 524	32	0.32 476	9.95 609	6	40	
2 I	9.63 159	27	9.67 556	33	0.32 444	9.95 603	6	39	
22	9.63 186	27	9.67 589	33	0.32 411	9.95 597	6	38	
24	9.63 239	26	9.67 654	32	0.32 346	9.95 585	6	36	
25	9.63 266	27	9.67 687	33	0.32 313	9.95 579	6	35	
26	9.63 292	26 27	9.67 719	32	0.32 281	9.95 573	6	34	27 26
27	9.63 319	26	9.67 752	33	0.32 248	9.95 567	6	33	I 2.7 2.6
28 29	9.63 345 9.63 372	27	9.67 785 9.67 817	32	0.32 215	9.95 561 9.95 555	6	32 31	2 5.4 5.2
30	9.63 398	26	9.67 850	33	0.32 150	9.95 549	6	30	3 8.1 7.8 4 10.8 10.4
31	9.63 425	27	9.67 882	32	0.32 118	9.95 543	6	20	5 13.5 13.0
32	9.63 451	26	9.67 915	33	0.32 085	9.95 537	6	28	6 16.2 15.6
33	9.63 478	27 26	9.67 947	32	0.32 053	9.95 531	6	27	7 18.9 18.2 8 21.6 20.8
34	9.63 504	27	9.67 980	33	0.32 020	9.95 525	6	26	9 24.3 23.4
35 36	9.63 531	26	9.68 012	32	0.31 988	9.95 519	6	25	
37	9.63 557 9.63 583	26	9.68 077	33	0.31 950	9.95 513	6	24 23	
38	9.63 610	27	9.68 109	32	0.31 891	9.95 500	7	22	
39	9.63 636	26 26	9.68 142	33	0.31 858	9.95 494	6	21	
40	9.63 662	27	9.68 174	32	0.31826	9.95 488	6	20	
41	9.63 689	26	9.68 206		0.31 794	9.95 482	6	19	
42	9.63 715	26	9.68 239 9.68 271	33	0.31 761	9.95 476	6	18	7 6 5
43	9.63 741	26	9.68 303	32	0.31 729	9.95 470	6	17	1 0.7 0.6 0.5
45	9.63 794	27	9.68 336	33	0.31 664	9.95 458	6	15	2 1.4 1.2 1.0
46	9.63 820	26 26	9.68 368	32	0.31 632	9.95 452	6 6	14	3 2.1 1.8 1.5
47	9.63 846	26	9.68 400	32	0.31 600	9.95 446	6	13	4 2.8 2.4 2.0
48 49	9.63 872 9.63 898	26	9.68 432	33	0.31 508	9.95 440	6	12 11	5 3.5 3.0 2.5 6 4.2 3.6 3.0
50	9.63 924	26	9.68 497	32	0.31 503	9.95 427	7	10	7 4.9 4.2 3.5
51	9.63 950	26	9.68 529	32	0.31 471	9.95 421	6	9	
52	9.63 976	26	9.68 561	32	0.31 439	9.95 415	6	8	9 6.3 5.4 4.5
53	9.64 002	26 26	9.68 593	32	0.31 407	9.95 409	6	7	
54	9.64 028	26	9.68 626	33	0.31 374	9.95 403	6	6	
55 56	9.64 054	26	9.68 658	32	0.31 342	9.95 397 9.95 391	6	5 4	
57	9.64 106	26	9.68 722	32	0.31 278	9.95 384	7	3	
58	9.64 132	26 26	9.68 754	32	0.31 246	9.95 378	6	2	
59	9.64 158	26	9.08 780	32 32	0.31 214	9.95 372	6	1	
60	9.64 184		9.68 818		0.31 182	9.95 366		-0	D.D.
ш	L Cos	d	L Cot	c d	L Tan	L Sin	d		PP

115° (363) **64°**

1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.64 184	26	9.68818	32	0.31 182	9.95 366	6	60	
I	9.64 210	26	9.68 850	32	0.31 150	9.95 360	6	59	
3	9.64 236	26	9.68 882	32	0.31 118	9.95 354 9.95 348	6	58 57	
4	9.64 288	26	9.68 916	32	0.31 054	9.95 341	7	56	
5 6	9.64313	25	9.68 978	32	0.31 022	9.95 335	6	55	
	9.64 339	26 26	9.69 010	32	0.30 990	9.95 329	6	54	
7 8	9.64 365	26	9.69 012	32	0.30 958	9.95 323 9.95 317	6	53	
9	9.64 417	26	9.69 106	32	0.30 894	9.95 317	7	51	32 31
10	9.64 442	25	9.69 138	32	0.30 862	9.95 304	6	50	I 3.2 3.I 2 6.4 6.2
II	9.64468	26	9.69 170	32	0.30 830	9.95 298	6	49	3 9.6 9.3
I 2	9.64 494	26 25	9.69 202	32	0.30 798	9.95 292	6	48	4 12.8 12.4
13	9.64 519	26	9.69 234	32	0.30 766	9.95 286	7	47	5 16.0 15.5 6 19.2 18.6
14 15	9.64 545	26	9.69 298	32	0.30 734	9.95 279 9.95 273	6	46 45	
16	9.64 596	25	9.69 329	31	0.30 671	9.95 267	6	44	8 25.6 24.8
17	9.64 622	26 25	9.69 361	32	0.30 639	9.95 261	7	43	9 28.8 27.9
18	9.64 647	26	9.69 393	32	0.30 607	9.95 254 9.95 248	6	42 41	
20	9.64 698	25	9.69 457	32	0.30 543	9.95 242	6	40	
21	9.64 724	26	9.69 488	31	0.30 512	9.95 236	6	39	
22	9.64 749	25	9.69 520	32	0.30 480	9.95 229	7	38	
23	9.64 775	26 25	9.69 552	32	0.30 448	9.95 223	6	37	
24	9.64 800	26	9.69 584	31	0.30 416	9.95 217	6	36	
25 26	9.64 826 9.64 851	25	9.69 615	32	0.30 385	9.95 211	7	35	26 25 24
27	9.64877	26	9.69 679	32	0.30 321	9.95 198	6	33	I 2.6 2.5 2.4
28	9.64 902	25 25	9.69 710	31	0.30 290	9.95 192	6 7	32	2 5.2 5.0 4.8
29	9.64 927	26	9.69 7.12	32	0.30 258	9.95 185	6	31	3 7.8 7.5 7.2 4 10.4 10.0 9.6
30	9.64 953	25	9.69 774	31	0.30 226	9.95 179	6	30	5 13.0 12.5 12.0
31 32	9.64 978	25	9.69 805	32	0.30 195	9.95 173 9.95 167	6	29 28	6 15.6 15.0 14.4
33	9.65 029	26	9.69 868	31	0.30 132	9.95 160	7	27	7 18.2 17.5 16.8 8 20.8 20.0 19.2
34	9.65 054	25	9.69 900	32	0.30 100	9.95 154	6	26	9 23.4 22.5 21.6
35	9.65 079	25 25	9.69 932	32 31	0.30 068	9.95 148	6 7	25	
36 37	9.65 104	26	9.69 963	32	0.30 037	9.95 141	6	24	
38	9.65 155	25	9.70 026	31	0.29 974	9.95 129	6	23	
39	9.65 180	25 25	9.70058	32	0.29 942	9.95 122	7	2 1	
40	9.65 205	25	9.70 089	31	0.29 911	9.95 116	6	30	
41	9.65 230	25	9.70121	31	0.29 879	9.95 110	7	19	
42 43	9.65 255 9.65 281	26	9.70 152	32	0.29 848	9.95 103	6	18	7 6
44	9.65 306	25	9.70 215	31	0.29 785	9.95 090	7	16	1 0.7 0.6
45	9.65 331	25	9.70 247	32	0.29 753	9.95 084	6 6	15	2 1.4 1.2
46	9.65 356	25 25	9.70 278	3I 3I	0.29 722	9.95 078	7	11	3 2.1 1.8
47 48	9.65 381	25	9.70 309	32	0.29 691	9.95 071	6	13	4 2.8 2.4 5 3.5 3.0
49	9.65 431	25	9.70 372	31	0.29 628	9.95 059	6	II	6 4.2 3.6
50	9.65 456	25	9.70 404	32	0.29 596	9.95 052	7	10	7 4.9 4.2
51	9.65 481	25	9.70 435	31	0.29 565	9.95 046	6	9	8 5.6 4.8 9 6.3 5.4
52	9.65 506	25 25	9.70 466	31 32	0.29 534	9.95 039	7	8	. 9100
53	9.65 531	25	9.70 498	31	0.29 502	9.95 033	6	6	
54 55	9.65 586	24	9.70 529	31	0.29 471	9.95 027	7	5	
56	9.65 605	25	9.70 592	32	0.29 408	9.95 014	6	4	
57	9.65 630	25 25	9.70 623	3I 3I	0.29 377	9.95 007	7	3	
58 59	9.65 655 9.65 680	25	9.70 654	31	0.29 346	9.95 001	6	2 I	
60	9.65 705	25	9.70 717	32	0.29 283	9.94 988	7	0	
		٠		<u> </u>				-	РР
\square	L Cos	d	L Cot	cd	L. Tan	L Sin	u	000	FF

116° (364) **63**°

27° 152°

Ľ	L Sin	d	L Tan	c d	L Cot	L Cos	d	_		F	P P
0	9.65 705	2.1	9.70717	31	0.29 283	9.94988	6	60			
1	9.65 729	25	9.70 748	31	0.29 252	9.94 982	7	59			
3	9.65 754	25	9.70 779	31	0.29 221	9.94 975	6	58			
4	9.65 804	25	9.70 841	31	0.29 159	9.94 962	7	56			
5	9.65 828	2.4	9.70 873	32	0.29 127	9.94 956	6	55			
6	9.65 853	25 25	9.70 904	3I 3I	0.29 096	9.94 949	7	54			
7 8	9.65 878	24	9.70 935	31	0.29 065	9.94 943 9.94 936	7	53 52		00	04 00
9	9.65 927	25	9.70 997	31	0.29 003	9.94 930	6	51		32	31 30
10	9.65 952	25	9.71 028	31	0.28 972	9.94 923	7	50	2	3.2 6.4	3. I 3.0 6.2 6.0
11	9.65 976	2.4	9.71 059	31	0.28941	9.94 917	6	49	3	9.6	9.3 9.0
I 2	9.66 001	25 24	9.71 090	31 31	0.28 910	9.94911	6	48	4	12.8	12.4 12.0
13	9.66 025	25	9.71 121	32	0.28 879	9.94 904 9.94 898	6	47 46	5	16.0	15.5 15.0 18.6 18.0
15	9.66 075	25	9.71 153	31	0.28 816	9.94 891	7	45	7	22.4	21.7 21.0
ıŏ	9.66 099	2.4	9.71 215	31	0.28 785	9.94 885	6	44	8	25.6	24.8 24.0
17	9.66 124	25 24	9.71 246	3 I 3 I	0.28 754	9.94 878	7	43	9	28.8	27.9 27.0
18	9.66 148	25	9.71 277	31	0.28 723	9.94 871 9.94 865	6	42 4I			
20	9.66 197	2.4	9.71 308	31	0.28 661	9.94 858	7	40			•
21	9.66 221	24	9.71 370	31	0.28 630	9.94 852	6	39			
22	9.66 246	25	9.71 401	3 I	0.28 599	9.94 845	7	38			
23	9.66 270	24	9.71 431	30	0.28 569	9.94 839	6	37			
2.4	9.66 295	25 24	9.71 462	3 I 3 I	0.28 538	9.94 832	7 6	36			
25 26	9.66 319	24	9.71 493 9.71 524	31	0.28 507	9.94 826 9.94 819	7	35 34		25	24 23
27	9.66 368	25	9.71 555	31	0.28 445	9.94 813	6	33	1	2.5	2.4 2.3
28	9.66 392	2.4	9.71 586	31	0.28 414	9.94 806	7	32	2	5.0	4.8 4.6
29	9.66 416	24 25	9.71 617	3 I 3 I	0.28 383	9.94 799	7	31	3	7.5	7.2 6.9
30	9.66 441	24	9.71 648	31	0.28 352	9.94 793	7	30	4	IO.0 I2.5	9.6 9.2 12.0 11.5
31	9.66 465	24	9.71 679	30	0.28 321	9.94 786	6	29	5 6	15.0	14.4 13.8
32	9.66 489	24	9.71 709	31	0.28 260	9.94 780	7	28	7 8	17.5	16.8 16.1
34	9.66 537	24	9.71 771	31	0.28 229	9.94 767	6	26	9	20.0	19.2 18.4 21.6 20.7
35	9.66 562	25	9.71 802	31	0.28 198	9.94 760	7	25	9	3	21.0 20.7
36	9.66 586	2.4 2.4	9.71 833	31 30	0.28 167	9.94 753	.7 6	24			
37 38	9.66 610	24	9.71 863 9.71 894	31	0.28 137	9.94 747 9.94 740	7	23			
39	9.66 658	24	9.71 925	3 I	0.28 075	9.94 734	6	21			
40	9.66 682	24	9.71 955	30	0.28 045	9.94 727	7	20			
41	9.66 706	24	9.71 986	31	0.28 014	9.94 720	7	19			
42	9.66 731	25 24	9.72 017	31 31	0.27 983	9.94714	6	18			
43	9.66 755	24	9.72 048	30	0.27 952	9.94 707	7	17		7	6
45	9.66 779	24	9.72 078	31	0.27 922	9.94 700 9.94 694	6	15		1 0.7	0.6
46	9.66 827	24	9.72 140	31	0.27 860	9.94 687	7	14		2 I.4 3 2.I	1.2
47	9.66 851	24	9.72 170	30 31	0.27 830	9.94 680	7	13		4 2.8	2.4
48 49	9.66 875	24	9.72 20I 9.72 23I	30	0.27 799 0.27 769	9.94 674	7	I2		5 3.5	3.0
50	9.66 922	23	9.72 262	31	0.27 738	9.94 660	7	10			3.6 4.2
51	9.66 946	24	9.72 202	31	0.27 707	9.94 654	6			8 5.6	4.8
52	9.66 970	24	9.72 323	30	0.27 677	9.94 647	7	9 8		9 6.3	5.4
53	9.66 994	24	9.72 354	31	0.27 646	9.94 640	6	7			
54	9.67 018	24	9.72 384	30 31	0.27 616	9.94 634	7	6			
55 56	9.67 066	2.4	9.72 415	30	0.27 585	9.94 627 9.94 620	7	5 4			
57	9.67 090	24	9.72 476	3 I	0.27 524	9.94614	6	3			
58	9.67 113	23 24	9.72 506	30	0.27 494	9.94 607	7	2			
59	9.67 137	24	9.72 537	31	0.27 463	9.94 600	7	I			
60	9.67 161	_	9.72 567		0.24 433	9.94 593		0			
	L Cos	d	L Cot	c d	L Tan	L Sin	d	′		F	Р

117° (365) **62**°

0	9.67 161	d	L Tan				d		PP
			9.72 567	c d	L Cot	9.94 593		60	1 F
I	9.67 185	24	9.72 598	31	0.27 402	9.94 587	6	59	
2	9.67 208	23	9.72 628	30	0.27 372	9.94 580	7	58	
3	9.67 232	24 24	9.72 659	30	0.27 341	9.94 573	7 6	57	
4	9.67 256	24	9.72 689	31	0.27 311	9.94 567	7	56	
5 6	9.67 280 9.67 303	23	9.72 720	30	0.27 280	9.94 560 9.94 553	7	55 54	
	9.67 327	24	9.72 780	30	0.27 220	9.94 546	7	53	
7 8	9.67 350	23	9.72811	31 30	0.27 189	9.94 540	6 7	52	31 30 29
9	9.67 374	24	9.72 841	31	0.27 159	9.94 533	7	51	I 3.I 3.0 2.9
10	9.67 398	23	9.72872	30	0.27 128	9.94 526	7	50	2 6.2 6.0 5.8
II I2	9.67 421	24	9.72 902 9.72 932	30	0.27 098	9.94 519 9.94 513	6	49 48	3 9.3 9.0 8.7
13	9.67 445 9.67 468	23	9.72 963	31	0.27 068	9.94 506	7	47	4 12.4 12.0 11.6 5 15.5 15.0 14.5
14	9.67 492	24	9.72 993	30	0.27 007	9.94 499	7	46	6 18.6 18.0 17.4
15	9.67 515	23 24	9.73 023	30 31	0.26 977	9.94 492	7	45	7 21.7 21.0 20.3 8 24.8 24.0 23.2
16	9.67 539	23	9.73 054	30	0.26 946	9.94 485	6	44	8 24.8 24.0 23.2 9 27.9 27.0 26.1
17	9.67 562 9.67 586	24	9.73 084 9.73 II4	30	0.26 916	9.94 479 9.94 472	7	43	1
19	9.67 609	23	9.73 144	30	0.26 856	9.94 465	7	41	
20	9.67 633	24	9.73 175	31	0.26 825	9.94 458	7	40	
21	9.67 656	23	9.73 205	1 -	0.26 795	9.94 451	6	39	
22	9.67 680	24 23	9.73 235	30	0.26 765	9.94 445	7	38	
23	9.67 703	23	9.73 265	30	0.26 735	9.94 438	7	37 36	
25	9.67 750	24	9.73 326	31	0.26 674	9.94 431	7	35	
26	9.67 773	23	9.73 356	30	0.26 644	9.94 417	7	34	24 23 22
27	9.67 796	23	9.73 386	30	0.26 614	9.94410	6	33	1 2.4 2.3 2.2 2 4.8 4.6 4.4
28 29	9.67 820 9.67 843	23	9.73 416 9.73 446	30	0.26 584	9.94 404	7	32 31	2 4.8 4.6 4.4 3 7.2 6.9 6.6
30	9.67 866	23	9.73 476	30	0.26 524	9.94 390	7	30	4 9.6 9.2 8.8
31	9.67 890	24	9.73 507	31	0.26 493	9.94 383	7	29	5 12.0 11.5 11.0 6 14.4 13.8 13.2
32	9.67 913	23	9.73 537	30	0.26 463	9.94 376	7	28	
33	9.67 936	23	9.73 567	30	0.26 433	9.94 369	7	27	8 19.2 18.4 17.6
34	9.67 959	23 23	9.73 597	30	0.26 403	9.94 362	7	26	9 21.6 20.7 19.8
35	9.67 982	24	9.73 627 9.73 657	30	0.26 343	9.94 355	6	25	
37	9.68 029	23	9.73 687	30	0.26 313	9.94 342	7	23	
38	9.68 052	23	9.73 717	30	0.26 283	9.94 335	7	22	
39	9.68 075	23 23	9.73 747	30	0.26 253	9.94 328	7	21	
40	9.68 098	23	9.73 777	30	0.26 223	9.94 321	7	20	
4I 42	9.68 121	23	9.73 807	30	0.26 193	9.94 314	7	18	
43	9.68 167	23	9.73 867	30	0.26 133	9.94 300	7	17	7 6
44	9.68 190	23	9.73 897	30	0.26 103	9.94 293	7	16	1 0.7 0.6
45	9.68 213	23 24	9.73 927	30	0.26 073	9.94 286	7	15	2 1.4 1.2
46 47	9.68 237	23	9.73 957 9.73 987	30	0.26 013	9.94 279	6	13	3 2.I I.8 4 2.8 2.4
48	9.68 283	23	9.73 907	30	0.25 983	9.94 266	7	12	
49	9.68 305	22	9.74 047	30	0.25 953	9.94 259	7	11	6 4.2 3.6
50	9.68 328	23	9.74 077	30	0.25 923	9.94 252	7	10	7 4.9 4.2 8 5.6 4.8
51	9.68 351	23	9.74 107	30	0.25 893	9.94 245	7	9	9 6.3 5.4
52 53	9.68 374	23	9.74 I37 9.74 I66	29	0.25 863	9.94 238	7	7	
54	9.68 420	23	9.74 196	30	0.25 804	9.94 224	7	6	
55	9.68 443	23	9.74 226	30	0.25 774	9.94 217	7	5	
56	9.68 466	23 23	9.74 256	30	0.25 744	9.94 210	7	4	
57 58	9.68 489	23	9.74 286	30	0.25 714	9.94 203	7	3 2	
59	9.68 534	22	9.74 345	29	0.25 655	9.94 189	7	ī	
60	9.68 557	23	9.74 375	30	0.25 625	9.94 182	7	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	1	PP

118° (366) **61**°

	29							OV.				
′	L Sin	d	L Tan	c d	L Cot	L Cos	d				PP	
0	9.68 557	22	9.74 375	30	0.25 625	9.94 182	7	60				
1	9.68 580	23	9.74 405	30	0.25 595	9.94 175	7	59				
2	9.68 603	23	9.74 435	30	0.25 565	9.94 168	7	58				
3	9.68 625	23	9.74 465	29	0.25 535	9.94 161	7	57 56				
5	9.68 671	23	9.74 524	30	0.25 476	9.94 147	7	55				
6	9.68 694	23	9.74 554	30 29	0.25 446	9.94 140	7	54				
7	9.68 716	23	9.74 583	30	0.25 417	9.94 133	7	53				
8	9.68 739 9.68 762	23	9.74 613	30	0.25 387	9.94 126	7	52 51				
10	9.68 784	22	9.74 673	30	0.25 327	9.94 112	7	50				
11	9.68 807	23	9.74 702	29	0.25 298	9.94 105	7	49				
I 2	9.68 829	22	9.74 732	30 30	0.25 268	9.94 098	7 8	48				
13	9.68 852	23 23	9.74 762	29	0.25 238	9.94 090	7	47		30	29	23
14 15	9.68 875	22	9.74 791	30	0.25 209 0.25 179	9.94 0 83 9.94 0 76	7	46 45	1	3.0	2.9	2.3
16	9.68 920	23	9.74 851	30	0.25 149	9.94 069	7	44	2	6.o 9.o	5.8 8.7	4.6 6.9
17	9.68 942	22	9.74 880	29	0.25 120	9.94 062	7	43	3	12.0	11.6	9.2
18	9.68 965	23	9.74 910	30 29	0.25 090	9.94 055	7	42	5	15.0	14.5	11.5
20	9.68 987	23	9.74 939	30	0.25 001	9.94 048	7	41 40	6	18.0	17.4	13.8 16.1
21	9.69 032	22	9.74 909	29	0.25 031	9.94 041	7	39	7 8	21.0	20.3	18.4
22	9.69 055	23	9.74 998	30	0.24 972	9.94 034	7	38	9	27.0	26.1	20.7
23	9.69 077	22	9.75 058	30 29	0.24 942	9.94 020	7 8	37				
24	9.69 100	23	9.75 087	30	0.24 913	9.94 012	7	36				
25 26	9.69 122	22	9.75 117	29	0.24 883	9.94 005	7	35				
27	9.69 167	23	9.75 176	30	0.24 824	9.93 990	7	33				
28	9.69 189	22	9.75 205	29	0.24 795	9.93 984	7	32				
29	9.69 212	23	9.75 235	30 29	0.24 765	9.93 977	7	31				
30	9.69 234	22	9.75 264	30	0.24 736	9.93 970	7	30				
31 32	9.69 256	23	9.75 294	29	0.24 706	9.93 963	8	29 28				
33	9.69 301	22	9.75 323 9.75 353	30	0.24 647	9.93 933	7	27				
34	9.69 323	22	9.75 382	29	0.24 618	9.93 941	7	26				
35	9.69 345	22	9.75 411	29 30	0.24 589	9.93 934	7	25	ĺ			
36 37	9.69 368 9.69 390	22	9.75 441	29	0.24 559	9.93 927	7	24				
38	9.69 412	22	9.75 500	30	0.24 500	9.93 912	8	22		22	8	7
39	9.69 434	22	9.75 529	29	0.24 47 I	9.93 905	7	2 I	1	2.2	0.8	0.7
40	9.69 456	23	9.75 558	30	0.24 442	9.93 898	7	20	3	4.4 6.6	1.6 2.4	I.4 2.I
4 I	9.69 479	22	9.75 588	29	0.24 412	9.93 891	7	19	4	8.8	3.2	2.8
42 43	9.69 501	22	9.75 647	30	0.24 383	9.93 884 9.93 876	8	18	5	11.0	4.0	3.5
44	9.69 545	22	9.75 676	29	0.24 324	9.93 869	7	16	6	13.2	4.8 5.6	4.2 4.9
45	9.69 567	22	9.75 705	30	0.24 295	9.93 862	7	15	7 8	17.6	6.4	5.6
46	9.69 589	22	9.75 735	29	0.24 265	9.93 855	8	14	9	19.8	7.2	6.3
47 48	9.69 633	22	9.75 764 9.75 793	29	0.24 236	9.93 847	7	13				
49	9.69 655	22	9.75 822	29	0.24 178	9.93 833	7	11				
50	9.69 677	22	9.75 852	30	0.24 148	9.93 826	7	10				
51	9.69 699	22	9.75 881	29	0.24 119	9.93 819	7 8	9	1			
52 53	9.69 721	22	9.75 910	29	0.24 090	9.93 811	7	8 7				
54	9.69 765	22	9.75 969	30	0.24 001	9.93 797	7	6				
55	9.69 787	22	9.75 998	29	0.24 002	9.93 789	8	5				
56	9.69 809	22	9.76 027	29 29	0.23 973	9.93 782	7 7	4				
57 58	9.69 831	22	9.76 o56 9.76 o86	30	0.23 944	9.93 775	7 8	3 2				
59	9.69 875	22	9.76 115	29	0.23 885	9.93 760		I				
60	9.69 897	22	9.76 144	29	0.23 856	9.93 753	7	0				
	L Cos	d	L Cot	c d	L Tan	L Sin	d	,			PΡ	
	1100			_				enc				

119° (367) **60**°

		_		_			_	40	
	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.69 897	22	9.76 144	29	0.23 856	9.93 753	7	60	
1 2	9.69 919	22	9.76 173	29	0.23 827	9.93 746	8	59	
3	9.69 941	22	9.76 202	29	0.23 798	9.93 738	7	58 57	
4	9.69 984	2 I	9.76 261	30	0.23 739	9.93 724	7	56	
5	9.70 006	22	9.76 290	29	0.23 710	9.93 717	8	55	
6	9.70028	22	9.76 319	29	0.23 681	9.93 709	7	54	
7 8	9.70 050	22	9.76 348	29	0.23 652	9.93 702 9.93 695	7 8	53 52	
9	9.70 093	21	9.76 406	29	0.23 594	9.93 687		51	30 29 28
10	9.70 115	22	9.76 435	29	0.23 565	9.93 680	7	50	I 3.0 2.9 2.8 2 6.0 5.8 5.6
11	9.70 137	22	9.76 464	29	0.23 536	9.93 673	7 8	49	2 6.0 5.8 5.6 3 9.0 8.7 8.4
12	9.70 159	2 2 2 I	9.76 493	29 29	0.23 507	9.93 665	0 7	48	4 12.0 11.6 11.2
13	9.70 180	22	9.76 522 9.76 551	29	0.23 478	9.93 658	8	47	5 15.0 14.5 14.0 6 18.0 17.4 16.8
15	9.70 202	22	9.76 580	29	0.23 449 0.23 420	9.93 650	7	46 45	6 18.0 17.4 16.8 7 21.0 20.3 19.6
16	9.70 245	2 I 2 2	9.76 609	29	0.23 391	9.93 636	7 8	44	8 24.0 23.2 22.4
17	9.70 267	21	9.76 639	30 29	0.23 361	9.93 628	7	43	9 27.0 26.1 25.2
18	9.70 288	22	9.76 668 9.76 697	29	0.23 332 0.23 303	9.93 621 9.93 614	7	42 41	
20	9.70 332	22	9.76 725	28	0.23 275	9.93 606	8	40	
21	9.70 353	2 I	9.76 754	29	0.23 246	9.93 599	7	39	
22	9.70 375	22	9.76 783	29	0.23 217	9.93 591	8	38	
23	9.70 396	2 I 2 2	9.76 812	29	0.23 188	9.93 584	7	37	
24	9.70 418	21	9.76 841	29	0.23 159	9.93 577	7 8	36	
25 26	9.70 439 9.70 461	22	9.76 870 9.76 899	29	0.23 I30 0.23 IQI	9.93 569	7	35	22 21
27	9.70 482	2 I	9.76 928	29	0.23 072	9.93 554	8	33	I 2.2 2.I
28	9.70 504	2 2 2 I	9.76 957	29	0.23 043	9.93 547	7 8	32	2 4.4 4.2
29	9.70 525	22	9.76 986	29	0.23 014	9.93 539	7	31	3 6.6 6.3 4 8.8 8.4
30	9.70 547	21	9.77 015	29	0.22 985	9.93 532	7	30	
31 32	9.70 568	22	9.77 044 9.77 0 73	29	0.22 956	9.93 525	8	29 28	6 13.2 12.6
33	9.70 611	2 I	9.77 101	28	0.22 899	9.93 517	7	27	7 15.4 14.7 8 17.6 16.8
34	9.70 633	22	9.77 130	29	0.22 870	9.93 502	8	26	9 19.8 18.9
35	9.70 654	2 I 2 I	9.77 159	29 29	0.22 841	9.93 495	7	25	
36	9.70 675	22	9.77 188	29	0.22 812	9.93 487	7	24	
38	9.70 718	2 I	9.77 246	29	0.22 754	9.93 472	8	23	
39	9.70 739	2 I 2 2	9.77 274	28	0.22 726	9.93 465	7	21	
40	9.70 761	2 I	9.77 303	29	0.22697	9.93 457	7	20	
41	9.70 782	21	9.77 332	29	0.22 668	9.93 450	8	19	
42 43	9.70 803	21	9.77 361 9.77 390	29	0.22 639	9.93 442		18	
43	9.70824	22	9.77 418	28	0.22 582	9.93 435	7 8	17	8 7
45	9.70 867	21	9.77 447	29	0.22 553	9.93 427	7 8	15	1 0.8
46	9.70 888	2 I 2 I	9.77 476	29	0.22 524	9.93 412	7	14	3 2.4 2.1
47 48	9.70 909 9.70 931	2 2	9.77 505 9.77 533	28	0.22 495	9.93 405	8	I3 I2	4 3.2 2.8
49	9.70 952	2 I	9.77 562	29	0.22 407	9.93 397 9.93 390	7	II	5 4.0 3.5 6 4.8 4.2
50	9.70 973	2 I	9.77 591	29	0.22 409	9.93 382		10	7 5.6 4.9
51	9.70 994	2 I	9.77 619	28	0.22 381	9.93 375	7	9	
52	9.71 015	2 I 2 I	9.77 648	29	0.22 352	9.93 367	8	8	9 7.2 6.3
53	9.71 036	22	9.77 677	29	0.22 323	9.93 360	7 8	7	
54 55	9.71 050	2 I	9.77 706	28	0.22 294	9.93 352	8	6	
56	9.71 100	2 I 2 I	9.77 763	29	0.22 237	9.93 337	7 8	4	
57	9.71 121	21	9.77 791	28	0.22 209	9.93 329	7	3	
58 59	9.71 142	2 I	9.77 820 9.77 849	29	0.22 180	9.93 322	8	2 I	
60	9.71 184	2 I	9.77 849	28	0.22 151	9.93 314	7	0	
	L Cos		L Cot	c d	L Tan	L Sin	d	-	PP
	- 008	u	L 000	Ç U	∟ ran	Lom	u	ا :	гг

1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.71 184	21	9.77 877	29	0.22 123	9.93 307	8	60	
1	9.71 205	21	9.77 906	29	0.22 094	9.93 299	8	59	
2	9.71 226	2 I	9.77 935 9.77 963	28	0.22 065	9.93 291	7	58	
3	9.71 247 9.71 268	2 I	9.77 903	29	0.22 037	9.93 284	8	57 56	
4 5	9.71 289	2 I	9.78 020	28	0.21 980	9.93 269	7 8	55	
ŏ	9.71 310	21	9.78 049	29	0.21 951	9.93 261	8	54	
7 8	9.71 331	2I 2I	9.78 077	28 29	0.21 923	9.93 253		53	
	9.71 352	21	9.78 106	29	0.21 894	9.93 246	7 8	52	29 28
9	9.71 373	20	9.78 135	28		9.93 238	8	51	1 2.9 2.8
10	9.71 393	21	9.78 163	29	0.21 837	9.93 230	7	50	2 5.8 5.6 3 8.7 8.4
II I2	9.71 414 9.71 435	2 I	9.78 192 9.78 220	28	0.21 808	9.93 223	8	49 48	
13	9.71 456	2 I	9.78 249	29	0.21 751	9.93 207	8	47	
14	9.71 477	21	9.78 277	28	0.21 723	9.93 200	7	46	6 17.4 16.8
15	9.71 498	2 I 2 I	9.78 306	29 28	0.21 694	9.93 192	8	45	7 20.3 19.6 8 23.2 22.4
16	9.71 519	20	9.78 334	29	0.21 666	9.93 184	7	44	8 23.2 22.4 9 26.1 25.2
18	9.71 539 9.71 560	21	9.78 363 9.78 391	28	0.21 637	9.93 177	8	43	9 20.1 25.2
10	9.71 58.	2 I	9.78 419	28	0.21 581	9.93 161	8	42 41	
20	9.71 602	21	9.78 448	29	0.21 552	9.93 154	7	40	
21	9.71 622	20	9.78 476	28	0.21 524	9.93 146	8	39	
22	9.71 643	21	9.78 505	29	0.21 495	9.93 138	8	38	
23	9.71 664	2I 2I	9.78 533	28 29	0.21 467	9.93 131	7	37	
24	9.71 685	20	9.78 562	28	0.21 438	9.93 123	8	36	
25 26	9.71 705	21	9.78 590 9.78 618	28	0.21 410	9.93 115 9.93 108		35	21 20
27	9.71 720	21	9.78 647	29	0.21 353	9.93 100	7 8	34	1 2.1 2.0
28	9.71 767	20	9.78 675	28	0.21 335	9.93 092	8	32	2 4.2 4.0
29	9.71 788	21	9.78 704	29 28	0.21 296	9.93 084	8	31	3 6.3 6.0
30	9.71 809	21	9.78 732	28	0.21 268	9.93 077	8	30	4 8.4 8.0
3 I	9.71 829	20	9.78 760		0.21 240	9.93 069	8	29	5 10.5 10.0 6 12.6 12.0
32	9.71 850	2I 2O	9.78 789	29 28	0.21 211	9.93 061	8	28	
33	9.71 870	21	9.78 817 9.78 845	28	0.21 183	9.93 053	7	27	8 16.8 16.0
34	9.71 911	20	9.78 874	29	0.21 155	9.93 046 9.93 038	8	26 25	9 18.9 18.0
36	9.71 932	21	9.78 902	28	0.21 098	9.93 030	8	24	
37	9.71 952	20	9.78 930	28	0.21 070	9.93 022	8	23	
38	9.71 973	2 I 2 I	9.78 959	29 28	0.21 041	9.93 014	8	22	
39	9.71 994	20	9.78 987	28	0.21 013	9.93 007	7 8	21	
40	9.72 014	20	9.79 015	28	0.20 985	9.92 999	8	20	
41	9.72 034	21	9.79 043	20	0.20 957	9.92 991	8	19	
42	9.72 O55 9.72 O75	20	9.79 072 9.79 100	2Ś	0.20 928	9.92 983	7 8	18	
44	9.72 096	21	9.79 128	28	0.20 872	9.92 978		16	8 7
45	9.72 116	20	9.79 156	28	0.20 844	9.92 960	8	15	1 0.8 0.7 2 1.6 1.4
46	9.72 137	2 I 20	9.79 185	29 28	0.20815	9.92 952	8	14	3 2.4 2.1
47	9.72 157	20	9.79 213	28	0.20 787	9.92 944	8	13	4 3.2 2.8
48 49	9.72 177	21	9.79 241 9.79 269	28	0.20 759	9.92 936	7 8	I 2	5 4.0 3.5 6 4.8 4.2
50	9.72 218	20	9.79 297	28	0.20 703	9.92 921		10	
51	9.72 238	20	9.79 326	29	0.20 674	9.92 913	8	9	8 6.4 5.6
52	9.72 259	21	9.79 320	28	0.20 646	9.92 913	8	8	9 7.2 6.3
53	9.72 279	2O 2O	9.79 382	28 28	0.20618	9.92 897	8	7	20
54	9.72 299	20	9.79 410	28	0.20 590	9.92 889	8	6	
55 56	9.72 320	20	9.79 438 9.79 466	28	0.20 562	9.92 881 9.92 874		5 4	
57	9.72 340	20	9.79 400	29	0.20 534	9.92 866	7 8	3	
58	9.72 381	21	9.79 523	28	0.20 477	9.92 858	8	2	
59	9.72 401	20	9.79 551	28	0.20 449	9.92 850	8	1	
60	9.72 421		9.79 579		0.20 421	9.92 842		0	
	L Cos	d	L Cot	cd	L Tan	L Sin	d	'	PP

	32°							47°	
′	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.72 421	20	9.79 579	28	0.20 421	9.92 842	8	60	
1	9.72 441	20	9.79 607	28	0.20 393	9.92 834 9.92 826	8	59 58	
3	9.72 461	21	9.79 635	28	0.20 365	9.92 818	8	57	
4	9.72 502	20	9.79 691	28	0.20 309	9.92810	8	56	
5	9.72 522	20 20	9.79 719	28 28	0.20 281	9.92 803	7 8	55	
6	9.72 542	20	9.79 747	29	0.20 253	9.92 795 9.92 787	8	54	
7 8	9.72 562 9.72 582	20	9.79 776 9.79 804	28	0.20 196	9.92 779	8	53 52	29 28 27
9	9.72 602	20	9.79 832	28 28	0.20 168	9.92771	8	51	I 2.9 2.8 2.7
10	9.72 622	20	9.79 860	28	0.20 140	9.92 763	8	50	2 5.8 5.6 5.4
11	9.72 643	20	9.79 888	28	0.20 112	9.92 755	8	49	3 8.7 8.4 8.1
12	9.72 663	20	9.79 916	28	0.20 084	9.92 747 9.92 739	8	48	
13 14	9.72 703	20	9.79 944	28	0.20028	9.92 731	8	46	5 14.5 14.0 13.5 6 17.4 16.8 16.2
15	9.72 723	20	9.80 000	28 28	0.20 000	9.92 723	8	45	7 20.3 19.6 18.9
16	9.72 743	20	9.80 028	28	0.19972	9.92715	8	44	
17	9.72 763	20	9.80 056 9.80 084	28	0.19 944	9.92 707	8	43	1
19	9.72 803	20	9.80 112	28	0.19 888	9.92 691	8	41	
20	9.72823	20	9.80 140	28	0.19860	9.92 683	8	40	
21	9.72843	20	9.80 168	28	0.19832	9.92 675	8	39	
22	9.72 863	20	9.80 195	27 28	0.19805	9.92 667	8	38	
23	9.72 883	19	9.80 223	28	0.19777	9.92 659	8	37	
24 25	9.72 902	20	9.80 251	28	0.19749	9.92 651	8	36	
26	9.72 942	20	9.80 307	28	0.19 693	9.92 635	8	34	21 20 19
27	9.72 962	20 20	9.80 335	28	0.19665	9.92627	8	33	1 2.1 2.0 1.9
28 29	9.72 982	20	9.80 363	28	0.19 637	9.92 619	8	32	2 4.2 4.0 3.8 3 6.3 6.0 5.7
30	9.73 002	20	9.80 391	28	0.19 609	9.92 611	8	31 30	1 0 0 - 2
31	9.73 022 9.73 041	19	9.80 417	28	0.19 553	9.92 595	8	20	5 10.5 10.0 9.5
32	9.73 061	20	9.80 474	27	0.19 535	9.92 587	8	28	6 12.6 12.0 11.4 7 14.7 14.0 13.3
33	9.73 081	20 20	9.80 502	28 28	0.19498	9.92 579	8	27	8 16.8 16.0 15.2
34	9.73 101	20	9.80 530	28	0.19 470	9.92 571	8	26	9 18.9 18.0 17.1
35 36	9.73 I2I 9.73 I40	19	9.80 558 9.80 586	28	0.19 442	9.92 563	8	25	
37	9.73 160	20	9.80 614	28	0.19386	9.92 546	9	23	
38	9.73 180	20	9.80 642	28 27	0.19358	9.92 538	8	22	
39	9.73 200	19	9.80 669	28	0.19 331	9.92 530	8	21	
40	9.73 219	20	9.80 697	28	0.19 303	9.92 522	8	20	i .
4I 42	9.73 239 9.73 259	20	9.80 725 9.80 753	28	0.19 275	9.92 514	8	18	
43	9.73 259	19	9.80 781	28	0.19 247	9.92 506	8	17	9 8 7
44	9.73 298	20	9.80 808	27	0.19192	9.92 490	8	16	
45	9.73 318	20 19	9.80 836	28 28	0.19 164	9.92 482	8	15	2 1.8 1.6 1.4
46 47	9.73 337 9.73 357	20	9.80 864	28	0.19136	9.92 473	8	14	3 2.7 2.4 2.1
48	9.73 337	20	9.80 919	27	0.19 103	9.92 405	8	13	4 3.6 3.2 2.8
49	9.73 396	19 20	9.80 947	28 28	0.19 053	9.92 449	8	11	5 4.5 4.0 3.5 6 5.4 4.8 4.2
50	9.73 416	19	9.80 975	28	0.19025	9.92 441	8	10	7 6.3 5.6 4.9
51	9.73 435	20	9.81 003	27	0.18 997	9.92 433	8	9	8 7.2 6.4 5.6 9 8.1 7.2 6.3
52 53	9.73 455	19	9.81 030	28	0.18 970	9.92 425		8	9 0.1 7.2 0.3
54	9.73 474	20	9.81 086	28	0.18 914	9.92 416	9 8	7 6	
55	9.73 513	19	9.81 113	27	0.18 887	9.92 400	8	5	
56	9.73 533	20 19	9.81 141	28 28	0.18 859	9.92 392	8	4	
57 58	9.73 552 9.73 572	20	9.81 169		0.18 831	9.92 384	8	3	
59	9.73 572	19	9.81 224	27 28	0.18 776	9.92 376 9.92 367	9	2 I	
60	9.73 611	20	9.81 252	28	0.18 748	9.92 359	8	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	,	PP

122° (370) **57**°

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	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.73 611	19	9.81 252	27	0.18 748	9.92 359	8	60	
1	9.73 630	20	9.81 279	28	0.18 721	9.92 351	8	59	
3	9.73 650 9.73 669	19	9.81 307 9.81 335	28	0.18 665	9.92 343 9.92 335	8	58 57	
4	9.73 689	20	9.81 362	27	0.18638	9.92 326	9	56	
5	9.73 708	19	9.81 390	28 28	0.18610	9.92 318	8	55	
6	9.73 727	20	9.81 418	27	0.18 582	9.92 310	8	54	
7 8	9.73 747 9.73 766	19	9.81 445 9.81 473	28	0.18 555	9.92 302 9.92 293	9	53 52	
9	9.73 785	19	9.81 500	27	0.18 500	9.92 285	8	51	28 27
10	9.73 805	20	9.81 528	28	0.18 472	9.92 277	8	50	I 2.8 2.7
11	9.73 824	19	9.81 556	28	0.18 444	9.92 269	8	49	2 5.6 5.4 3 8.4 8.1
I 2	9.73 843	20	9.81 583	27 28	0.18417	9.92 260	8	48	3 8.4 8.1 4 11.2 10.8
13	9.73 863	19	9.81611	27	0.18 389	9.92 252	8	47	5 14.0 13.5
14 15	9.73 882 9.73 901	19	9.81 638 9.81 666	28	0.18 362	9.92 244 9.92 235	9	46	
16	9.73 921	20	9.81 693	27	0.18 307	9.92 227	8	44	7 19.6 18.9 8 22.4 21.6
17	9.73 940	19	9.81 721	28 27	0.18 279	9.92 219	8	43	9 25.2 24.3
18	9.73 959	19	9.81 748	28	0.18 252	9.92 211	9	42	
20	9.73 978	19	9.81 776	27	0.18 197	9.92 202	8	41 40	
21	9.73 997	20	9.81 831	28	0.18 169	9.92 194	8		
22	9.74 017	19	9.81 858	27	0.18 142	9.92 177	9	39 38	
23	9.74 055	19	9.81 886	28 27	0.18114	9.92 169	8	37	
24	9.74 074	19	9.81 913	28	0.18 087	9.92 161	9	36	
25 26	9.74 093 9.74 II3	20	9.81 941	27	0.18 059	9.92 152 9.92 144	8	35	20 19 18
27	9.74 113	19	9.81 996	28	0.18 004	9.92 144	8	34	
28	9.74 151	19	9.82 023	27	0.17 977	9.92 127	9 8	32	1 2.0 1.9 1.8 2 4.0 3.8 3.6
29	9.74 170	19	9.82 051	28	0.17 949	9.92 119	8	31	3 6.0 5.7 5.4
30	9.74 189	19	9.82 078	28	0.17 922	9.92 111	9	30	4 8.0 7.6 7.2
31	9.74 208	19	9.82 106	27	0.17 894	9.92 102	8	29	5 10.0 9.5 9.0 6 12.0 11.4 10.8
32 33	9.74 227 9.74 246	19	9.82 133	28	0.17 867	9.92 094 9.92 086	8	28 27	7 14.0 13.3 12.6 8 16.0 15.2 14.4
34	9.74 265	19	9.82 188	27	0.17812	9.92 077	9	26	8 16.0 15.2 14.4
35	9.74 284	19	9.82 215	27 28	0.17 785	9.92 069	8	25	9 18.0 17.1 16.2
36	9.74 303	19	9.82 243	27	0.17 757	9.92 060	8	24	
37 38	9.74 322 9.74 341	19	9.82 270 9.82 298	28	0.17 730	9.92 052 9.92 044	8	23	
39	9.74 360	19	9.82 325	27	0.17 675	9.92 044	9	21	
40	9.74 379	19	9.82 352	27	0.17 648	9.92 027	8	20	
41	9.74 398	19	9.82 380	28	0.17 620	9.92 018	9	19	
42	9.74 417	19	9.82 407	27	0.17 593	9.92 010	8	18	
43	9.74 430	19	9.82 435	27	0.17 505	9.92 002	9	17	9 8
44 45	9.74 455 9.74 474	19	9.82 489	27	0.17 538	9.91 993	8	15	1 0.9 0.8
46	9.74 493	19	9.82 517	28	0.17 483	9.91 976	9	14	2 1.8 1.6
47	9.74 512	19	9.82 544	27 27	0.17 456	9.91 968	9	13	3 2.7 2.4 4 3.6 3.2
48 49	9.74 531 9.74 549	18	9.82 571 9.82 599	28	0.17 429	9.91 959	8	I2 II	5 4.5 4.0
50	9.74 549	19	9.82 599	27	0.17 374	9.91 951	9	10	6 5.4 4.8
51	9.74 587	19	9.82 653	27	0.17 3/4	9.91 942	8	9	7 6.3 5.6 8 7.2 6.4
52	9.74 507	19	9.82 681	28	0.17 347	9.91 934	9	8	8 7.2 6.4 9 8.1 7.2
53	9.74 625	19	9.82 708	27	0.17 292	9.91 917	8	7	
54	9.74 644	18	9.82 735	27	0.17 265	9.91 908	8	6	l
55	9.74 662 9.74 681	19	9.82 762	28	0.17 238	9.91 900	9	5	1
57	9.74 700	19	9.82 817	27	0.17 183	9.91 883	8	3	[
. 58	9.74 719	19 18	9.82 844	27	0.17 156	9.91 874	9 8	2	
59	9.74 737	19	9.82 871	27	0.17 129	9.91 866	9	I	l
60	9.74 756		9.82 899	_	0.17 101	9.91 857	_	_0	
L	L Cos	d	L Cot	c d	L Tan	LSin	d	'	PP

° (371) **56**°

	34°						1	45°	
7	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.74 756	19	9.82 899	27	0.17 101	9.91 857	8	60	
1	9.74775	19	9.82 926	27	0.17 074	9.91 849	9	59	
3	9.74 794 9.74 812	18	9.82 953	27	0.17 047	9.91 840 9.91 832	8	58 57	
4	9.74831	19	9.83 008	28	0.16 992	9.91 823	9	56	
5	9.74 850	19 18	9.83 035	27 27	0.16 965	9.91815	8	55	
6	9.74 868	19	9.83 062	27	0.16 938	9.91 806	8	54	
7 8	9.74 887 9.74 906	19	9.83 0 89 9.83 11 7	28	0.16 883	9.91 798 9.91 789	9	53 52	
9	9.74 924	18	9.83 144	27	0.16856	9.91 781	8	51	28 27 26
10	9.74 943	19	9.83 171	27	0.16 829	9.91 772	9	50	I 2.8 2.7 2.6 2 5.6 5.4 5.2
11	9.74 961	19	9.83 198	27 27	0.16802	9.91 763	8	49	2 5.6 5.4 5.2 3 8.4 8.1 7.8
12	9.74 980	19	9.83 225 9.83 252	27	0.16 775	9.91 755 9.91 746	9	48	4 11.2 10.8 10.4
13 14	9.74 999	18	9.83 280	28	0.16 720	9.91 748	8	47	5 14.0 13.5 13.0 6 16.8 16.2 15.6
15	9.75 036	19	9.83 307	27	0.16 693	9.91 729	9	45	
16	9.75 054	18	9.83 334	27 27	0.16 666	9.91 720	8	44	8 22.4 21.6 20.8
17 18	9.75 073 9.75 091	18	9.83 361	27	0.16 639	9.91 712	9	43	9 25.2 24.3 23.4
19	9.75 110	19	9.83 415	27	0.16 585	9.91 695	8	41	
20	9.75 128	18	9.83 442	27	0.16 558	9.91 686	9	40	
21	9.75 147	19	9.83 470	28	0.16 530	9.91 677	9	39	_
22	9.75 165	18	9.83 497	27 27	0.16 503	9.91 669	9	38	
23 24	9.75 184 9.75 202	18	9.83 524	27	0.16 476	9.91 660	9	37	
25	9.75 202	19	9.83 578	27	0.16 449	9.91 643	8	35	
2Ğ	9.75 239	18	9.83 605	27	0.16 395	9.91 634	9	34	19 18
27	9.75 258	18	9.83 632	27 27	0.16 368	9.91 625	8	33	1 1.9 1.8
28 29	9.75 276 9.75 294	18	9.83 659 9.83 686	27	0.16 341	9.91 617 9.91 608	9	32 31	2 3.8 3.6
30	9.75 313	19	9.83 713	27	0.16 287	9.91 599	9	30	3 5.7 5.4 4 7.6 7.2
31	9.75 331	18	9.83 740	27	0.16 260	9.91 591	8	29	5 9.5 9.0
32	9.75 350	19	9.83 768	28	0.16 232	9.91 582	9	28	6 11.4 10.8
33	9.75 368	18	9.83 795	27 27	0.16 205	9.91 573	8	27	7 13.3 12.6 8 15.2 14.4
34 35	9.75 386	19	9.83 822	27	0.16 178	9.91 565 9.91 556	9	26	9 17.1 16.2
36	9.75 423	18	9.83 876	27	0.16 131	9.91 547	9	24	
37	9.75 441	18	9.83 903	27	0.16 097	9.91 538	9 8	23	
38	9.75 459	18 19	9.83 930	27 27	0.16 070	9.91 530	9	22	
39 40	9.75 478	18	9.83 957	27	0.16 043	9.91 521	9	21 20	
	9.75 496	18	9.83 984	27	0.16 016	9.91 512	8		
41 42	9.75 514 9.75 533	19	9.84 011	27	0.15 989	9.91 504	9	18	
43	9.75 551	18 18	9.84 065	27	0.15 935	9.91 486	9	17	9 8
44	9.75 569	18	9.84 092	27 27	0.15 908	9.91 477	9 8	16	1 0.9 0.8
45 46	9.75 587 9.75 605	18	9.84 119 9.84 146	27	0.15 881	9.91 469	9	15	2 1.8 1.6
47	9.75 624	19	9.84 173	27	0.15 827	9.91 451	9	13	3 2.7 2.4
48	9.75 642	18 18	9.84 200	27 27	0.15 800	9.91 442	9	12	4 3.6 3.2 5 4.5 4.0
49 50	9.75 660	18	9.84 227	27	0.15 773	9.91 433	8	11	5 4.5 4.0 6 5.4 4.8
	9.75 678	18	9.84 254	26	0.15 746	9.91 425	9	10	7 6.3 5.6
51 52	9.75 696	18	9.84 280 9.84 307	27	0.15 720	9.91 416	9	8	8 7.2 6.4 9 8.1 7.2
53	9.75 733	19	9.84 334	27	0.15 666	9.91 398	9	7	,
54	9.75 751	18	9.84 361	27	0.15 639	9.91 389	8	6	
55 56	9.75 769	18	9.84 388	27	0.15 612	9.91 381	9	5	
57	9.75 805	18	9.84 442	27	0.15 558	9.91 3/2	9	3	
58	9.75823	18	9.84 469	27	0.15 531	9.91 354	9	2	1
59	9.75 841	18	9.84 496	27 27	0.15 504	9.91 345	9	I	
60	9.75 859	_	9.84 523		0.15 477	9.91 336		0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	'	PP

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'	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.75 859	18	9.84 523	27	0.15 477	9.91 336	8	60	
1	9.75 877	18	9.84 550	26	0.15 450	9.91 328	9	59 58	
3	9.75 895	18	9.84 576 9.84 603	27	0.15 424	9.91 319	9	50	
4	9.75 931	18	9.84 630	27	0.15 370	9.91 301	9	56	
5	9.75 949	18 18	9.84 657	27 27	0.15 343	9.91 292	9	55	
6	9.75 967	18	9.84 684	27	0.15 316	9.91 283	9	54	
7 8	9.75 985 9.76 003	18	9.84 711	27	0.15 262	9.91 2/4	8	53 52	
9	9.76 021	18	9.84 764	26 27	0.15 236	9.91 257	9	51	27 26
10	9.76 039	18	9.84 79 1	27	0.15 209	9.91 248	9	50	1 2.7 2.6 2 5.4 5.2
11	9.76 057	18	9.84 818	27	0.15 182	9.91 239	9	49	2 5.4 5.2 3 8.1 7.8
12	9.76 0 75 9.76 0 93	18	9.84 845 9.84 872	27	0.15 155	9.91 230	9	48 47	4 10.8 10.4
14	9.76 111	18	9.84 899	27	0.15 101	9.91 212	9	46	5 13.5 13.0 6 16.2 15.6
15	9.76 129	18	9.84 925	26 27	0.15075	9.91 203	9	45	7 18.9 18.2 8 21.6 20.8
16	9.76 146	17 18	9.84 952	27	0.15 048	9.91 194	9	44	
17 18	9.76 164 9.76 182	18	9.84 979 9.85 00 6	27	0.15 021	9.91 185 9.91 176	9	43 42	9 24.3 23.4
19	9.76 200	18	9.85 033	27	0.14 967	9.91 167	9	41	
20	9.76 218	18	9.85 059	26	0.14 941	9.91 158	9	40	
21	9.76 236		9.85 086	27	0.14 914	9.91 149	9 8	39	
22	9.76 253	17 18	9.85 113	27 27	0.14887	9.91 141	9	38 37	
23	9.76 271	18	9.85 140	26	0.14 834	9.91 132	ģ.	36	
25	9.76 307	18	9.85 193	27	0.14 807	9.91 114	9	35	18 17
26	9.76 324	17	9.85 220	27 27	0.14780	9.91 105	9	34	
27	9.76 342	18	9.85 247	26	0.14 753	9.91 0 96 9.91 0 87	9	33	1 1.8 1.7 2 3.6 3.4
29	9.76 360 9.76 378	18	9.85 273 9.85 300	27	0.14 727	9.91 037	9	32 31	3 5.4 5.1
3 0	9.76 395	17	9.85 327	27	0.14 673	9.91 069	9	30	4 7.2 6.8
31	9.76 413	18	9.85 354	27	0.14 646	9.91 060	9	29	5 9.0 8.5 6 10.8 10.2
32	9.76 431	18	9.85 380	26	0.14 620	9.91 051	9	28	7 12.6 11.9
33	9.76 448	17 18	9.85 407	27 27	0.14 593	9.91 042	9	27 26	
34	9.76 466 9.76 484	18	9.85 434 9.85 460	26	0.14 566	9.91 033 9.91 023	10	25	9 16.2 15.3
36	9.76 501	17	9.85 487	27	0.14 513	9.91 014	9	24	
37	9.76 519	18	9.85 514	27 26	0.14 486	9.91 005	9	23	
38 39	9.76 537	17	9.85 540 9.85 567	27	0.14 460	9.90 996 9.90 987	9	22 21	
40	9.76 554	18		27	0.14 433	9.90 978	9	20	
41	9.76 572	18	9.85 594	26	0.14 406	9.90 978	9	19	
42	9.76 590	17	9.85 647	27	0.14 353	9.90 960	9	18	10 9 8
43	9.76 625	18	9.85 674	27 26	0.14 326	9.90 951	9	17	1 1.0 0.9 0.8
44	9.76 642	18	9.85 700	27	0.14 300	9.90 942	9	16	2 2.0 1.8 1.6
45 46	9.76 660	17	9.85 727 9.85 754	27	0.14 273	9.90 933	9	14	3 3.0 2.7 2.4
47	9.76 695	18	9.85 780	26	0.14 220	9.90 915	9	13	4 4.0 3.6 3.2 5 5.0 4.5 4.0
48	9.76 712	17	9.85 807	27	0.14 193	9.90 906	9	12	6 6.0 5.4 4.8
49	9.76 730	17	9.85 834	26	0.14 166	9.90 896	9	11	7 7.0 6.3 5.6
50	9.76 747	18	9.85 860	27	0.14 140	9.90 887	9	10	8 8.0 7.2 6.4 9 9.0 8.1 7.2
51 52	9.76 765 9.76 782	17	9.85 887 9.85 913	26	0.14 113	9.90 878 9.90 869	9	8	9,9.0 0.1 7.2
53	9.76 800	18	9.85 940	27	0.14 060	9.90 860	9	7	
54	9.76817	17	9.85 967	27	0.14 033	9.90 851	9	6	
55 56	9.76 835	17	9.85 993 9.86 020	26	0.14 007	9.90 842	10	5	
57	9.76 870	18	9.86 046	26	0.13 980	9.90 823	9	4 3	
58	9.76 887	17	9.86 073	27	0.13 934	9.90 814	9	2	
59	9.76 904	17	9.86 100	27	0.13 900	9.90 805	9	1	
60	9.76 922		9.86 126		0.13874	9.90 796		0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	′	PP

_	90						_	40	
Ľ	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.76 922	17	9.86 126	27	0.13874	9.90 796	_	60	
1	9.76 939	18	9.86 153	26	0.13 847	9.90 787	9	59	
2	9.76 957	17	9.86 179	27	0.13821	9.90 777	10	58	
3	9.76 974	17	9.86 206	26	0.13 794	9.90 768	9	57	
4	9.76 991	18	9.86 232	27	0.13 768	9.90 759	9	56	7.4
5	9.77 026	17	9.86 285	26	0.13 715	9.90 741	g g	54	
7	9.77 043	17	9.86 312	27	0.13 688	9.90 731	10	53	
8	9.77 061	18	9.86 338	26 27	0.13 662	9.90 722	9	52	27 26
9	9.77 078	17 17	9.86 365	27	0.13 635	9.90 713	9	51	
10	9.77 095	17	9.86 392	26	0.13 608	9.90 704	10	50	I 2.7 2.6 2 5.4 5.2
11	9.77 112	18	9.86 418	27	0.13 582	9.90 694		49	2 5.4 5.2 3 8.1 7.8
12	9.77 130	17	9.86 445	26	0.13 555	9.90 685	9	48	4 10.8 10.4
13	9.77 147	17	9.86 471	27	0.13 529	9.90 676	9	47	5 13.5 13.0
14	9.77 164 9.77 181	17	9.86 524	26	0.13 502	9.90 667	10	46	6 16.2 15.6 7 18.9 18.2
16	9.77 199	18	9.86 551	27	0.13 449	9.90 648	9	44	7 18.9 18.2 8 21.6 20.8
17	9.77 216	17	9.86 577	26	0.13 423	9.90 639	9	43	9 24.3 23.4
18	9.77 233	17	9.86 603	26 27	0.13 397	9.90 630	9	42	
19	9.77 250	18	9.86 630	26	0.13 370	9.90 620	10	41	
20	9.77 268	17	9.86 656	27	0.13 344	9.90 611	9	40	
21	9.77 285	17	9.86 683	26	0.13317	9.90 602		39	
22	9.77 302	17	9.86 709	27	0.13 291	9.90 592	10	38	
23	9.77 319	17	9.86 736 9.86 762	26	0.13 264	9.90 583	9	37	
24 25	9.77 336	17	9.86 789	27	0.13 238	9.90 574 9.90 565	9	36	
26	9.77 370	17	9.86 815	26	0.13 185	9.90 555	10	34	18 17 16
27	9.77 387	17	9.86 842	27	0.13 158	9.90 546	9	33	1 1.8 1.7 1.6
28	9.77 405	18	9.86 868	26 26	0.13 132	9.90 537	9	32	2 3.6 3.4 3.2
29	9.77 422	17	9.86 894	27	0.13 106	9.90 527	10	31	3 5.4 5.1 4.8
30	9.77 439	17	9.86 921	26	0.13 079	9.90 518	9	30	4 7.2 6.8 6.4
31	9.77 456		9.86 947	27	0.13 053	9.90 509		29	5 9.0 8.5 8.0 6 10.8 10.2 9.6
32	9.77 473	17	9.86 974	26	0.13 026	9.90 499	10	28	7 12.6 11.9 11.2
33	9.77 490	17	9.87 000	27	0.13 000	9.90 490	10	27	8 14.4 13.6 12.8
34 35	9.77 507 9.77 524	17	9.87 027 9.87 053	26	0.12 973 0.12 947	9.90 480	9	26	9 16.2 15.3 14.4
36	9.77 541	17	9.87 079	26	0.12 921	9.90 462	9	24	
37	9.77 558	17	9.87 106	27	0.12894	9.90 452	10	23	
38	9.77 575	17	9.87 132	26 26	0.12868	9.90 443	9	22	
39	9.77 592	17 17	9.87 158	27	0.12842	9.90 434	9	21	
40	9.77 609	17	9.87 185	26	0.12815	9.90 424	9	20	
41	9.77 626	17	9.87 211	27	0.12789	9.90 415	10	19	
42	9.77 643	17	9.87 238	26	0.12 762	9.90 405	9	18	
44	9.77 677	17	9.87 290	26	0.12 730	9.90 390	10	16	10 9
45	9.77 694	17	9.87 317	27	0.12683	9.90 377	9	15	1 1.0 0.9
46	9.77 711	17	9.87 343	26 26	0.12657	9.90 368	9	14	2 2.0 1.8
47	9.77 728	17 16	9.87 369	27	0.12631	9.90 358	10	13	3 3.0 2.7 4 4.0 3.6
48	9.77 744	17	9.87 396	26	0.12 604	9.90 349	10	12	5 5.0 4.5 6 6.0 5.4
49 50	9.77 761	17	9.87 422	26	0.12 578	9.90 339	9	10	
	9.77 778	17	9.87 448	27	0.12552	9.90 330	10		7 7.0 6.3 8 8.0 7.2
51 52	9.77 795	17	9.87 475	26	0.12 525	9.90 320	9	8	9 9.0 8.1
53	9.77 829	17	9.87 527	26	0.12 473	9.90 301	10	7	1
54	9.77 846	17	9.87 554	27	0.12 446	9.90 292	9	6	
55	9.77 862	16	9.87 580	26	0.12420	9.90 282	10	5	-3
56	9.77 879	17 17	9.87 606	26 27	0.12 394	9.90 273	10	4	
57	9.77 896	17	9.87 633	26	0.12 367	9.90 263	9	3	
58 59	9.77 913	17	9.87 685	26	0.12 341	9.90 254 9.90 244	10	2 I	
60	9.77 946	16	9.87 711	26	0.12 289	9.90 235	9	0	
Г	L Cos	d	L Cot	c d	L Tan	L Sin	d	,	PP
								•	

1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.77 946		9.87 711		0.12 289	9.90 235		60	
1	9.77 963	17	9.87 738	27 26	0.12 262	9.90 225	10	59	
2	9.77 980	17 17	9.87 764	26	0.12 236	9.90 216	9	58	
3	9.77 997	16	9.87 790	27	0.12 183	9.90 206 9.90 197	9	57	
4 5	9.78 013	17	9.87 843	26	0.12 157	9.90 187	10	56 55	
6	9.78 047	17	9.87 869	26	0.12131	9.90 178	9	54	
7 8	9.78 063	16	9.87 895	26	0.12 105	9.90 168	10	53	
	9.78 080	17	9.87 922	27 26	0.12078	9.90 159	9	52	27 26
9	9.78 097	16	9.87 948	26	0.12052	9.90 149	10	51	
10	9.78 113	17	9.87 974	26	0.12 026	9.90 139	9	50	I 2.7 2.6 2 5.4 5.2
11	9.78 130	17	9.88 000	27	0.12000	9.90 130	10	49	3 8.1 7.8
12	9.78 147	16	9.88 027	26	0.11 973	9.90 I 20 9.90 I I I	9	48 47	4 10.8 10.4
14	9.78 180	17	9.88 079	26	0.11 947	9.90 101	10	46	5 13.5 13.0
15	9.78 197	17	9.88 105	26	0.11 895	9.90 091	10	45	6 16.2 15.6 7 18.9 18.2
16	9.78 213	16	9.88 131	26	0.11 869	9.90 082	9	44	8 21.6 20.8
17	9.78 230	17 16	9.88 158	26	0.11 842	9.90 072	9	43	9 24.3 23.4
18	9.78 246	17	9.88 184	26	0.11816	9.90 063	10	42	
19 20	9.78 263	17	9.88 210	26	0.11 790	9.90 053	10	41 40	
	9.78 280	16	9.88 236	26	0.11764	9.90 043	9	1 1	
2 I 2 2	9.78 296 9.78 313	17	9.88 262 9.88 289	27	0.11 738	9.90 034 9.90 024	10	39 38	
23	9.78 329	16	9.88 315	26	0.11 685	9.90 014	10	37	
24	9.78 346	17	9.88 341	26	0.11659	9.90 005	9	36	
25	9.78 362	16	9.88 367	26 26	0.11633	9.89 995	10	35	
26	9.78 379	17	9.88 393	27	0.11 607	9.89 985	9	34	17 16
27 28	9.78 395	17	9.88 420 9.88 446	26	0.11580	9.89 976 9.89 966	10	33	1 1.7 1.6
29	9.78 412	16	9.88 472	26	0.11 554	9.89 956	10	31	2 3.4 3.2
30	9.78 445	17	9.88 498	26	0.11 502	9.89 947	9	30	3 5.1 4.8 4 6.8 6.4
31	9.78 461	16	9.88 524	26	0.11 476	9.89 937	10	29	4 0.8 0.4 5 8.5 8.0
32	9.78 478	17	9.88 550	26	0.11 450	9.89 937	10	28	6 10.2 9.6
33	9.78 494	16	9.88 577	27 26	0.11 423	9.89 918	9	27	7 11.9 11.2 8 13.6 12.8
34	9.78 510	16	9.88 603	26	0.11 397	9.89 908	10	26	8 13.6 12.8 9 15.3 14.4
35	9.78 527	17 16	9.88 629	26	0.11 371	9.89 898	10	25 24	9 13.3
36	9.78 543 9.78 560	17	9.88 655 9.88 681	26	0.11 345	9.89 888	9	23	
37 38	9.78 576	16	9.88 707	26	0.11 293	9.89 869	10	22	•
39	9.78 592	16	9.88 733	26	0.11 267	9.89 859	10	21	
40	9.78 609	17	9.88 759	26	0.11 241	9.89 849	10	20	
41	9.78 625	16	9.88 786	27	0.11 214	9.89 840	9	19	
42	9.78 642	17 16	9.88812	26 26	0.11 188	9.89830	10	18	
43	9.78 658	16	9.88 838	26	0.11162	9.89820	10	17	10 9
44	9.78 674 9.78 691	17	9.88 864	26	0.11 136	9.89810	. 9	16	1 1.0 0.9
45 46	9.78 707	16	9.88 916	26	0.11 084	9.89 791	10	14	2 2.0 1.8
47	9.78 723	16	9.88 942	26	0.11058	9.89 781	10	13	3 3.0 2.7
48	9.78 739	16	9.88 968	26 26	0.11032	9.89 771	10	12	4 4.0 3.6 5 5.0 4.5
49	9.78 756	17	9.88 994	26	0.11006	9.89 761	9	II	5 5.0 4.5 6 6.0 5.4
50	9.78 772	16	9.89 020	26	0.10 980	9.89 752	10	10	7 7.0 6.3
51	9.78 788	17	9.89 046	27	0.10 954	9.89 742	10	8	
52	9.78 805	16	9.89 073	26	0.10 927	9.89 732	10	7	9 9.0 8.1
53 54	9.78 837	16	9.89 125	26	0.10 901	9.89 712	10	6	
55	9.78 853	16	9.89 151	26	0.10849	9.89 702	10	5	
56	9.78 869	16	9.89 177	26	0.10823	9.89 693	9	4	
57	9.78 886	17	9.89 203	26	0.10 797	9.89 683	10	3	
58	9.78 902	16	9.89 229	26	0.10 771	9.89 663	10	2 1	
59 60	9.78 918	16	9.89 255	26	0.10745	9.89 653	10	0	
00	9.78 934		9.89 281	_	0.10 /19	9.09 033		-	
	L Cos	d	L Cot	c d	L Tan	L Sin	ld	1	PP

	38°				-			41°	
1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.78 934	16	9.89 281	26	0.10719	9.89 653	10	60	
1	9.78 950	17	9.89 307	26	0.10 693	9.89 643	10	59	
2	9.78 967 9.78 983	16	9.89 333 9.89 359	26	0.10667	9.89 633	9	58	
3 4	9.78 999	16	9.89 385	26	0.10 615	9.89 614	10	56	
5	9.79 015	16	9.89 411	26	0.10 589	9.89 604	10	55	
6	9.79 031	16 16	9.89 437	26 26	0.10 563	9.89 594	10	54	
7 8	9.79 047	16	9.89 463	26	0.10 537	9.89 584 9.89 574	10	53 52	22 25
9	9.79 003	16	9.89 515	26	0.10 485	9.89 564	10	51	26 25
10	9.79 095	16	9.89 541	26	0.10 459	9.89 554	10	50	I 2.6 2.5 2 5.2 5.0
11	9.79 111	16	9.89 567	26	0.10433	9.89 544	10	49	3 7.8 7.5
12	9.79 128	17 16	9.89 593	26 26	0.10 407	9.89 534	10	48	4 10.4 10.0
13	9.79 144	16	9.89 619	26	0.10 381	9.89 524 9.89 514	10	47	5 13.0 12.5 6 15.6 15.0
14 15	9.79 160	16	9.89 671	26	0.10 355	9.89 504	10	45	7 18.2 17.5
16	9.79 192	16 16	9.89 697	26 26	0.10 303	9.89 495	9	44	8 20.8 20.0
17	9.79 208	16	9.89 723	26	0.10 277	9.89 485	10	43	9 23.4 22.5
18 19	9.79 224	16	9.89 749 9.89 775	26	0.10 251	9.89 475 9.89 465	10	42 41	
20	9.79 256	16	9.89 801	26	0.10 199	9.89 455	10	40	
21	9.79 272	16	9.89 827	26	0.10 199	9.89 445	10	39	
22	9.79 288	16	9.89 853	26	0.10 147	9.89 435	10	38	
23	9.79 304	16	9.89 879	26 26	0.10121	9.89 425	10	37	
24	9.79 319	16	9.89 905	26	0.10 095	9.89 415	10	36	
25 26	9.79 335 9.79 351	16	9.89 931 9.89 957	26	0.10 069	9.89 405	10	35	17 16 15
27	9.79 367	16	9.89 983	26	0.10 017	9.89 385	10	33	1 1.7 1.6 1.5
28	9.79 383	16 16	9.90 009	26 26	0.09 991	9.89 375	IO II	32	2 3.4 3.2 3.0
29	9.79 399	16	9.90 035	26	0.09 965	9.89 364	10	31	3 5.1 4.8 4.5
30	9.79 415	16	9.90 061	25	0.09 939	9.89 354	10	30	4 6.8 6.4 6.0 5 8.5 8.0 7.5
31	9.79 431	16	9.90 086	26	0.09 914	9.89 344	10	29 28	6 10.2 9.6 9.0
32 33	9.79 447	16	9.90 138	26	0.09 862	9.89 334 9.89 324	10	27	7 11.9 11.2 10.5 8 13.6 12.8 12.0
34	9.79 478	15	9.90 164	26	0.09836	9.89 314	10	26	8 13.6 12.8 12.0 9 15.3 14.4 13.5
35	9.79 494	16	9.90 190	26 25	0.09810	9.89 304	10	25	71-3:0 -4:4 -3:0
36	9.79 510	16	9.90 216	26	0.09 784	9.89 294	IO	24	
37 38	9.79 542	16	9.90 242	26	0.09 732	9.89 274	10	23	
39	9.79 558	16	9.90 294	26 26	0.09 706	9.89 264	10	21	
40	9.79 573	15 16	9.90 320	26	0.09 680	9.89 254	10	20	
41	9.79 589	16	9.90 346	- 1	0.09 654	9.89 244		19	
42	9.79 605 9.79 621	16	9.90 371	25 26	0.09 629	9.89 233 9.89 223	II	18	
43	9.79 636	15	9.90 397	26	0.09 577	9.89 223	10	17	11 10 9
45	9.79 652	16	9.90 449	26	0.09 551	9.89 203	10	15	I I.I I.O 0.9 2 2.2 2.0 I.8
46	9.79 668	16 16	9.90 475	26 26	0.09 525	9.89 193	10	14	3 3.3 3.0 2.7
47 48	9.79 684 9.79 699	15	9.90 501	26	0.09 499	9.89 183 9.89 173	10	13	4 4.4 4.0 3.6
49	9.79 715	16	9.90 527	26	0.09 473 0.09 447	9.89 173	II	12	5 5.5 5.0 4.5 6 6.6 6.0 5.4
50	9.79 731	16	9.90 578	25	0.09 422	9.89 152	10	10	
51	9.79 746	15	9.90 604	26	0.09 396	9.89 142	10	9	8 8.8 8.0 7.2
52	9.79 762	16 16	9.90 630	26	0.09 370	9.89 132	10	8	9 9.9 9.0 8.1
53	9.79 778	15	9.90 656	26 26	0.09 344	9.89 122	10	7	
54 55	9.79 793 9.79 809	16	9.90 682	26	0.09 318	9.89 112	11	5	
56	9.79 825	16	9.90 734	26	0.09 266	9.89 091	10	4	
57	9.79 840	15 16	9.90 759	25 26	0.09 241	9.89 081	10	3	
58 59	9.79 856	16	9.90 785	26	0.09 215	9.89 071	10	2	
59 60	9.79 887	15	9.90 811	26	0.09 189	9.89 060	10	1 0	
٣	L Cos	d	L Cot	c d	L Tan	L Sin		-	PP
		ч	- 000	o u	- I all	- 3111	u	1	

		39°							40°				
1			d	L Tan	c d	L Cot	L Cos	d			PΙ	P	
1 9.79 993	0	9.79 887	76	9.90 837	26	0.09 163	9.89 050	TO	60				
2 9,79,913 16 9,90,914 26 0,90,906 36 0,90,906 57 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 58 0,90,906 59 0,90,906 59 0,90,906 50 0,90,906									59				1
4			16		25								
5 9,799 65 15 9,909 66 7 9,909 7 7 9,799 6 7 9,799 6 7 9,799 6 7 9,799 6 7 9,799 7 10 9,80 27 10 9,80 28 10 9,91 69 9,80 28 10 9,91 69 9,80 10 10 9,80 10 9,91 69 10 9,91 69 10 10 9,80 68 10 9,91 69 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,80 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 9,91 69 10 10 10 9,91 69 10 10 9,91 60 10 9,													1
The color of the	5			9.90 966		0.09 034			55				- 1
7 9,79906 9,9106 9,9106 10 9,9106 10 9,9006 11 9,9006 10 9,9012 12 13 9,9006 10 9,91147 12 13 9,9006 10 9,91147 13 9,9006 10 9,91147 15 9,9117 15 9,9117 15 9,9117 16 9,9117 16 9,9117 17 18 9,8016 15 9,91130 15 9,91130 15 9,91130 15 9,91130 15 9,91130 16 9,91130													Ì
9 9.80 cot 10 9.91 cot 9.91 cot 9.91 cot 10 9.90 cot 10 9.91 cot 10 9.	7 8										0.0	0.5	
10													
11	10												
12 9.80 o74 10 0.91 171 20 0.08 583 9.88 97 10 47 51 13.0 12.5 15 15 15 15 15 15 15	11	9.80 058		9.91 121			9.88 937		49	_	7.8		
14		9.80 074		9.91 147		0.08853	9.88 927		48				
15										5			
17 9.80 15 5 9.91 276 26 0.08 274 9.88 875 10 12 12 12 12 12 12 13 13					26			10					
17 9,80 151 15 9,91 301 20 9.88 855 10 12 10 12 10 10 10 10						0.08 750							
10 9.80 182 15 9.91 353 26 0.08 673 9.88 854 10 39 39 39 30 30 30 30 3	17	9.80 151		9.91 276		0.08 724	9.88 875		43	9	23.4	22.5	
19 9.80 197 15 9.91 25 0.86 26 0.86 26 0.86 27 0.86 28 11 27 29 28 28 29 28 28 28 28													
1													j
22 9.80 228 15 9.91 430 26 0.08 570 9.88 824 10 36 27 28 9.80 274 15 9.91 436 26 0.08 544 9.88 803 10 36 36 27 28 9.80 274 15 9.91 585 26 0.08 447 9.88 772 10 33 1 1.6 1.5					26			10					
23 9.80 244 16 9.91 430 26 0.08 570 9.88 813 11 37 36 36 36 36 36 36 36			15		25			10					
24 9.80 259 15 9.91 482 25 0.08 431 9.88 731 11 134 15 15 15 15 15 15 15 1			16		26								
25 9.80 274 15 9.91 672 25 0.80 8493 9.88 793 11 3.5 26 9.80 305 15 9.91 533 26 0.08 467 9.88 772 11 3.3 1 1.6 1.5 27 9.80 305 15 9.91 585 26 0.08 441 9.88 761 10 3.2 2 3.2 3.2 3.0 30 9.80 351 15 9.91 585 25 0.08 493 9.88 772 11 3.3 1 1.6 1.5 30 9.80 351 15 9.91 585 25 0.08 441 9.88 761 10 3.2 2 3.2 3.2 3.0 31 9.80 360 15 9.91 602 25 0.08 441 9.88 761 10 3.0 4 6.4 6.0 32 9.80 382 16 9.91 602 25 0.08 390 9.88 741 10 30 4 6.4 6.0 33 9.80 397 15 9.91 602 25 0.08 393 9.88 772 11 29 6 9.6 9.6 9.6 33 9.80 493 15 9.91 793 26 0.08 383 9.88 770 10 26 9.88 531 34 9.80 412 15 9.91 793 26 0.08 383 9.88 770 10 26 9.88 683 35 9.80 443 15 9.91 793 26 0.08 287 9.88 699 11 27 8 12.8 12.0 37 9.80 483 15 9.91 842 9.08 504 15 9.91 842 9.08 504 15 9.91 842 26 0.08 203 9.88 6678 10 24 38 9.80 473 15 9.91 842 26 0.08 203 9.88 6678 10 24 39 9.80 483 15 9.91 905 26 0.08 203 9.88 6678 10 24 39 9.80 504 15 9.91 905 26 0.08 203 9.88 6578 10 21 40 9.80 505 15 9.91 905 26 0.08 203 9.88 6578 10 21 41 9.80 505 15 9.91 905 26 0.08 203 9.88 6578 10 21 42 9.80 505 15 9.91 905 26 0.08 205 9.88 5675 10 10 43 9.80 605 15 9.92 202 26 0.08 203 9.88 563 10 10 10 10 10 10 10 1						0.08 544							
20 9.80 305 15 9.91 533 26 0.88 467 9.88 775 10 31 32 2 3.2 3.0	25	9.80 274		9.91 482		0.08 518					10	15	
28 9.80 336 15 9.91 559 26 0.08 441 9.88 751 10 31 33 4.8 4.5 30 9.80 351 15 9.91 636 26 0.08 348 9.88 751 10 30 4 6.4 6.0 31 9.80 366 15 9.91 636 26 0.08 383 9.88 720 10 28 7 11 20 33 9.80 387 15 9.91 713 25 0.08 881 9.88 720 11 27 8 12.8 12.0 34 9.80 412 15 9.91 713 25 0.08 826 9.88 688 10 27 8 12.8 12.0 35 9.80 428 16 9.91 739 26 0.08 261 9.88 688 10 27 8 12.8 12.0 36 9.80 443 15 9.91 761 26 0.08 261 9.88 688 10 27 8 12.8 12.0 37 9.80 458 15 9.91 816 25 0.08 826 9.88 688 10 24 10 39 9.80 458 15 9.91 816 25 0.08 132 9.88 668 10 23 10 40 9.80 504 15 9.91 842 26 0.08 132 9.88 669 10 24 10 10 41 9.80 519 15 9.91 919 26 0.08 0.08 132 9.88 668 10 23 10 24 10 42 9.80 550 15 9.91 919 26 0.08 081 9.88 665 10 10 10 10 43 9.80 550 15 9.91 919 26 0.08 081 9.88 665 10 10 10 10 10 44 9.80 505 15 9.92 927 26 0.08 081 9.88 563 10 10 10 10 10 10 10 1													
29 9.80 336 15 9.91 636 25 0.08 415 9.88 731 10 31 3 4.8 4.5 4		9.80 305			26		9.88 772	11					
30 9.80 351 15 9.91 610 26 0.08 390 9.88 741 10 30 5 8.0 6.08 391 39.80 397 15 9.91 610 20 0.08 338 9.88 730 10 28 7 11.2 10.5 39.80 39.80 397 15 9.91 713 26 0.08 261 9.88 683 15 9.91 713 26 0.08 261 9.88 683 15 9.91 713 26 0.08 261 9.88 683 10 24 33.5 38.80 38.			16				9.88 751						
31 9.80 366 15 9.91 636 26 0.08 338 9.88 730 17 28 7 11.2 10.5	30					0.08 390				4		6.0	
32 9.80 382 10 9.91 688 383 9.80 372 15 9.91 783 25 0.08 287 9.88 699 10 26 368 383 9.80 428 15 9.91 791 26 0.08 263 9.88 688 10 25 0.08 263 9.80 438 15 9.91 791 26 0.08 263 9.88 688 10 25 0.08 263 9.88 688 10 25 0.08 263 9.88 688 10 25 0.08 263 9.88 688 10 25 0.08 263 9.88 688 10 27 88 12.8 12.0 12	31		-						29	5			
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5	- 1					0.07 516	9.88 383			
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33 9.81 314 15 9.93 227 20 0.06 773 0.88 072 11 27 7 10.5 9.8						0.06 799				6 9.0 8.4
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59 9.81 685 14 9.93 891 20 0.06 684 9.87 789 11 0				9.93 840						
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L Cos d L Cot cd L Tan L Sin d / PP	60	9.81 694	-+		-5	0.06 084	9.87 778		0	
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7	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
6	9.81 694	-	9.93 916	_	0.06 084	9.87 778	<u> </u>	60	
1	9.81 709	15	9.93 910	26	0.06 058	9.87 767	11	59	
2	9.81 723	14	9.93 967	25	0.06 033	9.87 756	II	58	
3	9.81 738	15	9.93 993	26 25	0.06 007	9.87 745	11	57	
4	9.81 752	15	9.94 018	26	0.05 982	9.87 734	11	56	
5	9.81 767 9.81 781	14	9.94 044	25	0.05 956	9.87 723 9.87 712	11	55 54	
7	9.81 796	15	9.94 095	26	0.05 905	9.87 701	ΙI	53	
8	9.81810	14	9.94 120	25 26	0.05 880	9.87 690	II	52	26 25
9	9.81 825	15 14	9.94 146	25	0.05 854	9.87 679	11	51	1 2.6 2.5
10	9.81 839	15	9.94 171	26	0.05 829	9.87 668	11	50	2 5.2 5.0
11	9.81 854	14	9.94 197	25	0.05 803	9.87 657 9.87 646	11	49 48	3 7.8 7.5 4 10.4 10.0
13	9.81 868 9.81 882	14	9.94 222	26	0.05 778	9.87 635	11	47	5 13.0 12.5
14	9.81 897	15	9.94 273	25	0.05 727	9.87 624	11	46	6 15.6 15.0
15	9.81911	14	9.94 299	26	0.05 701	9.87 613	11	45	7 18.2 17.5 8 20.8 20.0
16	9.81 926	15	9.94 324	25 26	0.05 676	9.87 601	11	44	9 23.4 22.5
17	9.81 940	15	9.94 350	25	0.05 650	9.87 590 9.87 579	11	43	,
19	9.81 969	14	9.94 373	26	0.05 599	9.87 568	11	41	
20	9.81 983	14	9.94 426	25	0.05 574	9.87 557	11	40	
21	9.81 998	15	9.94 452	26	0.05 548	9.87 546	11	39	
22	9.82 012	14	9.94 477	25	0.05 523	9.87 535	II	38	
23	9.82 026	14	9.94 503	26 25	0.05 497	9.87 524	II	37	
24	9.82 041	15	9.94 528	26	0.05 472	9.87 513	12	36	
25 26	9.82 055 9.82 069	14	9.94 554 9.94 579	25	0.05 446	9.87 501 9.87 490	11	35 34	15 14
27	9.82 084	15	9.94 579	25	0.05 396	9.87 479	11	33	I 1.5 I.4
28	9.82 098	14	9.94 630	26	0.05 370	9.87 468	II	32	2 3.0 2.8
29	9.82 112	14	9.94 655	25 26	0.05 345	9.87 457	11	31	3 4.5 4.2 4 6.0 5.6
30	9.82 126	15	9.94 681	25	0.05 319	9.87 446	12	30	4 6.0 5.0 5 7.5 7.0
31	9.82 141	14	9.94 706	26	0.05 294	9.87 434	11	29	6 9.0 8.4
32	9.82 155	14	9.94 732 9.94 757	25	0.05 268	9.87 423 9.87 412	II	28	7 10.5 9.8 8 12.0 11.2
33	9.82 184	15	9.94 783	26	0.05 217	9.87 401	11	26	8 12.0 11.2 9 13.5 12.6
35	9.82 198	14	9.94 808	25	0.05 192	9.87 390	11	25	91 -0.3
36	9.82 212	14	9.94834	26 25	0.05 166	9.87 378	12	24	
37	9.82 226	14	9.94 859	25	0.05 141	9.87 367 9.87 356	11	23	
38 39	9.82 240	15	9.94 884	26	0.05 116	9.87 345	11	21	
40	9.82 269	14	9.94 935	25	0.05 065	9.87 334	11	20	
41	9.82 283	14	9.94 961	26	0.05 039	9.87 322	12	19	
42	9.82 297	14	9.94 986	25	0.05 014	9.87 311	11	18	
43	9.82 311	14	9.95 012	26	0.04 988	9.87 300	11	17	12 11
44	9.82 326	14	9.95 037	25	0.04 963	9.87 288	11	16	1 1.2 1.1
45 46	9.82 340	14	9.95 062	26	0.04 912	9.87 266	11	14	2 2.4 2.2
47	9.82 368	14	9.95 113	25	0.04 887	9.87 255	11	13	3 3.6 3.3 4 4.8 4.4
48	9.82 382	14	9.95 139	26	0.04 861	9.87 243	12	12	5 6.0 5.5
49	9.82 396	14	9.95 164	26	0.04 836	9.87 232	11	11	5 6.0 5.5 6 7.2 6.6 7 8.4 7.7
50	9.82 410	14	9.95 190	25	0.04 810	9.87 221	12	10	7 8.4 7.7 8 9.6 8.8
51	9.82 424	15	9.95 215	25	0.04 785	9.87 209	11	8	9 10.8 9.9
52 53	9.82 439 9.82 453	14	9.95 240 9.95 266	26	0.04 760	9.87 187	11	7	
54	9.82 467	1.4	9.95 291	25	0.04 709	9.87 175	12	6	
55	9.82 481	14	9.95 317	26	0.04 683	9.87 164	II	5	
56	9.82 495	14	9.95 342	25	0.04 658	9.87 153	12	4	
57 58	9.82 509	14	9.95 368	25	0.04 632	9.87 141	11	3 2	
59	9.82 537	14	9.95 418	25	0.04 582	9.87 119	11	1	
60	9.82 551	14	9.95 444	26	0.04 556	9.87 107	I 2	0	
	L Cos	d	L Cot	cd	L Tan	L Sin	d	1	PP

131° (379) **48°**

	42		10 100		-				
'	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.82 551	7.4	9.95 444	25	0.04 556	9.87 107	11	60	
1	9.82 565	14	9.95 469	26	0.04 531	9.87 096	11	59 58	
3	9.82 579 9.82 593	14	9.95 495 9.95 520	25	0.04 505	9.87 085 9.87 073	I 2	57	
4	9.82 607	14	9.95 545	25	0.04 455	9.87 062	11	56	
5	9.82 621	14	9.95 571	26 25	0.04 429	9.87 050	I2 II	55	
6 7	9.82 635	14	9.95 596	26	0.04 404	9.87 039	11	54	
8	9.82 663	14	9.95 647	25	0.04 353	9.87 016	I 2	52	26 25
9	9.82 677	14 14	9.95 672	25 26	0.04 328	9.87 005	II I2	51	
10	9.82 691	14	9.95 698	25	0.04 302	9.86 993	11	50	I 2.6 2.5 2 5.2 5.0
11	9.82 705	14	9.95 723	25	0.04 277	9.86 982	12	49	3 7.8 7.5
13	9.82 719	14	9.95 748 9.95 774	26	0.04 252	9.86 959	ΙI	48 47	4 10.4 10.0 5 13.0 12.5
14	9.82 747	14	9.95 799	25	0.04 201	9.86 947	12	46	5 13.0 12.5 6 15.6 15.0
15	9.82 761	14	9.95 825	26 25	0.04 175	9.86 936	II I2	45	7 18.2 17.5
16	9.82 775	13	9.95 850	25	0.04 150	9.86 924	II	44	8 20.8 20.0 9 23.4 22.5
18	9.82 802	14	9.95 901	26	0.04 123	9.86 902	II	43	9 23.4 22.3
19	9.82816	14 14	9.95 926	25 26	0.04 074	9.86 890	I 2 I I	41	
20	9.82 830	14	9.95 952	25	0.04 048	9.86 879	12	40	
21	9.82 844	14	9.95 977	25	0.04 023	9.86 867	12	39	
22	9.82 858 9.82 872	1.4	9.96 002	26	0.03 998	9.86 855 9.86 844	11	38 37	
24	9.82 885	13	9.96 053	25	0.03 947	9.86 832	I 2	36	
25	9.82 899	14	9.96 078	25 26	0.03 922	9.86 821	II I2	35	14 13
26	9.82 913	14	9.96 104	25	0.03 896	9.86 809	II	34	1 1.4 1.3
27 28	9.82 927 9.82 941	14	9.96 129 9.96 155	26	0.03 871	9.86 786	12	33	2 2.8 2.6
29	9.82 955	14	9.96 180	25	0.03 820	9.86 775	11	31	3 4.2 3.9
30	9.82 968	13	9.96 205	25 26	0.03 795	9.86 763	11	30	4 5.6 5.2 5 7.0 6.5
31	9.82 982	14	9.96 231	25	0.03 769	9.86 752	12	29	6 8.4 7.8
33	9.82 996	14	9.96 256	25	0.03 744	9.86 740	12	28	7 9.8 9.1 8 11.2 10.4
34	9.83 023	13	9.96 307	26	0.03 693	9.86 717	11	26	8 11.2 10.4 9 12.6 11.7
35	9.83 037	14	9.96 332	25 25	0.03 668	9.86 705	12	25	,
36	9.83 051	14	9.96 357	26	0.03 643	9.86 694	12	24	
37 38	9.83 078	13	9.96 383	25	0.03 592	9.86 670	I 2	23	
39	9.83 092	14	9.96 433	25 26	0.03 567	9.86 659	II I2	21	
40	9.83 106	14	9.96 459	25	0.03 541	9.86 647	12	20	
41	9.83 120	13	9.96 484	26	0.03 516	0.86 635	11	19	
42	9.83 133	14	9.96 510	25	0.03 490	9.86 624	12	18	12 11
44	9.83 161	14	9.96 560	25	0.03 440	9.86 600	I 2	16	1 1.2 1.1
45	9.83 174	13	9.96 586	26 25	0.03 414	9.86 589	11	15	2 2.4 2.2
46 47	9.83 188	14	9.96 636	25	0.03 389	9.86 577	12	14	3 3.6 3.3 4 4.8 4.4
48	9.83 215	13	9.96 662	26	0.03 364	9.86 554	11	13	5 6.0 5.5
49	9.83 229	14	9.96 687	25	0.03 313	9.86 542	12	11	6 7.2 6.6
50	9.83 242	13	9.96 712	25 26	0.03 288	9.86 530	12	10	7 8.4 7.7 8 9.6 8.8
51	9.83 256	14	9.96 738	25	0.03 262	9.86 518	11	9	9 10.8 9.9
52 53	9.83 270 9.83 283	13	9.96 763	25	0.03 237	9.86 507	12	8 7	
54	9.83 297	14	9.96 814	26	0.03 186	9.86 483	I 2	6	
5.5	9.83 310	13	9.96 839	25 25	0.03 161	9.86 472	11	5	
56 57	9.83 324 9.83 338	14	9.96 864	26	0.03 136	9.86 460	12	4	
58 58	9.83 351	13	9.96 915	25	0.03 110	9.86 436	12	3 2	
59	9.83 365	14	9.96 940	25	0.03 060	9.86 425	11	1	
60	9.83 378	-3	9.96 966	-20	0.03 034	9.86 413		0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	′	PP

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		-							D. D.	
′	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP	
0	9.83 378	14	9.96 966	25	0.03 034	9.86 413	12	60		
1	9.83 392	13	9.96 991	25	0.03 009	9.86 401	12	59		
2	9.83 405	14	9.97 016 9.97 042	26	0.02 984	9.86 389 9.86 377	I 2	58		
3	9.83 419	13	9.97 042	25	0.02 933	9.86 366	11	56		
4 5	9.83 446	14	9.97 007	25	0.02 908	9.86 354	12	55		
6	9.83 459	13	9.97 118	26	0.02 882	9.86 342	12	54		
7	9.83 473	14	9.97 143	25 25	0.02 857	9.86 330	12	53		
8	9.83 486	13 14	9.97 168	25	0.02 832	9.86 318 9.86 306	12	52 51	26 25	
9	9.83 500	13	9.97 193	26			11	50	1 2.6 2.5	
10	9.83 513	14	9.97 219	25	0.02 781	9.86 295	12		2 5.2 5.0	
11	9.83 527	13	9.97 244 9.97 269	25	0.02 756	9.86 283 9.86 271	12	49 48	3 7.8 7.5	
13	9.83 540 9.83 554	14	9.97 295	26	0.02 705	9.86 259	I 2	47	4 10.4 10.0 5 13.0 12.5	
14	9.83 567	13	9.97 320	25	0.02 680	9.86 247	12	46	6 15.6 15.0	
15	9.83 581	14	9.97 345	25	0.02 655	9.86 235	I 2 I 2	45	7 18.2 17.5	
16	9.83 594	13 14	9.97 371	26 25	0.02 629	9.86 223	12	44	8 20.8 20.0	
17	9.83 608 9.83 621	13	9.97 396	25	0.02 579	9.86 200	11	43	9 23.4 22.5	
19	9.83 634	13	9.97 421	26	0.02 553	9.86 188	I 2	41		
20	9.83 648	14	9.97 472	25	0.02 528	9.86 176	12	40		
21	9.83 661	13	9.97 497	25	0.02 503	9.86 164	12	39		
22	9.83 674	13	9.97 523	26	0.02 477	9.86 152	12	38		
23	9.83 688	14	9.97 548	25	0.02 452	9.86 140	12	37		
24	9.83 701	13	9.97 573	25 25	0.02 427	9.86 128	12	36	*	
25 26	9.83 715	13	9.97 598	26	0.02 402	9.86 116 9.86 104	12	35	14 13	
27	9.83 728 9.83 741	13	9.97 649	25	0.02 370	9.86 092	12	33	1 1.4 1.3	
28	9.83 755	14	9.97 674	25	0.02 326	9.86 080	12	32	2 2.8 2.6	
29	9.83 768	13	9.97 700	26	0.02 300	9.86 068	I 2 I 2	31	3 4.2 3.9	
30	9.83 781	13	9.97 725	25	0.02 275	9.86 056	12	30	4 5.6 5.2 5 7.0 6.5	
31	9.83 795	14	9.97 750	25 26	0.02 250	9.86 044	12	29	6 8.4 7.8	
32	9.83 808	13	9.97 776	25	0.02 224	9.86 032 9.86 020	12	28	7 9.8 9.1 8 11.2 10.4	
33	9.83 821	13	9.97 801	25	0.02 199	9.86 008	12	26	8 11.2 10.4	
35	9.83 848	14	9.97 851	25	0.02 1/4	9.85 996	I 2	25	9 12.0 11.7	
36	9.83 861	13	9.97 877	26	0.02 123	9.85 984	12	24		
37	9.83 874	13	9.97 902	25	0.02 098	9.85 972	12	23		
38	9.83 887	13	9.97 927	25	0.02 073	9.85 960 9.85 948	12	22 21		
39 40	9.83 901	13	9.97 953	25	0.02 047		12	20		
	9.83 914	13	9.97 978	25		9.85 936	12	19		
4I 42	9.83 927	13	9.98 003	26	0.01 997	9.85 912	12	18		
43	9.83 954	14	9.98 054	25	0.01 946	9.85 900	12	17	12 11	
44	9.83 967	13	9.98 079	25	0.01 921	9.85 888	12	16	I I.2 I.I	
45	9.83 980	13	9.98 104	25	0.01 896	9.85 876	12	15	2 2.4 2.2	
46	9.83 993	13	9.98 130	25	0.01 870	9.85 864	13	14	3 3.6 3.3 4 4.8 4.4	
47 48	9.84 006	14	9.98 155	25	0.01 845	9.85 839	12	13	5 6.0 5.5	
49	9.84 033	13	9.98 206	26	0.01 794	9.85 827	12	11	6 7.2 6.6	
50	9.84 046	13	9.98 231	25	0.01 769	9.85 815	12	10	7 8.4 7.7 8 9.6 8.8	
51	9.84 059	13	9.98 256	25	0.01 744	9.85 803	12	9	8 9.6 8.8 9 10.8 9.9	
52	9.84 072	13	9.98 281	25	0.01 719	9.85 791	12	8	1	
53	9.84 085	13	9.98 307	25	0.01 693	9.85 779	13	7		
54	9.84 098	14	9.98 332 9.98 357	25	0.01 668	9.85 766	12	6 5		
55 56	9.84 125	13	9.98 383	26	0.01 043	9.85 742	12	1 4		
57	9.84 138	13	9.98 408	25	0.01 592	9.85 730	12	3		
58	9.84 151	13	9.98 433	25	0.01 567	9.85 718	12	2		
59		13	9.98 458		0.01 542		13	I		
60		-	9.98 484	-	0.01 516	9.85 693 L Sin	d	- 0	PP	
	L Cos	d	L Cot	cd	L Tan	I F SIU	1 4	1	F	

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	44							99	
1	L Sin	d	L Tan	c d	L Cot	L Cos	d		PP
0	9.84 177	13	9.98 484	25	0.01 516	9.85 693	12	60	
1	9.84 190	13	9.98 509	25	0.01 491	9.85 681	12	59 58	
3	9.84 203	13	9.98 534	26	0.01 466	9.85 669 9.85 657	I 2	57	
4	9.84 229	13	9.98 585	25	0.01 415	9.85 645	12	56	
5	9.84 242	13	9.98 610	25 25	0.01 390	9.85 632	13	55	
6 7	9.84 255	14	9.98 635	26	0.01 365	9.85 620	I 2	54 53	
8	9.84 282	13	9.98 686	25	0.01 314	9.85 596	12	52	
9	9.84 295	13	9.98 711	25 26	0.01 289	9.85 583	13	51	
10	9.84 308	13	9.98 737	25	0.01 263	9.85 571	12	50	
II I2	9.84 321 9.84 334	13	9.98 762 9.98 787	25	0.01 238	9.85 559 9.85 547	I 2	49 48	
13	9.84 347	13	9.98 812	25	0.01 188	9.85 534	13	47	
14	9.84 360	13	9.98 838	26	0.01 162	9.85 522	12	46	26 25 14
15 16	9.84 373 9.84 385	13	9.98 863 9.98 888	25 25	0.01 137	9.85 510	13	45 44	1 2.6 2.5 1.4
17	9.84 398	13	9.98 913	25	0.01 087	9.85 485	I 2	43	2 5.2 5.0 2.8 3 7.8 7.5 4.2
18	9.84411	13	9.98 939	26	0.01 061	9.85 473	12	42	4 10.4 10.0 5.6
19	9.84 424	13	9.98 964	25 25	0.01 036	9.85 460	13	41	5 13.0 12.5 7.0
50	9.84 437	13	9.98 989	26	0.00 985	9.85 448	12	40	
2I 22	9.84 450 9.84 463	13	9.99 015	25	0.00 985	9.85 436 9.85 423	13	39	8 20.8 20.0 11.2
23	9.84 476	13	9.99 065	25	0.00 935	9.85 411	I 2 I 2	37	9 23.4 22.5 12.6
24	9.84 489	13	9.99 090	25 26	0.00 910	9.85 399	13	36	
25 26	9.84 502 9.84 515	13	9.99 116	25	0.00 884	9.85 386	12	35	
27	9.84 528	13	9.99 166	25	0.00 834	9.85 361	13	33	
28	9.84 540	12	9.99 191	25 26	0.00 809	9.85 349	I 2	32	
29 30	9.84 553	13	9.99 217	25	0.00 783	9.85 337	13	31 30	
1	9.84 566	13	9.99 242	25	0.00 758	9.85 324	12	29	
3I 32	9.84 579 9.84 592	13	9.99 207	26	0.00 733	9.85 312 9.85 299	13	28	
33	9.84 605	13	9.99 318	25	0.00 682	9.85 287	12	27	Ì
34	9.84 618	13	9.99 343	25 25	0.00657	9.85 274	13	26	
35 36	9.84 630 9.84 643	13	9.99 368	26	0.00 632	9.85 262	12	25	
37	9.84 656	13	9.99 419	25	0.00 581	9.85 237	13	23	13 12
38	9.84 669	13	9.99 444	25 25	0.00 556	9.85 225	I 2 I 3	2 2 2 I	1 1.3 1.2
39 40	9.84 682	12	9.99 469	26	0.00 531	9.85 212	12	20	2 2.6 2.4
41	9.84 694	13	9.99 495	25	0.00 505	9.85 200	13	19	3 3.9 3.6 4 5.2 4.8
42	9.84 720	13	9.99 545	25	0.00 455	9.85 175	12	18	5 6.5 6.0
43	9.84 733	13	9.99 570	25 26	0.00 430	9.85 162	13	17	6 7.8 7.2
44 45	9.84 745 9.84 7 58	13	9.99 596	25	0.00 404	9.85 150 9.85 137	13	16	7 9.1 8.4 8 10.4 9.6
46	9.84 771	13	9.99 646	25	0.00 379	9.85 125	12	14	9 11.7 10.8
47	9.84 784	13	9.99672	26	0.00 328	9.85 112	13	13	
48 49	9.84 796 9.84 809	13	9.99 697	25 25	0.00 303	9.85 100	13	12	
50	9.84 822	13	9.99 747	25	0.00 278	9.85 074	13	10	
51	9.84835	13	9.99 773	26	0.00 227	9.85 062	12	9	
52	9.84 847	12	9.99 798	25	0.00 202	9.85 049	13	8	
53	9.84 860	13	9.99 823	25 25	0.00 177	9.85 037	I 2 I 3	7	
54 55	9.84 873 9.84 885	12	9.99 848	26	0.00 152	9.85 024	12	5	
56	9.84 898	13	9.99 899	25	0.00 101	9.84 999	13	4	
57	9.84 911	13	9.99 924	25 25	0.00 076	9.84 986	13	3	
58 59	9.84 923 9.84 936	13	9.99 949 9.99 975	26	0.00 051	9.84 974 9.84 961	13	2 I	
60	9.84 949	13	0.00 000	25	0.00 000	9.84 949	12	0	
	L Cos	d	L Cot	c d	L Tan	L Sin	d	7	PP

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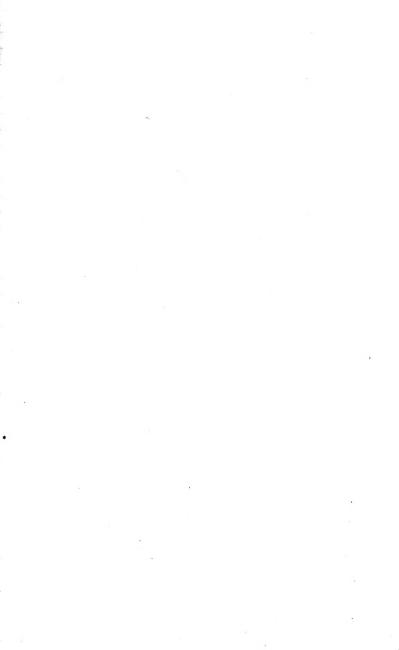
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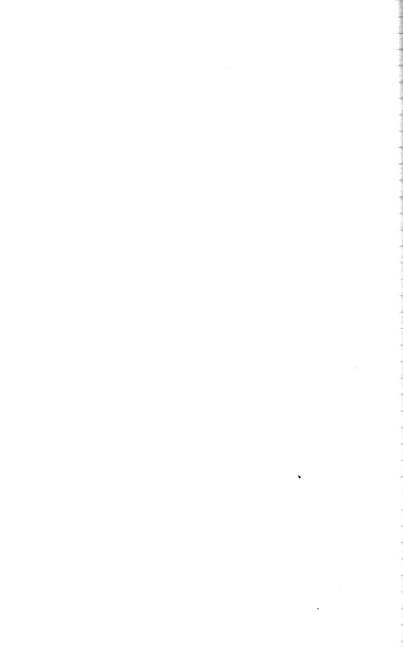
























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